60856
School of
no. 85
cop. 2
Marint
sol. cred

## OCEANOGRAPHY



Towed Thermistor Chain Observations in FRONTS-80
by
C. A. Paulson, R. J. Baumann, L. M. deWitt, T. J. Spoering and J. D. Wagner

Ottice of Naval Research No0014-76-C-0067 NOOO14-79-C-0004 NR 083102

Relerence $\mathbf{8 0}$-18
October 1980
Data Report 85

Reproduction in whole or in part is permitted for any purpose of the Unlted States Government

SECURITY CLASSIFICATION OF THIS PAGE (When Data Entorod)

| REPORT DOCUMENTATION PAGE | READ INSTRUCTIONS |
| :---: | :---: |
| 1. REPORT NUMEER <br> $80-18$$\quad 2$. GOVT ACCESSION NO. | 3. Reciplent's Catalog number |
| TOWED THERMISTOR CHAIN OBSERVATIONS IN FRONTS-80 | 5. TYPE OF REPORT A PERIOD COVERED data |
|  | 6. PERFORMING ORG. REPOOT NUMEER |
| 7. AUTHOR(s) Paulson, R. J. Baumann, L. M. deWitt, <br> T. J. Spoering and J. D. Wagner | 8. CONTRACT OR GRANT NUMEER(o) N00014-79-C-0004 |
| 9. PERFORMING ORGANIZATION NAME AND ADDRESS SCool of Oceanography Oregon State University Corvallis, OR 97331 | 10. PROGRAM ELEMENT, PROJECT, TASK AREA Q WORK UNIT NUMBERS <br> NR 083-102 |
| 11. CONTROLLING OFFICE NAME AND ADDRESS Office of Naval Research Ocean Science and Technology Division Arlington, VA 22217 | 12. REPORT DATE October 1980 |
|  | 13. Number of pages |
|  | 15. SECURITY CLASS, (of this roport) Unclassified |
|  | 15a. DECLEASSIEIECATION/DOWNGRADING |
| 16. DISTRIBUTION STATEMENT (of thls Roport) <br> Approved for public release; distribution unlimited |  |
|  |  |
| 17. DISTRIBUTION STATEMENT (of the abstract ontorod in Block 20, If diltorent from Report) |  |
| 18. SUPPLEMENTARY NOTES |  |
| KEY WORDS (Continue on revorso oido it nocoosacy end idontly by block numbor) |  |
| Towed Thermistor Chain Open Ocean Fronts North Pacific Subtropical Front FRONTS-80 Experiment |  |
| STRACT (Continue on revorse oido il necossary end idonity by block number) |  |
| Observations of temperature and pressure in the upper 100 m were taken with a towed thermistor chain in January 1980 north of Hawaii. The observations were taken as a part of a cooperative investigation of the North Pacific subtropical front entitled FRONTS-80. The chain was towed on four occasions over a total of 700 nautical miles between latitudes of 26 and 34 degrees $N$. The observations were averaged over sequential $30-s$ intervals and cross-sections of temperature and temperature profiles were plotted. |  |

The observations show that the surface expression of the North Pacific subtropical front was composed of multiple fronts having temperature contras ts ranging from a few tenths to about $2^{\circ} \mathrm{C}$. The horizontal gradients of surface temperature were as large as $0.5^{\circ} \mathrm{C}$ in 300 m . Vertical temperature gradients associated with the fronts were both positive and negative. Changes in surface temperature across the fronts were usually, but not always, associated with salinity changes tending to minimize the change in density. On one occasion a $2^{\circ} \mathrm{C}$ change in temperature across a front with no change in salinity was observed.

## TOWED THERMISTOR CHAIN

OBSERVATIONS IN FRONTS-80
by

C. A. Paulson, R. J. Baumann, L. M. deWitt, T. J. Spoering and J. D. Wagner

> School of Oceanography Oregon State University Corvallis, Oregon 97331

DATA REPORT
Office of Naval Research Contract N00014-79-C-0067

Project NR 083-102

Approved for public release; distribution unlimited
G. Ross Heath

## ACKNOWLEDGMENTS

The design and construction of the thermistor chain were carried out by the Technical Planning and Development Group at Oregon State University under the direction of Rod Mesecar. We gratefully acknowledge the cooperation of the officers, crew and scientists aboard the NOAA Ship OCEANOGRAPHER, Gerald C. Saladin, commanding and Stanley P. Hayes, Chief Scientist. This research was supported by the Office of Naval Research through contract N00014-79-C-0004 under project NR 083-102.

## TABLE OF CONTENTS

ACKNOWLEDGMENTS ..... -i
INTRODUCTION ..... $-1$
INSTRUMENTATION ..... -2
OBSERVATIONS ..... -4
REFERENCES ..... 18
APPENDICES
A. Highest and Lowest Temperature vs. Time ..... 19
B. Temperature Cross-Sections ..... 30
C. Temperature Profiles ..... 78
D. Configuration of the Chain Under Tow- ..... 176

This report presents observations of temperature in the upper ocean obtained by use of a towed thermistor chain. The observations were taken as a part of a cooperative investigation of the wintertime North Pacific subtropical front entitled FRONTS-80. An overview of the experiment together with preliminary results from each of the principal investigators is given in a report edited by Paulson and Niiler (1980).

The objectives of the towed chain investigation in FRONTS-80 were:

- To describe the spatial variability of temperature and salinity across the front.
- To describe the characteristics of the internal wave field near the front.
- To describe mixing processes associated with the front.
- To compare our measurements with those of other investigators.
- To test improved conductivity sensors.

INSTRUMENTATION

The thermistor chain consisted of sensors, electrical conductors, plastic fairing, a strain member and a 450 kg lead-filled depressor. The fairing was manufactured by Fathom Oceanology. The thermistors were manufactured by Thermometrics (Model P-85) and had a time constant of about 0.1 s (D. Caldwell, personal communication). The thermistors were molded into sections of fairing together with bridge/amplifiers. Power and signals were transmitted by electrical conductors running through the tail sections of the fairing. The thermistors were calibrated in the laboratory prior to the experiment.

Pressure sensors were also installed on the chain. The pressure sensors were manufactured by Kulite and were installed in tail sections of fairing together with bridge/amplfiers in a fashion similar to the thermistor electronics. The pressure sensors were calibrated in a pressure bomb prior to the experiment. Prototype conductivity sensors were also installed on the chain. Unfortunately they did not operate sufficiently well to provide data of value.

The locations of the sensors relative to the depressor are shown in Table 1. The instrumented section of the chain was 82 m in length. The total length of the chain was 120 m .

Signals from the sensors were recorded, processed and displayed by use of a minicomputer system manufactured by Digital Equipment Corporation (PDP 11/05). Calibrated cross-sections and vertical profiles of temperature were plotted simultaneous to data acquisition.

A more complete description of the thermistor chain system is given by Spoering and Paulson (1980).

Table 1. Location and operation of sensors on the towed chain. The stations have either a temperature, conductivity or pressure sensor installed denoted by $\mathrm{T}, \mathrm{C}$ or P . The distance along the chain from the depressor to the sensors is denoted by $S$ which has units of "chain-meters." One chain-meter equals 40 in or 1.016 m .

| ChanneI No. | Station | $\begin{gathered} \mathrm{S} \\ \text { Chain-Meters } \end{gathered}$ | Operating Sensors (yes $=\mathrm{y}$ ) |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Run 1 | Run 2 | Run 3 | Run 4 |
| 0 | T0 | 8.5 | y | y |  |  |
| 1 | CO | 9.0 |  |  |  |  |
| 2 | T1 | 9.5 |  |  |  |  |
| 3 | PO | 11.0 | y | y |  |  |
| 4 | T2 | 13.0 |  |  | y | Y |
| 5 | T3 | 17.0 | Y | y |  |  |
| 6 | T4 | 21.0 | y | y |  |  |
| 7 | T5 | 24.5 | y | y |  |  |
| 8 | Cl | 25.0 |  |  |  |  |
| 9 | T6 | 25.5 |  | y |  |  |
| 10 | T7 | 29.0 | y | y | y |  |
| 11 | T8 | 33.0 | y | y | y |  |
| 12 | T9 | 37.0 |  | y |  | y |
| 13 | T10 | 40.5 | Y | y |  |  |
| 14 | C2 | 41.0 |  |  |  |  |
| 15 | T11 | 41.5 |  | y | y | y |
| 16 | T12 | 45.0 | y | y | y |  |
| 17 | Pl | 47.0 | Y | Y | Y | Y |
| 18 | T13 | 49.0 | y |  |  |  |
| 19 | T14 | 53.0 | y | y | y | y |
| 20 | T15 | 56.5 | y | y |  |  |
| 21 | C3 | 57.0 |  |  |  |  |
| 22 | T16 | 57.5 | y | y | y | y |
| 23 | T17 | 61.0 | Y |  | y | y |
| 24 | T18 | 65.0 | y | y | y |  |
| 25 | T19 | 69.0 |  | y | y | y |
| 26 | T20 | 72.5 | y | y |  |  |
| 27 | C4 | 73.0 |  |  |  |  |
| 28 | T21 | 73.5 | y | y | Y |  |
| 29 | T22 | 77.0 | y | y | y | y |
| 30 | T23 | 81.0 | y | y | y | y |
| 31 | T24 | 85.0 | y |  |  |  |
| 32 | P2 | 87.0 |  |  |  |  |
| 33 | T25 | 88.5 | Y |  | y | y |
| 34 | C5 | 89.0 |  |  |  |  |
| 35 | T26 | 89.5 | y | y | Y |  |

## OBSERVATIONS

The thermistor chain was towed by the NOAA Ship OCEANOGRAPHER north of Hawaii on four occasions during the month of January 1980. The tow tracks for each of the four runs are shown in Figures 1 and 2. The times at the beginning and end of each run are given in the captions of the figures. The positions at two-hour intervals from the beginning of each run are plotted in Figures 1 and 2 and are given in Table 2. The tow track was determined from a combination of satellite fixes and dead reckoning. Tow speeds tabulated in Table 2 were determined from satellite fixes and from a time series of the output of the ship's speed $\log$ which was recorded simultaneous to towing. Tow directions tabulated in Table 2 are determined from satellite fixes and from a time series of the output of the ship's gyro. The depths of the highest and lowest temperature measurements are also tabulated in Table 2. The depths of sensors were determined from a combination of the pressure measurements and a model of the configuration of the chain under tow. The model is described by Baumann et al. (1980) supplemented by material in Appendix $D$ of this report.

The temperature observations were low-pass filtered by computing sequential $30-s$ averages. Filtering removes variations caused by surface gravity waves and the pitch, roll and heave of the ship. The filtered observations are shown in Appendices A, B, and C.

An example of the frontal structure observed near $33^{\circ} \mathrm{N}$ is shown in Figure 3. Immediately following 0910 there was a small temperature inversion below an isothermal surface layer. Just after 0940, warming began at a depth of 94 m and progressed upward. The temperature of the surface layer remained nearly uniform in the vertical, although its depth and temperature varied in the horizontal. Following 1030 warming occurred near the surface


Figure 1. Track of the towed thermistor chain during Runs 1 and 2. Run 1 began near $34 \mathrm{~N}, 150 \mathrm{~W}$ at 0040 GMT, 16 January 1980, and ended at 1600 on the same date. Symbols (diamonds) are plotted at the beginning and end of the track and in two-hour intervals from the beginning. Run 2 began near $32 \mathrm{~N}, 152 \mathrm{~W}$ at $0520 \mathrm{GMT}, 17$ January 1980 and ended at 0245 , 19 January. As in Run 1, symbols are plotted at the beginning and end of the track and in two-hour intervals from the beginning. The turn to the north at 29 N occurred at 1655 GMT, 18 January 1980.


Figure 2. Track of the towed thermistor chain during Runs 3 and 4, Run 3 began near $30.5 \mathrm{~N}, 153.2 \mathrm{~W}$ at 0700 GMT, 25 January 1980, and ended at 1700 on the same date. The turn toward the southwest occurred at 0820 GMT. A course change of $180^{\circ}$ was made at 1312 GMT. Run 4 began near $29.6 \mathrm{~N}, 154.4 \mathrm{~W}$ at 1900 GMT, 27 January 1980 and ended at 1650, 28 January. The symbols in both tracks are plotted at the beginning and end of each track and at intervals of two hours from the beginning.

Table 2. Navigation during tows and depths of the highest and lowest temperature measurements on the chain during FRONTS-80.
Positions are tabulated at the beginning and end of each run and at two-hour intervals from the beginning. The positions were determined from navigational satellite fixes and dead reckoning. Distance traveled, tow direction from positions and the ship's gyro, and tow speed from positions and the ship's log are tabulated for intervals subsequent to the given times and positions. Tow direction from the gyro and tow speed from the ship's log were corrected to agree in the mean with directions and speeds determined from the satellite fixes.


| 1 | 16 | 0040 | 33 | 51.12 | 150 | 04.98 | 19.05 | 223.4 | 223.5 | 2.65 | 2.42 | 15.2 | 96. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 0240 | 33 | 43.62 | 150 | 13.50 | 20.12 | 220.7 | 223.1 | 2.79 | 2.88 | 14.6 | 95.5 |
|  |  | 0440 | 33 | 35.40 | 150 | 21.96 | 21.99 | 221.4 | 224.9 | 3.05 | 3.00 | 14.4 | 95.0 |
|  |  | 0640 | 33 | 26.46 | 150 | 31.38 | 23.16 | 223.8 | 228.0 | 3.22 | 3.16 | 14.1 | 94.4 |
|  |  | 0840 | 33 | 17.40 | 150 | 41.70 | 24.35 | 225.7 | 227.9 | 3.38 | 3.25 | 14.0 | 94.0 |
|  |  | 1040 | 33 | 08.22 | 150 | 52.92 | 23.32 | 219.6 | 221.3 | 3.24 | 3.26 | 14.0 | 94.0 |
|  |  | 1240 | 32 | 58.50 | 151 | 02.52 | 21.07 | 208.3 | 213.9 | 2.93 | 2.84 | 14.7 | 95.6 |
|  |  | 1440 | 32 | 48.48 | 151 | 08.88 | 9.57 | 209.8 | 214.4 | $1.99^{1}$ | $2.24{ }^{1}$ | 15.3 | 97.1 |
|  |  | 1600 | 32 | 43.98 | 151 | 11.94 | - | - | - | - | - | - | - |
| 2 | 17 | 0520 | 31 | 54.00 | 152 | 05.46 | 18.22 | 219.9 | 215.7 | 2.53 | 3.35 | 8.0 | 87.7 |
|  |  | 0720 | 31 | 46.44 | 152 | 12.90 | 25.16 | 219.2 | 216.3 | 3.49 | 3.52 | 7.7 | 86.9 |
|  |  | 0920 | 31 | 35.94 | 152 | 22.98 | 25.75 | 223.1 | 219.9 | 3.58 | 3.50 | 7.7 | 87.0 |
|  |  | 1120 | 31 | 25.74 | 152 | 34.08 | 25.75 | 223.7 | 219.6 | 3.58 | 3.54 | 7.7 | 86.8 |
|  |  | 1320 | 31 | 15.66 | 152 | 45.30 | 25.33 | 222.6 | 218.9 | 3.52 | 3.52 | 7.7 | 86.9 |
|  |  | 1520 | 31 | 05.58 | 153 | 56.10 | 24.99 | 222.3 | 216.7 | 3.47 | 3.44 | 7.8 | 87.3 |
|  |  | 1720 | 30 | 55.62 | 153 | 06.66 | 24.40 | 222.4 | 217.3 | 3.39 | 3.39 | 7.9 | 87.5 |
|  |  | 1920 | 30 | 45.84 | 153 | 16.98 | 23.02 | 219.2 | 215.8 | 3.20 | 3.39 | 7.9 | 87.5 |
|  |  | 2120 | 30 | 36.18 | 153 | 26.10 | 22.83 | 215.9 | 215.9 | 3.17 | 3.16 | 8.2 | 88.5 |
|  |  | 2320 | 30 | 26.16 | 153 | 34.50 | 23.29 | 214.3 | 218.3 | 3.24 | 3.38 | 7.9 | 87.6 |
|  | 18 | 0120 | 30 | 15.78 | 153 | 42.66 | 22.91 | 220.3 | 227.1 | 3.18 | 3.09 | 8.3 | 88.7 |
|  |  | 0320 | 30 | 06.30 | 153 | 51.90 | 23.20 | 221.5 | 229.6 | 3.22 | 3.09 | 8.5 | 88.7 |
|  |  | 0520 | 29 | 56.94 | 154 | 01.50 | 24.11 | 223.0 | 229.7 | 3.35 | 3.32 | 8.0 | 87.8 |
|  |  | 0720 | 29 | 47.40 | 154 | 11.70 | 24.70 | 223.6 | 226.3 | 3.43 | 3.32 | 8.0 | 87.8 |
|  |  | 0920 | 29 | 37.74 | 154 | 22.26 | 24.98 | 224.7 | 225.7 | 3.47 | 3.34 | 8.0 | 87.8 |
|  |  | 1120 | 29 | 28.14 | 154 | 33.18 | 25.01 | 225.3 | 221.2 | 3.47 | 3.38 | 7.9 | 87.6 |
|  |  | 1320 | 29 | 18.60 | 154 | 44.16 | 25.75 | 220.8 | 217.5 | 3.58 | 3.35 | 8.0 | 87.7 |
|  |  | 1520 | 29 | 08.04 | 154 | 54.54 | 26.98 | - 2 | - 2 | $3.75{ }^{2}$ | $3.42^{2}$ | 7.9 | 87.4 |
|  |  | 1720 | 29 | 03.30 | 155 | 02.82 | 36.54 | 003.2 | 010.1 | 5.08 | 5.04 | 4.5 | 76.4 |
|  |  | 1920 | 29 | 23.04 | 155 | 01.56 | 36.60 | 005.1 | 007.8 | 5.08 | 4.91 | 4.8 | 77.5 |
|  |  | 2120 | 29 | 42.78 | 154 | 59.58 | 32.70 | 005.3 | - | 4.54 | 4.65 | 5.4 | 79.6 |
|  |  | 2320 | 30 | 00.42 | 154 | 57.66 | 43.38 | 044.2 | 043.2 | 6.02 | 6.00 | 2.2 | 67.5 |
|  | 19 | 0120 | 30 | 17.22 | 154 | 38.82 | 23.97 | - 3 | - 3 | 4.70 | 5.67 | 3.0 | 70.6 |
|  |  | 0245 | 30 | 28.44 | 154 | 34.32 | - | - | - | - |  |  |  |

Table 2. (con't)

| $\begin{aligned} & \text { Run } \\ & \text { No. } \end{aligned}$ | Date <br> (Jan <br> GMT) | Time <br> (GMT) | $(d \in g)$ | Lat. <br> (min) | W. (deg) | ong. <br> (min) | Dist. <br> (km) | Nav. <br> Dir. <br> (deg) | Gyro <br> Dir. <br> (deg) | Nav. <br> Speed <br> (m/s) | Log Speed (m/s) | T-D <br> Top <br> (m) | ths <br> Bot. <br> (m) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 3 | 25 | 0700 | 30 | 33.66 | 153 | 12.42 | 38.88 | 4 | - 4 | 5.40 | 5.43 | 3.6 | 68.4 |
|  |  | 0900 | 30 | 27.18 | 153 | 33.60 | 39.74 | 216.9 | 215.5 | 5.52 | 5.39 | 3.7 | 68.8 |
|  |  | 1100 | 30 | 09.96 | 153 | 48.48 | 39.76 | 221.1 | 218.0 | 5.52 | 5.41 | 3.6 | 68.6 |
|  |  | 1300 | 29 | 53.76 | 154 | 04.80 | 36.26 | -5 | 5 | 5.04 | 5.23 | 4.0 | 70.2 |
|  |  | 1500 | 30 | 05.16 | 153 | 52.86 | 33.33 | 043.1 | 047.4 | 4.63 | 5.19 | 4.1 | 70.6 |
|  |  | 1700 | 30 | 19.08 | 153 | 38.04 | - | - | - | - | - | - | - |
| 4 | 27 | 1900 | 29 | 37.62 | 154 | 23.52 | 36.26 | 6 | -6 | 4.99 | 5.36 | 4.4 | 69.0 |
|  |  | 2100 | 29 | 20.34 | 154 | 33.72 | 35.42 | 200.2 | 196.8 | 4.92 | 5.34 | 4.5 | 69.2 |
|  |  | 2300 | 29 | 02.34 | 154 | 41.28 | 35.39 | 198.1 | 196.8 | 4.91 | 5.33 | 4.5 | 69.3 |
|  | 28 | 0100 | 28 | 44.16 | 154 | 48.06 | 37.65 | 198.6 | 197.0 | 5.23 | 5.38 | 4.4 | 68.8 |
|  |  | 0300 | 28 | 24.84 | 154 | 55.44 | 39.02 | 197.1 | 196.8 | 5.42 | 5.39 | 4.4 | 68.8 |
|  |  | 0500 | 28 | 04.68 | 155 | 02.46 | 38.41 | 195.0 | 193.9 | 5.34 | 5.38 | 4.4 | 68.8 |
|  |  | 0700 | 27 | 44.58 | 155 | 08.52 | 39.29 | 195.3 | 193.8 | 5.46 | 5.37 | 4.4 | 68.9 |
|  |  | 0900 | 27 | 24.06 | 155 | 14.82 | 38.86 | 197.4 | 196.8 | 5.40 | 5.43 | 4.3 | 68.4 |
|  |  | 1100 | 27 | 03.96 | 155 | 21.84 | 38.34 | 200.1 | 196.5 | 5.32 | 5.44 | 4.2 | 68.3 |
|  |  | 1300 | 26 | 44.46 | 155 | 29.82 | 38.91 | 199.9 | 196.4 | 5.40 | 5.38 | 4.4 | 68.8 |
|  |  | 1500 | 26 | 24.66 | 155 | 37.86 | 34.23 | 200.7 | 196.5 | 5.19 | 5.31 | 4.6 | 69.5 |
|  |  | 1650 | 26 | 07.32 | 15.5 | 45.12 | - | - | - | - | - | - | - |

[^0]

Figure 3. An example of frontal structure observed near $33.3^{\circ} \mathrm{N}$, $150.0^{\circ} \mathrm{W}$ during FRONTS-80. The temperature sensors are distributed between depths 14 to 94 m .
and the temperature gradient changed sign with warm water overlying cold water. The cold spike at 0955 occurred at a depth of 94 m and is believed to have been caused by the upward displacement of cold water in the seasonal thermocline. Most of the fronts observed during the experiment were not as complex as the example shown in Figure 3 in that they did not exhibit a reversal of vertical temperature gradient.

A second example of frontal structure is shown in Figure 4. As shown in Figure 2, the tow direction at 1130 GMT was toward the southwest. Sudden warming together with stratification was encountered at 1236. This was followed by sudden cooling and vanishing stratification at 1255. A course change of $180^{\circ}$ was made at 1312 and the same warm dome was observed while towing toward the northeast. The temperature structure is remarkably symmetric with respect to 1312 GMT. The width of the warm dome is a little greater on the tow toward the northeast, but this might be accounted for by a variation in tow speed and by traversing the warm dome in a slightly different location.

A third example of frontal structure observed near $26.6^{\circ} \mathrm{N}$ is shown in Figure 5. The change in surface temperature of nearly two degrees across the front was the largest observed during the experiment. The maximum horizontal temperature gradient at the surface exceeds $1^{\circ} \mathrm{C} / 3 \mathrm{~km}$.

Near-surface observations of temperature and salinity were taken aboard the NOAA Ship OCEANOGRAPHER throughout the experiment. Hourly positions from the bridge $\log$ are plotted in Figure 6 as a function of time. Hourly observations of temperature, salinity and density are plotted in Figure 7, also as a function of time. Temperature in a sea chest at a depth of about 5 m was measured continuously and hourly samples were logged. Water from the sea chest was pumped to the lab and circulated through a container where conductivity and temperature were measured continuously by use of a CTD


Figure 4. An example of frontal structure observed during Run 3. There was a $180^{\circ}$ course change at 1312 . Temperature sensors were distributed between denthc of 1 and


Figure 5. An example of frontal structure observed during Run 4
near $26.6^{\circ} \mathrm{N}$. Temperature sensors were distributed


Figure 6: Hourly positions of the NOAA Ship OCEANOGRAPHER during FRONTS-80. The thin line is N. latitude and the thick line is $W$. longitude.



Figure 7. Observations from the NOAA Ship OCEANOGRAPHER of nearsurface intake temperature (light line), salinity (heavy line), and density (intermediate line).
(Bisset Berman Model 9040). Hourly values were logged and water samples were also taken each hour. Salinity of the samples was determined by use of a salinometer and occasionally by titration. A time series of salinity determined by the three aforementioned methods appears in Figure 8. Some of the obviously erroneous values have been removed. The difference between salinity from the CTD and from the salinometer and titration is shown in Figure 9. The mean difference is about $0.02 \%$ with little evidence of systematic variation during the experiment.

The variations in surface salinity and density shown in Figure 7 are useful for interpreting temperature structure of the type shown in Figures 3-5. Variations in surface temperature and salinity tend to be in phase, with some exceptions, thereby reducing fluctuations in density. The increase in surface temperature shown in Figure 3 (16 January) was associated with an increase in salinity resulting in a small change in density. However, the increase in temperature shown in Figure 5 ( 28 January) was associated with negligible change in salinity and a correspondingly large change in density ( $\sim 0.5 \sigma_{t}$ ).


Figure 8. Observations of near-surface intake salinity from the NOAA ship OCEANOGRAPHER. The solid line is from a CTD, + and $o$ are from samples evaluated by use of a salinometer and by titration respectively.


Figure 9. Observations from the NOAA ship OCEANOGRAPHER of nearsurface intake salinity determined by use of a CTD minus salinity samples evaluated by a salinometer (+) and by titration (0).

## REFERENCES

Baumann, R. J., C. A. Paulson and J. Wagner, 1980: Towed chain observations in JASIN. Report, Reference 80-14, School of Oceanography, Corvallis, OR 97331, 202 pp.

Paulson, C. A. and P. P. Niiler, editors, 1980: FRONTS-80: Preliminary results from an investigation of the wintertime North Pacific subtropical front. Report, School of Oceanography, Oregon State University, Corvallis, OR 97331.

Spoering, T. J. and C. A. Paulson, 1980: Towed observations of internal waves in the upper ocean. (Submitted to J. Phys. Oceanog.).

## APPENDIX A

Highest and Lowest Temperature vs Time

On the following pages are 5 plots of the tow track of the thermistor chain given as north latitude (thin line) and west longitude (thick line) vs time. Following the tow tracks are 5 plots of the highest (thick line) and lowest (thin line) temperature measurements vs time. The depths of these measurements are given in Table 2. The temperature measurements are low-passed, computed by averaging over sequential $30-s$ intervals.











## APPENDIX B

Temperature Cross-Sections

On the following pages there are plots, one for each two-hour period from the beginning of each run, of temperature measurements as a function of time and distance along the tow. The operating temperature sensors are shown in Table 1. In the case of operating sensors one meter apart, only one of the measurements was plotted. The tow speeds and directions and the depth of the highest and lowest temperature measurements are given in Table 2. The temperature measurements are low-pass filtered, computed by averaging over sequential $30-\mathrm{s}$ intervals.
















































## APPENDIX C

Temperature Profiles

On the pages following Table 3 are plotted sequential temperature profiles observed during tows of the thermistor chain. Intervals for plotting were selected to include periods when frontal structure was observed. The intervals are given in Table 3. Each profile is an average over 30 s of measurements. The depths of the thermistors are marked on the right side of each illustration. The temperature scale on the abcissa is correct for the first profile at the left of each illustration. Subsequent profiles have their temperature scale shifted $0.15^{\circ} \mathrm{C}$ from their predecessor. Missing profiles are indicated by a black dot.

Table 3. Intervals for which temperature profiles are plotted.

| Run No. | Date (Jan GMT) | Time Begin (GMT) | Time <br> End <br> (GMT) |
| :---: | :---: | :---: | :---: |
| 1 | 16 | 0430 | 0450 |
|  |  | 0620 | 0640 |
|  |  | 0820 | 0900 |
|  |  | 0940 | 1440 |
| 2 | 17 | 0525 | 0550 |
|  |  | 0630 | 0710 |
|  |  | 0750 | 0910 |
|  |  | 0930 | 1120 |
|  |  | 1150 | 1300 |
|  |  | 1610 | 1650 |
|  |  | 1850 | 1930 |
|  |  | 2050 | 2200 |
|  |  | 2220 | 2330 |
|  | 18 | 0500 | 0520 |
|  |  | 1130 | 1320 |
|  |  | 1440 | 1720 |
|  |  | 1820 | 1840 |
|  |  | 1902 | 1920 |
|  |  | 2050 | 2118 |
|  |  | 2120 | 2200 |
|  |  | 2250 | 2310 |
|  |  | 2313 | 2320 |
| 3 | 25 | 1320 | 1400 |
| 4 | 27 | 2220 | 2350 |
|  | 28 | 0100 | 0120 |
|  |  | 0240 | 0420 |
|  |  | 0540 | 0610 |
|  |  | 0740 | 0930 |
|  |  | 1330 | 1420 |
































































































$\nabla \angle 1$


## APPENDIX D

## Configuration of the Chain Under Tow

Expressions for the shape of the chain under tow were derived by Baumann et al. (1980). The analytical expressions were derived by neglecting accelerations so that the problem reduced to finding a solution to the problem of the hanging chain. A model for the shape of the chain is required for interpolating between measurements of depth on the chain and to predict the depths of sensors for various lengths of submersion and tow speeds.

One of the parameters required by the models is the drag force $D$ per unit length of chain or per unit vertical distance. This force was assumed to be of the form

$$
D=C A \rho U^{2}
$$

where $C$ is the drag coefficient, $A$ the cross-sectional area of the chain per unit length, $\rho$ the density of water and $U$ the tow speed. Baumann et al. assumed the value of $C=0.13$ as suggested by the manufacturer of the fairing and found reasonable agrement between models and observations for tow speeds up to $3.5 \mathrm{~m} / \mathrm{s}$ and submerged lengths of 70 m . Given that $C=0.13, C A \rho$ equals 2.6 Newtons $/ \mathrm{m}^{3} \mathrm{~s}^{-2}$ for the chain in question.

During FRONTS-80 we had about 100 m of submerged chain in the water and towed at speeds up to $6 \mathrm{~m} / \mathrm{s}$ thereby providing a more critical test of models and the drag coefficient $C$. We found that the value of $C$ suggested by the manufacturer of the fairing was too large. A value of $C A \rho=1.7$ Newtons $/ \mathrm{m}^{3} \mathrm{~s}^{-2}$ gives good agreement between observations and predictions of the mode1. This corresponds to a value of $C=0.085$. The model chosen assumed drag proportional to $s$, the distance along the chain.

The difference between observations of depth and predictions of the model is shown for two depths as a function of tow speed in Figure 10. The mean difference is about 1 m which is mostly likely due to uncertainty in the calibration of the pressure sensors. The scatter at tow speeds below $4 \mathrm{~m} / \mathrm{s}$ is about $\pm 1 \mathrm{~m}$. At tow speeds greater than $4 \mathrm{~m} / \mathrm{s}$, the scatter is $\pm 2 \mathrm{~m} / \mathrm{s}$ and shows a systematic difference dependent on sensor.

The observed and predicted difference in depth between the pressure sensors as a function of tow speed is shown in Figure 11. The shapes of the curves are similar although there is a systematic difference ranging from about 0.5 m at low tow speeds to about 1 m at high tow speeds.

We conclude that there is satisfactory agreement between the model and the measurements to within $\pm 1 \mathrm{~m}$ at tow speeds below $3 \mathrm{~m} / \mathrm{s}$ and to within $\pm 2 \mathrm{~m}$ at speeds between 3 and $6 \mathrm{~m} / \mathrm{s}$. The lack of agreement is partly if not substantially caused by uncertainty in the calibrations of the pressure sensors as shown by lack of consistency between the measurements.


Figure 10. The difference in depths predicted by a model of the shape of the towed chain and depths measured at 11 and 47 m upward along the chain from its bottom. The difference is plotted as a function of tow speed.


Figure 11. The distance between pressure sensors on the towed chain as calculated from a model and as measured. Both estimates are plotted as a function of tow speed.

In Figures 12, 13 and 14 the shape of the chain is plotted using the new value of the drag coefficient. The origin of the curves ( $x=z=0$ ) is at the depressor. The curves may be compared with similar curves in Baumann et al. which resulted from the old value of $C$ (0.13). All other parameters were assumed to be the same. For tow speeds less than $3 \mathrm{~m} / \mathrm{s}$ the chain is not far from vertical and predictions of sensor depths from the models depend weakly on choices of parameters or models.


Figure 12. The shape of a towed thermistor chain, 100 m in length, for tow speeds ranging from 1 to $6 \mathrm{~m} / \mathrm{s}$. The drag force on the chain is assumed proportional to $s$, the distance along the chain.


Figure 13. The shape of a towed thermistor chain, 100 m in length, for tow speeds ranging from 1 to $6 \mathrm{~m} / \mathrm{s}$. The chain is assumed to be weightless in water and the drag force is assumed proportional to $Z$.


Figure 14. The shape of a towed thermistor chain, 100 m in length, for tow speeds ranging from 1 to $6 \mathrm{~m} / \mathrm{s}$. The chain is assumed to be weightless in water and the drag force is assumed proportional to $s$ the distance along the chain.


[^0]:    ${ }^{1}$ Slow decrease in speed from 1330 to 1430 as the wind and seas picked up (ship made constant turns during this period).
    ${ }^{2}$ Course changed at 1655 hours from 220 to 003 speed also increased.
    ${ }^{3}$ Course change at 2320 hours from 003 to 040. Course change at 0152 hours from 035 to 015. Course change at 0200 hours from 015 to 345.
    ${ }^{4}$ Course change at 0820 hours from 270 to 218.
    ${ }^{5}$ Course change at 1312 hours from 222 to 042.
    ${ }^{6}$ Course change at 1959 hours from 221 to 199.

