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COMPARATIVE STRENGTH PROPERTIES OF WOODS GROWN IN THE UNITED STATES 1930 No. Con IPN

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L. J. MARKWARDT Assistant in Charge, Section of Timber Mechanics Forest Products Laboratory, Forest Service

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UNITED STATES DEPARTMENT OF AGRICULTURE, WASHINGTON, D. C.

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FOREWORD

The information contained in this bulletin is of value in making comparisons of species of wood in order to determine the choice of species for specific uses. Technical terms have, as far as possible, been omitted from the body of the bulletin, and the various properties determined from over a quarter million tests have been combined into simple comparative figures. This bulletin supplements but does not supersede United States Department of Agriculture Bulletin 556, Mechanical Properties of Woods Grown in the United States, (4)³ which presents the basic information from which the comparative figures have been derived. Since Bulletin 556 was issued additional tests have been made and some additional species have been tested. In all cases the comparative figures presented here are based on the latest available results. Bulletin 556 should be used when technical data on the properties of clear wood are required by engineers, archi-

¹Acknowledgment is made to J A. Newlin and T. R. C. Wilson of the Forest Product Laboratory for assistance in the preparation of this bulletin, and to W. A. Shewhart of the Bell Telephone laboratories for suggestions regarding variability analysis. ⁴Maintained by the Forest Service. United States Department of Agriculture, at Madison, Wis., in cooperation with the University of Wisconsin. ⁴Reference is made by italic numbers in parentheses to "Literature cited," p. 38.

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tects, and others, or when, in the judgment of the user, it is more applicable than the comparative figures presented here.

Although this bulletin gives figures only on weight, shrinkage, and strength, it is of course evident that other properties and factors, such as resistance to decay, painting and finishing qualities, tendency to leach coloring matter, size and character of prevalent defects, marketing practice, and the like must also be considered in selecting a species or in determining the suitability of a wood for different uses. Attention is also called to the fact that, because of the considerable variation in properties of all species of wood, it is often possible to select individual pieces of a weak species exceeding in strength the average of a stronger one, and to segregate the wood of a species into classes according to weight and strength, so that each class may be directed to the uses for which the class is best suited. In this way the variability of wood may be turned from a liability to an asset.

> CARLILE P. WINSLOW, Director, Forest Products Laboratory.

HISTORICAL

The strength of wood has always been an important factor in its use, but it is becoming even more significant with the increasing competition from other materials, the increasing production of new or little-used species, and the changing requirements of consuming markets. Considered broadly, three periods can be recognized in our forest history as affecting timber utilization: The land-clearing period, the timber-mining period, and the timber-crop period, which we are now entering.

During the so-called land-clearing period some of the best-known hardwoods, such as yellow poplar and black walnut, occupied the richer agricultural regions in the East before giving way to the plow. Together with the softwoods they furnished from selected logs abundant material to supply the building and other needs of the time. Consequently, lumber was used in greater quantities and in better grades than were actually required. Often the best species found their way into commonplace uses, as, for example, the employment of black walnut for floor joists, fence rails, and the like. Utilization of local supplies prevailed, and long expensive hauls were not required. While these forests were giving way to agriculture, timber was a by-product of land clearing, and economy was neither practiced nor necessary.

The period of timber mining, which followed, furnished the material to meet much of the industrial growth of the country. Only the most far-seeing could realize that such extensive forests as the magnificent white pine stand of Michigan and Wisconsin were exhaustible. The abundance of desirable species admirably adapted to the needs of the country, the short haul to market, and cheap labor resulted in a period of timber use with a per capita consumption far exceeding that of most other countries. The Nation became wood dependent, and timber, like ore, was removed without thought of replacement. As in the land-clearing period, lumber was still used in better grades than necessary, although there was a gradual awakening to the need of using wood more efficiently.

COMPARATIVE STRENGTH PROPERTIES OF WOODS

We are now on the threshold of the timber-crop period, which is based on the conception that timber is reproducible, like any other crop, except that the period of rotation is longer. Progressive lumber operators are carefully studying how to keep their forest lands actively growing timber, and a few are now operating on a sustained-yield basis. If forestry is practiced on land not suited to ordinary crops and if timber is efficiently utilized, the United States can reasonably be expected to meet most of its future timber requirements at least after an initial adjustment period.

NEED FOR INFORMATION ON PROPERTIES

Timber utilization in the present forest-crop period with its longer haul to market demands a higher degree of efficiency than that of previous periods, since modern competition necessitates that all materials be used to their best advantage to maintain their markets. A first requirement of efficient use is a knowledge of the properties. This knowledge is of value in several ways.

The increasing scarcity of certain species of timber which had become more or less standard in various wood-using industries, the wider competition in practically all markets, increased transportation facilities, and other factors are opening the field for other species. Through long use the properties which have made a species more or less standard are quite well understood, but it is not so generally known to what extent other available species possess these same properties, and to what extent they might supplement the established species.

Another need for information on properties is in the introduction of so-called little-used species. In the pushing of timber production into new regions, new species are encountered. Good crop management as conceived by many foresters and wood-utilization experts necessitates, at least so far as lumber and timber purposes are concerned, that certain species, such as western hemlock and white fir, be logged along with the well-known woods with which they grow rather than be left to dominate and propagate the succeeding crop. A knowledge of the properties is one of the first requirements in the use of alternate species and in the use of little-known woods.

PURPOSE

Wood utilization in the future must depend more and more on the true value of the product as determined by exact information on the properties rather than on rule-of-thumb practice. This bulletin presents exact information for the comparison of the strength properties of many of our native species. Other publications have usually presented strength data in technical terms familiar principally to architects and engineers, but here the technical values are combined into simplified comparative figures, which are more readily intelligible to the average person. For many purposes these simplified comparative figures will be found as useful as the technical values on which they are based.

The figures presented are especially applicable for two types of use (1) that relating to the alternation of one species with another and (2) that involved in selecting species for uses in which the strength

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requirements are known. The significance of the figures is shown and examples of their use are given.

PROPERTIES OTHER THAN STRENGTH

Although this bulletin presents figures only on weight, shrinkage, and strength, it should not be overlooked that other properties and factors must also be considered in the utilization of wood, and that the value of a wood for a given use is ordinarily based upon a combination of properties rather than upon a single property. Among other properties which may be of importance are nail-holding ability; splitting; tendency to warp; gluing qualities; painting and finishing characteristics; resistance to decay, weathering, and insects; insulating properties; and acid resistance. Information on these latter properties, however, does not come within the scope of this bulletin.

The relative usefulness of any lumber may also depend upon the characteristics of the stock in its entirety, as well as upon the properties of the clear wood, and may be influenced by sizes available, degree of seasoning, and marketing practice. Thus the mechanical properties of the clear wood may indicate that a species is an excellent wood for boxes for bulk commodities, but the lumber may be unsuited for such use because of a characteristic tendency of the knots to loosen and fall out. Furthermore, the advantage of inherently low shrinkage or high nail-holding power in a species may be lost through the method of marketing or the use of the species before it is sufficiently dry.

IMPORTANCE OF STRENGTH

There are few uses of wood in which its serviceability is not somewhat dependent upon one or more of its strength properties. Airplane wing beams, floor joists, and wheel spokes typify familiar uses in which strength is the principal consideration. Often strength in combination with other important properties is required. Thus, telephone poles, railroad ties, and bridge stringers require not only the capacity to carry loads, but also resistance to decay. In addition, a large number of uses of wood, not usually thought of in connection with strength, are dependent, at least to some degree, on strength properties. For example, finish and trim for buildings should be sufficiently hard to prevent easy marring; window sash must have screw-holding ability to permit secure attachment of hardware, as well as adequate stiffness to prevent springing when the window is opened and closed. Even matches must have strength to prevent their breaking when being lighted. Information on strength is therefore essential not only for the design of such engineering structures as airplanes, buildings, and bridges, but also as a guide for the selection of suitable species for a great variety of uses, whether it be the soft, light woods or the inherently stronger ones that are required.

⁴ Information on properties other than those presented in this bulletin may be obtained from the Forest Products Laboratory, Madison, Wis,

COMPARATIVE STRENGTH PROPERTIES OF WOODS

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EXPLANATION OF "STRENGTH"

Much confusion exists in regard to the meaning of "strength." In its broader sense, strength includes all the properties which enable wood to resist different forces or loads. In its more restricted sense, strength may apply to any one of the mechanical properties; in which event, the name of the property under consideration should be stated. If the several strength properties had the same relation to each other in all species, a wood which excelled in one strength property would be higher in all, and misunderstandings about the word "strength" would be less likely to occur. But such is not the case. A wood may rank better in one kind of resistance to load than in another. Longleaf pine averages higher than white oak in compressive strength (endwise), but is lower in hardness. Hence, it can not be said that longleaf pine is "stronger" than white oak without stating the kind of strength referred to. To be precise, in making a comparison of species, it is necessary to consider the kind of strength properties or combination of properties essential to the particular use, since different kinds of strength are essential in different uses. Thus, longleaf pine, because of its higher compressive strength (endwise), is superior to oak for use in short posts that carry heavy endwise loads, whereas oak, because of greater hardness, is superior in resistance to the wear and marring to which some floors are subjected.

NATURE AND SCOPE OF STRENGTH FIGURES

Several publications (3, 4, 5, and 10) present figures upon the strength properties of wood for small clear specimens and for structural timbers containing defects. Although such technical strength figures can be applied to all strength problems, there are, nevertheless, many uses of wood involving the selection of suitable species where the conversion of technical figures into simple comparative figures as is done in this bulletin would serve equally well. Since the strength figures given are composite values, or, in effect, index numbers, they are mainly for comparative purposes and are consequently not suitable for calculating the load-carrying capacity of wood.

The comparative figures for 164 native species are given in Table 1. The figures are based on an extensive series of tests on small clear specimens of wood begun by the Forest Products Laboratory in 1910. Each kind of wood, with few exceptions is represented by five or more trees. Some of the specimens were tested green from the tree, others after thorough seasoning (1). Collectively, the results include for each species figures on over 25 strength and other properties obtained from 10 different kinds of tests (4).

The more important test results for each species have been averaged and combined into comparative or composite figures which represent six properties, namely, bending strength, compressive strength (endwise), stiffness, hardness, shock resistance, and volumetric shrinkage. Definite figures for these essential properties are presented in Table 1, from which numerical comparisons may be made among the different species. Average figures on specific gravity, weight per cubic foot, and radial and tangential shrinkage (p. 20) are also included. The methods of computing the comparative figures of Table 1 are described in Appendix 2. TABLE 1.—Average comparative properties of the clear wood of species grown in the United States ¹ [For definition of terms and discussion of table see "Explanation of Table 1" in text]

Compara-tive figure 71 146 1147 123 123 153 139 Shock resistance id. 12 Compara-tive figure 48 119 104 64 119 107 103 103 108 Hardness Composite strength values² 12 Compara-tive figure 139 139 126 157 143 118 168 161 Stiffness Ħ Compara-tive figure 75 Compres-sive strength (endwise) 108 107 8888 106 -10 Compara-tive figure 76 85 110 107 107 88 88 113 Bending strength 0 metric (composite value)² Compara-tive figure 123 170 Shrinkage from green to oven-dry condition based on dimensions when green 121 144 113 1123 126 Volu-00 Per cent 7.3 10.1 Tangential 6.20 10.00 7.5 1-- cent 4.4 5.6 3.05 44.64 4.6 ACCOUNTINES. Radial 0 Per Pounds 28 47 At 12 per cent mois-ture con-404 428840 41 Weight per cubic foot NO. Pounds 46 55 Green 48 45 53 46 4 dry, based on volume when green Specific gravity, oven 0.37 . 51 55 48 53 . 54 0 10 110 80 m m 43 Trees Num-ber 64 Alder, red (Alnus rubra). Apple (Malus pumila var.) Ash, biltmore white (Fraxinus bilt--(Fraxinus pennsylvanica Ash, green (Fraxinus pennsylvanica lanceolata)...... Ash, Oregon (Fraxinus oregona)..... Ash, pumpkin (Fraxinus profunda)..... Ash, white (Fraxinus americana)..... Ashes, commercial white (ave. of 4 Common and botanical name of species species 3) -Hardwoods:

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Birch, Alaska white (Betula neoalas-	kana) Birch, gray (Betula populifolia)	Birch, paper (Betula papyrifera) Birch, sweet (Betula lenta) Birch, yellow (Betula lutea)	Blackwood (Avicennia nitida) Buckeye, yellow (Aesculus octandra) Bustic (Dipholis salicifolia)	Buttonwood (Conocarpus erecta)	Cascara (Rhamnus purchiana) Catalpa, hardy (Catalpa speciosa) Cherry, black (Prunus serotina) Cherry, pin (Prunus pennsylvanica) Chestnut (Castanea dentata)	Chinquapin, golden (Castanopsis chrys- ophylla)	Cottonwood, black (Populus trichocarpa) Cottonwood, eastern (Populus deltoides) Dogwood (Cornus florida) Dogwood, Pacific (Cornus nuttallii)	Elder, blueberry (Sambucus coerulea) Elm, American (Ulmus americana) Elm, rock (Ulmus racemosa) Elm, slippery (Ulmus fulva)	FIG, golden (Ficus aurea)	dum, plack (tystas sylvatica). Gum, plue (Eucalyptus globulus) Gum, red (Liquidambar styraciflua) Gum, tupelo (Nyssa aquatica) Gumbo-limbo (Bursera simaruba)	Hackberry (Celtis occidentalis). Haw, pear (Crataegus tomentosa) Dickory, bigleaf shagbark (Hicoria	Hickory, bitternut (Hicoria cordiformis).	Based on tests of small clear snortmore 91

wide, and 1 inchlong. Bending spectments, z by z incues in section except radial and tangential shrinkage which are based on width measurements of pieces 1 inch thick, 4 inches ber or in grades containing like defects, except structural material. Structural material which conforms to American lumber standards should be compared by means of alear lumworking stresses, values for which are presented in the Appendix 1. We find the method used in establishing the composite values, each of which is based on conforms to American lumber standards should be compared by means of allowable a The method used in establishing the composite values, each of which is based on combinations of several similar properties is presented in Appendix 2.

COMPARATIVE STRENGTH PROPERTIES OF WOODS

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	-	Specific	Weigh cubic	it per foot	Shrinkage condition when gre	from green t t based on en	o oven-dry dimensions		Compo	site strength	values	
Common and botanical name of species	Trees tested	gravity, oven dry, based on volume		At 12 per cent	Radial	Tangential	Volu- metric (composite value)	Bending strength	Compres- sive strength (endwise)	Stiffness	Hardness	Shock resistance
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Hardwoods-Continued. Hievery, nutmeg (Hicoria myristicae-	Num- ber		Pounds	Pounds	Per cent	Per cent	Compara- tive figure	Compara- tive figure	Compara- tive figure	Compara- tive figure	Compara- tive figure	Compara- tive figure
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Hickories, pecan (ave. of 4 species 4)	23.6	. 59	88	45	4.9	8.9	137	120	116	165	142	207
Hickories, true (ave. of 4 species 9)	122	.65	63	51	7.3	11.4	182	138	123	188		292
Hop-hornbeam (Ostrya virginiana)	145 55 25 22	50 50 73 73	63 57 71	5045 805 80	1.4.8.0 0.704.0	11.3 9.6 10.9	180 155 183 184	135 76 101 124	122 71 100 110	184 102 150 182	142 86 126 181	279 124 169
Ironwood, black (Krugiodendron fer- reum). Laurel, mountain (Kalmia latifolia). Locust, black (Robinia pseudoacacia) Locust, honey (Gleditsia triacanthos) Madroño (Arbutus menziesii).	400000	1.04 .62 .66 .58	. 22255	88 88 88 84 84 84 84 84 84 84 84 84 84 8	ది సా 4 లే గా లా సా 4 లే గాల్ల లా సా 4 లా 4	11.0000 11.0000	125 144 103 107 173	157 97 1157 112 86	168 110 111 88 88	254 110 153 117	143 161 155 114	130 113 144 93
Magnolia, cucumber (Magnolia acumi- nata)		. 44	49	34	5.2	* 00 00	137	90	88	175	57	103
Magnolia, evergreen (Magnolia grandi-	2	.46	62	35	5.4	6.6	126	81	82	136	80	141

TABLE 1.—Average comparative properties of the clear wood of species grown in the United States-Continued

[For definition of terms and discussion of table see "Explanation of Table 1" in text]

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Oak, southern red (Quercus rubra) 4 .52 62 41 4.5 Oak, swamp red (Quercus rubra pagodae- folia) 3 .61 68 48 5.2 Oak, swamp chestnut (Quercus prinus) 3 .61 68 47 5.9 Oak, swamp chestnut (Quercus bicolor) 1 .64 69 50 5.5	Oak, hooky mountain white (Quercus Utabensis) 3 .62 62 51 4.1 Oak, scarlet (Quercus coccinea) 5 .60 62 47 4.6	Oak, pin (Quercus palustris) 5 5 58 63 44 4.3 Oak, post (Quercus stellata) 10 60 63 47 5.4 4.0 Oak, post (Quercus borealis) 33 .56 63 44 4.0	Oak, canyon live (Quercus chrysolepis) 3 .70 71 54 5.5 Oak, chestnut (Quercus montana) 5 .57 61 46 5.5 Oak, laurel (Quercus laurifolia) 5 .56 65 44 4.0 Oak, laurel (Quercus laurifolia) 5 .56 65 44 4.0 Oak, live (Quercus virginiana) 5 .81 76 62 6.6 Oak, Oregon white (Quercus garryana) 10 .64 63 51 4.2	Mastic (Sideroxylon foetidissimum) 5 .89 77 65 6.1 Myrtle, Oregon (Umbellularia californica) 5 51 54 39 2.8 Oak, black (Quercus velutina) 8 .56 63 43 4.5 Oak, bur (Quercus macrocarpa) 5 .51 66 63 43 4.5 Oak, bur (Quercus macrocarpa) 10 .51 66 40 3.6	Maple, black (Acer nigrum). 1 .52 54 40 4.8 Maple, red (Acer rubrum). 14 .49 50 38 4.0 Maple, silver (Acer saccharinum). 5 .44 45 33 3.0 Maple, silver (Acer pennsylvanicum). 5 .44 45 33 3.0 Maple, striped (Acer pennsylvanicum). 22 .57 56 44 4.9	Magnolia, mountain (Magnolia fraser1)5.4047314.4Mangrove (Rhizophora mangle)5.4447675.4Maple, bigleaf (Acer macrophyllum)5.4447343.7

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COMPARATIVE STRENGTH PROPERTIES OF WOODS

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TABLE 1.-Average comparative properties of the clear wood of species grown in the United States-Continued [For definition of terms and discussion of table see "Explanation of Table 1" in text]

49 21 156 136 411 49 58 58 104 $^{98}_{162}$ 116 78 78 124 Shock resistance Compara-tive figure 100 Compara-tive figure 21 162 162 162 40 25 25 60 80 80 104 85558 8228 Hardness 3 Composite strength values Compara-tive figure 55 162 172 99 95 135 100 103 1103 1133 1133 103 94 167 Stiffness H sive strength (endwise) Compara-tive figure 84291 57 68 68 68 91 37 22 87 237 Compres-10 Compara-tive figure 74 74 91 Bending strength 40 120 120 120 120 248008 85 122483 6 Volu-metric (composite value) to oven-dry dimensions Compara-tive figure 89 250 82 137 137 145 1115 1104 158 652280 126 136 00 5.2 10.8 Shrinkage from green condition based on when green 7.12.8 98.7.08 9.99 9.1 Tangential 8.7 7.3 1.6 1 Per cent 1-2412 4400 6.3 1000010 10.04 5.0 cent Katanan Radial 40000 9 Per (At 12 per cent mois-ture con-Pounds 88338 40 524 227 633223 633336 Weight per cubic foot 10 Green Pounds 631462 34048 62 45435 522468 4 on volume when green Specific dry, based 38821 833 50 42 833 50 42 833 50 42 gravity 85883 50 **U**ADO \$ Trees -10 +10 10 11645 10 ເວັດເວັດເວັ Lo Door Num-ber 64 Sugarberry (Celtis laevigata)...... Sumach, staghorn (Rhus hirta)..... Sycamore (Platanus occidentalis)..... Walnut, black (Juglans nigra)...... Walnut, little (Juglans rupestris)...... Polsonwood (Metopium toxilerum) Poplar, balsam (Populus balsamifera) Poplar, Yellow (Liriodendron tulipifera). Rhododendron, great (Rhododendron Common and botanical name of species Osage-orange (Toxylon pomiferum) -Palmetro, cabbage (Sabal palmetto) Paradise-tree (Simarouba glauce).... Pecan (Hicoria pecan) -... Persimmon (Diospyros virginiana)... Sulvernen (ratesia caronna). Sourwood (Oxydendrum arboreum). Stopper, red (Eugenia confusa)...... Pigeon-plum (Coccolobis laurifolia) Hardwoods-Continued, maximum)

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COMPARATIVE STRENGTH PROPERTIES OF WOODS 93 53 53 79 52 47 551 81 72 72 91 187 35 50 107 38 188 47 5885254 885544 528 54 848834 886554 22023 8080 97 78 93 181 159 94 104 104 156 127 127 141 121 131 53 111028 88 83 41 818 2828 52 61 92 107 8 45 8658 28 126 18 280 69 63 121 112 92 103 103 103 1126 1142 95 110 803 127 127 127 98 1114 73 73 9.0 10.0 7.9 7.9 6.0 6.9 4.7 0.2 7.8 2.6 9.4.0.4.2 6.8 01 ró có 100 00 00 4.0.0 00 00 01 00 44400 5.0 12 00 00 CL CD 10 00 10 01 00 01 2.1 4.1 040 101 cici Nico 40.400 mainini 5 4 4 ci ti 0.4010 H 31 26 31 888 88 88 34 31 . 888888 882228 8888 ន្តន្តន្តន្ត 36 2926 37 33 45 8 88 38 37 4235235 414888 444 42 547 39 39 34 339 35 35 848 53 31 .45 41 452885 35 35 35 $\frac{38}{38}$ 48 30 37 38 38 38 concolor. 0000 00 00 5 26 26 15 15 34 10 100000 400000 13.03 1810 80000aa talis Cedar, southern white (Chamaecyparis thyoides) Cypress, southern (Taxodium distichum) Douglas fir (Pseudotsuga taxifolia) Douglas fir (Pseudotsuga taxifolia) (Rooky Mountain type). Fir, alpine (Abies balscarpa). Fir, corkbark (Abies balsamea). Fir, corkbark (Abies arizonica). Fir, lowland white (Abies grandis)..... Pine, jack (Pinus banksiana). Pine, jeffrey (Pinus jeffreyi). Pine, jimber (Pinus flexilis). Pine, loblolly (Pinus taeda) Pine, lodgepole (Pinus contorta) (coast type)______ Douglas fir (Pseudotsuga taxifolia), (in-Fir, noble (Abies nobilis)...... Fir, California red (Abies magnifica).... Fir, silver (Abies magnifis)..... Fir, white (Abies concolor)..... Firs, white (ave. of 4 species ¹⁰)..... Hemlock, eastern (Tsuga canadensis)... Hemlock, mountain (Tsuga mertensiana) Hemlock, western (Tsuga heterophylla). Cedar, northern white (Thuja occidenalligator (Juniperus pachy-Larch, western (Larix occidentalis) land empire type) Juniper, phloea).

Y. 10 Abies grandis, A. nobilis, A. amabilis, and

TABLE 1.-Average comparative properties of the clear wood of species grown in the United States-Continued

[For definition of terms and discussion of table see "Explanation of Table 1" in text]

		Specific.	Weigh	foot	Shrinkage condition when gree	based on en	to oven-dry dimensions		Compos	ite strength	values	
id botanical name of species	Trees tested	oven dry, based on volume	100 D	At 12 per cent	Radial	Tangential	Volu- metric (composite value)	Bending strength	Compres- sive strength (endwise)	Stiffness	Hardness	Shock resistance
		when green	паато	ture con- tent				- _	-==]	-	-[]	
1	2	3	4	10	9	7	ø	6	10	11	12	13
<pre>>ontinued. leaf (Pinus palustris) ntain (Pinus pungens) hern white (Pinus strobus) way (Pinus resinosa)</pre>	Num- ber 34 34 18 18 18 10	. 55 . 49 . 44 . 45	Pounds 50 54 36 42 36 50	Pounds 37 37 34 34	Per cent 5.3 3.4 4.6 4.0	Per cent 7.5 6.8 6.0 7.1 7.1	Compara- tive figure 124 107 107 107 116 116	Compara- tive figure 91 85 85 80 80	Compara- tive figure 93 67 91 76	Compara- tive figure 151 119 163 163	Compara- Compara- tive figure 76 35 46 56	Compara- tive figure 92 55 86 96
 (Pinus rigida serotina)	9012aa	8344 844 855 855 855 855 855 855 855 855 8	49 56 51 51 51 51	25 88 33 38 25 88 33 48	ය හති සං වි හි හි හි හි සං වි හි හි හි සං සං සං සං සං සං සං සං සං සං සං සං සං	0.020 0.0200 0.0200 0.0200000000	115 104 128 128 131	89 97 116 64	103 89 104 126 68	154 135 170 195 112	4888888	90 86 111 105 55
ern white (Pinus monticola) ern yellow (Pinus ponderosa) nus edulis) ¹¹ (Sequoia sempervirens) ock (Picea mariana)	418 55 30 57	8.50 8.50 8.80 8.80 8.80 8.80 8.80 8.80	* 55 32 55 32 55	883883	4.0.4.0.4 1.0.6 1.1.7 1.	1.0.1.4.0 48008	118 97 99 65 112	8 0 0 8 9	75 69 75 104 70	137 112 108 134 143	40 53 40 53 40 53 53 53 50 54 50 54 50 54 50 55 54 55 55 55 55 55 55 55 55 55 55 55	65 65 70 82
ngelmann (Picea engelmannii) . d (Picea rubra)	11 25 51 51	337.33	30 32 33 34 35 35 35 35 35 35 35 35 35 35 35 35 35	នេននេន	ಲ್ಲಲ್ಲು 4, 4, 4, 4, 00 ಲು 1- ಲು	180100 18000 19000 10000 100000 100000000	102 117 116 116 134	55 72 68 71	57 75 75 75 74	100 138 123 136	44 37 44 42 42	45 68 67 71

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Tamarack (Larix laricina) Yew, Pacific (Taxus brevifolia)	010	. 49	547	37	4.0	5.4	128 96	84 115	96 112	147	138	85
Percentage estimated probable varia- tion of species average when based on 5 trees ¹³		2, 1			5.2	4 0	0 m	20	с С		6	
Percentage estimated probable varia-						ł		2	0.0	0. 2	XX Ni	5.0
tion of an individual piece.		00		1			12	12	14	18	16	20
				-		-	-					

¹¹ The trees on which these values are based were somewhat higher in density than the general average for the species. It is, therefore, very probable that further tests which are now under way will slightly lower the present figures, although it is not expected that this will necessitate any change in the working stresses recommended for structural timber as ¹² *Picea rubra*, *P. sitchensis*, and *P. glauca*. ¹³ For percentage estimated variation of species when humber of trees see Table 6.

COMPARATIVE STRENGTH PROPERTIES OF WOODS

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VARIABILITY

Variability is common to all materials. If one tests pieces of wire from a roll, the loads necessary to pull the wire apart will vary for the different pieces. In the same way, the breaking strengths of different pieces of the same kind of string or rope will not be the same. Materials, however, differ considerably in the amount of variation or the spread of values.

Everyone who has handled and used lumber has observed that no two pieces, even of the same species, are exactly alike. The differences most commonly recognized are in the appearance, but differences in the weight and in the strength properties are of even greater importance. Fortunately, appearance and weight are related to strength. This relation, which is very definite in some species, affords the basis of grading and selecting wood for strength.

In determining the strength properties of wood many individual specimens of each species are tested, and consequently many individual test values are obtained. It would be very laborious and confusing to present the values for each individual test. The figures in Table 1 are, therefore, average values from tests on specimens selected to represent the different species of wood.

The strength properties of individual pieces may vary considerably from the averages shown. Therefore, the fact that one species of wood averages higher than another in a certain property does not mean that every piece of that species will be better than every piece of the other species. A percentage figure is shown in the last line of Table 1 to indicate the range above and below the average which may be expected to include half of all the material of a species.

Because of the variation among individual specimens, the more tests made on a species the greater is the probability that the average obtained will represent the true average. The number of test specimens must be limited, however, because of the expense of determining the properties, and as a result units of five trees have. in general, been used to obtain the test figure for a wood from any one site or locality.

For the more important species, two and often more 5-tree units representing different localities have been tested. The tests vary in number from about a hundred to many thousand for a species, making a total of over a quarter million for all species studied. The present figures (Table 1) are the best available determinations of the true averages, although the figures for the less important species, which are based on fewer tests, would be more subject to change on additional testing than those for the common species.

For the foregoing reason, and since individual pieces of wood or lots of material purchased for any use vary from the averages, too much emphasis should not be placed on small differences in average The importance of such differences, however, will depend figures. largely on the use to which the wood is put. Detailed information on the range of variations to be expected and a discussion of their significance are presented in Appendix 3.

SELECTION FOR PROPERTIES

The fact that a piece of wood differs in properties from another of the same species often makes it more suitable for a given use. This suggests the possibility of selecting pieces to meet given requirements. For example, selection may be made at the sawmill so that the heavier, harder, and stronger pieces go into structural timbers, flooring, or other uses for which the higher measure of these properties particularly adapt them, while the lightweight pieces may preferably be used for such purposes as trim or heat insulation; or selection may be made at the lumber yard when material of either high or low weight is required. By means of selective methods the variability of wood can be made an asset. Selection on the basis of freedom from defects is a common practice. Selection on the basis of quality of clear wood is much less common, but is frequently very desirable.

Aside from actual strength tests, the specific gravity or density gives the best indication of the strength properties of any piece of wood. Within any species there exists a relatively small range in the strength of pieces of like density.

When different species are considered, the range in strength for pieces of like density may be quite large. To illustrate the difference in density-strength relations between species, consider the values for Douglas fir (coast type) and red gum in Table 1. These woods are about equal in weight when dry per unit volume as shown by their specific gravities, but Douglas fir averaged 39 per cent higher in compressive strength than red gum and 18 per cent lower in shock resistance.

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It may be shown, likewise, that certain species of wood of medium density are equal in some properties to species of higher density. Douglas fir (coast type) with only three-fourths the density of commercial white oak is about equal to the oak in bending strength and compressive strength, and excels it in stiffness. Hence, Douglas fir is higher for its weight in these properties than white oak. In hardness and shock resistance, however, white oak averages much higher than Douglas fir.

HOW TO USE THE COMPARATIVE STRENGTH FIGURES

The strength figures in Table 1 (columns 9 to 13) are not percentages but are index numbers. They have no significance other than to give relative position in comparing species of wood for any specific use with respect to the several properties listed. The figures on weight and radial and tangential shrinkage, on the other hand, are in unit terms which can be used directly in making calculations or estimates.

In order properly to interpret and apply the figures in a comparison of species, one should be familiar with the requirements of his particular use. Unfortunately, no thorough study has been made to determine the properties essential to most uses, although in many cases much general information is available concerning them. Long usage has in some cases established what properties are required, but opinion frequently differs as to their importance. The most effective application of the figures, therefore, calls for judgment.

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WORKING STRESSES RECOMMENDED FOR COMPARING STRUCTURAL MATERIAL

For comparing structural material of grades in which the size. location, and number of defects are limited with reference to their effect on strength, the allowable working stresses of Table 2 (Appen: dix 1) are recommended in preference to the figures of Table 1. However, the figures of Table 1, although primarily for the comparison of species in the form of clear lumber, are second in importance only to permissible defects ⁵ in deriving safe working stresses (8). Other factors, such as differences in the variability of the clear wood, tendency of defects to develop in service, and tendency to run high or low in the grade, and the like, are, of course, also taken into account in determining working stresses.

Table 2 presents working stresses for a number of common species. Should working stresses be required for other species, they may be derived through the joint use of Tables 1 and 2. The method suggested is to assign to the species under consideration working stresses 10 per cent lower than are given in Table 2 for species having about the same comparative strength values. The 10 per cent reduction is suggested to provide for safety and to allow for the various factors that must be taken into account in assigning safe working stresses. If, however, the species on which working stresses are desired is known to be quite similar in all respects to the species used for comparison, the 10 per cent reduction need not be applied. (See example p. 18.)

EXAMPLES OF GENERAL COMPARISONS

1. Everyone knows how important strength is for shovel handles. Suppose that a manufacturer who has been using ash satisfactorily for shovel handles is offered a supply of hackberry as an alternate. How does hackberry compare with ash? Assuming the most important properties required in a shovel handle to be bending strength, hardness, shock resistance, lightness, and freedom from warping, then from Table 1 the following tabulation may be made:

	Bending strength	Hard- ness	Shock resistance	Weight (specific gravity)	Volu- metric shrinkage
Ash, commercial white	110	108	139	0.54	126
Hackberry	76	74	145	. 49	138

The lighter weight of hackberry would be an advantage. With the exception of shock resistance, hackberry is decidedly inferior to commercial white ash in the other properties listed. It would not only break more easily in bending, but because of its lower hardness it would also be more subject to mashing at the bolts or rivets. In addition, the slightly higher shrinkage indicates it would not stay in place so well as ash. The conclusion to be drawn from the comparison is not that hackberry is entirely unusable for shovel handles, but rather that average material could not be expected to be as satisfactory as ash.

⁵ Tests on structural timbers have established the effect of knots and other defects on strength, and have afforded the basis for preparing structural grades which develop any desired proportion of the strength of the clear wood.

If the inducement is sufficient the user may feel justified in accepting a lower standard of service. By selection methods, however (see p. 15), a wood which averages weaker can frequently be used without lowering the standard of service. If the difference in the average strength of two species is not too great, individual pieces of the weaker species can be obtained which will exceed in strength properties the average of the stronger one. Thus, carefully selected hackberry would make an acceptable shovel handle and one that would be unquestionably better than a handle of poor-quality ash.

This comparison is based on the assumption that the two species would be used in the same sizes. It is possible to make up for certain limitations in the strength of a weaker species of wood by increasing the dimensions of the part. Redesign involving change of size, however, may not always be feasible. In shovel handles the diameter must be such that the handle can be grasped readily. When the usable size is fixed, only species that are strong enough in this size are acceptable. Such practical questions as size must be considered in any change of design or substitution of species.

2. As another example of the practical application of the figures in Table 1, let it be required to compare sugar maple, beech, and yellow birch for flooring. These species are similar in structure in that they all belong to a class known as diffuse-porous woods, which do not have a marked difference in spring wood and summer wood. Among the properties of importance in flooring are shrinkage and hardness. For a comparison of these properties the following figures may be taken from Table 1:

	Radial shrinkage	Tangential shrinkage	Volumetric shrinkage	Hardness
Sugar maple	_ 4.9	9.5	147	115
Beech	_ 5.1	11.0	162	96
Yellow birch	- 7.2	9.2	166	86

From the figures listed sugar maple, on the average, would be expected to show slightly less change of dimension with given moisture changes than beech or yellow birch, and to offer greater resistance to indentation, wear, and scratching. There is little difference in the volumetric shrinkage figures for beech and yellow birch. Beech, however, averages somewhat higher in hardness.

The comparisons just given do not consider appearance. Since all three species rank relatively high in the physical properties listed, choice may frequently be based on other factors, such as color or price.

3. Just as the figures of Table 1 may be used to select species which are high in certain strength properties, they also serve in choosing the woods to use where ease of manufacture, which is associated with low mechanical properties, is desired. For example, it is generally recognized that wood used to make patterns for metal castings should be readily fashioned to any desired shape and should not change in size. Northern white pine admirably meets these requirements, and has for years been a standard wood for patterns that do not receive such continual use as to require a harder wood. Suppose that because of the scarcity of northern white pine other species are desired. From Table 1 it may be noted that sugar pine and western white pine are much like northern white pine in those

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properties which seem to be of first importance, and would, consequently, be among the best species to consider for pattern stock.

4. The preceding examples involve comparisons of species of wood for uses where clear straight-grained material is required. For structural material of grades in which the size, location, and number of defects are limited with reference to their effect on strength by the basic provisions for American lumber standards (8), the sizes should be determined and comparisons made as far as possible by means of the safe working stresses of Table 2, Appendix 1, except where these are in conflict with stresses fixed by law. The safe working stresses of Table 2 take into account not only the weakening effect of the defects permitted in the grade, variability, duration of stress, and similar factors, but also the natural chracteristics of the species.

When working stresses or comparisons for structural purposes are desired among species not listed in Table 2, the method suggested on page 16 involving the joint use of Tables 1 and 2 may be applied. Suppose, for instance, that working stresses are desired for lodgepole pine. From Table 1 it may be noted that in bending strength, compressive strength (endwise), stiffness, and hardness, lodgepole pine falls within the range of average values for northern white pine, western white pine, western yellow pine, and sugar pine. For the same grades and conditions of use, therefore, lodgepole pine may be assigned working stresses 10 per cent lower than the values given in Table 2 for northern white pine, without further detailed knowledge of the species. If the fact is known that lodgepole pine is similar to northern white pine in other respects than strength of the clear wood, the 10 per cent reduction in working stresses may be omitted. Hence, if lodgepole pine were included in Table 2, it would be listed with the species which take the same working stresses as northern white pine.

SPECIAL USES

Innumerable comparisons can readily be made from the figures of Table 1. However, there is still another useful type of comparison, namely, that in which several of the different comparative strength properties are combined to give a single figure. This offers an effective way of handling certain problems and has been used in comparing woods for railroad ties and for airplane wing beams, as well as in classifying species for ladder construction. To combine properly the comparative figures of Table 1, however, requires an accurate basic knowledge of the figures, as well as judgment of their relative importance in the proposed use. Because of the complicated nature of these comparisons their further consideration is postponed to Appendix 2.

EXPLANATION OF TABLE 1

(See Table, 1, p. 6.)

COLUMN 1. COMMON AND BOTANICAL NAME OF SPECIES

Column 1 gives the common and botanical names of the various species of wood as adopted by the Forest Service (7).

There are a number of closely related species that are very similar in their mechanical properties that can not be distinguished from an examination of the wood alone and that are generally marketed as a group under a single common name, as, for example, commercial white ash. For several such groups the values listed for the individual species comprising the group have been averaged to give a single figure for each property. The species combined are indicated for each group.

COLUMN 2. TREES TESTED

The number of trees tested shows the extent of the work done on each species, and is an aid in estimating the reliability of the average figures. The greater the number of trees tested, the closer may the figures be expected to approach the true average of the species. (See discussion under Variability, p. 14.)

COLUMN 3. SPECIFIC GRAVITY

Specific gravity is the relation of the weight of a substance to that of an equal volume of water. The specific-gravity figures in column 3 are based on the weight of the oven-dry wood and its volume when green.

Column 3 affords an excellent means for making comparisons of the weight of the dry wood of different species. The specific-gravity value gives a direct indication of the amount of wood substance in a given volume.

The weight of oven-dry wood in pounds per cubic foot (based on the volume when green) can be calculated from column 3 by multiplying the specific gravity by 62.4, the weight of water in pounds per cubic foot. The difference between the weight of any oven-dry wood calculated in this manner and the corresponding weight when green is the average weight of moisture present per cubic foot in the unseasoned wood just as it comes from the saw. The moisture present in green wood is of course subject to large variations.

COLUMNS 4 AND 5. WEIGHT PER CUBIC FOOT

Ordinarily, wood is spoken of as "dry" or as "green" or "wet." In order to be specific, various stages of drying or dryness must be recognized in establishing the weight, not only because of the effect of the moisture content on weight, but because of change in volume with moisture changes. The weights of wood at two important stages are given in columns 4 and 5.

When wood is green,⁶ or freshly cut, it contains a considerable quantity of water. After wood has dried by exposure to the air until its weight is practically constant, it is said to be "air dry." If dried in an oven at 212° F. until all moisture is driven off, wood is "oven dry."

The weight when green as given in column 4 includes the moisture present at the time the trees were cut, and is based on the average of heartwood and sapwood pieces as represented by test specimens taken from pith to circumference. The moisture content of green timber varies greatly among different species. Thus, in white ash it averages

⁶ Green wood usually contains "absorbed" water within the cell walls and "free" water in the cell cavities. In drying, the free water from the cell cavities is the first to be evaporated. The fiber-saturation point is that point at which no water exists in the cell cavities of the timber but at which the cell walls are still saturated with moisture. The fiber-saturation point varies with the species. The ordinary proportion of moisture—based on the weight of the dry wood—at the fiber-saturation point is from 22 to 30 per cent. As a rule, the strength properties of wood begin to increase, and shrinkage begins to occur when the fiber-saturation point is reached in seasoning.

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42 per cent, whereas in chestnut it averages 122 per cent.⁷ The moisture content also varies among different trees of the same species and among different parts of the same tree. In most softwood species the sapwood has more moisture than the heartwood. For instance the sapwood of southern yellow pine usually contains moisture in excess of 100 per cent, whereas the heartwood has only about 30 to 40 per cent moisture. Particularly in these species which have a higher moisture content in the sapwood, large variations in weight when green may occur, depending on the proportion of sapwood. Since young softwood trees contain a larger proportion of sapwood than old trees, their wood averages heavier when green.

The amount of moisture in air-dried wood depends on the size and form of the pieces and on the climate. The species vary widely in the rate at which they give off moisture in drying, and also in the rate at which they take up moisture during periods of wet or damp weather. The average air-dry condition reached in the northern Central States in material 2 inches and less in thickness, when sheltered from rain and snow and without artificial heating, is a moisture content of about 12 per cent. The figures given in column 5 are for this moisture content. The moisture content of thoroughly air-dry material may be 3 to 5 per cent higher in humid areas, and in very dry climates as much lower. Large timbers will have a higher average moisture content when thoroughly air dry than small pieces.

When the moisture content in comparatively dry wood changes. two actions which counteract one another take place, so that the unit weight or weight per cubic foot changes but little. Thus, if the wood dries further, the weight per cubic foot tends to become lower because of loss in moisture, while at the same time it tends to increase because shrinkage causes more wood substance to occupy the same space. Conversely, if wood absorbs moisture both the weight and volume are increased.

An approximate method for estimating the weight of wood per cubic foot at a moisture content near 12 per cent is to regard a onehalf per cent change in weight as accompanying a 1 per cent change in moisture content. For example, wood at 8 per cent moisture content weighs about 2 per cent less than at 12 per cent, whereas at 14 per cent moisture content the weight is about 1 per cent greater than at 12 per cent.

COLUMNS 6, 7, AND 8. SHRINKAGE

Shrinkage across the grain (in width and thickness) results when wood loses some of the absorbed moisture.⁶ Likewise, swelling occurs when dry or partially dry wood is soaked or when it takes up moisture from the air, similar to a sponge getting larger when wet. Shrinkage of wood in the direction of the grain (length) is usually too small to be of practical importance.⁸

The figures in columns 6 and 7 are average values of the measured radial and tangential shrinkages of small clear specimens in drying from a green to an oven-dry condition. The radial shrinkage is that across the annual growth rings in a cross section, such as in the width

⁶ See footnote 6 on page 19. ⁷ The moisture content of wood is commonly¹ expressed as a percentage of the weight of the oven-dry or moisture-free wood. If a specimen from an air-dry board weighed 112 grams immediately after being cut, and after oven drying weighed 100 grams, it is said to have contained 12 per cent moisture. In other words, the moisture content is the original weight minus the oven-dry weight divided by the oven-dry weight, which may be expressed as a percentage by multiplying by 100. ⁶ A ppreciable longitudinal shrinkage is associated with "compression wood," and other abnormal wood

structure. (See p. 34.)

of a quarter-sawed board; the tangential shrinkage is that parallel to the annual-growth rings in a cross section, such as in a flat-sawedboard.

Column 8 lists figures on the relative shrinkage in volume from the green to the oven-dry condition for the various species. These figures are computed from actual volume measurements of small clear specimens, combined with actual radial and tangential shrinkage measurements, the results of which are recorded in columns 6 and 7. Volumetric shrinkage values that are comparable with those of columns 6 and 7 may be obtained from column 8 by dividing the figures listed by 10.

The shrinkage which will take place in any piece of wood depends on a great many factors, some of which have not been thoroughly studied. In all species the tangential shrinkage is more than the radial, the average ratio being about 9 to 5. Hence, quartersawed (edge-grained) boards shrink less in width but more in thickness than flat-sawed boards. The ratio of radial to tangential shrinkage for a species is of value in determining the desirability of using quarter-sawed wood and indicates the checking which may be expected in large pieces containing pith. Ordinarily, the less the difference between radial and tangential shrinkage, the less is the tendency of such pieces to check in drying.

Air-dry wood is continually taking on and giving off moisture with changing weather or heating conditions. Time is required for these moisture changes, however, so there is always a lag between changes in the humidity of the air and their full effect on the moisture condition of the wood. The lag is greater in some species than in others. As a result some species having a large shrinkage from the green to the oven-dry condition do not cause as much inconvenience in use as woods with lower shrinkage, because they do not follow atmospheric changes so closely. The figures given do not take into account the readiness with which the species take on and give off moisture, and therefore should be considered as the relative shrinkage between woods after long exposure to fairly uniform atmospheric conditions or after the same change in moisture content.

COLUMN 9. BENDING STRENGTH

Column 9 gives figures on bending strength. Bending strength is a measure of the load-carrying capacity of beams, which are usually horizontal members resting on two supports. Examples of members subjected to bending are stadium seats, scaffold platforms, ladder steps, shovel handles, girders, bridge stringers, and floor joists. The figures for bending strength afford a direct comparison of the breaking strength of clear wood of the various species. They may also be used under certain conditions for comparing structural material in which defects are limited with reference to their effect on strength. (See p. 16.)

Bending strength in addition to other properties is essential in many uses, such as airplane-wing beams or spars, telephone and telegraph poles, mine lagging, railway ties, ladder side rails, pike poles, insulator pins, and wagon tongues. It is of less importance in studding, flooring, and subflooring.

If a species is low in bending strength it does not necessarily follow that it is unsuited for uses requiring this property. It does indicate, however, that larger sizes are required to carry given loads than are required for species which rank higher in this property.

COLUMN 10. COMPRESSIVE STRENGTH (ENDWISE)

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The figures of column 10, compressive strength, apply to comparatively short compression members. Compression members are generally square or circular in cross section, usually upright, supporting loads which act in the direction of the length. The loads tend to shorten the piece. Some examples of endwise-compression members are upright members in grand stands, mine props, vertical pieces which support girders in buildings, and vertical scaffold frame pieces.

When compression members are of a length about 11 times the least dimension, the slenderness has increased to such an extent that stiffness begins to be a factor in the strength. The quantities in column 10 are applicable to short columns having a ratio of length to least dimension of 11 (or less) to 1.

If one species is lower in compressive strength than another, the difference may be compensated by using a member of correspondingly larger cross-sectional area.

COLUMN 11. STIFFNESS

When any weight or load is placed on a member, a deflection is produced. Stiffness is a measure of the resistance to deflection and relates particularly to beams. It is one of the properties required in ladder side rails, golf shafts, floor joists, girders, rafters, and other beams as well as in long columns. The figures in column 11 give the average stiffness of the different species. Generally beams of species having high stiffness values deflect less under a load than the same sized beams of species having lower stiffness values. Difference in stiffness between species may be compensated by changing the size of members.

COLUMN 12. HARDNESS

Hardness is the property which makes a surface difficult to dent or scratch. The harder the wood, other things being equal, the better it resists wear, the less it crushes or mashes under loads, and the better it can be polished; on the other hand, the more difficult it is to cut with tools, the harder it is to nail and the more it splits in nailing. Hardness is desirable in such uses as flooring, furniture, railroad ties, and small handles. Some lack of hardness, that is, a degree of softness, is particularly desirable for uses such as drawing boards. The greater the figure given in the table, the greater the hardness of the wood.

There is a pronounced difference in hardness between the spring wood and the summer wood of some species, such as southern yellow pine and Douglas fir. In these species the summer wood is the denser, darker-colored portion of the annual growth ring. In such woods differences in surface hardness occur at close intervals on a piece, depending on whether spring wood or summer wood is encountered. In woods like maple, which do not have pronounced spring wood and summer wood, the hardness of the surface is more nearly uniform.

COLUMN 13. SHOCK RESISTANCE

Shock resistance is the capacity to withstand suddenly applied loads. Hence, woods high in shock resistance withstand repeated shocks, jars, jolts, and blows such as are given ax handles, wheel spokes, and golf shafts. Hickory possesses this shock resistance property to the highest degree of any of the common and well-known woods. The greater the figure in column 13, the greater is the shock resistance of the species.

PERCENTAGE ESTIMATED PROBABLE VARIATION

The percentage figures in the bottom two lines of Table 1, exclusive of footnotes, offer a means of estimating the variability, a detailed discussion of which is given in the Appendix 3.

The percentage figures in the last line of Table 1 indicate the variation, above and below the average, which may be expected to include half of all the material of a species. For example, consider the bending strength of red alder in Table 1. The bending strength (column 9) is 76, and the variation of an individual piece is 12 per cent. From these figures it may be estimated that the bending strength of one-half of the red alder would fall within the limits 67 and 85. The approximate proportion of material of a species falling within certain other percentages of the Table 1 values may be estimated on the basis of the following relations:

75 per cent is within 1.71 times the percentage probable variation. 82 per cent is within 2.00 times the percentage probable variation. 90 per cent is within 2.44 times the percentage probable variation. 96 per cent is within 3.00 times the percentage probable variation.

The percentage figures in the next to the last line indicate that there is an even chance that the true average is within these percentages of the figures in Table 1. The percentages given apply to species which are represented by five trees. Percentages applying to species represented by various numbers of trees from 1 to 50 are presented in Table 6.

Mortality statistics upon which insurance rates are based tell very closely how many men of any large group will live to be a certain age, but they do not enable one to say whether John Doe at that age will be included among the living. In a similar manner, the variability figures given in the next to the last line of Table 1 permit one to estimate how many of the species of wood will have their averages raised or lowered by a specified amount by additional tests, but one can not say that red alder or any other designated species will be raised by this amount.

APPENDIX 1

For the aid of engineers, architects, and others who desire additional information on the application and derivation of the figures in Table 1 the following information is given. A study of the three appendixes is not essential for the use of Table 1 for comparative purposes.

STRENGTH OF STRUCTURAL MATERIAL

The figures in Table 1 are most directly applicable to the comparison of species for uses requiring wood free from defects. For structural material of grades in which the size, location, and number of defects are limited with reference to their effect on strength, the relative strengths of the species are better represented by allowable working stresses used in design. Working stresses for select and common structural grades conforming to the basic provisions of the American lumber standards are given in Table 2. They are technical in nature and have been arrived at from a consideration of the strength and variability of the clear wood, the relation of density to strength, the effect of defects in structural sizes, the effect of long-continued loading, and the inherent characteristics of the species, such as prevalence of knot clusters, tendency to check in seasoning, and prevalence of the different species; those of Table 2 are assigned values, based not only on tests, but on experience and judgment. $\mathbf{24}$

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CANDOL Y ASSIN & BIRA (CI DADITATITIONAL SY)	TO AN OF A DO AN OF A			FI	oer stress i	n bending				
	Continuo	usly dry	Occasio	aally wet l	out quick!	y dried	More or l	ess continu	ously dam	p or wet
Species	All thic	knesses	Material and th	4 inches inner	Material and th	5 inches ticker	Material and th	4 inches inner	Material and th	5 inches icker
	Select grade	Common grade	Select grade	Common grade	Select grade	Common grade	Select grade	Common grade	Select grade	Common grade
Ash, black Ash, commercial white Aspen and largetooth aspen Basswood Beech	$\begin{array}{c} Lb8. \ per\\ sq. \ in.\\ 1,\ 000\\ 1,\ 400\\ 1,\ 800\\ 1,\ 500\end{array}$	Lbs. per sq. in. 840 1, 120 1, 120 1, 200	Lbs. per sq. in. 1, 070 1, 580 580 1, 150	Lbs. per sq. in. 910 490 490 490	Lbs. per sq. in. 1, 200 1, 200 1, 300 1, 300	Lbs. per sq. in. 960 520 520 1,040	Lbs. per sq. in. 710 890 440 440 890	Lbs. per sq. in. 760 770 370 370	Lbs. per sq. in. 1, 000 500 1, 000	Lbs. per sq. in. 640 800 400 400 800 800
Birch, paper. Birch, yellow and sweet Cedar, Alaska Cedar, western red Cedar, northern and southern white	1,500 1,100 750	1, 200 1, 200 720 600	1, 150 710 580	570 980 600 490	$\begin{array}{c} 750\\ 1,300\\ 1,000\\ 800\\ 650\end{array}$	1, 040 600 800 640 520	530 890 670 530	450 760 680 570 450	1, 000 750 600 600	480 800 600 480 480
Cedar, Port Orford Chestnut. Cottonwood, eastern and black Cypress, southern Douglas fir (western Washington and Oregon type) ³ .	1, 100 950. 1, 300 1, 600	$\substack{ 880 \\ 760 \\ 640 \\ 1, 040 \\ 1, 200 \\ \end{array}$	890 760 580 980 1, 233	760 650 830 983	$1,000\\850\\650\\1,100\\1,387$	800 680 520 880 1, 040	800 530 948 948	680 530 450 680 680	900 700 900 1, 067	720 560 880 800 800
Douglas fir (dense) ³ . Douglas fir (Rocky Mountain type) Elm, rock Elm, slippery and American. Fir, balsam	1, 750 1, 100 1, 100 1, 100	1,400 880 1,200 720	1, 349 800 1, 150 800 670	$1, 147 \\ 680 \\ 980 \\ 680 \\ 680 \\ 570 \\$	$1,517 \\ 900 \\ 1,300 \\ 750 \\ 750 \\$	1, 213 720 1, 040 600	1, 037 620 890 710 530	882 530 600 450	$1, 167 \\ 700 \\ 1, 000 \\ 800 \\ 600 \\ 600 \\$	933 560 800 840 480
Fir, commercial whits. Gum, red, black, and tupelo. Hemlock, eastern. Hemlock, western. Hickory (true and pecan)	1, 100 1, 100 1, 300 1, 900	880 880 880 880 1, 040 1, 520	800 800 800 1, 330	680 680 680 830 1, 130	900 900 1, 500 1, 500	720 720 720 1, 200	710 710 800 1, 070	009 009 009	800 800 1, 200	640 640 640 720 960

TABLE 2.—Working stresses for timber conforming to the basic provisions for select and common structural material of American lumber standards¹

COMPARATIVE STRENGTH PROPERTIES OF WOODS

800 220 800 220 800 220 800 200 200	933 640 640 640 640 640 640
1, 000 1, 000 1, 000	1, 167 800 800 800 800 800 800 800 800 800 80
680 530 760 750 750	882 600 600 830 600 600 600 600 600 600 600 600 600 6
800 830 830 830 830 830 830 830 830 830	1, 037 670 710 710 710 710 710 830
1, 040 720 960 1, 040	1, 213 640 800 800 800 800 800 800 800 800 800 8
1,100 1,300 900 1,200	$\begin{array}{c} 1,517\\ 800\\ 1,900\\ 1,900\\ 1,900\\ 1,900\\ 850\\ 1,100\\ 1,100 \end{array}$
830 910 983 983	1, 147 600 760 760 760 760 760 880 880 830
1, 150 1, 070 1, 070	1, 349 710 890 890 800 800 800 980 980
1, 200 1, 200 1, 120 1, 200	400 720 880 880 880 880 880 880 880 880 880 8
1, 200 1, 500 1, 400 1, 400	1,200 1,200 1,200 1,200 1,200 1,200
Maple, sugar and black Maple, sugar and black Maple, red and silver Plue, southern yellow 3. Pine, southern yellow 4.	Pine, Norway weater white, western yellow, and sugar Poplar, yellow Redwood Spruce, red, white, and Sitka Spruce, Engelmann Tamarack (eastern)

¹ American lumber standards: Basic provisions for American lumber standards grades are published by the United States Department of Commerce in Simplified Practice for Testing Materials, and in Amer. Ry. Engineering Assoc. Bul., vol. 30, No. 31, dated February, 1929. ² Stress in tension: The working stresses recommended for fiber standards of the Amer. Soc. ⁵ Extess in tension: The working stresses recommended for fiber stress in bending may be safely used for tension parallel to grain. ⁵ Extess in order to preserve the exact numerical relations among working stresses for grades involving rate of grades in volved and so fire states are bublished in when standards of the Amer. Soc. ⁵ Exact figures given: In order to preserve the exact numerical relations among working stresses for grades involving rate of growth and density requirements the values for ⁶ Exact figures fiven Washington and Oregon type) and for southern yellow pine have not been rounded off, as have the values for the other species.

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	Aver modu of el ticit	Nc vari with dition	expo or w gra	Lbs. 200 1, 100 1, 500 1, 500 1, 500 1, 600	88888 88888	11 11 11 1000 1000 1000 1000 1000 1000	44444	1,10 1,10 800 1,10 10 1,10 10 10 10 10 10 10 10 10 10 10 10 10 1
	g ratio of	less con- ly damp	Common grade	Lbs. per sq. in. 720 360 360 720	360 720 520 360	600 480 640 680 680 680 680	733 560 720 720 720 720 720	480 520 640 800
	nns having or less)	More or tinuous or wet	Select grade	Lbs. per sq. in. 500 900 450 900 900	450 900 650 650 450	750 600 800 907	992 900 500 500	600 650 800 1, 000
	short colui nsion of 11	ally wet dy dried	Common grade	Lbs. per sq. in. 440 440 440 880	440 880 560 400	660 800 800 800 800	933 640 880 600 480	560 560 720 960
	l to grain (least dime	Occasion but quick	Select grade	Lbs. per sq. in. 550 1,000 550 1,100	1, 100 750 700 500	$\begin{array}{c} 825\\700\\1,000\\1,000\\1,067\end{array}$	1, 167 800 1, 100 750 600	700 750 700 1, 200
	ion paralle length to	usly dry	Common grade	Lbs. per sq. tn. 520 880 880 560 560 560 960	520 960 560 440	720 640 880 880 880	1, 027 640 960 640 560	560 640 560 720 1, 200
	Compress	Continuo	Select grade	Lbs. per sq. in. 1, 100 1, 200 1, 200	1, 200 700 550	900 800 1,100 1,173	1, 283 800 1, 200 700	700 800 700 1, 500
inued	l shear 4	ad with ns of ex-	Common grade	Lbs. per sq. tn. 72 100 64 64 64 100	201 222 222 222 222 222 222 222 222 222	72 864 73 80 73 80 73 80 73 80 73 80 73 80 73 80 73 80 73 80 73 80 73 73 73 73 74 74 74 74 74 74 74 74 74 74 74 74 74	2880 100 88 88 88 88 88 88 88 88 88 88 88 88 8	112 858 856 856 856 856 856 856 856 856 856
s-Cont	Horizonta	Not vari conditio posure	Select grade	Lbs. per sq. tn. 125 80 80 80 125	70890 128 200 200 200 200 200 200 200 200 200 2	808898 808898	105 125 100 100	70 100 140 140
itandard	ndicular 1d com-	More or less contin-	uously damp or wet	Lbs. per sq. tn. 300 100 100 300 300	100 150 125 100	150 150 100 225 6 213	233 200 300 125 100	200 200 350 350
9	on perpe , select ar des	Occa- sionally	quickly dried	Lbs. per sq. tn. 375 125 125 375 375	150 375 200 150 140	200 200 125 250 6 240	262 225 375 175 125	225 225 400
8	Compressi to grain mon gra	Contin-	dry	Lbs. per sq. in. 500 150 150 500	200 250 175	250 300 350 347	379 275 500 250 150	0000000 000000000000000000000000000000
		Species		Ash, black Ash, commercial white Aspen and largetooth aspen Baseod Beech	Birch, paper Birch, yellow and sweet Cedar, Alaska Cedar, western red Cedar, northern and southern white	Cedar, Port Orford Chestnut. Contonwood, eastern and black. Cypress, southern Douglas fir (western Washington and Oregon type) ⁵ .	Douglas fir (dense) ³ . Douglas fir (Rocky Mountain type). Elm, rock. Elm, slippery and American. Fir, balsam.	Fir, commercial white. Gum, red, black, and tupelo. Hemlock, eastern. Hemlock, western. Hickory (true and pecan).

TABLE 2.—Working stresses for timber conforming to the basic provisions for select and common structural material of American lumber

COMPARATIVE STRENGTH PROPERTIES OF WOODS

Larch, western. Maple, sugar and black	325	225 375	300	125	001	1, 100	096	1,000	008	008	640	1, 300, 000
Maple, red and silver Oak, commercial red and white	350 500	250 375	300 300 300	100	001 001	1,000	640 800	006	560	88	480 640	1, 100, 000
Fine, southern yellow ^s	(0)	٢	۲		88		880		800		680	1, 600, 000
Pine, southern yellow (dense) ³	379	262	233	128	103	1, 283	1, 027	1, 167	933	992	262	1, 600, 000
and sugar Pine. Norway	250	150	125	20°	88	750	009	150	. 600	650	520	1,000,000
Poplar, yellow	250	150	125	88	83	200	640	80	560 560	9 <u>9</u> 99	560 480	1, 200, 000
	. 250	150	125	20	56	1, 000	800	006	720	150	009	1, 200, 000
Spruce, red, white, and Sitka	250	150	125	32	68	800	640	750	600	650	520	1, 200, 000
Sycamore.	300	200	150	28	28	000	480	550	440 600	450	360	800,000
Tamarack (eastern)	300	225	200	95	26	1,000	008	006	720	200	640	1, 300, 000
8 Wordd Amund Amund To and a to a	-	-			-							
A DESCRIPTION OF THE RESERVED AND A DESCRIPTION OF THE PARTY OF THE PA									1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1			

[•] Exact figures given: In order to preserve the exact numerical relations among working stresses for grades involving rate of growth and density requirements the values for longlas fir (western Washington and Oregon type) and for southern yellow pine have not been rounded off, as have the values for the other species.
[•] Joint details: The shearing stresses for joint details may be taken for any grades as 50 per cent greater than the horizontal shear values for the Select grade.
[•] Factors to be applied to average modulus of lasticity values: The values for modulus of elasticity are average for species and not safe working stresses. They may be used as values for computing average deflection of beams. When it is desired to prevent sag in beams values one-half those given should be used. In figuring safe loads for long columns we working stresses for the Common grade: The values given are for the Select grade.
[•] Working stresses for the Common grade: The values given are average for species and not safe working stresses. They may be used.
[•] Working stresses for the Common grade: The values given are for the Select grade. Working stresses in compression perpendicular to grain for the common grades of Douglas for western Washington and Oregon type) and southern yellow pine are 325, 225, and 200, respectively, for continuously dry, occasionally wer but quickly dried, and more or less continuously damp or wet conditions.

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Since moisture influences the strength and the durability of wood, certain of the allowable working stresses are varied with the moisture conditions to which the timber will be exposed. All of the values in any one vertical column of Table 2 are on the same basis, and comparison of species may be made for the specified conditions of use. Allowable working stresses also depend on the grade of timber, as determined by the size and location of defects. The figures in Table 2 apply to timber conforming to the basic provisions of American lumber standards for select and common structural material (2, 8).

EXPLANATION OF TABLE 2

(See Table 2, p. 24)

The following explanation of the values given in Table 2 may be of aid in their use:

Fiber stress in bending is a measure of the bending strength and is proportional to the load which can be carried by a beam of a given size. It is the same kind of strength measure as "Bending strength," as defined on page 21.

Compression perpendicular to grain is a measure of the bearing strength of wood across the grain. The surfaces of contact between a floor joist and a girder in a building are in compression perpendicular to grain. A high value in this property indicates that large loads across the grain can be supported without injury to the wood.

Horizontal shear is a measure of the capacity of a beam to resist slipping of the upper half upon the lower along the grain. This property becomes of great importance in beams whose depth is more than about one-twelfth the distance between supports.

Compression parallel to grain is a measure of the capacity of a short column to withstand loads acting in the direction of the length. It is similar to compressive strength (endwise) described on page 22. As the ratio of length to least dimension exceeds 11, the column becomes more slender and the capacity to carry end loads becomes more and more dependent upon stiffness until in long columns a length is reached where modulus of elasticity (stiffness) determines the loadcarrying ability. The values given are consequently not applicable to columns in which the ratio of length to least dimension exceeds 11 to 1.

Modulus of elasticity is a measure of the stiffness or rigidity of a material. It indicates the resistance of a beam to deflection. It measures the same property as stiffness, described on page 22. The higher the modulus of elasticity, the less will be the deflection under a given load.

Working stresses for design will also be found in the report of the building code committee (10) and in standards of the American Society for Testing Materials (2).

APPENDIX 2

METHOD OF COMPUTING COMPARATIVE STRENGTH AND SHRINKAGE FIGURES IN TABLE 1

There is a need for a system of simplified strength figures for wood whereby comparisons may be made by the average wood user without employing highly technical terms. To supply this need the Forest Products Laboratory has developed a method of combining various test results into five composite strength values 9 for which data are given in Table 1. Any method of combining data must involve considerable judgment and must be somewhat empirical; consequently, differences of opinion may exist as to the best procedure. This appendix presents the method used in deriving the composite figures presented in Table 1.

The method involves (1) determining what properties should be combined in each composite figure; (2) reducing the values which have been obtained in different tests and which may be in various units to a common basis; (3) weighting the individual properties according to their estimated relative importance; and (4) weighting and combining the composite values for green and air-dry material in a single composite figure.

⁹ These five strength values are bending strength, compressive strength (endwise), stiffness, hardness, and shock resistance,

PROPERTIES STUDIED

The fundamental data used as a basis for establishing the comparative figures were obtained from a comprehensive study begun by the Forest Service in 1910 to determine certain mechanical properties of woods grown in the United States (4). Data on 25 or more different properties were obtained from standard tests (1) on small clear specimens of both green and air-dry wood. These properties, listed under the standard tests used for determining them, are as follows:

1. Compression parallel to grain: Fiber stress at elastic limit. Maximum crushing strength. Modulus of elasticity.

2. Static bending:

- Fiber stress at elastic limit. Modulus of rupture. Modulus of elasticity. Work to elastic limit. Work to maximum load. Total work.
- 3. Impact bending: Fiber stress at elastic limit. Modulus of elasticity.
 - Work to elastic limit.

Height of drop of hammer causing complete failure.

- Compression perpendicular to grain: Fiber stress at elastic limit.
 Hardness (load required to imbed a ball 0.444 inch in diameter to one-half its diameter): Side grain (radial; tangential).

End surface.

- 6. Shear parallel to grain: Shear stress (radial; tangential).
- 7. Cleavage:
- Load per inch of width (radial; tangential). Tension perpendicular to grain: Tensile stress (radial; tangential).
 Tension parallel to grain: Tensile stress.

10. Shrinkage:

Radial. Tangential. Volumetric.

11. Specific gravity.

In several instances two or more of these tests yield data on the same property. For example, modulus of elasticity (stiffness) values are obtained from three different tests. Likewise hardness is indicated by both the compression perpendicular to grain and hardness tests. Bending strength is indicated by fiber stress at elastic limit in impact bending and by fiber stress at elastic limit and modulus of rupture in static bending. The comparative figures (Table 1) are the result of combining the values for each group of similar properties. However, several of the properties just listed were not used in determining the figures in Table 1.

REDUCTION FACTORS

On account of the differences in the nature, significance, and magnitude of these related test results they should not be combined by a direct average. Combining such properties as work to maximum load and total work in static bending (inchpounds per cubic inch) and height of drop in impact bending (inches), therefore, can best be done by first applying "reduction factors" to adjust the properties to a common basis. Numerical values of the reduction factors were established from formulas expressing the relation of each property to specific gravity. The specific gravity-strength relations determined from the average data for different species are given in Table 3. The equations as tabulated have recently been reestablished on the basis of all available data and for this reason differ somewhat from those previously published (5).

	Moisture condition			
Unit	Green	Air dry (12 per cent mois- ture content)		
ands per square inch do h-pounds per cubic inch do	10200G1.25 17600G1.25 35. 6G1.75 103G2	16700G1.26 25700G1.28 32.4G1.75 72.7G2		
o pounds per square men-	2360Gf	2800G		
ands per square inch 00 pounds per square inch. hes	23700G ^{1.25} 2940G 114G ^{1.75}	31200G1.28 3380G 94. 6G1.75		
unds per square inch _do, 0 pounds per square inch.	5250G 6730G 2910G	8750G 12200G 3380G		
unds per square inch	3000G2.25	4630G1.26		
unds do do	3740G2.25 3380G2.25 3460G2.25	4800G2.25 3720G2.25 3820G2.25		
	Unit Unit do	Unit Moisture unds per square inch		

TABLE 3.—Specific gravity-strength relations ¹

¹ The values listed in this table are to be read as equations, for example: Modulus of rupture for green material=17600G^{1.25}, where G represents the specific gravity, oven dry, based on volume at moisture condition indicated.

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For shock resistance the basis to which all component properties are adjusted is work to maximum load in static bending. Consequently, the reduction factor for work to maximum load is unity. The reduction factor for height of drop in impact bending is determined by its average relation to work to maximum load. For green material, the reduction factor is

$$\frac{35.6G^{1.75}}{114G^{1.75}} = 0.31^{-10}$$

The reduction factor for total work in static bending is likewise determined by its average relation to work to maximum load, and for green material is

$\frac{35.6G^{1.75}}{103G^2}$ = 0.41 ¹⁰

when G=0.50. Reduction factors applicable to the values for air-dry material were established in the same manner.

Unity reduction factors were used for each of the three determinations of modulus of elasticity in arriving at the composite stiffness figure, rather than the equation relations, since the modulus of elasticity values are all measures of the same property and are in like units.

WEIGHTING FACTORS

In combining the mechanical properties into comparative strength figures, weighting factors were applied according to the estimated relative importance of the properties entering into the combination. In bending strength, for example, modulus of rupture was given a weight of 2 as compared to each of the fiber stresses at elastic-limit values because of the greater importance of the modulus of rupture, and because the determinations of the elastic limit from curves are subject to the personal equation.

Table 4 lists the mechanical properties which enter into the composition of each comparative figure, together with the corresponding reduction and weighting factors.

¹⁰ When the equations of properties to be combined involve different exponents, the reduction factor obtainable varies with the specific gravity (G). In such cases the reduction factor used corresponds to a specific gravity of 0.50, this being approximately the average specific gravity of all species tested.

TABLE 4.—Properties	combined a	and rea	luction	and	weighting	factors	used in	deriving
	C	compan	ative fi	gure	8			

	Reducti	on factor	
Property	Green	Air-dry at 12 per cent moisture	Weight- ing factor
Bending strength:			
Fiber stress at elastic limit, static bending	1.72	1.54	1
Modulus of rupture, static bending	1.00	1.00	2
Fiber stress at elastic limit, impact bending	. 74	. 82	1
Compressive strength (endwise):			
Fiber stress at elastic limit, compression parallel to grain	1 2.82	1 2. 52	1
Maximum crushing strength, compression parallel to grain	1 2. 20	1 1.805	2
Stiffness:			
Modulus of elasticity, static bending	1.00	1.00	2
Modulus of elasticity, impact bending	1.00	1.00	1
Modulus of elasticity, compression parallel to grain	1.00	1.00	1
Hardness:			
Fiber stress at elastic limit, compression perpendicular to grain	1.00	1.00	2
End hardness, hardness test	. 80	. 96	1
Radial hardness, hardness test	. 89	1.24	1
Tangential hardness, hardness test	. 87	1. 21	1
Shock resistance:			
Work to maximum load, static bending	1.00	1.00	2
Total work, static bending	. 41	. 52	1
Height of drop, impact bending	. 31	. 34	2
Volumetric shrinkage:			
Radial plus tangential shrinkage (green to oven-dry)	\$ 1.00		1
Volumetrie shrinkage (green to oven dry)	\$1.00	a transmission of all the second second	2

¹ The reduction factors for compressive strength translate the values into terms of modulus of rupture so that the resulting values can be combined directly with "bending strength" to give a joint figure repre-senting "bending or compressive strength" (formerly called "strength as a beam or post"). To get "bending or compressive strength" give "bending strength" a weight of 4 and "compressive strength (endwise)" a weight of 3. ¹ Apply to values which represent shrinkage from the green to the oven-dry condition.

In calculating the comparative strength values the average test results for each species were used. The comparative values for green material (A) and for air-dry material (B) were separately calculated and were then combined as follows:

 $\frac{2A+B}{2}$ = comparative strength value (bending strength, etc.),

where A = value as calculated from averages for green material,

B = value as calculated from averages for air-dry material (12 per cent moisture).

It may be noted that the averages for green material were multiplied by 2 and those for air-dry material by 1 in arriving at the comparative strength values. This gives the figures for green material an apparent weight of 2, but in reality they receive an actual weight somewhere between 1 and 2 because no reduction factor was used to bring the figures for air-dry material to the same magnitude as those for green material. However, the averages for green material were intentionally given a somewhat greater weight than those from the air-dry because a larger number of tests are included.

The final comparative figure, therefore, does not represent either green or dry material, but approximates a condition of 20 per cent moisture content. The calculated results are indicated to only two or three significant figures in Table 1 and have, consequently, lost their identity as far as stress units are concerned. As tabulated, they are in effect index numbers.

SAMPLE CALCULATION

The following example will illustrate in detail the calculation method:

Required, the "bending strength" value for red alder (Alnus rubra). Given, the following average values (4) for the species, in pounds per square inch:

P:	Green	Air-dry
Mode stress at elastic limit, static bending	3,800	7, 100
Fib.	6, 500	10,000
"mer stress at elastic limit, impact bending	8,000	11, 700

¹Adjusted to 12 per cent moisture.

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(3) Calculation for green material (A):

Fiber stress at elastic limit, static bending	Strength value 3, 800	×	Reduction factor 1.72	w ×	eightin factor 1	ng ==	Product 6, 540
Fiber stress at elastic limit, impac	. 6, 500 t	×	1.00	×	2		13, 000
bending	- 8,000	Х	0.74	X	1	=	5, 920
Total Value for green material	-		25.460	÷	4 4		25,460 6,365 - 4
(4) Calculation for air-dry material (12 per ce	ent	moisture	co	ntent) (1	$B)^{0,000=A}$
Fiber stress at elastic limit, static	Strength value		Reduction factor	W	eightir facto <mark>r</mark>	ıg	Product
bending	7, 100	×	1.54	X	1 2		10, 930
Fiber stress at elastic limit, impact	10, 000	^	1. 00		2		20,000
bending	11, 700	X	0.82	Х	1		9, 594
Total					4		40, 524
cent moisture content)			40, 524	- ;-	4	==	10, $131 = B$
$94 \perp B$ (9 \vee	$6365) \pm 1$	013	1				

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(5) Bending strength
$$=\frac{2A+B}{3}=\frac{(2\times0505)+10151}{3}=7620.$$

The "bending-strength" values as calculated by the foregoing formula were divided by 100 before entering them in Table 1. This gives the value 76 for red alder, which agrees with the table.

The procedure for deriving the other comparative strength properties from the original data is similar.

SHRINKAGE IN VOLUME

The comparative shrinkage in volume figures (column 8, Table 1) were calculated according to the following formula:

Volumetric shrinkage =
$$\frac{R+T+2V}{3}$$

where R =average radial shrinkage,

T = average tangential shrinkage,

V = average volumetric shrinkage.

The volumetric shrinkage values as calculated by the foregoing formula were multiplied by 10 before being entered in column 8 of Table 1.

Radial and tangential shrinkage measurements were made on specimens 1 inch thick by 4 inches wide by 1 inch long, and shrinkage in volume measurements on specimens 2 by 2 inches in cross section by 6 inches long.

LIMITATIONS

There are certain limitations to the use of comparative strength figures or index numbers because the individual basic properties are masked. Therefore, when the data on individual basic properties can be more logically applied than the comparative strength values, they should be used in preference (4).

Another possible limitation of the comparative strength figures is that they represent neither green nor thoroughly air-dry material. In most instances practically the same comparisons would result if figures from green material only or from air-dry material only were combined. This will not be true, however, if a species is exceptional in its moisture-strength relations. Redwood, one of the common commercial species, is such an example, being very high in strength for its density when green and increasing less in strength with seasoning than most other woods. Comparisons from Table 1 will give such species too low a rating for a use in which the material will remain wet and too high for a use requiring dry stock. The comparative figures, except shrinkage, may be considered to represent material at about 20 per cent moisture content for bending strength, compressive strength, stiffness, and hardness. Shock resistance is not affected greatly by moisture changes, but usually incurs a slight loss rather than a gain with decrease in moisture,

In spite of such limitations, the comparative values are useful for many types of comparisons. Whether comparative strength values or basic strength properties should be used is a matter of judgment.

SPECIAL USES OF COMPARATIVE FIGURES

RAILROAD TIES

As illustrative of the special uses referred to on page 18, let it be required to sum into a single figure for each species the mechanical properties of most importance in railroad ties. Knowledge of the properties involved and their relative importance must be available (9) or assumed before attempting to arrive at such a figure. In ties bending strength is required to resist bending; compressive strength (endwise) to resist rail thrust against spikes; and hardness to resist rail cutting and mechanical wear. A method which has been used for combining these figures to obtain strength figures for crossties, in which hardness is given equal importance with bending strength and compressive strength combined (see footnote 1, Table 4), is as follows: Multiply the value given in Table 1 for bending strength by 4, that for com

pressive strength by 3, and that for hardness by 7. Add these products and divide by 14 to get the final number. This may be expressed by the formula:

Tie strength figure =
$$\frac{4D+3E+7F}{14}$$

where D = bending strength (column 9, Table 1),

E =compressive strength (column 10, Table 1), F =hardness (column 12, Table 1).

The strength figure for a chestnut crosstie, as calculated by this method, is 59; that for white oak, 104; from which it is seen that white oak, as is well known, is the better as far as strength is concerned. Other factors must, of course, be taken into account in selecting woods for ties, especially resistance to decay. This again calls for judgment and experience in evaluating the relative importance of durability (resistance to decay) and strength, in accordance with service conditions.

AIRPLANE WING BEAMS

The comparative strength values were used by the Forest Products Laboratory as a guide for appraising the relative suitability of the different species for airplane wing beams. The properties considered were specific gravity, bending and compressive strength, stiffness, and shock resistance. The weights given each of these properties were as follows: Weight

Bending and compressive strength (combined)	1
Stiffness	1
shock resistance	1.5

The values for bending and compressive strength, stiffness, and shock resistance were first expressed as ratios of the corresponding values for spruce, which was taken as the basis of comparisons. These ratios were then weighted as just shown and averaged. This average was divided by the specific-gravity ratio raised to the 3/2 power to get the final index of suitability.

In this analysis the consideration of such factors as influence of size on the strength, stiffness, and buckling of thin parts, together with the essential requirement in aircraft of keeping weight to a minimum, necessitated that a power of the specific gravity be used. Here, again, judgment was called for in the proper selection and weighting of the factors involved.

A somewhat similar system of analysis was used in classifying species in the development of the safety code for ladder construction. The data of Table 1 offer opportunity for many other types of analyses and comparisons, limited only by the judgment employed in their use.

APPENDIX 3

SIGNIFICANCE OF VARIABILITY

Brief reference has been made on page 14 to the variability of wood and other materials. It is important to know that wood is variable, but it is more important to know something of the nature and extent of this variability. The range of variability can be illustrated and better understood by considering the results of specific gravity determinations on 2,105 separate pieces of Sitka spruce which have been studied at the Forest Products Laboratory. These specific-gravity values are presented in Table 5, which lists the highest and lowest observed results, together with the number of pieces in different groups.

TABLE	5.—Results	of	specific	gravity	determinations	on	2,105	samples	of	Sitka
				S	pruce					

Specific gravity ¹ group limits	Pieces i	n group	Vari 0	ability 100	diag 200	ram 300	(number group) 400	of	specimens	in
$\begin{array}{c} 0.\ 220\ to\ 0.\ 239\\ .\ 240\ to\ .\ 259\\ .\ 260\ to\ .\ 279\\ .\ 280\ to\ .\ 279\\ .\ 280\ to\ .\ 279\\ .\ 280\ to\ .\ 319\\ .\ 320\ to\ .\ 319\\ .\ 320\ to\ .\ 339\\ .\ 340\ to\ .\ 359\\ .\ 360\ to\ .\ 379\\ .\ 380\ to\ .\ 379\\ .\ 400\ to\ .\ 419\\ .\ 420\ to\ .\ 439\\ .\ 440\ to\ .\ 459\\ .\ 440\ to\ .\ 459\\ .\ 480\ to\ .\ 479\\ .\ 480\ to\ .\ 579\\ .\ 520\ to\ .\ 559\\ .\ 560\ to\ .\ 559\\ .\ 560\ to\ .\ 559\\ .\ 580\ to\ .\ 559\\ .\ 580\ to\ .\ 559\\ .\ 600\ to\ .\ 619\\ .\ 620\ to\ .\ 639\end{array}$	Number 1 3 18 70 133 359 411 392 345 211 91 43 16 3 1 4 2 .1 0 0 1	$\left \begin{array}{c} Per \ cent \\ 0.\ 05 \\ .14 \\ .86 \\ 3.\ 33 \\ 6.\ 32 \\ 17.\ 05 \\ 19.\ 53 \\ 18.\ 62 \\ 16.\ 39 \\ 10.\ 02 \\ 4.\ 32 \\ 2.\ 04 \\ .76 \\ .14 \\ .05 \\ .19 \\ .09 \\ .05 \\ .00 \\ .05 \\ .00 \\ .05 \end{array} \right $						verag	26 3	

¹ Specific gravity oven-dry based on volume when green. Average specific gravity equals 0.364; highest observed specific gravity 0.626; lowest 0.236.

It may be noted that the specific gravity of the heaviest piece ¹¹ included in the series was two and two-third times that of the lightest, and that the number of very heavy and very light pieces is quite small. Most of the values are grouped quite closely about the average.

The manner is which the samples tend to group themselves about the average is called a frequency distribution, from which the chances of departure from the average can be estimated by computation. Such a calculation, assuming a socalled normal distribution and representative material, leads to the expectation that one-half of the Sitka spruce samples would be within less than 7.5 per cent of the average specific gravity, or between the limits 0.337 and 0.391, and that approximately only one-fourth would be below 0.337 and one-fourth above 0.391. The figure defining such limits, 7.5 per cent in this case, is called the probable variation. By actual count, 51.7 per cent of the pieces studied (1,089) have a specific gravity between 0.337 and 0.391, whereas that of 24.8 per cent (522) was below 0.337 and that of 23.5 per cent (494) was above 0.391. As might be

¹¹ The exceptionally heavy pieces of Sitka spruce result from an abnormal growth called compression wood frequently occurring in the underside of leaning trees and limbs. Compression wood also forms in other softwood species, and, unlike normal wood, it has a large endwise or longitudinal shrinkage which causes softwood species, and, unlike normal wood, it has a large endwise or longitudinal shrinkage which causes warping and twisting when it occurs in the same piece with wood of normal growth. Longitudinal shrink-age as high as 2½ per cent has been observed in compression wood, whereas the longitudinal shrinkage of normal wood is a small fraction of 1 per cent. Compression wood is very dense and includes what appears to be an excessive summer-wood growth. Compression wood in most species shows but little contrast in color between spring wood and summer wood. Large differences in weight from causes other than com-pression wood are also found. Thus, in certain softwood species some pieces are increased in weight because of the resinous materials they contain, while in some hardwoods, such as tupelo and ash, unusually light-weight wood is formed in the swelled butts of swamp-grown trees.

expected, the percentages determined by actual count do not agree exactly with the foregoing calculated percentages, but the agreement is sufficiently close to show the value of the theory in estimating the variability even when a normal distribution is assumed. The frequency distribution of the specific gravity values for these 2,105 samples of Sitka spruce is shown as a diagram in the last column in Table 5.

The figures in Table 1 are each based on tests of a number of pieces, some of which were above and some below the average, just as with the specific gravity of Sitka spruce. In using wood of any species one may desire to know the proportion of material within a given range in any property or to know the probable amount the averages may be changed by additional tests. After tests have been made it is of course easy from the results to determine the proportion of the test pieces which were within any given range, but one can only estimate the degree to which this test data applies to other specimens and to the reliability of the averages. In other words, one would like to know the true average values of each species, a quantity which can not actually be obtained. The best that can be done is to consider the laws of chance operative and thus estimate the probable variation which may be expected from given average values. Such is the basis of the suggestions and estimates of variability presented in Table 1 and Appendix **3**.

It would be desirable to present the variation of each property of each species as determined from the detailed data. However, the extensive calculations involving all properties and species have not been completed; and even if available, their presentation would be more involved than the nature of this bulletin warrants. Although it is known that all species are not exactly equal in variability, it is felt that they are enough alike so that estimates made on the assumption of an equal percentage variability for all species in a given property will be sufficient for most practical purposes.

PROBABLE VARIATION

EXPLANATION OF FIGURES

The variability of each property is indicated by the probable variation figures in the last two lines at the bottom of Table 1. In the next to the last line is given the estimated probable variation of the observed species average from the true species average. The value listed applies only when the observed average is based on tests from five trees.¹² The values for other numbers of trees may be obtained from Table 6. In the last line of Table 1 is given the estimated probable

¹² The method of calculating the variation of an individual tree is as follows:

$$\frac{\Sigma\left(\frac{a-\bar{a}}{\bar{a}}\right)^2 + \Sigma\left(\frac{b-\bar{b}}{\bar{b}}\right)^{2\!\!\!\!/} + \Sigma\left(\frac{c-\bar{c}}{\bar{c}}\right)^2 + \dots}{n_a + n_b + n_c + \dots}$$

where $\Sigma\left(\frac{a-\bar{a}}{\bar{a}}\right)^2 = \left(\frac{a_1-\bar{a}}{\bar{a}}\right)^2 + \left(\frac{a_2-\bar{a}}{\bar{a}}\right)^2 + \left(\frac{a_3-\bar{a}}{\bar{a}}\right)^2 \dots$

 $a_1, a_2, a_3 \dots$ being averages for specimens from each of the n_a trees (usually 5) of species-locality a and $a_1+a_2+a_3 \dots$

$$\ddot{a} = \frac{n_1 + a_2 + a_3 + a_4}{n_a}$$

 b_1 , c_1 , b_2 , c_2 , \overline{b} , \overline{c} , n_b , n_e ... being similarly defined.

It may be seen that σ as thus defined is not the usual root-mean-square deviation but is somewhat analogous to the coefficient of variation. It is in fact the weighted root-mean-square value of coefficient of variation as obtained from a number of samples. This may be seen by writing the above formula in the equivalent form:

$$n_{a}\left(\frac{\sigma_{a}}{\tilde{a}}\right)^{2} + n_{b}\left(\frac{\sigma_{b}}{\tilde{b}}\right)^{2} + n_{c}\left(\frac{ac}{\tilde{c}}\right)^{2} + \dots$$

$$n_{a} + n_{b} + n_{c} + \dots$$

Correcting for size of sample, $\sigma' = \frac{\sigma}{0.8407}$ (6), 0.8407 being used because the modal value is 5. Probable variation = 0.6745 σ' .

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variation of an individual piece ¹³ from the true average. The probable variation of 8 per cent for the specific gravity of an individual piece indicates that there is an even chance that a random specimen will fall within 8 per cent (above or below) of the average, and an even chance that it will differ more than 8 per cent from the average. To illustrate, suppose that the hardness of red alder is under consideration. The probable variation in hardness for an individual piece is found from Table 1 to be 16 per cent. Taking the hardness of red alder as 48, the hardness of one-half of the pieces will, on the average, fall between the values 40.3 and 55.7, while approximately one-fourth would be below 40.3 and one-fourth above 55.7. The greater the probable variation, the greater the difference that may be expected in values, and the less the certainty with which the average figures can be applied to individual pieces.

PROBABLE CHANGES IN OBSERVED AVERAGE

The extent of the probable change in the observed average for the different properties should be considered in comparing species. The estimated probable variation in the observed average of the species, when based on different numbers of trees, is given in Table 6.

N 1 4	G		Shrinkage			Com-		IS.	
trees	gravity	Radial	Tangen- tial	Volu- metric	strength	strength (endwise)	Stiffness	Hardness	Shock resistance
1	4.7	11.6	9.0	8.8	5. 5	7.3	7.2	6.3	11, 1
2	3.3	8.2	6.4	6.2	3.9	5.2	5.1	4.5	7.9
ð	2.7	6.7	5.2	5.1	3.2	4.2	4.2	3.6	6.4
5	2.4	0.0	4.0	4.4	2.0	3.0	0.0	0. Z	5.6
10	1.5	37	9.8	0.9	2.0	93	93	2.8	5.0
15	1.2	3.0	2.3	2.3	1.4	1.9	1.9	1.6	0.0
20	1.0	2.6	20	2.0	1.1	1.6	1.6	1.0	4. S
30	0.9	2.1	1.6	1.6	10	1.3	1.3	12	2.0
40	0.7	1.8	1.4	1.4	0.9	1.2	1.1	1.0	1.9
50	0.7	1.6	1.3	1.2	0.8	1.0	1.0	0.9	1.6

TABLE 6.—Percentage probable variation ¹ of the observed average from the true average of the species, when based on material from different numbers of trees

¹ The percentage probable variation of the average of the species is a figure such that there is an even chance that the true average is within this percentage of the observed average in Table 1.

Occasionally the variation The average is always the most probable value. may be much larger than indicated, but the probability of occurrence of a variation decreases rapidly as the magnitude of the variation increases.

The importance of the differences between species with respect to averages is dependent on the magnitude of this difference in relation to the probable variation of the averages, as well as on how exacting the strength requirements are for the particular use under consideration.

HOW TO ESTIMATE THE SIGNIFICANCE OF DIFFERENCES IN THE AVERAGE PROPERTIES OF TABLE 1

If the averages of any property of two species (Table 1) differ by an amount equal to the probable variation of the difference,¹⁴ there is one chance in four that

¹³ Estimated for each component property by combining the corrected probable variation of a tree, and the probable variation of an individual specimen from the tree, according to the usual method. The probable variation of composite figures was calculated by combining the probable variation of component properties, and second, complete correlation of properties. The correlation coefficient of component properties was found to approach unity (0.90 between fiber stress at elastic limit in compression parallel to grain and maximum crushing strength; 0.92 between fiber stress at elastic limit in impact bending and modulus of rupture in static bending). Values of probable variation for composite figures presented in Table 1 are estimated from calculations just referred to, and those of the last line, Table 1 further compared with calculations of probable variation of an individual piece from the species averages for a limited number of species. It is hoped that ultimately such calculations will be made with the data on all species.
¹⁴ The probable variation of the difference of two average figures is the square root of the sum of the squares of the probable variations of the averages. The probable variation of the average of any property may be estimated from the figures in Table 6. For an example, see page 37.

COMPARATIVE STRENGTH PROPERTIES OF WOODS

the true average for the species which is lower in that property on the basis of present data equals or exceeds the true average of the other. There is also one chance in four that the true average for the higher species exceeds that of the lower one by as much as twice the observed difference. When the averages differ by amounts which are 1, 2, 3, 4, or 5 times the probable variation of their difference, the chances of the true average of the lower species equaling or exceeding the true average of the higher, or of the observed difference being at least doubled are as follows:

TABLE 7.—Chance that if the true average were available the order would be reversed, or the true difference found to be at least twice as great as the observed, when the observed difference is 1, 2, 3, 4, or 5 multiples of the probable variation of the difference

Multiples	Chance	Multiples	Chance
1 2 3	1 in 4. 1 in 11. 1 in 46.	4 5	1 in 285. 1 in 2,850.

As an example, consider the figures for bending strength of 60 and 62 for black and eastern cottonwood, respectively (Table 1). These figures are based on five trees of each species. From Table 6 or the next to the last line of Table 1, the probable variation of the species when based on five trees is 2.5 per cent of the bending strength. Two and five-tenths per cent of 60 equals 1.50, and 2.5 per cent of 62 equals 1.55, the probable variations of these averages. The probable variation of the difference between the averages is then $\sqrt{(1.50)^2 + (1.55)^2}$ or 2.16; the observed difference in the average figures for bending strength (60 and 62) is 2, which is less than its probable variation, 2.16. The chance that the true average bending strength for black cottonwood equals or exceeds that for eastern cottonwood is approximately one in four. There is the same chance that the true average of eastern cottonwood exceeds that for black cottonwood by at least 4 (twice the difference in present average figures as shown in Table 1). Hence, the difference between the figures for black and eastern cottonwood with respect to bending strength is not important for most practical purposes.

As a second example, consider the figures for bending strength of 117 and 106 for sweet birch and yellow birch, respectively. (Table 1.) The figures for sweet birch are based on 10 trees, those for yellow birch on 17. From Table 6 the probable variation of the species average when based on 10 trees is 1.7 per cent and when based on 17 trees it is 1.3 per cent. (The figure for 17 trees is taken as midway between that given for 15 trees and 20 trees.) The probable variation in bending strength of sweet birch is 1.7 per cent of 117, or 1.99; of yellow birch is 1.3 per cent of 106, or 1.38. The probable variation of the difference between the averages is $\sqrt{(1.99)^2 + (1.38)^2}$ or 2.42. The difference between the observed averages (117 and 106) is 11, which is about four and one-half times its probable variation of 2.42. From Table 7 it may be estimated that the chances are only one in more than 285 that the true average for bending strength of yellow birch would equal or excel that for sweet birch. The importance of such differences will depend on the use to be made of the wood.

Calculations of probable variation as suggested above should not be taken too literally but should rather be regarded as estimates.

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