Kevin Donald Boston for the degree of _ Master of Forestry in Forest Engineering presented on May 31, 1991. Title: THE DEVELOPMENT OF A RAIL TRANSPORT MODEL AND ITS USE FOR THE PREDICTION OF RAIL SHIPPING COSTS FOR FOREST PRODUCTS IN OREGON. Abstract Approved: Dr. John Sessions

Transportation costs compose fifty to sixty percent of the total operating cost in the forest products industry. This paper develops a framework for incorporating rail transportation into a statewide multi-modal transportation planning model. It will allow for the analysis of various transportation scenarios that can possibly increase the efficiency of the forest products industry by reducing transportation costs.

This paper has two objectives. First, to develop a rail transport model (RTM) that is capable of predicting shipping cost for forest products within Oregon as a function of route alignment, grade, and volume shipped. second, to construct a model of the Oregon rail network. The nodes in the network were created at rail intersections, major cities, and towns with wood processing facilities.

The Rail Transport Model was constructed by simulating train performance over the 47 rail routes in the state with
varying quantities of lumber, plywood, and wood chips. The simulation results were then analyzed using simple linear regression to produce an equation for each route that predicts transportation cost for the quantity of wood products shipped. The coefficient of determination ( $\mathrm{R}^{\mathcal{F}}$ for the individual products varies from 0.50 to 0.99 . The average coefficient of determination for the regression equations over all links in the rail network for lumber, plywood, and chips is $0.736,0.828$, and 0.930 respectively. The average coefficient of determination for the combination of forest products is lower at 0.445.

An example of the use of transport cost equations is developed to find the breakeven volume between truck and rail transport for the route between Eugene and Coos Bay.

THE DEVELOPMENT OF A RAIL TRANSPORT MODEL AND ITS USE FOR THE PREDICTION OF RAIL SHIPPING COSTS FOR FOREST PRODUCTS IN OREGON
by
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THE DEVELOPMENT OF A RAIL TRANSPORT MODEL AND ITS USE FOR THE PREDICTION OF RAIL SHIPPING COSTS FOR FOREST PRODUCTS IN OREGON

## INTRODUCTION

There are approximately 2700 miles of track in Oregon (Figure 1). The track can be divided between main lines and secondary or branch lines sometimes referred to as shortlines . Of these 2700 miles, 970 miles of track are main lines; the remainder of the track are secondary lines. There are three principal owners of track in Oregon. The major owner is Southern Pacific Transportation Company, followed by Union Pacific Railroad and Burlington Northern (Oregon Department of Transportation, 1986). There are 47 branch lines in Oregon. They are owned by the large railroad companies, timber companies, small railroad companies or municipalities such as the City of Prineville Railroad.

The decline of the railroads began in the late $1950^{\prime} \mathrm{s}$ following the completion of the tax-funded interstate highway system. These highways were designed for large capacity trucks that competed directly against railroad for long-haul transportation. The deregulation of the trucking industry in the $1970^{\prime}$ 's further increased the competition from trucking. The number of trucking firms increased and trucking rates decreased (Ascot, 1986). Another factor

contributing to the decline of the railroads was the change in United States economy. The economy has changed from a manufacturing economy --where raw materials needed to be transported to the factories and final products are shipped to markets-- to a service economy. The manufacturing economy required periodically transporting large loads of a single commodity, a strength for railroads, to a service economy which favored diversified shipments and flexibility in scheduling that trucking provides.

Transportation costs compose fifty to sixty percent of the total operating cost in the forest products industry (Conway, 1976). As energy prices increase and the forest products industry becomes increasingly centralized, transportation costs will become an increasingly larger portion of the total product cost and will merit closer examination in order to determine the potential importance of railroads in the forest products industry. Railroad shipping costs are difficult to obtain in terms useful for policy analyses involving economies of scale. On routes with currently low traffic, fixed costs of line maintenance prorated into variable costs may provide biased cost estimates for alternative evaluation.

Existing cost data are not only difficult to find, but it may also be difficult to interpret. Not only are railroads the most frugal users of cost data (Carruthers,
1983), but cost data gathered by rail companies are limited to the circumstances in which they were gathered. An example is a line where rail traffic is diminishing. The company may defer maintenance if the long term plan is to abandon the line. The maintenance cost data collected will underestimate the maintenance cost required to keep the line in its optimal working condition; therefore, analysis of the data for historic maintenance cost will underestimate the actual maintenance cost required to operate the line.

This project is part of a larger effort to develop a comprehensive model for analyzing road, water, and rail transportation issues in the forest products industry. This Master of Forestry project concentrates upon the development of the rail transport portion of the overall model. It is envisioned that results from this project will be combined with similar models for the other transport modes to develop a network analysis system to analyze various policy questions concerning transportation problems in the Oregon timber industry, such as the location of sawmills, transfer yards, and sort yards.

## OBJECTIVES

The objectives of the Rail Transport Model are threefold:
(1) Assemble a rail network database containing the track structure and track geometry for the state of Oregon.
(2) Develop a train simulator that will estimate cost based upon the quantity of goods shipped.
(3) Develop cost equations for each link in the rail network for lumber, plywood, and wood chips.

SCOPE
Due to the time and resources available for this project, the rail model developed for the Oregon used many assumptions. Among the most significant largest are:
(1) Due to lack of data, main lines are modeled in the same manner as branch lines. However, there are some assumptions that will hold true on the branch lines that will not be valid on the main lines. First, the model only looks at three forest products, lumber, plywood, and veneer. The contribution of other commodities to the fixed cost is ignored. Most of the branch lines in Oregon are entirely dependent on wood products for their traffic. On main lines there is traffic from multiple commodities as well as from freight passing through Oregon; thus, the fixed cost contribution from this traffic is not accounted for.
(2) This study ignores interference from trains traveling in opposite directions. Trains generally run less than once a day on most branch lines so this will have little effect on cost for branch lines. On mainlines with multiple trains each day as well as Amtrak traffic, long delays can occur from trains traveling in both directions over a segment of track with no side tracks. The model does not account for this added cost on main lines.
(3) The model will use a single maintenance level and a single engine type. Although there are an infinite number of locomotive combinations, this model uses only 2500 dieselelectric locomotives.

## METHODOLOGY

To accomplish the objectives of this project, the following steps were undertaken:
(1) Compile a data base for all the rail routes in the state of Oregon.-- This data base provided information for investment and route maintenance costs as well as data for route simulation. The data base for each link in the rail network contains information on rail size, ballast, grade, curvature, and the location of tunnels and bridges.
(2) Develop a railroad performance simulator.-- This permitted calculation of travel times and costs as a function of route alignment, grade, and volume transported. Although various train simulators already exist, a new train performance simulation model was developed because the available models do not meet the needs of this project. Existing models require more information than is available, or they do not have the ability to predict travel costs.
(3) Simulate train performance for various tonnages of forest products over each rail route. -- These simulations provided cost data to derive relationships between product type and tonnages for each rail route.
(4) Derive cost equations from train simulation data.--Using regression analysis, the results of the train simulations were used to derive a relationship between transport costs, product type and tonnage over each route.


#### Abstract

At one time tariff bureaus set all rates for rail transportation. The tariff bureaus are an independent board set up by the rail companies and state governments. The tariff rates are the rates charged to ship a specified product a given distance. Tariff rates were excluded from anti trust legislation with the Reed Bulwinkle Act of 1948 (Leilich, 1983). The tariff rates are based upon the cost of shipping plus a fair return to the rail company. Prior to the Staggers Rail Act of 1980, tariff rates were the cost basis for interstate shipping (Leilich, 1983). Although the power to set rail rates has been diminished, the tariff bureaus still exist.


The Staggers Rail Act did several things. Two of the most significant were:
(a) It reduced the control of published tariff bureau rates and allowed the railroad corporations and shippers to negotiate rates (deregulated the industry), and
(b) It allowed rail companies to abandon unprofitable lines with less government interference.

An important objective of the Staggers Rail Act was to make rail transportation more competitive with trucking by
allowing the rail companies more freedom in determining the rates. In fact, shippers now may have to negotiate with multiple rail companies when shipping products across several different rail systems. Because rail companies can now negotiate rates based on competition with other modes of shipping, the negotiated rates may not be based upon actual costs with a fair return on investment, but be based upon strategies to achieve or maintain a market share.

Several regional studies have used tariff rates to compare the relative advantages of rail and truck transport. At least one of these was in Oregon. Hyde and Corder (1971) compared both interstate and intrastate transportation cost for rail, truck and barges for mill residues in Oregon. Their interstate transportation rates are based on tariff rates, while intrastate transportation rates are based on negotiated rates between the mills and rail companies. The contract rail rates for wood chips varied from 3.85 cents per ton-mile for a 48 mile haul to 1.6 cents per ton-mile for a 377 mile haul. These are negotiated rates and may not reflect the actual cost for shipping. Their model did not permit the user to predict the shipping cost based on the quantity of goods shipped across the line, the physical condition of the track, and the distance traveled.

A number of analytical railroad modeling studies have been done. These can be divided into two categories: (a)

Table 2: Data required for Train Performance Simulator

| Item | Units |
| :--- | :--- |
| Beginning and ending mile post | miles |
| Curvature of track | degrees |
| Average grade of track | percent |
| Rail weight | pounds per yard |
| Maximum speed | miles per hour |
| Ballast | tons per mile |
| Ballast life | years |
| Bridges | number per link |
| Tunnels | number per link |
| Trains | number per week |

The data for the model comes from a variety of sources. The track geometry for the Southern Pacific lines are from track charts obtained from the Oregon Department of Transportation. For other rail lines, the geometry from the closest Southern Pacific line is used. For example, the track geometry data for the Toledo line was used for the Astoria to Portland line.

Rail weight -- For the Southern Pacific lines, rail weights were obtained from the track chart. The rail weights for
the other lines were obtained from the Oregon Rail Report (1986).

Maximum speed -- For the Southern Pacific lines, maximum speeds were obtained from the track chart. The maximum speeds for the other lines were obtained from the Oregon Rail Report (1986).

Ballast -- The tons of ballast per mile and ballast life were obtained from communication with the Oregon Department of Transportation.

Tunnels and Bridges -- The number of bridges and tunnels for the Southern Pacific lines was obtained from the Southern Pacific Conductors Handbook; for the other lines, the information was obtained from the Oregon Rail Report.

Trains per week -- The number of trains per week was obtained from the Oregon Rail Report.

Car Combinations

The Oregon Forest Products model assumes that trains can carry three types of forest products: lumber, plywood, and chips. Lumber is carried in box cars, plywood is carried in box cars, and chips are carried in chip cars. The maximum net load used for flatcars is 100 tons, for wood chip cars -

- 121 tons; and for box cars -- 70 tons (Railtex, 1985). The tare weight for these cars arc 30 tons for flat cars, 40 tons for box cars and 35 tons for wood chip cars (Grunman Corp, 1986).

The weight of green Douglas fir lumber is assumed to be 2830 pounds per Mbf. Green wood chips are assumed to weigh 38 lbs per solid cubic foot with 71 solid cubic feet per Unit (200 cubic feet). Plywood is assumed to weigh the same as green lumber, 38 pounds per cubic feet. (Wenger, 1984).

Car combinations are created automatically. The model builds unit trains of lumber, plywood, and wood chips. Lumber trains begin with 1.5 MMBF and increase to 7 MMBF , while plywood trains begin with 1.5 MSQFT $3 / 8$ inch to 7 MSQFT 3/8 inch. Wood chip trains begin with 1500 units and increase to 7000 units. This is one of the main differences between the Rail Transport Model and other models which require you to specify the locomotive and car combinations prior to running the program. The train building subroutine will calculate the number of rail cars and engines required to haul the specified mix of products.

The following relationships were developed (Appendix A) to determine the number of cars required for quantity of each product shipped:

Number of flat cars $=0.01429 \times \mathrm{MBF}$
Number of box cars $=0.0069$ x MSQFT 3/8" plywood Number of wood chip cars $=0.0270 \mathrm{x}$ Units

## Engine Requirements

The number of engines is determined by the relationship of $3 / 4$ horsepower per ton of traveling weight (Leilich, 1986). Locomotives range from 500 horsepower to 3600 horsepower (Leilich, 1983). This model has assumed that each engine has 2500 horsepower. This assumption may overestimate the cost on small shortline railroads which may not be able to afford an engine of this size, or prefer to use a small engine at slower speeds. Helper units are an extra source of horsepower. They are an extra locomotive or a slave unit that is controlled from another locomotive. They are used to help a train over a steep grades. They are incorporated into this model.

## Resisting Forces

Given a train configuration, resisting forces are calculated based upon the track geometry from the input file. The MOTION subroutine sums the resisting forces acting on the train. The horsepower required to overcome the resistance is subtracted from the total horsepower; the remaining horsepower is available for acceleration.

Resistance forces are calculated for grade resistance, curvature resistance, internal resistance, air resistance and wheel rolling resistance.

Grade resistance -- Grade resistance is the change in potential energy. This model assumes the train behaves as a single point with all of the forces acting on that point. Grade resistance is calculated from the following equation:

```
Grade resistance = SIN (ARCTAN(grade/100))
```

Eq. [4]

Curve resistance -- Curve resistance is the resistance caused by centripetal force while traveling in a curve. Curve resistance is empirically estimated as 0.8 pounds per ton per degree of curvature (Hay, 1982).

Internal resistance -- Internal resistance is the forces which resists rolling within each freight car. It varies with the condition of the rail car and the track. The range of internal resistance has been empirically measured and varies between three pounds per ton to twenty-eight pounds per ton (Hay, 1982). Eight pounds per ton was chosen for this model.

Combined rolling resistance and air resistance -- Rolling resistance and air resistance are functions of train
velocity. The equation for rolling and air resistance used in this model is the modified Davis equation (Hay 1982):
$R=.6+20 /(W / 2000)+.01 x V+\left(.035 \mathrm{x}^{2}\right) /(W / 2000) \mathrm{Eq} . \quad[5]$

$$
\begin{aligned}
& \mathrm{R}=\text { Rolling and air resistance, lbs } \\
& \mathrm{V}=\text { Velocity, mph } \\
& \mathrm{W}=\text { Weight of train, tons } \\
& \mathrm{N}=\text { Number of axles }
\end{aligned}
$$

Equation. 5 underestimates the air resistance as it does not include resistance on the sides of the car which is a function of car type and velocity, and the car placement in the train.

Train Velocity

Train velocity is derived by solving the relationship that power is equal to the product of force multiplied by velocity. The efficiency rate for diesel-electric engines of 82\% (Hay, 1982).

$$
V=375 \times \mathrm{E} \times \mathrm{HP} / \mathrm{TR}
$$

Eq. [6]

$$
\begin{aligned}
V= & \text { train speed, mph } \\
H P= & \text { engine horsepower } \\
T R= & \text { total resistance, lb } \\
E= & \text { efficiency for diesel-electric } \\
& \text { engines }
\end{aligned}
$$

Since the total resistance is also a function of velocity, the secant method was used to solve Eq. 5 and Eq. 6 simultaneously.

Track Cost and Wear

The TRACK subroutine is used to calculate the fixed costs for rail, ballast, and ties.

Ballast Investment

The ballast used in this model is crushed rock. Ballast cost is estimated by calculating the average annual investment for ballast per mile of rail. The Oregon Department of Transportation provided information on ballast life and tons of ballast used per mile. Real costs and an inflation free discount rate of $4 \%$ were used to estimate the average annual investment cost. Row et al. (1981) have proposed 4 웋 as an average return on investment for long term investment. A ballast cost of $\$ 52.00$ per ton was used (O.D.O.T., 1986). The ballast cost includes excavation, crushing, transportation to the site, and tamping to place the ballast at the proper density. This cost may be low for certain coastal regions where a shortage of suitable ballast rock exists.

Rail Ties

Rail tie cost is based on replacing 150 ties per mile per year at a cost of $\$ 46.00$ per tie (Oregon Department of Transportation, 1986). This cost includes the cost of the tie and its installation and the salvage value of the remaining tie.

Right-Of-Way Maintenance

The annual cost for vegetation removal has been estimated by the Oregon Department of Transportation (1986) as $\$ 160$ mile per year. The same cost was provided by ODOT for ballast resurfacing cost per mile per year. In areas of rapid vegetative growth, such as the coastal mountains, the cost for vegetation removal will be much higher; while in the basin area of Eastern Oregon very little vegetation removal will be required. The total right-of-way maintenance cost is $\$ 320.00$ per mile.

## Rail wear

Rail wear is based on the size of the rail and the annual tonnage that travels across the rail. Rail life is determined by the following empirical relationship (Hay, 1982):

Rail life=(Annual tonnage). 565 x .92 x Rail weight Eq. [7]

$$
\begin{aligned}
& \text { Rail life = years } \\
& \text { Rail Weight = pounds per yard }
\end{aligned}
$$

Rail cost used in this model is $\$ 190.00$ per ton (O.D.O.T., 1986). The cost includes installation labor and assumes that the salvage value is equal to removal cost.

Additional factors that affect rail wear are grade and curvature. Changing from a zero percent grade to a 2.5 percent grade can increase rail wear by almost fifty percent (Table 4). Curvature can increase rail wear by thirteen percent for a 2.5 degree curve to 150 percent for a 8.5 degree curve (Table 5). The combined effects of increasing rail wear due to grade and curvature are additive. It has been assumed that both rails wear evenly.

Table 3. Increase in Track Wear Due to Grade

| Grade Range (\%) | Rail Wear Increase |
| :---: | :---: |
| $1.0-1.5$ | 0.035 |
| $1.5-2.0$ | 0.107 |
| $2.0-2.5$ | 0.248 |
| $2.5>$ | 0.466 |

Table 4. Increase in Track Wear Due to Curvature

| Curvature (degree) | Rail Wear Increase |
| :---: | :---: |
| $1.5-2.5$ | 0.136 |
| $2.5-3.5$ | 0.260 |
| $3.5-4.5$ | 0.429 |
| $4.5-5.5$ | 0.613 |
| $5.5-6.5$ | 0.818 |
| $6.5-7.5$ | 1.083 |
| $7.5-8.5$ | 1.273 |
| $8.5-9.5$ | 1.500 |
| $9.5>$ | 1.703 |

Special Structures

Both tunnels and bridges use a thirty year economic life. The annual cost for bridges is $\$ 7900.00$, and for a tunnel is $\$ 8500.00$ a year. These figures are from the total cost for tunnels and bridges from 1985 road and equipment property accounting form \#410 for the Oregon division of the Southern Pacific Transportation Company (personal communication). These figures are for existing structures only. Any new structures will have to be determined on a project by project basis.

## Operating Cost

The locomotive ownership cost is $\$ 14.75$ per hour for a 2500 hp locomotive based upon a thirty year economic life and a purchase price of $\$ 1,000,000$ (Appendix B). Flat car cost is $\$ 29,300$ per car; box car cost is $\$ 40,100$; and chip car cost is $\$ 34,300$ (Liech, 1982). The economic life of the rail car is 25 years with salvage value equal to removal. The hourly costs are computed using the following car utilization. Flat cars are utilized for 365 days per year, while box cars are utilized 264 days per year, wood chip cars have a car utilization of 165 days per year (Liech, 1982). The estimated ownership cost is $\$ 0.26$ per hour per car for flat cars, $\$ 0.49$ per hour per car for box cars and $\$ 0.66$ per hour for wood chip cars (Appendix B).

A fuel consumption rate of 3.2 gallons per mile is based on the steady state condition reported by General Electric Electromotive Division. This value appears reasonable as a combined loaded and unloaded rate for a 2500 hp. For example, a typical diesel engine consumes about . 4 lb per hp-hour at full throttle. If we assume that the train is using 2500 hp , it would consume (.4)(2500) or 1000 lbs per hour or about 142 gallons per hour. A train speed of 30 mph would equate to 4.7 gallons per mile in the loaded direction. If we assume that the empty weight is about $1 / 4$ of the loaded weight for the train, and that we are using
about 0.6 lb per hp at partial throttle and going the same speed, the fuel consumption would be 1.8 gallons per mile. The average $(4.7+1.8) / 2$ is 3.25 gallons per hour. Due to the difficulty in modeling braking, accelerating, fuel consumption at partial throttle, this model assumes that fuel consumption is constant at 3.2 gallons per mile.

## Labor Cost

Labor costs were difficult to model in this type of analysis. Crews are paid for a full day when they complete a given route. The time required can vary based upon traffic, weather or a variety of other factors. Three categories of labor are used on the train; engineers, firemen and brakemen. Firemen and brakemen are on some trains but not on others. The people in fireman and brakeman positions are moving into other areas as these positions are being eliminated. The best available labor cost for this model is an average of $\$ 25.00$ per man-hour including benefits with a three man crew. It was not possible to incorporate full pay for a route completed in this model. The routes are not specified in this model, and with the location of additional facilities such as sort yards and transfer yards, the traffic patterns may change.

Loading Cost

Loading costs vary with the facility, the product, and car type. Based on personal communications, loading costs are estimated at $\$ 30.00$ per hour, including labor and equipment. Loading time for flatcars is thirty minutes per car, thirty minutes for chip cars, and two hours for box cars. Using the same relationships to calculate the number of cars required, the loading costs are as follows:

| For Lumber: | $\$ 30.00 \mathrm{x} 0.5 \mathrm{x} 0.0142 \mathrm{x} \mathrm{MBF}$ | Eq. [8] |
| :--- | :--- | :--- | :--- |
| For Plywood: | $\$ 30.00 \mathrm{x} 2.0 \mathrm{x} 0.0067 \mathrm{x}$ Msqft 3/8" | Eq. [9] |
| For Chips: | $\$ 30.00 \mathrm{x} 0.5 \times 0.0270 \times$ Units | Eq. [10] |

Inventory Cost

Inventory cost is the cost of having the material in shipping. One of the common complaints against rail transportation is the length of time it takes to get products to market compared to truck transportation. The model assumes that the product will spend the first day in the yard. The inventory cost is calculated by the following equation:

$$
I C=[7 / N+T] \times V \times(I / 365)
$$

Eq. [11]

```
IC = Inventory Cost, dollars
N = Number of trains per week
T = Total travel time in days
V = Value of product, dollars
I = Annual interest rate, decimal
```

The values used are $\$ 225.00$ for lumber per $\mathrm{MBF}, \$ 500.00$ per thousand square feet $3 / 8$-inch basis for plywood, and $\$ 40.00$ per Unit for chips. These values were derived from the 1986 Western Wood products index and from USDA Forest Service Region Six Appraisal Handbook. This assumes that proper car tracking occurs, allowing each rail car to reach its proper destination with no side trips.

## MODEL VALIDATION

Three comparisons between the TPS train performance simulator (Transportation Systems Center, 1979) and the Rail Transport Model developed in this project are briefly described.

The first comparison is on a section of track that has a moderate degree of curvature and a slight downhill grade (Figure 2). The model developed for this project has a longer travel time and lower fuel consumption than TPS, but it does have a higher ending velocity. This is due to a slower acceleration rate for the Oregon State train model.

The second comparison has no grade and a high degree of curvature. Both TPS and this model have the same ending velocity, with travel time and fuel consumption that are almost identical (Figure 2).

The third comparison has a $2 \%$ grade and no curvature. The travel time, fuel consumption, and ending velocity are similar. From these three comparisons, our train model develops a slightly longer travel time and less fuel consumption than TPS. TPS has had limited validation against actual train operations, although no statistical test were performed; our model produces results similar to TPS.


Figure 2: Comparison of Travel Time, Fuel Consumption, Ending Velocity Between TPS and the Oregon Forest Products Train Simulator.

## Comparison with Tariff Rates

As previously discussed, tariff rates are suggested prices charged to ship a specific product a given distance. The Willamette Tariff Bureau has established prices for lumber for Oregon. Three comparisons between tariff bureau rates and the cost per ton from the Rail Transport Model are presented. These comparisons were made in the following way. Three sections of track were selected. These line sections represented line lengths of 20 to 100 miles. The tonnage for each train is 2000 tons of cargo, which is a common train size on many short lines in Oregon.

The first comparison (Figure 3) is between a tariff rate for 20 miles and the City of Prineville line, a line of about 20 miles. The tariff rate for 20 miles is $\$ 0.66$ per 100 pounds or $\$ 13.20$ per ton.

The second comparison (Figure 4) is between a tariff rate for 60 miles and the line section between Albany and Canby in the Willamette Valley. The tariff rate for 60 miles is $\$ 1.09$ per 100 pounds or $\$ 21.80$ per ton.

The third comparison (Figure 5) is between a tariff rate for 100 miles and the line section between Junction City to Milwaukie in the Willamette Valley. The tariff rate for 100 miles is $\$ 1.34$ per 100 pounds or $\$ 26.80$ per ton.

For all three comparisons, the tariff rate is much greater than the cost predicted by this model. The difference between this model and tariff rate does not indicate that this model is incorrect. The simulation predicts cost based on a round trip basis, with the return trip having all cars unloaded. Without having access to rail traffic flow data, this is a worst case approach, there is some return traffic from the branch line and the tariff rates will account for this traffic. Some of the other differences are due to the method in which tariff rates are developed. Tariff rates include a fair return on investment, while this model includes a cost of money for multiple year investments, no profit and risk are added to the total cost. Tariff rates also consider rates charged by other modes of transportation; thus, the cost for transportation in only one consideration in the tariff rate. In this model, the cost for transportation is the only consideration.


Figure 3. Cost per ton comparison between Tariff Rate and the Oregon Forest Product Simulator for 20 mile trip one -way.


Figure 4. Cost per ton comparison between Tariff Rate and the Oregon Forest Product Simulator for 60 miles trip oneway.


Figure 5. Cost per ton comparison between Tariff Rate and the Oregon Forest Product Simulator for 100 miles trip one -way.

## TRANSPORT COST EQUATIONS

To facilitate policy analysis, transport cost equations were developed for each line by simulating train performance and then by fitting a regression equation to the cost points derived by simulation. A cost equation was derived for each product; lumber, plywood, and chips for each line. A fourth cost equation for carrying multiple products over each line was also developed. Carruthers (1983) has suggested that a linear model in the form

$$
\text { cost }=a+b x \text { Tonnage }
$$

Eq. [12]
where

$$
\begin{aligned}
\text { cost } & =\text { total shipping cost, \$/train } \\
a & =\text { fixed cost component, \$/train } \\
b & =\text { variable cost component, \$/train/ton }
\end{aligned}
$$

is useful for modeling a single locomotive type and a single track maintenance level. In this model, a 2500 hp diesel electric is used. The maintenance level is a composite of vegetation removal, track maintenance, including ballast replacement and resurfacing, and tie and rail replacement. If a combination of $1500 \mathrm{hp}, 2000 \mathrm{hp}$, or 2500 hp locomotives are used, a multiple regression equation would be required (Carruthers, 1983). If multiple maintenance levels are to be modeled, they too would require multiple regression
equations. Such a scenario would exist if a transportation company were planning to abandon a rail line because it forecasted low volumes of traffic in the future. The company would no longer resurface the track with the same frequency and would not replace the ties and rails with such regularity. The Federal Railroad Administration may reduce the speed and decrease the maximum load limit on the line; thus increasing the variable cost of travel. The model would need to have these items incorporated into a multiple regression analysis.

The products varied from 1500 MBF to 7000 MBF for lumber, $1500 \mathrm{MSQFT} 3 / 8$ inches to $7000 \mathrm{MSQFT} 3 / 8$ inches for plywood, and 1500 to 7000 units for wood chips. There were 55 simulation runs for each product. The transportation cost for each run was calculated for the loaded and the unloaded direction. The output is a table containing the link name, the product code, the tonnage shipped, the distance traveled, and the shipping cost. These data are transferred into SAS, where the data are fit to a linear equation using the least squares procedure. An equation is developed which predicts the cost for each train for a given level of product shipped.

The coefficient of determination is high for all three single product simulations. The coefficient of determination for lumber averaged from all lines is 0.736;
while the coefficient of determination for plywood is 0.828 . The coefficient of determination for the wood chips is 0.930. The coefficient of determination for a combination of wood products is much lower at 0.445 . The increase in variation with the combination of wood products is due to variation in the car cost and car capacity over the three products.

There are over 120 links in the Oregon rail network. The link between Eugene and Noti is shown as an example of the output from the rail transportation model. The simulations for the line between Eugene to Noti in Figures 6-8 for lumber, plywood, and wood chips respectively. For lumber, the total cost rises steeply to a point of approximately 5000 tons, then the slope becomes more gradual. For plywood, there is a steady increase throughout the range of tons shipped. For wood chips there is a slight but steady increase in total cost through the range.


Figure 6. Total cost as a function of tonnage for lumber for the Oregon Forest Product Simulator.


Figure 7. Total cost as a function of tonnage for plywood for the Oregon Forest Product Simulator.


Figure 8. Total cost as a function of tonnage for wood chips for the Oregon Forest Product Simulator.

Table 5. Regression Equations for Eugene to Noti

| Product | Intercept | Slope | R2 |
| :--- | :---: | :---: | :---: |
| Lumber | 4346 | .41 | .810 |
| Chips | 6857 | .09 | .941 |
| Plywood | 2854 | .47 | .959 |
| Combination | 5032 | .28 | .427 |

The regression equations for each product and combined products for the Oregon rail network are in the Appendices (Lumber, Appendix C; Plywood, Appendix D, and Wood Chips, Appendix E, and the Combined Products are in Appendix F). Those links with lower coefficients of determination have shorter distances where the high fixed cost dominates travel cost, and there is little effect for increased tonnage on the total cost.

It is anticipated that the information from the rail model will be used in analyses to compare the rail transport cost with other modes of transport or to evaluate mixed mode transportation alternatives. An example of the application of the information developed from this model is presented.

Let's assume a company with sawmill and wood chipping facilities in Eugene foresees a strong export market for wood chips. The company has decided to expand into this market. Storage and stevedoring of wood chips has been obtained at Coos Bay. Two options exist for transporting the chips to Coos Bay; one is by rail from Eugene through Noti to Mapleton, then along the coast to Coos Bay. The truck route is south along Interstate 5 to Drain. At Drain, the route turns left along State Highway 38 towards U.S. 101. At Reedsport Junction the route turns left on to U.S. 101 heading south to Coos Bay. Establishment of a rail loading facility in Eugene will cost $\$ 250,000$, while the trucking requires no new facility. The company wants to determine the break-even point between the truck and rail shipping. The company would like to determine the quantity of chips that would have to be shipped by rail to recover the $\$ 250,000$ loading facility cost. The cost equations for each arc in the rail network from Eugene to Coos Bay are:

| Eugene | to Noti | $6,857+.09 \mathrm{x}$ (tonnage) |
| :--- | :--- | :--- | :--- | :--- |
| Noti | to Swiss Home | $1,785+.16 \mathrm{x}$ (tonnage) |
| Swiss Home to Mapleton | $8,017+.04 \mathrm{x}$ (tonnage) |  |
| Mapleton | to Florence | $6,917+.16 \mathrm{x}$ (tonnage) |
| Florence | to Gardner Jct | $7,442+.09 \mathrm{x}$ (tonnage) |
| Gardner Jct to Reedsport | $1,298+.01 \mathrm{x}$ (tonnage) |  |
| Reedsport to Lakeside | $6,789+.04 \mathrm{x}$ (tonnage) |  |
| Lakeside to North Bend | $8,643+.30 \mathrm{x}$ (tonnage) |  |
| North Bend to Coos Bay | $4,591+.06 \mathrm{x}$ (tonnage) |  |
|  |  |  |

The truck operating cost is $\$ 42.00$ per operating (traveling) hour and $\$ 27.00$ per hour for standby cost. The highway distance is 118 miles with a round-trip travel time of 4 hours 55 minutes. Standby time for loading and unloading is 1 hour. The total cost per trip is $\$ 233.50$. Each truck contains 15 units, which is 20.50 tons. The cost per ton is $\$ 11.39$.

The break-even point for the facility requires a two step process. The first step is to determine if a break-even point exists. The cost for each train from Eugene to Coos Bay is represented by equation 13. The cost for truck transportation is represented by equation 14.

$$
52,339+.95 \times T=\text { Total Cost }
$$

```
T = Tons of wood chips shipped for each train
```

$$
11.39 \times \mathrm{T}=\text { Total Cost }
$$

Eq. [14]
$T$ = Tons of wood chips shipped for each truck

The break-even point is represented by equation 15.

$$
\begin{aligned}
& 52,339+.95 \times T=11.39 \times \mathrm{T} \\
& T=\text { Tons of wood chips shipped }
\end{aligned}
$$

The break-even point is 5,013 tons. This size train, about 101 cars, can easily travel the route. The route from Eugene to Coos Bay has no train length restriction noted in the Southern Pacific Conductors Handbook.

The firm must decide what quantity of wood chips can be stored. Assuming the firm has decided it can ship in 6,000 ton trains and make three trips per week, the cost for each train would be $\$ 58,039$ or $\$ 9.67$ dollars per ton. The breakeven point for the new facility is represented by the following equation.

$$
250,000+9.67 \times \mathrm{T} 12=11.39 \times \mathrm{T} 12
$$

Eq. [16]

$$
\text { T12 }=\text { The number of } 6,000 \text { ton trains }
$$

The break-even point for the 6,000 ton trains is 145,348 tons of wood chips. This equates to twenty-four 6000 ton trains.

## CONCLUSIONS AND FUTURE RESEARCH

The Oregon Forest Products Transportation Model could be a useful element in the overall transportation planning model for wood products in Oregon. The rail transportation model produces results similar to TPS; a train simulator which has had been validated with actual train operation. The regression equations derived from the simulations have high coefficients of determination for predicting the travel cost. The combination of products regression equations have a much lower value due to the variability in the cost due to the variability in car cost and car capacity. These equations can be easily incorporated into a network analysis software where a variety of transportation policies can be investigated.

Further research is needed to refine all parts of the model. The first element of the modeling is the track data. Actual track data needs to be specified. One source is Rail Garrison Data for the United States Air Force. This data would provide the complete track geometry and the location of all rail structures such as tunnels and bridges. The next element needing improvement is the train building subroutine. RTM uses $3 / 4$ horsepower per trailing ton. This is an average number that can vary between 0.6 to 3.0 depending on the grade and condition of the track. Each route should have a horsepower per trailing ton ratio
specified. Multiple locomotive power ratings need to be included. The last element that needs improvement is the economic model. The model currently uses statewide averages. For example, it is assumed that 150 ties per mile are replaced per year and that ballast is resurfaced annually at a cost of $\$ 160.00$ per mile. The economic data needs to be route specific in order to develop more precise cost information.

To accomplish these goals, a geographic information system (GIS) could be implemented to collect and manage this data. Track data could be digitized as line data. The attributes assigned to the track would be the track geometry such as grade and curvature. The track components such as number of ties, rail weight and ballast can also be managed. Other point data would include crossings, culverts, bridges and tunnels.

The geographic information system can store tabular data while maintaining the relation between the tabular data and the geographic feature. Maintenance records such as vegetation management and the quantity of ballast replaced for rail right-of-way can be collected and maintained in the data base manager that is included in the geographic information system. Once this data set is complete, files for both cost and track geometry can easily be created. Simple modification to the train program can be made to read

```
these files. The program would then use the actual track data and cost data that is specific to each segment of track in the rail network. This complete system could be used for transportation planning, rail line abandonment, and taxation with accurate data. Such a system would also allow provide sufficient information to develop a multi-variate cost equation based on track maintenance class and engine type. Within the GIS, overlays can be made with the rail lines and mill locations; thus allowing the interaction between the location of timber stands that supply raw materials, the demands points, and the transportation routes.
```


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APPENDIX A<br>Derivation of Rail Car Capacities

```
Flat Cars
```

Using a weight of 2830 pounds per $M B F$ and car capacity of
100 tons
$200,000 / 2850=70 \mathrm{MBF}$ per car or . 01429 cars per MBF

## Chip Cars

Using a weight of 38 pounds per cubic foot with 71 feet of solid wood per Unit.

37 Unit per rail car capacity
$1 / 37=47.85$ Units per Car or .0270 cars per Unit

Box Cars

150,000 Msqft 3/8" per car and car capacity of 75 tons $150,000 / 150=.0067$ cars per Msqft 3/8"

## APPENDIX B

Derivation of Machine Rates for Rail Cars and Locomotives

Engine cost:

Purchase Price $=1,000,000$
Economic Life $=30$ years
Number of day utilized per year $=365$
Number of hours utilized per day $=18$
Interest $=4 \%$
Taxes (\% of AAI) $=3$

Cost per hour \$10.59
Maintenance Cost \$4.16

Total Hourly cost: \$14.75

Rail Car Cost:
Flat Car
Box Car
Chip Car

| Purchase Cost | 29,305 | 40,065 | 34,320 |
| :--- | :---: | :---: | :---: |
| Economic Life (years) | 25 | 25 | 25 |
| Days utilized/year | 365 | 264 | 165 |
| Hours utilized per day | 24 | 24 | 24 |
| Interest | 4 | 4 | 4 |
| Taxes (\% of AAI) | 3 | 3 | 3 |
| Cost Per Hour | .26 | .49 | .66 |


|  | Intercept | Slope | R2 |
| :---: | :---: | :---: | :---: |
| Worden - Klamath Falls | 1164.0 | 0.035 | 0.2421 |
| Klamath Falls - Chiloquin | 1183.0 | 0.100 | 0.6818 |
| Chiloquine - Chemault | 8645.4 | 0.160 | 0.7344 |
| Chemault - Gilchrist Jct. | 2819.0 | 0.080 | 0.9819 |
| Gilchrist Jct.- Oakridge | 1882.0 | 0.189 | 0.9696 |
| Oakridge - Springfield | 1108.0 | 0.032 | 0.3800 |
| Santiam Branch |  |  |  |
|  | Intercept | Slope | R2 |
| Foster - Sweet Home | 6970.4 | 0.029 | 0.9898 |
| Sweet Home - Lebanon | 6120.8 | 0.045 | 0.9671 |
| Astoria Line |  |  |  |
|  | Intercept | Slope | R2 |


| Hammon - Warrenton | 5176.6 | 0.151 | 0.7266 |
| :--- | :--- | :--- | :--- |
| Warrenton - Astoria | 8416.7 | 0.180 | 0.6166 |
| Astoria - Clatskanie | 2785.9 | 0.100 | 0.9612 |
| Clatskanie - St. Helens | 1405.0 | 0.067 | 0.9515 |
| St. Helens - Portland | 3191.9 | 0.068 | 0.9506 |

Forest Grove Branch
Intercept Slope R2

| Forest Grove - Hilsboro | 3214.5 | 0.056 | 0.9039 |
| :---: | :---: | :---: | :---: |
| Oregon Electric |  |  |  |
|  | Intercept | Slope | R2 |
| Junction City - Albany | 9383.6 | 0.379 | 0.6933 |
| Albany - Independence | 3660.8 | 0.242 | 0.6061 |
| Independence - Salem | 3409.4 | 0.074 | 0.7942 |
| Salem -"Brooks | 4265.3 | 0.038 | 0.9508 |
| Brooks - Beaverton | 1721.7 | 0.062 | 0.9546 |
| Beaverton - United Jct. | 3024.8 | 0.048 | 0.9656 |
| Mt Hood Railway |  |  |  |
|  | Intercept | Slope | R2 |


| Hood River - Odell | 7552.1 | 0.051 | 0.9900 |
| :--- | :--- | :--- | :--- |
| Odell - Park Dale | 7532.8 | 0.049 | 0.9919 |



| Broadman - Echo | 9136.2 | 0.187 | 0.5639 |
| :---: | :---: | :---: | :---: |
| Echo - Pendleton | 1011.0 | 0.175 | 0.6722 |
| Pendleton - LaGrande | 2953.0 | 0.511 | 0.3001 |
| LaGrande - Union | 8328.1 | 0.296 | 0.7519 |
| Union - North Power | 1119.0 | 0.373 | 0.7471 |
| North Power - Haines | 6970.2 | 0.141 | 0.8536 |
| Haines - Baker | 7703.0 | 0.221 | 0.7950 |
| Baker - Durkee | 5887.7 | 0.563 | 0.7073 |
| Durkee - Idahoe | 6347.0 | 0.563 | 0.7007 |
| Monroe - Dawson |  |  |  |
|  | Intercept | Slope | R2 |
| Monroe - Dawson | 3808.6 | 0.337 | 0.7757 |
| Geer - Salem |  |  |  |
|  | Intercept | Slope | R2 |
| Geer - Salem | 2939.2 | 0.120 | 0.6029 |
| Theilsen - Dallas |  |  |  |
|  | Intercept | Slope | R2 |
| McMinnville - Dallas | 4687.0 | 0.455 | 0.8718 |
| Thielsen - Dallas | 2839.0 | 1.338 | 0.8924 |
| Alturas - Lakeview |  |  |  |
|  | Intercept | Slope | R2 |
| Lakeview - California Bdr. | 6636.1 | 0.046 | 0.9686 |
| Condor - Arlington |  |  |  |
|  | Intercept | Slope | R2. |
| Condor - Arlington | 1313.0 | 0.236 | 0.7158 |
| Heppner - Heppner JT |  |  |  |
|  | Intercept | Slope | R2 |
| Heppner - Heppner Jct. | 1309.0 | 0.133 | 0.9656 |
| Klammath - Bly |  |  |  |
|  | Intercept | Slope | R2 |
| Klammath Falls - Olean | 8216.6 | 0.074 | 0.7836 |
| Olean - Dary | 5915.0 | 0.036 | 0.9779 |
| Dary - Beaty | 4257.4 | 0.084 | 0.9462 |


| Beaty - Bly | 3013.4 | 0.042 | 0.9704 |
| :---: | :---: | :---: | :---: |
| Oregon - East |  |  |  |
|  | Intercept | Slope | R2 |
| Culp Creek - Cottage Grove | 6988.4 | 0.550 | 0.9557 |
| Springfield - Shelburn |  |  |  |
|  | Intercept | Slope | R2 |
| Springfield - Coburg | 8808.2 | 0.405 | 0.6286 |
| Coburg - Lebanon | 8324.1 | 0.952 | 0.7570 |
| Lebanon - Scio | 9066.1 | 0.585 | 0.8761 |
| Scio - Shelburn | 7178.4 | 0.076 | 0.9554 |
| Portland Traction Co. |  |  |  |
|  | Intercept | Slope | R2 |
| Portland - Milwaukie | 5710.9 | 0.098 | 0.7706 |
| Milwaukie - Gresham | 4079.0 | 0.029 | 0.7537 |
| Gresham - Boring | 4346.7 | 0.053 | 0.3891 |
| Oregon \& Northwest Railroad |  |  |  |
|  | Intercept | Slope | R2 |
| Seneca - Burns | 4529.6 | 0.100 | 0.9401 |
| Burns - Hines | 1526.4 | 0.021 | 0.9958 |
| Woodburn - Stayton |  |  |  |
|  | Intercept | Slope | R2 |
| Woodburn - silverton | 1315.0 | 0.937 | 0.9611 |
| Silverton - Stayton | 3166.4 | 0.795 | 0.9612 |
| Wilsonia - Jefferson |  |  |  |
|  | Intercept | slope | R2 |
| Wilsoniá - Jefferson | 7080.6 | 0.507 | 0.9267 |
| Eugene - Portland |  |  |  |
|  | Intercept | Slope | R2 |
| Eugene - Junction City | 3249.4 | 0.131 | 0.7397 |
| Junction City - Halsey | 1287.0 | 0.062 | 0.9850 |
| Halsey - Albany | 9053.7 | 0.119 | 0.5705 |
| Albany - Salem | 6339.1 | 0.091 | 0.9365 |
| Salem - Brooks | 4265.3 | 0.038 | 0.9508 |


| Brooks - Woodburn | 4043.5 | 0.035 | 0.9483 |
| :---: | :---: | :---: | :---: |
| Woodburn - Canby | 4163.0 | 0.076 | 0.9644 |
| Canby - Oregon City | 3403.0 | 0.030 | 0.4740 |
| Oregon City - Milwaukie | 1286.0 | 0.043 | 0.9632 |
| Milwaukie - Portland | 5710.9 | 0.098 | 0.7706 |
| Canby - Molalla |  |  |  |
|  | Intercept | Slope | R2 |
| Canby - Molalla | 1465.9 | 0.924 | 0.9766 |
| Mohawk Jct. - Marcola |  |  |  |
|  | Intercept | Slope | R2 |
| Springfield - Marcola | 3559.6 | 0.000 | 0.2000 |
| Medford - White City |  |  |  |
|  | Intercept | Slope | R2 |
| Medford - White City | 4422.0 | 0.090 | 0.9135 |
| Whiteson - Willamina |  |  |  |
|  | Intercept | Slope | R2 |
| Whiteson - Sheridan | 1373.0 | 0.072 | 0.9302 |
| Sheridan - Willamina | 5800.1 | 0.147 | 0.5836 |
| West stayton - Stayton |  |  |  |
|  | Intercept | Slope | R2 |
| West Stayton - Stayton | 7818.3 | 0.035 | 0.2751 |
| Wallual Branch |  |  |  |
|  | Intercept | Slope | R2 |
| Wallual - Branch | 1161.0 | 0.081 | 0.9711 |
| California - Springfield |  |  |  |
|  | Intercept | Slope | R2 |
| Cal Border - Ashland | 1104.0 | 0.071 | 0.9540 |
| Ashland - Medford | 4136.9 | 0.069 | 0.6384 |
| Medford - Goldhill | 998.0 | 0.265 | 0.9619 |
| Goldhill - Rogue River | 3150.1 | 0.025 | 0.6318 |
| Rogue River - Grants Pass | 5770.7 | 0.309 | 0.9850 |
| Grants Pass - Glendale | 1961.0 | 0.084 | 0.8126 |
| Glendale - Correct | 1354.0 | 0.582 | 0.7374 |


| Correct - Dillard | 7812.0 | 0.252 | 0.4604 |
| :---: | :---: | :---: | :---: |
| Dillard - Roseburg | 3494.7 | 0.033 | 0.3700 |
| Roseburg - Sutherline | 995.0 | 0.008 | 0.2650 |
| Sutherline - Anlauf | 1066.0 | 0.192 | 0.7640 |
| Anlauf - Cottage Grove | 6930.7 | 0.076 | 0.7435 |
| Cottage Grove - Creswell | 3036.1 | 0.044 | 0.8602 |
| Creswell - Goshen | 2139.0 | 0.002 | 0.0439 |
| Goshen - Springfield | 3661.1 | 0.056 | 0.2362 |
| Portland - Boring |  |  |  |
|  | Intercept | Slope | R2 |
| Portland - Line Jct. | 1178.0 | 0.269 | 0.5825 |
| Line Jct.- Boring | 985.0 | 0.275 | 0.5724 |
| Eugene - Myrtle Point |  |  |  |
|  | Intercept | Slope | R2 |
| Eugene - Noti | 4346.7 | 0.414 | 0.8099 |
| Noti - Swiss Home | 1125.0 | 1.004 | 0.7519 |
| Swiss Home - Mapleton | 6972.6 | 0.193 | 0.7508 |
| Mapleton - Florence | 5368.2 | 0.313 | 0.4286 |
| Florence - Gardner | 4600.1 | 0.460 | 0.7605 |
| Gardner - Reedsport | 1211.0 | 0.049 | 0.9787 |
| Reedsport - Lakeside | 6240.4 | 0.123 | 0.2574 |
| Lakeside - North Bend | 8403.3 | 0.186 | 0.4585 |
| North Bend - Coos Bay | 4620.6 | 0.052 | 0.1735 |
| Coos Bay - Coquille | 8432.4 | 0.099 | 0.0805 |
| Coquille - Myrtle Point | 3419.9 | 0.270 | 0.8395 |
| Portland - Tillamook |  |  |  |
|  | Intercept | Slope | R2 |
| Portland - Lake Oswego | 8127.7 | 0.254 | 0.8672 |
| Lake Oswego - Beaverton | 6081.1 | 0.051 | 0.9869 |
| Beaverton - Hillsboro | 8734.9 | 0.065 | 0.9742 |
| Hillsboro - Tillamook | 2616.0 | 1.386 | 0.8692 |
| St. Joseph - Cook |  |  |  |
|  | Intercept | Slope | R2 |
| St. Joseph - Cook | 9143.7 | 0.167 | 0.4511 |
| Boardman - Perrydale |  |  |  |
|  | Intercept | Slope | R2 |
| Boardman - Perrydale | 1343.7 | 0.072 | 0.0688 |
| Page - Tallman |  |  |  |


|  | Intercept | Slope | R2 |
| :---: | :---: | :---: | :---: |
| Page - Tallman | 1332.0 | 0.887 | 0.7905 |
| California - Klamath Falls |  |  |  |
|  | Intercept | Slope | R2 |
| CA OR - Klamath Falls | 6324.1 | 0.079 | 0.2400 |
| Albany - Toledo |  |  |  |
|  | Intercept | Slope | R2 |
| Albany - Corvallis | 4024.5 | 0.092 | 0.8229 |
| Corvallis - Philomath | 2262.2 | 0.045 | 0.9806 |
| Philomath - Edyville | 1852.0 | 0.935 | 0.8653 |
| Edyville - Toledo | 7702.3 | 0.498 | 0.6772 |
| Gardner - Gardner Jct |  |  |  |
|  | Intercept | Slope | R2 |
| Gardner - Gardner Jct. | 4697.6 | 0.022 | 0.0953 |
| Joseph Branch |  |  |  |
|  | Intercept | Slope | R2 |
| Lagrand - Island City | 4765.3 | 0.038 | 0.9986 |
| Island City - Elgin | 7561.1 | 0.102 | 0.5418 |
| Elgin - Walla | 9372.6 | 0.066 | 0.9807 |
| Walla - Enterprise | 8990.4 | 0.377 | 0.7716 |
| Enterprise - Joseph | 2197.0 | 0.087 | 0.1398 |
| Oregon Eastern Branch |  |  |  |
|  | Intercept | Slope | R2 |
| Ontario - Vale | 6664.8 | 0.062 | 0.9811 |
| Vale - Burns | 3331.0 | 0.300 | 0.9355 |
| Pilot Röck - Pendleton |  |  |  |
|  | Intercept | Slope | R2 |
| Pilot Rock - Pendleton | 5275.4 | 0.043 | 0.9691 |
| Umatila - Pendleton |  |  |  |
|  | Intercept | Slope | R2 |
| Umatila - Pendleton | 9007.2 | 0.041 | 0.9752 |


|  | Intercept | Slope | R2 |
| :---: | :---: | :---: | :---: |
| Line Jct.- Gresham | 6654.7 | 0.208 | 0.6921 |

## Cost Prediction Equations for Plywood

Worden - Springfield
Intercept slope
R2

| Worden - Klamath Falls | 1134.0 | 0.026 | 0.1989 |
| :---: | :---: | :---: | :---: |
| Klamath Falls - Chiloquin | 1063.0 | 0.145 | 0.9113 |
| Chiloquine - Chemault | 8770.5 | 0.210 | 0.9394 |
| Chemault - Gilchrist Jct. | 4522.5 | 0.055 | 0.0890 |
| Gilchrist Jct.- Oakridge | 1867.0 | 0.228 | 0.9758 |
| Oakridge - Springfield | 979.0 | 0.198 | 0.8394 |
| Santiam Branch |  |  |  |
|  | Intercept | Slope | R2 |


| Foster - Sweet Home | 6970.2 | 0.042 | 0.9961 |
| :--- | :--- | :--- | :--- |
| Sweet Home - Lebanon | 6203.5 | 0.092 | 0.7722 |

Astoria Line

|  | Intercept | Slope | R2 |
| :---: | :---: | :---: | :---: |
| Hammon - Warrenton | 4254.7 | 0.250 | 0.9516 |
| Warrenton - Astoria | 6988.0 | 0.320 | 0.9352 |
| Astoria - Clatskanie | 2772.3 | 0.120 | 0.9786 |
| Clatskanie - st. Helens | 1393.2 | 0.074 | 0.9689 |
| st. Helens - Portland | 3179.7 | 0.075 | 0.9680 |
| Forest Grove Branch |  |  |  |
|  | Intercept | Slope | R2 |
| Forest Grove - Hilsboro | 2819.7 | 0.124 | 0.9185 |
| Oregon Electric |  |  |  |
|  | Intercept | Slope | R2 |


| Junction City - Albany | 7119.7 | 0.554 | 0.9135 |
| :--- | :--- | :--- | :--- |
| Albany - Independence | 2520.7 | 0.317 | 0.9132 |
| Independence - Salem | 3168.4 | 0.099 | 0.9469 |
| Salem -"Brooks | 4036.0 | 0.076 | 0.9010 |
| Brooks - Beaverton | 1711.3 | 0.070 | 0.9719 |
| Beaverton - United Jct. | 3018.2 | 0.058 | 0.9815 |

Mt Hood Railway
Intercept Slope

| Hood River - Odell | 7551.6 | 0.078 | 0.9966 |
| :---: | :---: | :---: | :---: |
| Odell - Park Dale | 7532.9 | 0.076 | 0.9974 |


|  | Intercept | Slope | R2 |
| :---: | :---: | :---: | :---: |
| Chemult - Bend | 1807.0 | 1.137 | 0.6930 |
| Bend - Redmond | 6362.3 | 0.064 | 0.1846 |
| Redmond - Prineville Jct. | 5360.9 | 0.059 | 0.7329 |
| Prineville Jct.- Madras | 1281.0 | 0.132 | 0.6449 |
| Madras - Maupin | 1760.0 | 0.208 | 0.3311 |
| Maupin - Celio | 8330.4 | 0.141 | 0.9712 |
| City of Prinevile | Intercept | Slope | R2 |
| City of Prineville | 7050.4 | 0.118 | 0.5528 |
| Gilchrist JCT | Intercept | Slope | R2 |
| Gilchrist - Gilchrist Jct. | . 3737.9 | 0.049 | 0.9882 |
| Shelburn - Mill City | Intercept | Slope | R2 |
| Shelburn - Lyon | 8982.4 | 0.473 | 0.9648 |
| Lyon - Mill City | 7210.0 | 0.196 | 0.9298 |
| Monroe - Hillsboro | Intercept | Slope | R2 |
| Monroe - Corvallis | 7097.8 | 0.575 | 0.9452 |
| Corvallis - Independence | 2859.9 | 0.132 | 0.9277 |
| Independence - McMinnville | 7886.9 | 0.403 | 0.8067 |
| McMinnville - Yamhill | 6545.4 | 0.159 | 0.8164 |
| Yamhill - Forest Grove | 6578.5 | 0.124 | 0.7225 |
| Forest Grove - Hillsboro | 2819.7 | 0.124 | 0.9185 |
| Portland - Idahoe | Intercept | Slope | R2 |
| Portland - Hood River | 1598.0 | 0.860 | 0.6846 |
| Hood River - Dalles | 9284.5 | 0.077 | 0.8379 |
| Dalles - Celio | 2883.8 | 0.176 | 0.7539 |
| Celio - Biggs | 2848.9 | 0.158 | 0.8924 |
| Biggs - Arlington | 8402.8 | 0.570 | 0.7446 |
| Arlington - Heppner Jct. | 1612.4 | 0.159 | 0.9290 |
| Heppner Jct.- Broadman | 8930.6 | 0.291 | 0.8185 |
| Broadman - Echo | 6929.9 | 0.481 | 0.7591 |
| Echo - Pendleton | 7690.8 | 0.496 | 0.7563 |


| Pendleton - LaGrande | 2406.0 | 1.156 | 0.7050 |
| :---: | :---: | :---: | :---: |
| LaGrande - Union | 7010.7 | 0.408 | 0.9561 |
| Union - North Power | 9335.4 | 0.519 | 0.9503 |
| North Power - Haines | 6492.6 | 0.209 | 0.9769 |
| Haines - Baker | 6690.2 | 0.322 | 0.9627 |
| Baker - Durkee | 3088.4 | 0.753 | 0.9433 |
| Durkee - Idahoe | 3603.0 | 0.748 | 0.9434 |
| Monroe - Dawson |  |  |  |
|  | Intercept | Slope | R2 |
| Monroe - Dawson | 1870.6 | 0.477 | 0.9356 |
| Geer - Salem |  |  |  |
|  | Intercept | Slope | R2 |
| Geer - Salem | 1947.4 | 0.216 | 0.8632 |
| Theilsen - Dallas |  |  |  |
|  | Intercept | Slope | R2 |
| McMinnville - Dallas | 4718.2 | 0.263 | 0.7790 |
| Thielsen - Dallas | 2906.0 | 1.600 | 0.9594 |
| Alturas - Lakeview |  |  |  |
|  | Intercept | Slope | R2 |
| Lakeview - California Bdr. | 5657.3 | 0.077 | 0.7836 |
| Condor - Arlington |  |  |  |
|  | Intercept | Slope | R2 |
| Condor - Arlington | 1233.0 | 0.483 | 0.8182 |
| Heppner - Heppner JT |  |  |  |
|  | Intercept | Slope | R2 |
| Heppner*- Heppner Jct. | 1307.0 | 0.165 | 0.9824 |
| Klammath - Bly |  |  |  |
|  | Intercept | Slope | R2 |
| Klammath Falls - Olean | 8538.0 | 0.092 | 0.8202 |
| Olean - Dary | 4819.9 | 0.057 | 0.7789 |
| Dary - Beaty | 9118.5 | 0.197 | 0.5037 |
| Beaty - Bly | 3316.0 | 0.080 | 0.7870 |



| Canby - Oregon City | 2712.6 | 0.053 | 0.9046 |
| :--- | :--- | :--- | :--- |
| oregon City - Milwaukie | 1285.0 | 0.055 | 0.9854 |
| Milwaukie - Portland | 5691.6 | 0.079 | 0.8646 |

Canby - Molalla
Intercept Slope R2


| Canby - Molalla | 1424.9 | 0.528 | 0.9070 |
| :---: | :---: | :---: | :---: |
| Mohawk Jct. - Marcola | Intercept | Slope | R2 |
| Springfield - Marcola | 3282.1 | 0.046 | 0.9585 |
| Medford - White City | Intercept | Slope | R2 |
| Medford - White City | 3915.6 | 0.134 | 0.8993 |
| Whiteson - Willamina | Intercept | Slope | R2 |
| Whiteson - Sheridan <br> Sheridan - Willamina | $\begin{aligned} & 1182.0 \\ & 5562.9 \end{aligned}$ | $\begin{aligned} & 0.188 \\ & 0.144 \end{aligned}$ | $0.7324$ $0.9700$ |

West stayton - Stayton
Intercept Slope R2

$\begin{array}{llll}\text { West stayton - Stayton } & 8170.3 & 0.019 & 0.1536\end{array}$
Wallual Branch
Intercept slope R2

|  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |

Wallual - Branch $1161.0 \quad 0.1030 .9861$

California - Springfield
Intercept Slope

| Cal Border - Ashland | 1103.0 | 0.077 | 0.9694 |
| :--- | ---: | ---: | ---: |
| Ashland - Medford | 3440.2 | 0.144 | 0.7571 |
| Medford - Goldhill | 9237.6 | 0.283 | 0.9298 |
| Goldhill - Rogue River | 3325.1 | 0.044 | 0.8430 |
| Rogue River - Grants Pass | 6219.4 | 0.162 | 0.8841 |
| Grants Pass - Glendale | 1506.0 | 0.140 | 0.4941 |
| Glendale - Correct | 963.0 | 0.864 | 0.9388 |
| Correct - Dillard | 5746.2 | 0.404 | 0.9336 |
| Dillard - Roseburg | 2225.5 | 0.153 | 0.9010 |


| Roseburg - Sutherline | 7463.3 | 0.164 | 0.8355 |
| :---: | :---: | :---: | :---: |
| Sutherline - Anlauf | 1049.0 | 0.408 | 0.8302 |
| Anlauf - Cottage Grove | 3446.2 | 0.146 | 0.6375 |
| Cottage Grove - Creswell | 2673.0 | 0.104 | 0.7881 |
| Creswell - Goshen | 2377.8 | 0.002 | 0.0111 |
| Goshen - Springfield | 3135.2 | 0.114 | 0.9603 |
| Portland - Boring |  |  |  |
|  | Intercept | Slope | R2 |
| Portland - Line Jct. | 1005.0 | 0.426 | 0.9363 |
| Line Jct.- Boring | 8125.5 | 0.442 | 0.8792 |
| Eugene - Myrtle Point |  |  |  |
|  | Intercept | Slope | R2 |
| Eugene - Noti | 2854.4 | 0.472 | 0.9591 |
| Noti - Swiss Home | 7239.8 | 1.135 | 0.9563 |
| Swiss Home - Mapleton | 6085.6 | 0.269 | 0.9516 |
| Mapleton - Florence | 4994.5 | 0.233 | 0.9140 |
| Florence - Gardner | 2750.9 | 0.547 | 0.9592 |
| Gardner - Reedsport | 1195.0 | 0.075 | 0.9914 |
| Reedsport - Lakeside | 5402.2 | 0.205 | 0.9718 |
| Lakeside - North Bend | 8051.7 | 0.179 | 0.6693 |
| North Bend - Coos Bay | 4598.5 | 0.075 | 0.7490 |
| Coos Bay - Coquille | 6148.4 | 0.353 | 0.8110 |
| Coquille - Myrtle Point | 3490.9 | 0.172 | 0.7937 |
| Portland - Tillamook |  |  |  |
|  | Intercept | Slope | R2 |
| Portland - Lake Oswego | 8081.3 | 0.184 | 0.9265 |
| Lake Oswego - Beaverton | 5722.9 | 0.115 | 0.8687 |
| Beaverton - Hillsboro | 3215.2 | 0.055 | 0.1329 |
| Hillsboro - Tillamook | 2738.0 | 1.655 | 0.9532 |
| St. Joseph - Cook |  |  |  |
|  | Intercept | Slope | R2 |
| St. Joseph - Cook | 7805.5 | 0.311 | 0.8006 |
| Boardman - Perrydale |  |  |  |
|  |  |  |  |
| Boardman - Perrydale | 454.2 | 0.177 | 0.9775 |
| Page - Tallman |  |  |  |
|  | Intercept | Slope | R2 |


| Page - Tallman | 1008.0 | 0.965 | 0.9517 |
| :---: | :---: | :---: | :---: |
| California - Klamath Falls |  |  |  |
|  | Intercept | Slope | R2 |
| CA OR - Klamath Falls | 5517.2 | 0.190 | 0.9302 |
| Albany - Toledo |  |  |  |
|  | Intercept | Slope | R2 |
| Albany - Corvallis | 3667.0 | 0.142 | 0.9036 |
| Corvallis - Philomath | 2036.4 | 0.096 | 0.9298 |
| Philomath - Edyville | 1470.0 | 1.023 | 0.9449 |
| Edyville - Toledo | 4632.6 | 0.705 | 0.9368 |
| Gardner - Gardner Jct |  |  |  |
|  | Intercept | Slope | R2 |
| Gardner - Gardner Jct. | 4662.9 | 0.037 | 0.7757 |
| Joseph Branch |  |  |  |
|  | Intercept | Slope | R2 |
| Lagrand - Island City | 4197.0 | 0.064 | 0.9553 |
| Island City - Elgin | 6600.3 | 0.239 | 0.7918 |
| Elgin - Walla | 9372.4 | 0.090 | 0.9919 |
| Walla - Enterprise | 7363.1 | 0.458 | 0.9626 |
| Enterprise - Joseph | 1556.6 | 0.160 | 0.9682 |
| Oregon Eastern Branch |  |  | R2 |
|  | Intercept | Slope | R2 |
| Ontario - Vale | 960.0 | 0.112 | 0.6542 |
| Vale - Burns | 5609.0 | 0.482 | 0.3541 |
| Pilot Rock - Pendleton |  |  |  |
|  | Intercept | Slope | R2 |
| Pilot Rock - Pendleton | 5270.3 | 0.054 | 0.9843 |
| Umatila - Pendleton |  |  |  |
|  | Intercept | slope | R2 |
| Umatila - Pendleton | 5984.2 | 0.055 | 0.3664 |
| Line Jct. - Gresham |  |  |  |


|  | Intercept | Slope | R2 |
| :---: | :---: | :---: | :---: |
| Line Jct. - Gresham | 5882.9 | 0.269 | 0.9761 |

## Cost Prediction Equations for Wood Chips

Worden - Springfield
Intercept Slope
R2

| Worden - Klamath Falls | 1076.0 | 0.056 | 0.9803 |
| :---: | :---: | :---: | :---: |
| Klamath Falls - Chiloquin | 1098.0 | 0.100 | 0.9754 |
| Chiloquine - Chemault | 9389.8 | 0.161 | 0.9716 |
| Chemault - Gilchrist Jct. | 3305.7 | 0.040 | 0.9792 |
| Gilchrist Jct.- Oakridge | 1914.0 | 0.240 | 0.9739 |
| Oakridge - Springfield | 1071.0 | 0.079 | 0.9775 |
| Santiam Branch |  |  |  |
|  | Intercept | Slope | R2 |
| Foster - Sweet Home | 6961.5 | 0.035 | 0.9926 |
| Sweet Home - Lebanon | 6513.7 | 0.055 | 0.9756 |
| Astoria Line |  |  |  |
|  | Intercept | Slope | R2 |


| Hammon - Warrenton | 6092.6 | 0.022 | 0.9905 |
| :--- | :--- | :--- | :--- |
| Warrenton - Astoria | 9484.2 | 0.029 | 0.9898 |
| Astoria - Clatskanie | 2741.2 | 0.114 | 0.9677 |
| Clatskanie - St. Helens | 1373.7 | 0.083 | 0.9654 |
| St. Helens - Portland | 3159.7 | 0.084 | 0.9645 |

Forest Grove Branch

Intercept Slope R2

| Forest Grove - Hilsboro | 3277.0 | 0.031 | 0.9841 |
| :---: | :---: | :---: | :---: |
| Oregon Electric |  |  |  |
|  | Intercept | Slope | R2 |
| Junction City - Albany | 1145.0 | 0.118 | 0.9752 |
| Albany - Independence | 5023.9 | 0.073 | 0.9752 |
| Independence - Salem | 3727.2 | 0.028 | 0.9793 |
| Salem - Brooks | 4316.0 | 0.032 | 0.9791 |
| Brooks - Beaverton | 1693.6 | 0.075 | 0.9670 |
| Beaverton - United Jct. | 3005.5 | 0.056 | 0.9735 |

Mt Hood Railway
Intercept Slope

Hood River - Odell
7536.3
0.040
0.9832

Odell - Park Dale
0.036
0.9852

|  | Intercept | Slope | R2 |
| :---: | :---: | :---: | :---: |
| Chemult - Bend | 2683.0 | 0.289 | 0.9777 |
| Bend - Redmond | 6098.3 | 0.069 | 0.9805 |
| Redmond - Prineville Jct. | 5280.9 | 0.014 | 0.9917 |
| Prineville Jct.- Madras | 1302.0 | 0.101 | 0.9793 |
| Madras - Maupin | 1821.0 | 0.164 | 0.9783 |
| Maupin - Celio | 8287.9 | 0.156 | 0.9679 |
| City of Prinevile Intercept slope R2 |  |  |  |
| City of Prineville | 7518.4 | 0.072 | 0.9757 |
| Gilchrist JCT |  |  |  |
| Gilchrist - Gilchrist Jct. | 3726.3 | 0.042 | 0.9780 |
| Shelburn - Mill City Intercept slope R2 |  |  |  |
| Shelburn - Lyon | 1249.0 | 0.065 | 0.9777 |
| Lyon - Mill City | 8029.6 | 0.038 | 0.9823 |
| Monroe - Hillsboro |  |  |  |
|  | Intercept | Slope | R2 |
| Monroe - Corvallis | 1253.0 | 0.224 | 0.5637 |
| Corvallis - Independence | 3870.6 | 0.076 | 0.7806 |
| Independence - McMinnville | 1096.0 | 0.104 | 0.9768 |
| McMinnville - Yamhill | 7251.4 | 0.045 | 0.9816 |
| Yamhill - Forest Grove | 7255.3 | 0.042 | 0.9797 |
| Forest Grove - Hillsboro | 3277.0 | 0.031 | 0.9841 |
| Portland - Idahoe |  |  |  |
|  | Intercept | Slope | R2 |
| Portland - Hood River | 2273.0 | 0.222 | 0.9774 |
| Hood River - Dalles | 9359.9 | 0.081 | 0.9784 |
| Dalles - Celio | 4054.2 | 0.043 | 0.9801 |
| Celio - Biggs | 3292.3 | 0.036 | 0.9850 |
| Biggs - Arlington | 1226.0 | 0.135 | 0.9794 |
| Arlington - Heppner Jct. | 2117.3 | 0.027 | 0.9877 |
| Heppner Jct.- Broadman | 1051.0 | 0.062 | 0.9819 |
| Broadman - Echo | 1006.0 | 0.111 | 0.9799 |
| Echo - Pendleton | 1094.0 | 0.115 | 0.9798 |




| Canby - Oregon City | 2745.5 | 0.038 | 0.9772 |
| :---: | :---: | :---: | :---: |
| Oregon City - Milwaukie | 1284.0 | 0.067 | 0.9889 |
| Milwaukie - Portland | 6152.2 | 0.050 | 0.8700 |
| Canby - Molalla |  |  |  |
|  | Intercept | Slope | R2 |
| Canby - Molalla | 7161.6 | 0.355 | 0.5853 |
| Mohawk Jct. - Marcola |  |  |  |
|  | Intercept | Slope | R2 |
| Springfield - Marcola | 3410.3 | 0.009 | 0.9852 |
| Medford - White City |  |  |  |
|  | Intercept | Slope | R2 |
| Medford - White City | 4826.1 | 0.035 | 0.9516 |
| Whiteson - Willamina |  |  |  |
|  | Intercept | Slope | R2 |
| Whiteson - Sheridan | 1270.0 | 0.066 | 0.9813 |
| Sheridan - Willamina | 6465.1 | 0.056 | 0.6618 |
| West stayton - Stayton |  |  |  |
|  | Intercept | Slope | R2 |
| West Stayton - Stayton | 7541.6 | 0.107 | 0.7875 |
| Wallual Branch |  |  |  |
|  | Intercept | Slope | R2 |
| Wallual - Branch | 1158.0 | 0.090 | 0.9755 |
| California - Springfield |  |  |  |
|  | Intercept | Slope | R2 |
| Cal Border - Ashland | 1100.0 | 0.109 | 0.9788 |
| Ashland - Medford | 4275.4 | 0.049 | 0.9787 |
| Medford - Goldhill | 1104.0 | 0.207 | 0.8654 |
| Goldhill - Rogue River | 2976.1 | 0.034 | 0.9649 |
| Rogue River - Grants Pass | 7378.5 | 0.135 | 0.6483 |
| Grants Pass - Glendale | 1540.0 | 0.145 | 0.9755 |
| Glendale - Correct | 1731.0 | 0.156 | 0.9579 |
| Correct - Dillard | 9154.3 | 0.101 | 0.9669 |
| Dillard - Roseburg | 3620.3 | 0.041 | 0.9387 |


| Roseburg - Sutherline | 8520.2 | 0.061 | 0.9827 |
| :---: | :---: | :---: | :---: |
| Sutherline - Anlauf | 1361.0 | 0.116 | 0.9808 |
| Anlauf - Cottage Grove | 4327.0 | 0.046 | 0.9795 |
| Cottage Grove - Creswell | 3187.3 | 0.037 | 0.9790 |
| Creswell - Goshen | 1964.4 | 0.019 | 0.9218 |
| Goshen - Springfield | 3883.6 | 0.023 | 0.9822 |
| Portland - Boring |  |  |  |
|  | Intercept | Slope | R2 |
| Portland - Line Jct. | 1306.0 | 0.101 | 0.7876 |
| Line Jct.- Boring | 1123.0 | 0.063 | 0.9831 |
| Eugene - Myrtle Point |  |  |  |
|  | Intercept | Slope | R2 |
| Eugene - Noti | 6857.1 | 0.091 | 0.9412 |
| Noti - Swiss Home | 1785.0 | 0.163 | 0.8855 |
| Swiss Home - Mapleton | 8017.0 | 0.040 | 0.9816 |
| Mapleton - Florence | 6917.8 | 0.162 | 0.6410 |
| Florence - Gardner | 7441.9 | 0.086 | 0.9337 |
| Gardner - Reedsport | 1298.6 | 0.010 | 0.9879 |
| Reedsport - Lakeside | 6788.6 | 0.034 | 0.9264 |
| Lakeside - North Bend | 8643.8 | 0.299 | 0.8799 |
| North Bend - Coos Bay | 4591.9 | 0.057 | 0.7123 |
| Coos Bay - Coquille | 8471.1 | 0.121 | 0.9138 |
| Coquille - Myrtle Point | 4321.4 | 0.323 | 0.8576 |
| Portland - Tillamook |  |  |  |
|  | Intercept | Slope | R2 |
| Portland - Lake Oswego | 9318.9 | 0.146 | 0.7415 |
| Lake Oswego - Beaverton | 6053.0 | 0.036 | 0.9820 |
| Beaverton - Hillsboro | 3009.4 | 0.041 | 0.9845 |
| Hillsboro - Tillamook | 4188.0 | 0.678 | 0.9119 |
| St. Joseph - Cook |  |  |  |
|  | Intercept | Slope | R2 |
| St. Josěph - Cook | 993.0 | 0.052 | 0.9836 |
| Boardman - Perrydale |  |  |  |
|  | Intercept | Slope | R2 |
| Boardman - Perrydale | 1574.0 | 0.015 | 0.9737 |
| Page - Tallman |  |  |  |
|  | Intercept | Slope | R2 |


| Page - Tallman | 1877.0 | 0.228 | 0.8525 |
| :---: | :---: | :---: | :---: |
| California - Klamath Falls |  |  |  |
|  | Intercept | Slope | R2 |
| CA OR - Klamath Falls | 6403.6 | 0.077 | 0.9766 |
| Albany - Toledo |  |  |  |
|  | Intercept | Slope | R2 |
| Albany - Corvallis | 4126.7 | 0.082 | 0.8966 |
| Corvaliis - Philomath | 2232.0 | 0.028 | 0.9835 |
| Philomath - Edyville | 2437.0 | 0.259 | 0.7487 |
| Edyville - Toledo | 1069.0 | 0.170 | 0.9615 |
| Gardner - Gardner Jct |  |  |  |
|  | Intercept | Slope | R2 |
| Gardner - Gardner Jct. | 4681.4 | 0.015 | 0.9853 |
| Joseph Branch |  |  |  |
|  | Intercept | Slope | R2 |
| Lagrand - Island City | 4161.8 | 0.013 | 0.9916 |
| Island City - Elgin | 8023.5 | 0.054 | 0.9816 |
| Elgin - Walla | 9344.3 | 0.074 | 0.9843 |
| Walla - Enterprise | 1121.0 | 0.084 | 0.9157 |
| Enterprise - Joseph | 2485.4 | 0.032 | 0.9491 |
| Oregon Eastern Branch |  |  |  |
|  | Intercept | Slope | R2 |
| Ontario - Vale | 977.0 | 0.067 | 0.9802 |
| Vale - Burns | 5747.0 | 0.562 | 0.9770 |
| Pilot Rock - Pendleton |  |  |  |
|  | Intercept | Slope | R2 |
| Pilot Rock - Pendleton | 5258.2 | 0.050 | 0.9746 |
| Umatila - Pendleton |  |  |  |
|  | Intercept | Slope | R2 |
| Umatila - Pendleton | 6027.8 | 0.041 | 0.9786 |
| Line Jct. - Gresham |  |  |  |

Intercept Slope R2
$7672.5 \quad 0.042 \quad 0.7811$

## APPENDIX F

Cost Prediction Equations for All Wood Products

|  | Intercept | Slope | R2 |
| :---: | :---: | :---: | :---: |
| Worden - Klamath Falls | 1121.0 | 0.043 | 0.0889 |
| Klamath Falls - Chiloquin | 1123.0 | 0.103 | 0.2625 |
| Chiloquine - Chemault | 8928.3 | 0.180 | 0.6204 |
| Chemault - Gilchrist Jct. | 1450.0 | 0.378 | 0.0005 |
| Gilchrist Jct.- Oakridge | 1897.0 | 0.205 | 0.7592 |
| Oakridge - Springfield | 1052.0 | 0.110 | 0.2964 |
| Santiam Branch | Intercept | Slope | R2 |
| Foster - Sweet Home | 6944.2 | 0.039 | 0.8749 |
| Sweet Home - Lebanon | 6237.5 | 0.073 | 0.4010 |
| Astoria Line | Intercept | Slope | R2 |


| Hammon - Warrenton | 5218.0 | 0.143 | 0.5660 |
| :--- | :--- | :--- | :--- |
| Warrenton - Astoria | 8397.9 | 0.171 | 0.4732 |
| Astoria - Clatskanie | 2735.5 | 0.117 | 0.9481 |
| Clatskanie - St. Helens | 1393.8 | 0.074 | 0.9443 |

st. Helens - Portland
$3180.7 \quad 0.075 \quad 0.9444$

Forest Grove Branch
Intercept Slope R2

| Forest Grove - Hilsboro | 3042.1 | 0.084 | 0.7235 |
| :--- | :--- | :--- | :--- |
| Oregon Electric | Intercept | Slope | R2 |


| Junction City - Albany | 963.0 | 0.317 | 0.4494 |
| :--- | ---: | ---: | ---: |
| Albany - Independence | 3932.5 | 0.188 | 0.4254 |
| Independence - Salem | 3447.3 | 0.068 | 0.7291 |
| Salem - Brooks | 4187.9 | 0.053 | 0.8053 |
| Brooks - Beaverton | 1707.5 | 0.069 | 0.9490 |
| Beaverton - United Jct. | 3003.4 | 0.056 | 0.9478 |

Mt Hood Railway
Intercept Slope R2

| Hood River - Odell | 7465.0 | 0.071 | 0.7102 |
| :--- | :--- | :--- | :--- |
| Odell - Park Dale | 7443.7 | 0.069 | 0.6815 |



| Echo - Pendleton | 965.0 | 0.268 | 0.4731 |
| :---: | :---: | :---: | :---: |
| Pendleton - LaGrande | 2923.0 | 0.616 | 0.3310 |
| LaGrande - Union | 8569.0 | 0.247 | 0.5696 |
| Union - North Power | 1153.0 | 0.302 | 0.5042 |
| North Power - Haines | 6954.3 | 0.142 | 0.7551 |
| Haines - Baker | 7794.1 | 0.199 | 0.6475 |
| Baker - Durkee | 6562.2 | 0.428 | 0.4273 |
| Durkee - Idahoe | 7036.9 | 0.426 | 0.4281 |
| Monroe - Dawson |  |  |  |
|  | Intercept | Slope | R2 |
| Monroe - Dawson | 4195.3 | 0.263 | 0.3976 |
| Geer - Salem |  |  |  |
|  | Intercept | Slope | R2 |
| Geer - Salem | 2912.2 | 0.117 | 0.4454 |
| Theilsen - Dallas |  |  |  |
|  | Intercept | Slope | R2 |
| McMinnville - Dallas | 6180.8 | 0.239 | 0.1785 |
| Thielsen - Dallas | 3463.0 | 1.058 | 0.2323 |
| Alturas - Lakeview |  |  |  |
|  | Intercept | Slope | R2 |
| Lakeview - California Bdr. | 6121.3 | 0.048 | 0.0926 |
| Condor - Arlington |  |  |  |
|  | Intercept | Slope | R2 |
| Condor - Arlington | 1291.0 | 0.349 | 0.6502 |
| Heppner - Heppner JT |  |  |  |
|  | Intercept | Slope | R2 |
| Heppner - Heppner Jct. | 1300.0 | 0.160 | 0.9364 |
| Klammath - Bly |  |  |  |
|  | Intercept | Slope | R2 |
| Klammath Falls - Olean | 8536.1 | 0.090 | 0.2935 |
| Olean - Dary | 5294.6 | 0.031 | 0.0217 |
| Dary - Beaty | 7275.0 | 0.225 | 0.0341 |
| Beaty - Bly | 3226.6 | 0.069 | 0.2749 |


|  | Intercept | Slope | R2 |
| :---: | :---: | :---: | :---: |
| Culp Creek - Cottage Grove | 8440.2 | 0.300 | 0.3063 |
| Springfield - Shelburn | Intercept | Slope | R2 |
| Springfield - Cobúrg | 979.0 | 0.287 | 0.3160 |
| Coburg - Lebanon | 1009.0 | 0.622 | 0.3601 |
| Lebanon - Scio | 1029.0 | 0.356 | 0.3931 |
| Scio - Shelburn | 7076.0 | 0.094 | 0.5920 |
| Portland Traction Co. | Intercept | Slope | R2 |
| Portland - Milwaukie | 5918.9 | 0.066 | 0.5392 |
| Milwaukie - Gresham | 3955.1 | 0.052 | 0.6853 |
| Gresham - Boring | 4305.4 | 0.064 | 0.5967 |
| Oregon \& Northwest Railroad | Intercept | Slope | R2 |
| Seneca - Burns | 4545.6 | 0.105 | 0.8738 |
| Burns - Hines | 1479.0 | 0.032 | 0.6069 |
| Woodburn - Stayton | Intercept | Slope | R2 |
| Woodburn - Silverton | 1558.0 | 0.522 | 0.2435 |
| Silverton - Stayton | 5888.4 | 0.357 | 0.1681 |
| Wilsonia - Jefferson | Intercept | Slope | R2 |
| Wilsonia - Jefferson | 8574.7 | 0.256 | 0.2636 |
| Eugene - Portland | Intercept | Slope | R2 |
| Eugene - Junction City | 3206.2 | 0.139 | 0.6798 |
| Junction City - Halsey | 9434.7 | 0.035 | 0.0503 |
| Halsey - Albany | 8961.2 | 0.132 | 0.6930 |
| Albany - Salem | 6321.9 | 0.105 | 0.9212 |
| Salem - Brooks | 4187.9 | 0.053 | 0.8053 |
| Brooks - Woodburn | 3409.5 | 0.018 | 0.0015 |


| Woodburn - Canby | 2575.0 | 0.478 | 0.0016 |
| :---: | :---: | :---: | :---: |
| Canby - Oregon City | 2991.6 | 0.035 | 0.0878 |
| Oregon City - Milwaukie | 1286.0 | 0.054 | 0.8543 |
| Milwaukie - Portland | 5918.9 | 0.066 | 0.5392 |
| Canby - Molalla |  |  |  |
|  | Intercept | Slope | R2 |
| Canby - Molalla | 4586.6 | 0.406 | 0.1917 |
| Mohawk Jct. - Marcola |  |  |  |
|  | Intercept | Slope | R2 |
| Springfield - Marcola | 3379.0 | 0.026 | 0.0857 |
| Medford - White City |  |  |  |
|  | Intercept | Slope | R2 |
| Medford - White City | 4439.9 | 0.082 | 0.5910 |
| Whiteson - Willamina |  |  |  |
|  | Intercept | Slope | R2 |
| Whiteson - Sheridan | 1285.0 | 0.099 | 0.1584 |
| Sheridan - Willamina | 6021.0 | 0.106 | 0.5388 |
| West stayton - Stayton |  |  |  |
|  | Intercept | Slope | R2 |
| West Stayton - Stayton | 7822.3 | 0.054 | 0.3699 |
| Wallual Branch |  |  |  |
|  | Intercept | Slope | R2 |
| Wallual - Branch | 1156.0 | 0.099 | 0.9232 |
| California - Springfield | Intercept | Slope | R2 |
| Cal Border - Ashland | 1106.0 | 0.079 | 0.8145 |
| Ashland - Medford | 3986.3 | 0.086 | 0.5338 |
| Medford - Goldhill | 1039.0 | 0.206 | 0.4570 |
| Goldhill - Rogue River | 3031.2 | 0.054 | 0.3690 |
| Rogue River - Grants Pass | 6728.9 | 0.158 | 0.3960 |
| Grants Pass - Glendale | 1719.0 | 0.044 | 0.3090 |
| Glendale - Correct | 1415.0 | 0.456 | 0.3460 |
| Correct - Dillard | 7891.6 | 0.213 | 0.3188 |


| fillard - Roseburg | 3256.2 | 0.058 | 0.0642 |
| :---: | :---: | :---: | :---: |
| illard - Roseburg | 8831.6 | $0.054$ | $0.0215$ |
| Roseburg - Sutherline | 1161.0 | 0.247 | 0.2290 |
| Sutherline - Cottage Grove | 5236.5 | 0.041 | 0.0458 |
| Anlaur - Grove - Creswell | 2955.4 | 0.066 | 0.6341 |
| cottage Grove | 2074.8 | 0.019 | 0.1051 |
| Goshen - Springfield | 3581.1 | 0.065 | 0.4548 |
| Portland - Boring | Intercept | Slope | R2 |
| Portland - Line Jct. | 1180.0 | 0.251 | 0.5140 |
| Line Jct. - Boring | 984.0 | 0.258 | 0.5159 |
| Eugene - Myrtle Point | Intercept | Slope | R2 |
| Eugene - Noti | 5032.6 | 0.283 | 0.4270 |
| Noti - Swiss Home | 1311.0 | 0.641 | 0.3337 |
| Swiss Home - Mapleton | 7103.2 | 0.163 | 0.5792 |
| Mapleton - Florence | 6146.6 | 0.176 | 0.2297 |
| Florence - Gardner | 5311.4 | 0.320 | 0.4149 |
| Gardner - Reedsport | 1141.3 | 0.062 | 0.5631 |
| Reedsport - Lakeside | 6187.2 | 0.120 | 0.4287 |
| Lakeside - North Bend | 8698.9 | 0.165 | 0.2789 |
| North Bend - Coos Bay | 4559.1 | 0.069 | 0.4902 |
| coos Bay - Coquille | 7825.6 | 0.180 | 0.3207 |
| Coquille - Myrtle Point | 4205.4 | 0.176 | 0.2317 |
| Portland - Tillamook | Intercept | Slope | R2 |
| Portland - Lake oswego | 8766.0 | 0.154 | 0.4075 |
| Lake Oswego - Beaverton | 5885.3 | 0.081 | 0.6986 |
| Beaverton - Hillsboro | 5512.4 | 0.028 | 0.0688 |
| Hillsboro - Tillamook | 3290.0 | 1.102 | 0.2245 |
| St. Joseph - Cook |  |  |  |
|  | Intercept | Slope | R2 |
| St. Joseph - Cook | 9025.2 | 0.177 | 0.4679 |
| Boardman - Perrydale |  |  |  |
|  | Intercept | Slope | R2 |
| Boardman - Perrydale | 1112.4 | 0.097 | 0.3062 |
| Page - Tallman |  |  |  |
|  | Intercept | Slope | R2 |


| Page - Tallman | 1498.0 | 0.571 | 0.3479 |
| :---: | :---: | :---: | :---: |
| California - Klamath Falls |  |  |  |
|  | Intercept | Slope | R2 |
| CA OR - Klamath Falls | 6080.2 | 0.121 | 0.6015 |
| Albany - Toledo |  |  |  |
|  | Intercept | Slope | R2 |
| Albany - Corvallis | 3935.6 | 0.109 | 0.8320 |
| Corvallis - Philomath | 2095.5 | 0.072 | 0.6602 |
| Philomath - Edyville | 2033.0 | 0.585 | 0.3001 |
| Edyville - Toledo | 8244.1 | 0.388 | 0.3532 |
| Gardner - Gardner Jct |  |  |  |
|  | Intercept | Slope | R2 |
| Gardner - Gardner Jct. | 4642.7 | 0.032 | 0.3724 |
| Joseph Branch |  |  |  |
|  | Intercept | Slope | R2 |
| Lagrand - Island City | 4332.5 | 0.047 | 0.1240 |
| Island City - Elgin | 7389.1 | 0.141 | 0.5509 |
| Elgin - Walla | 9312.9 | 0.086 | 0.8879 |
| Walla - Enterprise | 9508.9 | 0.269 | 0.4264 |
| Enterprise - Joseph | 2081.4 | 0.098 | 0.3865 |
| Oregon Eastern Branch |  |  |  |
|  | Intercept | Slope | R2 |
| Ontario - Vale | 8298.9 | 0.143 | 0.0477 |
| Vale - Burns | 4680.0 | 0.790 | 0.0218 |
| Pilot Rock - Pendleton | Intercept | Slope | R2 |
| Pilot Rock - Pendleton | 5250.0 | 0.052 | 0.9381 |
| Umatila - Pendleton |  |  |  |
|  | Intercept | Slope | R2 |
| Umatila - Pendleton | 7299.9 | 0.000 | 0.0654 |

Line Jct. - Gresham
Intercept Slope R2

| Line Jct.- Gresham | 6789.4 | 0.173 |  |
| :---: | :---: | :---: | :---: |
|  |  |  |  |

APPENDIX G<br>Programming Notes and User's Guide

The Train Simulator is written in FORTRAN 77. The command TRAIN executes the program. There are two input files for the train model. The first is a fixed format file call TRACKS.ALL. This file contains the list of all of track segments to be processed. The next files are the track segments to be processed.

There are ten subroutines in the program. The main subroutine is TRAIN. This program increments the loops for the three products and calls the remainder of the subroutine. At the beginning of the subroutine the interest rate is defined. The first subroutine called from TRAIN is DATENT. DATENT reads the TRACKS.ALL file for the list of links to be processed. The subroutine then opens each link file and reads the track description file. The first line of the file contains the number of track segments, the number of trains per week, and the beginning mile post. The format for this line is I4, I4, F7.3. The remainder of the file is the track description file. The variables are ending segment mile post, grade, curvature, rail weight, maximum velocity, tons of ballast, ballast life, number of tunnels, and number of bridges. The format is 9(F7.2).

BUILD. Build creates the train by calculating the number and type of rail cars and the number of engines. The total weight of the train is calculated.

The next set of subroutines calculates the total resisting forces, the velocity, and the travel time for the train. The first subroutine is MOTION. It calls RESIST, which calculates the forces acting upon the train. The velocity is calculated by the secant method in the subroutine SECANT. Once the final velocity has been calculated, the travel time is calculated in subroutine MOTION.

The next subroutine, TRACKS, calculates the track cost. TRACKS calculates the vegetation removal cost along the track, ballast cost, the rail tie cost, and the rail wear increase due to the curvature and grade resistance.

The next subroutine, OPCOST, calculates the operation cost. The OPCOST subroutine calculates the engine cost, car cost and the fuel cost.

The last cost subroutine is SUMCST. It calculates the total cost for each segment in the link. This subroutine calculates the train operation labor cost. The output from this file is written to a temporary file.

The final subroutine is WRITER. It creates a fixed format with the link name, product code (1 for lumber, 2 for plywood and 3 for wood chips), the tonnage shipped, the distance traveled in feet, and the total cost. The format is 1X,A10,I5,1X,F11.3, 1X,F11.3. The output from WRITER provides the input for statistical analysis.

APPENDIX H

Source Code

```
C
```



```
        PROGRAM TRAIN
            CHARACTER * 2 ENDO
            INTEGER TKT,PROD
$INCLUDE: 'TRAIN.INC'
ENDO = 'NO'
C
F RATRTN=.04
C
TKT=6
OPEN(UNIT=TKT,FILE='TRACKS.ALL',STATUS='UNKNOWN',
1 ACCESS='SEQUENTIAL',FORM='FORMATTED',RECL=20)
DO WHILE (ENDO .EQ. 'NO')
CALL DATENT(ENDO,TKT)
C
DO 40 P=1,3
    IF(P . EQ. 1)THEN
        UNITS=7000
        RATE=100
        PROD=1500
        END IF
        IF(P . EQ . 2)THEN
            UNITS=7000
            RATE=100
            PROD=1500
        END IF
        IF(P .EQ. 3)THEN
            UNITS=7000
            RATE=100
            PROD=1500
        END IF
        DO 30 K=PROD,UNITS,RATE
            DO 20 L=1,2
                CALL BUILD
                    DO 10 I=1,NSEC
                    CALL MOTION
                    CALL TRACK
                    CALL OPCOST
                CONTINUE
                    CALL SUMCST
        CONTINUE
        CONTINUE
CONTINUE
REWIND OUT
CALL WRITER
GOTO 5
CLOSE(TKT,STATUS='KEEP')
- END DO

500 FORMAT (1X,'*****',A2,'*****') 1000 FORMAT(1X,'ENTER FILE NAME') 2000 FORMAT (A20)

END
```

C***********************************************************************
C* MM/DD/YY WHO STER DESCRIPTION
C* 07/07/88 KDB ---- ORIGINAL DEVELOPMENT
C*
C***********************************************************************
SUBROUTINE OPCOST
\$INCLUDE: 'TRAIN.INC'
C
FC=.65
ENGCOS=14.75
ENGCST (I)=ENGCOS/60*TIMTOT (I) *NE
IF(P . EQ . 1)THEN
CARPUR=29303
NTUY=365
TCRCOS = . 26 /60
END IF
IF(P .EQ. 2) THEN
CARPUR=40065
NTUY=264
TCRCOS = . 49 /60
END IF
IF(P .EQ. 3)THEN
CARPUR=34320
NTUY=165
TCRCOS = . 66 /60
END IF
CARMAN=0.015
CMANCS=CARMAN*LENSEC(I)/5280
TCRCSS=TCRCOS*TIMTOT(I)
TCRCST = (TCRCSS+CMANCS)*NC
OPRCST (I)=TCRCST+ENGCST (I)
C FUEL COST
C
FULCON(I) $=3.2 * \operatorname{LENSEC}(I) / 5280 * N E$
FULCST(I) = FULCON(I) * . }6
VCOST (I) =TRKWAR (I) +OPRCST (I) +FULCST (I)
RETURN
END

```

SUBROUTINE MOTION
\$INCLUDE: 'TRAIN.INC'
C
VENDO \(=0\)
IF (I . EQ. 1) THEN
\(\mathrm{VB}(\mathrm{I})=\) VENDO
ELSE
\(\mathrm{VB}(\mathrm{I})=\mathrm{VB}(\mathrm{I}-1)\)
END IF
CALL RESIST
IF (VEND(I) .GT. VMAX (I)) THEN
PD (I) =1
DIS=ABS (VB(I) **2-VEND (I) **2) *70* (WTOT/2000) /RTOT
IF (DIS . LT. LENSEC(I))THEN
\(\operatorname{DIS}=\mathrm{ABS}(\mathrm{VB}(\mathrm{I}) * * 2-\operatorname{VEND}(\mathrm{I}) * * 2) * 70 *(\) WTOT \(/ 2000) /\) RTOT
DISACC=DIS
DISCON=LENSEC (I) -DIS
\(\operatorname{TIMEAC}(I)=\operatorname{ABS}(\operatorname{VEND}(I)-\operatorname{VB}(I)) * 95.6 *(\) WTOT \(/ 2000) / R T O T / 60\)
\(\operatorname{TIMCON}(I)=\) DISCON \(/(\operatorname{VEND}(I) * 88)\)
TIMTOT (I) =TIMEAC (I) +TIMCON (I)
ELSE
DISACC=DIS
DISCON=LENSEC(I) -DIS
\(\operatorname{TIMEAC}(I)=\operatorname{ABS}(\operatorname{VEND}(I)-\operatorname{VB}(I)) * 95.6 *(W T O T / 2000) / R T O T / 60\)
\(\operatorname{TIMCON}(I)=\operatorname{DSCON} /(\operatorname{VEND}(I) * 88)\)
\(\operatorname{TIMTOT}(I)=T I M E A C(I)+T I M C O N(I)\)
END IF
ELSE
DISACC=DIS
DISCON=LENSEC (I)-DIS
TIMEAC (I) =ABS (VEND (I) -VB (I) ) *95.6* (WTOT/2000)/RTOT/60
END IF
RETURN
END
```

| C* | MM/DD/YY | WHO | STER |
| :--- | :--- | :--- | :--- |
| C* | $07 / 07 / 88$ | KDB | DESCRIPTION |
| ORIGINAL DEVELOPMENT |  |  |  |

C*
C**************************************
CHARACTER EXIST
INTEGER TKT
\$INCLUDE: 'TRAIN.INC'
C
C WRITE (*,1000)
READ(TKT,2000,END=15) FILNAM
EXIST='N'
C WRITE(*,1100)
C READ(*,2100)EXIST
C

```
```

COL=INDEX(FILNAM,'.')
FILTRK=FILNAM(1:COL)//'TRK'
J=0
NSEC=0
INP=2
IF(EXIST .EQ. 'N')THEN
OPEN(UNIT=INP,FILE=FILTRK,STATUS='UNKNOWN',
ACCESS='SEQUENTIAL',FORM='FORMATTED', RECL=80)
READ (INP, 3000) NSEC,NTRW,MPO
DO }10\textrm{J}=1,NSE
READ(INP, 3100)MP(J),GR(J),CURVE (J) ,RAIL(J),VMAX(J),
BALAST(J),BALIFE (J) ,NTNEW(J) ,NBNEW(J)
CONTINUE
ELSE
OPEN(UNIT=INP,FILE=FILTRK,STATUS='UNKNOWN',
1 ACCESS='SEQUENTIAL',FORM='FORMATTED',RECL=80)
WRITE(*,1400)
READ (*,1500)MP0
WRITE(*,1600)
J=J+1
NSEC=NSEC+1
READ (*,4000)MP (J),GR(J),CURVE (J) ,RAIL (J) ,VMAX (J),
BALAST(J),BALIFE (J) ,NTNEW(J) ,NBNEW(J)
IF (MP (J) .LT. 0) THEN
NSEC=NSEC-1
J=J+1
WRITE(*,1200)
READ (*,1300) NTRW
ELSE
GOTO 20
END IF
WRITE(INP, 3000)NSEC,NTRW,MP0
DO 30 J=1,NSEC
WRITE(INP, 3100)MP (J) ,GR(J),CURVE (J),GR(J),RAIL(J),
VMAX(J),BALAST(J),BALIFE(J) ,NTNEW(J) ,NBNEW(J)
CONTINUE
END IF
DO 40 J=1,NSEC

IF (J . EQ. 1) THEN
$\operatorname{LENSEC}(J)=A B S((M P(J)-M P 0)) * 5280$

```
        BALLST (J)=ABS ((MP (J)-MP0))*BALAST (J)
```

        NT \(=\) NT + NTNEW ( \(J\) )
        \(\mathrm{NB}=\mathrm{NB}+\mathrm{NBNEW}(\mathrm{J})\)
        ELSE
        \(\operatorname{LENSEC}(J)=\operatorname{ABS}((\operatorname{MP}(J)-\operatorname{MP}(J-1))) * 5280\)
        \(\operatorname{BALLST}(J)=\operatorname{ABS}((\operatorname{MP}(J)-\operatorname{MP}(J-1))) * \operatorname{BALAST}(J)\)
        \(\mathrm{NT}=\mathrm{NT}+\mathrm{NTNEW}\) (J)
        \(\mathrm{NB}=\mathrm{NB}+\mathrm{NBNEW}(\mathrm{J})\)
        END IF
    FORMAT(1X,'MILE POST CURVE GRADE RAIL VMAX BALLAST LIFE TUN BRD')
    FORMAT (A1)
2200 FORMAT (1X,I4,I4,F7.3)
2300 FORMAT(1X,9(F7.3))
3000 FORMAT (1X,I4,I4,F7.3)
3100 FORMAT (1X,9(F7.3))
4000 FORMAT (9 (F7.3))
RETURN
END

```
C*****************************************************************
C* MM/DD/YY WHO STER DESCRIPTION
C* 07/07/88 KDB ---- ORIGINAL DEVELOPMENT
C*
C****************************************************************
SUBROUTINE TRACK
$INCLUDE: 'TRAIN.INC'
C
    RC=190
    VEGCOS=160
    RTON=2*1760*RAIL(I)/2000
    BALCOS=52.00
    BALFE=BALIFE(I)
    NTRY=NTRW*52
    MTONY=WTOT / (2000*1000000) *NTRY
    BALCST=BALAST (I) *BALCOS
    BCAPRC=BALCST* (RATRTN* (1+RATRTN) **BALFE / ((1+RATRTN) **BALFE-1))
    BALWAR=BCAPRC/NTRY
C
C TIE WEAR
C
TIECST=150*46*LENSEC(I) /5280
TCAPRC=TIECST*(RATRTN* (1+RATRTN)**30/((1+RATRTN)**30-1))
TIEWAR=TCAPRC/NTRY
C
C SURFACE WEAR
C
SURWAR=(160*LENSEC(I)/5280)/NTRY
VEGCST=(VEGCOS*LENSEC(I))/5280/NTRY
C
C
RAIL WEAR
TON=WTOT / (2000*1000000)
RAILOD=(TON*NTRY)**.565*.92*RAIL(I)
RAILCS=RC*RTON
RCAPRC=RAILCS* (RATRTN* (1+RATRTN) **RAILOD/((1+RATRTN) **RAILOD-1))
RAILWR=RCAPRC/NTRY
C
C INCREASE RAIL WEAR DUE TO GRADE
C
GRADE=ABS (GR(I))
IF (GRADE .GE. 0 . AND. GRADE .LE. . 5)THEN
    RALWRG=0
END IF
IF (GRADE .GT. . 5 . AND. GRADE .LE. 1)THEN
    RALWRG=0
END IF
IF (GRADE .GT. 1 . AND. GRADE .LE. 1.5)THEN
    RALWRG=0.035
END IF
IF(GRADE .GT. 1.5 .AND. GRADE .LE. 2.0)THEN
    RALWRG=0.107
END IF
IF(GRADE .GT. 2.0 .AND. GRADE .LE. 2.5)THEN

RALWRG=0.248
END IF
IF (GRADE . GT. 2.5) THEN
RALWRG \(=0.466\)
END IF

INCREASE FOR CURVITURE
IF (CURVE (I) . GE . 0 . AND. CURVE (I) . LT . . 5) THEN
RALWRC=0
END IF
IF (CURVE (I) : GE. . 5 . AND. CURVE (I) .LT. 1.5) THEN
RALWRC=0
END IF
IF (CURVE (I) .GE. 1.5 .AND. CURVE (I) .LT. 2.5) THEN RALWRC \(=0.136\)
END IF
IF (CURVE (I) .GE. 2.5.AND. CURVE (I) .LT. 3.5)THEN RALWRC=0.260
END IF
IF (CURVE (I) .GE. 3.5 . AND. CURVE (I) .LT 4. 4) THEN RALWRC=0.429
END IF
IF (CURVE (I) .GE. 4.5 .AND. CURVE (I) .LT. 5.5) THEN RALWRC \(=0.613\)
END IF
IF (CURVE (I) .GE. 5.5 .AND. CURVE (I) .LT. 6.5) THEN RALWRC=0.818
END IF
IF (CURVE (I) .GE. 6.5 .AND. CURVE (I) .LT. 7.5) THEN RALWRC=1.083
END IF
IF (CURVE (I) .GE. 7.5 . AND. CURVE (I) .LT . 8.5) THEN RALWRC=1.273
END IF
IF (CURVE (I) .GE. 8.5 . AND. CURVE (I) .LT. 9.5)THEN RALWRC \(=1.500\)
END IF
IF (CURVE (I) .GE. 9.5) THEN
RALWRC=1.703
END IF
TRKWAR (I) \(=(1+R A L W R G+R A L W R C) * R A I L W R+B A L W A R+T I E W A R+S U R W A R+V E G C C T\)
TWEAR \(=\) TRKWAR (I) *5280/LENSEC (I)
C

```

C************************************************************************
C* MM/DD/YY WHO STER DESCRIPTION
C* 07/07/88 KDB ---- ORIGINAL DEVELOPMENT
C********************************************************************C
SUBROUTINE BUILD
\$INCLUDE: 'TRAIN.INC'
C
IF(P . EQ . 1)THEN
LUMBER(L)=K
PLYWD (L)=0
CHIP (L)=0
END IF
IF(P . EQ . 2)THEN
LUMBER (L)=0
PLYWD (L) =K
CHIP(L)=0
END IF
IF(P . EQ . 3) THEN
LUMBER(L)=0
PLYWD (L) =0
CHIP (L) =K
END IF
NOFLAT (L) =INT (LUMBER (L) *.0142+.5)
NOBOX(L)=INT (PLYWD (L) *.0067+.5)
NOHOP(L)=INT(CHIP (L)*.0270+.5)
NC=NOFLAT (L) +NOBOX(L) +NOHOP (L)
IF (L . EQ . 1) THEN
CARGO=1.415*LUMBER(L)+1.35*CHIP (L) +1.70*PLYWD (L)
ELSE
CARGO=0
END IF
TCARWT=30*NOFLAT (L) +35*NOHOP (L) +40*NOBOX(L) +CARGO
NE=INT (.75*TCARWT/2500)
IF(NE .LT. 1)THEN
NE=1
END IF
HPTOT=2500*NE
BRAK=3500*NE
BRAKE=3500*NE
WTOT=(TCARWT+NE*175)*2000
IF(L .EQ. 2)THEN
WTOT=(NOFLAT (L) *30+NOBOX (L) *40+NOHOP (L) *35+NE*175) *2000
ELSE
WTOT=(NOFLAT (L) *30+NOBOX(L) *40+NOHOP (L) *35+
NE*175+CARGO)*2000
END IF
VALUE = 40*CHIP(L)+225*LUMBER(L)+500*PLYWD (L)
IF(L .EQ. 2)THEN
VALUE=0
END IF
RETURN
END

```
```

C***********************************************************************
C* MM/DD/YY WHO STER DESCRIPTION
C* 07/07/88 KDB ---- ORIGINAL DEVELOPMENT
C*
C*********************************************************************
SUBROUTINE RESIST
\$INCLUDE: 'TRAIN.INC'
REAL M
C
GRDRES(I)=WTOT*SIN(ATAN(GR(I)/100))
IF(GRDRES(I) .LT. 0)THEN
GRDRES (I) =0
END IF
ROLERR(I)=WTOT*8/2000
IF (CURVE(I) . EQ. 0)THEN
CURES (I) =0
ELSE
CURES (I)=WTOT/2000*.8/CURVE(I)
END IF
IF(PD(I) .EQ. 3)THEN
BRAKF (I) =BRAK
ELSE
BRAKF (I) =0
END IF
RODRES (I) =GRDRES (I) +ROLERR (I) +CURES (I) +BRAKF (I)
VO=VB (I)
CALL SECANT (VO,RR,V)
RR1=RR
V1=V
VO=VMAX (I)
CALL SECANT(VO,RR,V)
RR2=RR
V2=V
M=(RR2-RR1)/(V2-V1)
RR1=RR2
V1=V2
VO=V2+RR2 / M
CALL SECANT(VO,RR,V)
IF (ABS (V-V1) .GT. 2.5)THEN
GOTO 10
ELSE
VEND (I) =V
RTOT=RR+RODRES(I)
END IF
RETURN
END

```
```

C
C********************************************************************
C* MM/DD/YY WHO STER DESCRIPTION
C* 07/07/88 KDB ---- ORIGINAL DEVELOPMENT
C*
C**********************************************************************
SUBROUTINE WRITER
CHARACTER * 20 FILIDT,FIL2DT,FIL3DT
\$INCLUDE: 'TRAIN.INC'
C
COL=INDEX(FILNAM,'.')
FIL1DT=FILNAM(1:COL)//'1DT'
FIL2DT=FILNAM(1:COL)//'2DT'
FIL3DT=FILNAM(1:COL)//'3DT'
IN1=7
IN2=8
IN3=9
OPEN(UNIT=IN1,FILE=FIL1DT,STATUS='UNKNOWN',
1 ACCESS='SEQUENTIAL',FORM='FORMATTED')
C
10 READ(OUT,1000,END=20)P,L,K,CARGO1,TOTSC1, CPTM1,SUMCS1
READ (OUT,1000,END=20)P,L,K,CARGO2,TOTSC2,CPTM2,SUMCS2
TOTCOS=(SUMCS1+SUMCS2)
WRITE(IN1, 2000) FILNAM(1:8),P,CARGO1,TOTSC1,TOTCOS
GOTO 10
C
1000 FORMAT(3(I5,2X),4(F11.3,2X))
2000 FORMAT(1X,A10,I3,F11.3,1X,F11.3,1X,F11.3)
20 CLOSE(IN1,STATUS='KEEP')
CLOSE(IN2,STATUS='KEEP')
CLOSE(IN3,STATUS='KEEP')
CLOSE(OUT,STATUS='KEEP')
RETURN
END

```
```

| C* | MM / DD / YY | WHO | STER | DESCRIPTION |
| :---: | :---: | :---: | :---: | :---: |
| C* | 07/07/88 | KDB |  | ORIGINAL DEVELOPMENT |

SUBROUTINE SUMCST
INTEGER B,T
\$INCLUDE: 'TRAIN.INC'
C
TOTSEC=0
TOTIME=0
TOTTRK=0
TOTFUL=0
TCOST=0
TOPERC=0
DO $10 \mathrm{I}=1$, NSEC
TOTSEC=TOTSEC+LENSEC (I)
TOTIME=TOTIME+TIMTOT (I)
TOTTRK =TOTTRK+TRKWAR (I)
TOTFUL=TOTFUL+FULCST (I)
TcosT=TcosT+VCOST (I)
TOPERC=TOPERC+OPRCST (I)
10 CONTINUE
TOTBC=0
TOTTC=0
TOTBM=0
TOTTM=0
BANMAN=7900
BCNSCT=5000
$\mathrm{XXX}=1.15 * * 30-1$
IF (NB . GT. 0) THEN
DO $20 \mathrm{~B}=1$, NB
BRIDGE (B) $=$ BCNSCT* (.15* (1.15)**30)/XXX
TOTBC=TOTBC+BRIDGE (B)
TOTBM=TOTBM+BANMAN
20 CONTINUE
END IF
TUNMAN $=8500$
TUNCST=5000
IF (NT . GT. 0) THEN
DO $30 \mathrm{~T}=1$, NT
TUNNEL $(\mathrm{T})=T U N C S T *(.15 *(1.15) * * 30) / X X X$
TOTTC=TOTTC+TUNNEL (T)
TOTTM=TOTTM+TUNMAN
30 CONTINUE
END IF
TOTSTR $=($ TOTTC + TOTTM + TOTBC + TOTBM $) /$ NTRY
INVDAY $=7 /$ NTRW+TOTIME / (60*24)
INVENC=VALUE*RATRTN*INVDAY/365
CREWC=25*3*TOTIME
SUMCOS=TCOST+TOTFUL+TOTSTR+INVENC+CREWC
IF (L . EQ. 1) THEN
CPTM=SUMCOS / (TOTSEC/5280*CARGO)
ELSE

CPTM $=0$
END IF
COL=INDEX (FILNAM,'.')
FILOUT=FILNAM(1:COL)//'OUT'
OUT=5
OPEN (UNIT=OUT, FILE=FILOUT,STATUS='UNKNOWN',
1 ACCESS='SEQUENTIAL', FORM=' FORMATTED')
WRITE (OUT, 1000) P, L, K, CARGO, TOTSEC, CPTM, SUMCOS , TOTIME
FORMAT (3 (I5, 2X) , 5(F11.3,2X))
RETURN
END

C TRAIN INCLUDE FILE

COMMON/VARIBL/NC,NE,NSEC,NTRW,NTRY, COL, OUT, P,L, K, I, RATE
1 FILOUT, FILNAM, UNITS,FILTRK,RATRTN,
2 LUMBER, PLYWD, CHIP, NOFLAT, NOBOX,
3 NTNEW, NBNEW, LENSEC, BALLST, NT, NB, VENDO,
4 VEND,VB,PD,DIS,DISACC,DISCON,TIMEAC,
5 TIMCON,TIMTOT,ENGCST,CARPUR,NTUY,OPRCST
INTEGER NC,NE,NSEC,NTRW,NTRY, COL,OUT,P,L,K,I,RATE,UNITS CHARACTER * 20 FILOUT,FILNAM,FILTRK
REAL LUMBER(25), PLYWD(25), CHIP (25), NOFLAT (25) ,NOBOX (25),
1 CARGO,TCARWT, HPTOT, BRAK, BRAKE,WTOT,VALUE,MPO,MP (25),
2 CURVE (25), GR(25), RAIL(25), VMAX (25), BALAST (25), BALIFE(25),
3 NTNEW (25), NBNEW(25),LENSEC (25), BALLST (25),NT,NB,VEND0,
4 VEND (25), VB(25), PD (25), DIS,DISACC,DISCON,TIMEAC(25),
5 TIMCON (25), TIMTOT (25), ENGCST (25), CARPUR,NTUY, OPRCST (25),
6 FULCON (25), FULCST (25), VCOST(25), GRDRES (25), ROLERR(25),
7 CURES (25), BRAKF (25), RODRES (25), RTOT,TOTSEC,TOTIME,TOTTRK, 8 TOTFUL,TCOST,TOPERC, BRIDGE (25), TUNNEL (25), TOTBC,TOTBM,TOTTM,
9 TOTSTR,INVENC,CREWC,SUMCOS,TWEAR,TRKWAR (25),NOHOP (25)

COMMON / ARRAY/FULCON, FULCST,VCOST, GRDRES,
1 CARGO,TCARWT, HPTOT, BRAK, BRAKE,WTOT,VALUE,MPO,MP,
2 CURVE, GR, RAIL, VMAX, BALAST, BALIFE,TRKWAR,
4 CURES, BRAKF,RODRES,RTOT,TOTSEC,TOTIME,TOTTRK,
5 TOTFUL,TCOST,TOPERC,BRIDGE,TUNNEL,TOTBC,TOTBM,TOTTM,
6 TOTSTR,INVENC, CREWC,SUMCOS,TWEAR,ROLERR

