

THESES

on  
/ Power Plant Design

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in

Electrical Engineering

by

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APPROVED

*D.* Redacted for privacy

Department of Electrical Engineering

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Dean School of Engineering

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### Introduction.

During the last five years the demand for electrical energy in the state of Oregon, and throughout the entire country, has increased to such an extent that electrical generating stations have become an important factor in the economic development of the common wealth.

Considering the great need for cheap power, which is mostly in the form of electrical energy, and that this state has abundant water power, the design of a hydro-electric generating station with transmission and distributing system seems to the writers of this thesis to be quite timely.

June 14,

Site.

The site of the proposed power plant is at Waterloo on the falls of the south fork of the Santiam River, twenty two miles south of Albany, Linn County Oregon.

Electricity is to be generated to supply the city of Albany and the smaller surrounding towns.

The present flow of water in the ditch at Albany is not sufficient to meet the increasing demand for power, hence an auxiliary steam plant is required, which makes the operation and maintenance costly. By constructing the generating station at the Waterloo Falls the use of steam will be unnecessary.

The proposed plant will be so situated that energy can be supplied to Albany and transmission lines can be erected to Lebanon and the other small towns. The capacity of the generating machines will be sufficient to operate cars and trains on all of the proposed electric railroads in the vicinity.

The falls are in the bend of the river and have a width of approximately one hundred and fifty feet at the crest.

The banks at the falls are thirty five or forty feet high and are formed of igneous rock. The bed of the

III.

stream is very rough and is also formed of igneous rock making a solid foundation for the building and dam.

Back of the falls is a large area which could be very easily utilized for pondage and would be sufficient if the plant were enlarged to maintain the supply of water throughout the summer months. It is so located that no damage could be done by flooding as no homes or farms exist in this area.

Flow and Conditions of Stream.

The river heads seventy five miles south-east of Sweet Home, in the Cascade Range. It is a mountainous stream having a broad water shed, and on account of its many small tributaries the heavy rain fall during the winter months cause oftentimes severe floods; consequently construction is attended with considerable risk.

The stream is free from ice throughout the year but some reliable means will have to be made in the construction to protect the station from the floating drift wood gathered by the floods.

Power Capacity of the Stream.

The stream has six hundred and forty square miles of drainage area and the coefficient of discharge at low

flow forty-seven hundred. Thus with the thirty foot head the minimum rate of discharge will be three hundred cubic feet per second.

The horse power of this stream is equal to rate of flow in cubic feet per second multiplied by the weight of one cubic foot of water multiplied by the head in feet and divided by five hundred and fifty; and has a value of one thousand one hundred and ninety.

The electric power realized is seventy-two per cent of the hydraulic energy. So that twelve and one half second feet with one foot fall, represents one electric horse power. Six hundred kilowatts of generated electricity is required, which corresponds to eight hundred horse power. Therefore with the seventy-two per cent efficiency one thousand one hundred and ten horse power of hydraulic energy must be utilized. Thus with the usual amount, of overload of twenty-five per cent, the turbine units must have a total capacity of one thousand one hundred and fifty horse power. This also makes an allowance of twenty-five horse power for excitors.

Considering the capacity of the stream and the amount of power that must be generated, the best combination of units would be three two hundred and fifty kilowatts each having an exciter of eight kilowatts and driven by three three hundred and eighty-five horse power turbines.

The modern practice is to use twin turbines, which

combination does away with end thrusts. It is found that a twin turbine of twenty-two inches in diameter will develop under these conditions three hundred and ninety-six horse power. This is the nearest to the required horse power of the standard size that can be used. And in accordance with the low head the turbine chosen will be of the drownded type.

#### The Dam.

The dam will be built at rhe edge where the water breaks over the falls and be of concrete. The best cross-section for this height of dam has a width of five feet at the top, giving a cross-section of eighteen cubic yards. Hence the structure will contain one thousand one hundred forty cubic yards.

#### Headgate.

The headgate that gives the best service for a medium heads is made of plank three inches thick bolted through a stem and braces which are placed at an angle of thirty degrees with the stem.

The gate is raised and lowered by means of a hand worm gear.

#### Power House.

In the construction of power houses the main object

is to keep the cost of construction and maintenance a minimum. Another important factor is to construct a building that will be saleable.

The power house under consideration will be of concrete foundation with the floor reinforced with steel I beams. The walls are to be of solid concrete and the roof is to be of galvanized iron and supported by steel structure, thus making the building fire proof.

#### Transmission Line

In order to transmit the power from Waterloo to Albany, there will be necessary twenty-two miles of pole line. The route of the transmission line follows comparatively level ground. The poles are to be fo fir, thirty-five feet long set five feet in the ground, are to number forty-five to the mile.

The wire used is number six B. S. gauge and placed forty-eight inches apart.

#### Substation.

In order to have an economic system the substation should be located at or near the center of gravity of the electrical distribution. This places the site on the corner of second and Ferry St. On account of the danger of fire from the high tension the incoming mains, the building will be made of non-combustible material; having a concrete

floor reinforced by steel I beams; concrete walls, and a steel roof.

It is provided with the following equipment; one fifteen foot switchboard consisting of five three foot panels; three step down transformers of two hundred kilo watts capacity, two constant current transformers, of ten kilowatts output each, and one one hundred kilowatt rotary converter for street car service.

#### Distribution System.

In considering the distribution system one of the main objects is to keep the regulation as good as possible for the cost of installation. With this object the layout of the circuits and the size of units are determined.

It is found that with the eleven hundred volts No. 8 and No. 6 wire could be used on the feeders with a three per cent regulation.

By running the No. 6 wire for feeders the cost of copper is not materially increased sufficiently to balance the mechanical increase of strength. This also gives a regulation slightly better than three per cent.

For the mains the regulation should not exceed one and one half per cent. It is found that No. 8 B. S. wire is sufficiently large to keep the drop within the desired limit.

The transformers are to be located so as to balance up the load as much as possible. It is found that one placed at the center of gravity of a section of sixteen blocks of strictly residence district, is very satisfactory.

In order to keep the regulation of the incandescent light circuit as high as possible, the motors are to be connected to a separate circuit on account of lower power factor. The voltage on this is to be two hundred twenty except to the carriage factory and saw mill at a distance of about a mile, the pressure to be used here to be twenty-two hundred volts.

The series arc lights are to be also on separate circuits and will require constant current. There are to be of these two circuits, the transformers being connected in open delta, with twenty lamps per circuit. The lamps are to be on the corners of every other block each way, except in the business district as shown on blue prints.

## Costs.

Land-----\$2000

Dam Erected----- 6000

## Power House

Concrete Foundation-----\$2250

Building Complete and Erected-----10200

Crane----- 210

Total-----\$12660

## Power House Equipment

Three three hundred eighty-five horse  
power Turbines and Governors-----\$5625

Three two hundred fifty kilowatt  
Generators and Exciters----- 6822

Switchboard----- 1800

Total-----\$14247

## Transmission Line

Copper-----\$4620

Poles Erected----- 5695

Stepup and Step down Transformers--- 7200

Total-----\$17515

## Substation

Building Complete-----\$3000

## Substation Equipment

Two ten kilowatt Constant Current  
Transformers-----\$ 480

Rotary Converter----- 2000

Total-----\$2480

## Distributing System

Copper for Feeders-----\$ 945

" " Mains----- 1853

" " Power Circuit----- 2154

" for Arc "----- 313

Fifteen Pole Transformers----- 3787

Street Car Circuit----- 300

Total-----\$9352

Total Cost-----\$67254

## Operating Expenses

Superintendent's Salary-----	\$1800 per year
Three Station Operators-----	2000
Two Substation Operators-----	1800
Two Line Men-----	1440
Total-----	\$7040

## Depreciation

Buildings-----	\$ 201
Generators-----	341
Transformers-----	202
Total-----	\$744

Arc Lamps-----	\$ 2880
Incandescent-----	15000
Power Motors-----	21528
Street Car-----	1000
Total-----	\$40408

## Summary

Gross Receipts-----	\$40408
Operating Expenses-----	7040
Depreciation and Maintenance-----	2314
Interest-----	4296
Taxes-----	1430
Net Profit-----	25695

## Conclusion.

The writers of this thesis have carefully considered this subject, of proposed plant for Albany, have placed all costs sufficiently high, have placed all receipts nearer the minimum than the average, and have found that this new system would be a financial success as well as consistent with good engineering.

This new project would cost as shown above approximately seventy-five thousand and could be incorporated for one hundred thousand or one hundred fifty thousand dollars.

## DATA SHEET I.

## Discharge Table.

Taken From U.S. Geological Survey

Gage Height	Discharge	Gage Height	Discharge
2.40	1730	4.70	6580
2.50	1870	4.80	6850
2.60	2020	4.90	7120
2.70	2180	5	7400
2.80	2340	5.10	7690
2.90	2510	5.20	7980
3.	2680	5.30	8280
3.10	2860	5.40	8580
3.20	3050	5.50	8880
3.30	3240	5.60	9190
3.40	3440	5.70	9500
3.50	3640	5.80	9810
3.60	3850	5.90	101300
4.40	5780	7440	15020
4.50	6040	7.60	15680

.....

Discharge in Sec. Ft. Run Off.

Month	Max.	Min.	Mean P Sq. M.	Depth in on drainage area	Total acre feet	
Jan.	25300	1730	7060	II	1268	434000
Feb.	63700	5780	23800	37.2	3874	1320000
March.	15400	2680	4430	6.9	7.98	27200

.....

## DATA SHEET 2

Load on the Transformers.

Sections	No. of Blocks	No. of Lamps	K.W.
I	I6	418	13
2	I6	635	22
3	I6	380	10
4	I6	515	17
5	I0	I636	42
6	I7	407	15
7	I2	830	52
8	8	I670	43
9	I6	510	10
10	I6	485	16
II	I4	325	6.9
I2	I2	86	12
I3	I2	229	14
I4	8	200	9
I5	2		35

## DATA SHEET 3

## Data on the Size of Wires

: :

.....Circuit I.....

Section	Length	K.W.	Cir. Mills.	Size of wire B&S.
8	420	43	11620	9
I3	3102	69	19620	7
Average				15620
				8

: :

Circuit 2.

Section	Length	K.W.	Cir.Mills.	Size of wire B&S.
5	924	42	232000	6
I4	420	8	3600	I4
Average				134000
				9

## Circuit 3

Section	Length	K.W.	Cir. Mills.	Size of wire B&S.
2	1518	22	19750	8
4	924	17	9460	11
Average			14605	9

## Circuit 4.

Section	Length	K.W.	Cir. Mills.	Size Of wire B&S
7	420	52	13000	9
10	1980	16	18690	8
12	2970	12	22680	6
Average			18123	7

## Circuit 5

Section	Length	K.W.	Cir. Mills.	Size of wire B&S
6	660	15	10220	10
9	1980	10	16400	8
II	3102	6.9	21560	6
Average			16055	8

## Circuit 6

Section	Length	K.W.	Cir. Mills.	Size of wire B&S.
I	2462	23 <sup>17</sup>	10000	10
3	1254	10	7450	II
Average			13 <sup>35</sup>	9

## DATA SHEET 4

Data on the Size of Wire.

Section I.

Section	Length	K.W.	Cir. Mills	Size of wire B & S
I to A.	462	2.17	10000	10
I to B.	198	2.76	5465	12
I to D.	396	5.47	19150	7
Average				14

Sec. 3.

Section	Length	K.W.	Cir. Mills	Size of wire B & S
3 to A.	462	3.51	162000	8
3 to B.	198	1.3	2576	16
3 to D/	396	5.47	21640	6
Average				14

## Section 4

Section	Length	K.W.	Cir. Mills	Size of wire B & S
4 to E.	330	5.38	17750	8
4 to G.	198	4.86	9640	10
4 to H.	462	5.44	25100	6
Average				12

## Section 5

Section	Length	K.W.	Cir. Mills	Size of Wire B & S
5 to L.	330	6.3	208000	7

## Section 6

Section	Length	K.W.	Cir. Mills	Size of Wire B & S
6 to Depot	792	1.85	14650	8
6 to D.	396	2	7220	II
6 to E.	132	2.59	3420	I3
6 to F.	198	3.22	6370	II
6 to G.	462	4.32	19900	7

## Section 7.

Section	Length	K.W.	Cir. Mills.	Size of W. 7 B & S
7 to H.	528	5.48	29000	8
7 to I.	198	5	9900	10
7 to J.	60	30.99	18975	8
Average				12.

## Section 8.

Section	Length	K.W.	Cir. Mills	Size of Wire. B & S
8 to K.	198	30.99	61300	3
8 to L.	99	37.59	37200	4

## Section 14.

Section	Length	K.W.	Cir. Mills	Size of Wire B & S
I4 to K	66	67	4420	I4
I4 to L.	330	58	191500	0000

## DATA SHEET 5

## Induction Motor Circuits.

	Length	K.W.	Cir. Mills.
2200 Volts			
.....			
Sub. to (L&S)	I5I8	60	28100
" " (M&I7&I8)	2376	65	48300
" " (First)	I98	2I5	II900
" " (Saw Mill)	5280	75	II2000
" " (H&I1)	4092	I50	I90500
" " (Saw Mill to First, 198)		30	18600
220 Volts			
.....			
" " (H&I5 to First)	I98	30	18400
" " (M&I7&I8 to First)	I98	65	40400
" " (L&I5&I6)	I00	40	
" " (J to 9)	I98	I0	
" " (L to 9)	I50	I0	
" " (L to Z)	I00	25	
.....			
Running First St.	3960	Size K.W.	Lbs.
		4	498
" to Saw Mill.	5280	000 I68	2722
.....			

B & S	Substitute	Weight	Volts
4	4	356	2200
4			"
9			"
0			"
0000			"
7	6	13	220
4			"
8			"
8			"
8			"
8			"

DATA SHEET 6

The Total Load.

Kind of Load	K.W.
Incandescent	300
Arcs	20
Motors	515
Total	835.

## DATA SHEET 7.

## The Main Feeder,

Line Block	Block Length	K.W.	Cir. Mills.
8	200	51	3600
7	330	80	5500
4	1188	39	9745
3	204	23	16480
6	1578	31.9	17280

## DATA SHEET 8

## Length and Weight of Secondaries.

:::::::::::::::::::::::::::::::::::::::

Transformers	B & S	Length	Lbs.
I	6	5016	396
2	6	5346	423
3	8	5214	281
4	6	6600	521
5	6	3894	301
6	8	7722	416
7	8	6138	331
8	6	3234	258
9	8	7722	416
10	8	7722	416
II	8	5082	281
12	8	6072	331
13	8	2310	124
14	8	2640	142

.....  
Using No8 wire      66776      9266Three wires 9266 x 3 is 27798 lbs.  
.....

## Electrical

## Centers of Gravity of Sections.

Sec I.	I.	2.	3.	4.	A.	B.	C.	D.
	.87	.87	.88	.88	.62	.62	.94	1.89
	.94	.62	.64	.88	.62	.62	.62	.87
	.62	.62	.64	.88	.31	.64	.64	.88
	.62	.62	.31	.62	.62	.88	.88	1.25
	4.05	2.73	2.47	3.63	2.17	2.76	3.08	4.87

Center            6.4 X            6 Y

Sec. 2 I.    2.    3.    4.    E.    F.    G.. H.

I.9	I.25	I.8	3.1	I.8	I.7	I.9	
I.7	I.25	.88	I.25	.94	I.25	I.25	I.25
I.8	I.25	.88	I.8	.88	.88	.88	I.9
.94	.88	.64	.64	I.8	I.25	3.	
5.5	4.79	4.44	6.79	4.26	5.63	4.47	6.05
Center	10.8 X			10	Y.		

Sec 3 5. 6. 7. 8.. 9 A. B. C. D.

I.25 .99 .62 .94 I.62 .77 .99 I.25 I.25  
I.25 .18 I.36 I.25 .31 .31 .18 .99  
.99 .31 .31 .31 I.9 I.25 .1 .62  
.77 .31 .31 .31 .18 .94  
.3 I.56 .94  
I.8 I.56

4.26 I.79 2.29 2.59 3.52 5.74 4.70 2.05 4.12

Center 7 X 8.5 Y.

Sec. 4 5. 6. 7. 8. 9. E. F. G. H.

.36 .99 I.25 I.65 .99 I.25 I.2 .9 .36  
.9 .99 .99 .94 .99 .99 .62 .99 .99  
I.2 .62 .99 I.25 I. .62 .99 .99 I.25  
I.25 .99 .62 I.9 .62 .62 I. .99 .99

3.71 3.35 3.75 5.94 3.60 5.38 4.06 4.84 5.44

Center 10.5 X 10 Y.

Sec 5. 6. 7. I. J. K. L.

.....

.62 16.6 12.6 .99 .31 .62 8.3

.31 1.2 20 1.56 5.6 10.12 6.3

.99 II.2 12.6 1.25 6.3 8

.....  
I.91 16.16 23.97 3.8 12.21 11.44 14.6

Center 20 X 20 Y.

.....

Sec. 6. 10. II. 12. 13. C. D. E. F. G. B.

.....

I.25 I .99 .99 .62 .62 .99 I.25 I.25 I.85

I.25 .36 .62 .99 .99 .3 .36 .36 I.

.99 .36 .62 .62 .3 .62 .62 .99

.62 .3 .62 .62 .62 .62 .99 .99

.62 .99 X

I.85

.....

4.73 3.86 2.53 3.22 I.61 I.30 2.69 3.22 4.23 I.85

.....

Center 7 X 7 Y.

.....

Sec. 7. I0. II. I2. I3. H. I. J.

I2.6 II.3 6.3 .99 I.25 I.25 6.3

I2.6 5.6 3.1 I.25 .99 I.25 5.6

II.2 I.25 I.25 I.25 .99 I.25 3.1

I.25 I.25 .99

13.85 I3.15 I0.65 3.45 4.48 55 15.99

Center 20 X I2 Y

Sec. 8 I0. II. I2. I3. K. L.

I6.8 I0.8 6 .99 6.3 9.9

I2.3 I2.6 I2.5 .6 6.3 5.3

6.3 3.

.6 .99

I6.2 I2.7 I0.6 2.89 I9.5 I9.29

Center I9 X I2. Y

Sec. 9. I4. I5. I6. I7. D. E. F. G.

.62 .99 .62 .99 .62 .62 .62 .62  
.62 .62 .3 .62 .62 .62 .62 .99  
.62 .62 .3 .3 .3 .3 .3 .62  
.62 .62 .3 .3 .3 .6 .62 .99

2.48 2.85 1.68 2.21 1.84 2.14 2.16 3.24

Center. 5 X 4.5 Y.

Sec. 10. I4. I5. I6. I7. H. I. J. K.

.99 1.09 .89 ,6 .62 .62 .99 .99  
.99 1.25 .62 1.25 1.25 1.25 1.25 1.09  
.62 1.25 .62 1.25 .62 .62 .62 .99  
.62 1.25 .62 1.25 1.25 1.25 1.25 ,6

3. 22 4.84 2.75 5. 3.74 3.74 4.11 3.67

Center. 8 X 8 Y.

Sec. II I4. I5. I6. I7. L. M.

.99 .99 .99 .6 .99 .99

.99 .62 .77 .3 .99 .62

.99 .77

.6 .3

I.98 I.6I I.76 .9 3.57 2.68

Center 3.5 X. 3.5 Y.

Sec. I2. I8. I9. 20. D. E. F. G.

.62 .62 .3 .3 .3 .17 .6

.77 .6 .3 .6 .6 .6 .6

.3 .6 .3 .3 .3 .3 .3

.3 .6 .3

I.99 2.42 I.2 I.2 I.2 I.67 I.5

Center. 3 X 2.8 Y.

/

Sec. I3. I8. I9. 20.. H. I. J. K.

.99 .77 .37 .99 .99 .99 .99  
.99 .79 .6 .99 .99 .79 .77  
99 .99 .6 .3 .6 .6 .37  
.99 .99 .3

4.06 3.54 1.85 2.10 2.58 2.38 2.13

Center 5.2 X 3.5 Y

Sec. I4. I8. I9. 20. L. M.

.99 .6 .6 .99 .99  
.99 .3 .6 .6 .3  
..... .6 .6

2.16 2.8 1.2 2.19 1.89

Center 3 X 2 Y.

Sec. I5 8. 9. I. J. K. L.

.....  
9.8 9.9 I.25 II.8 II.8 9.8

II.2 6.3 I.25 6.3 6.3 9.9

II.8 6.3

I.25 I.25

.....  
25.05 23.55 2.50 18.1 18. 1.9

Center 24. X. 25 Y.

## WATTS LOAD,

Per Block.

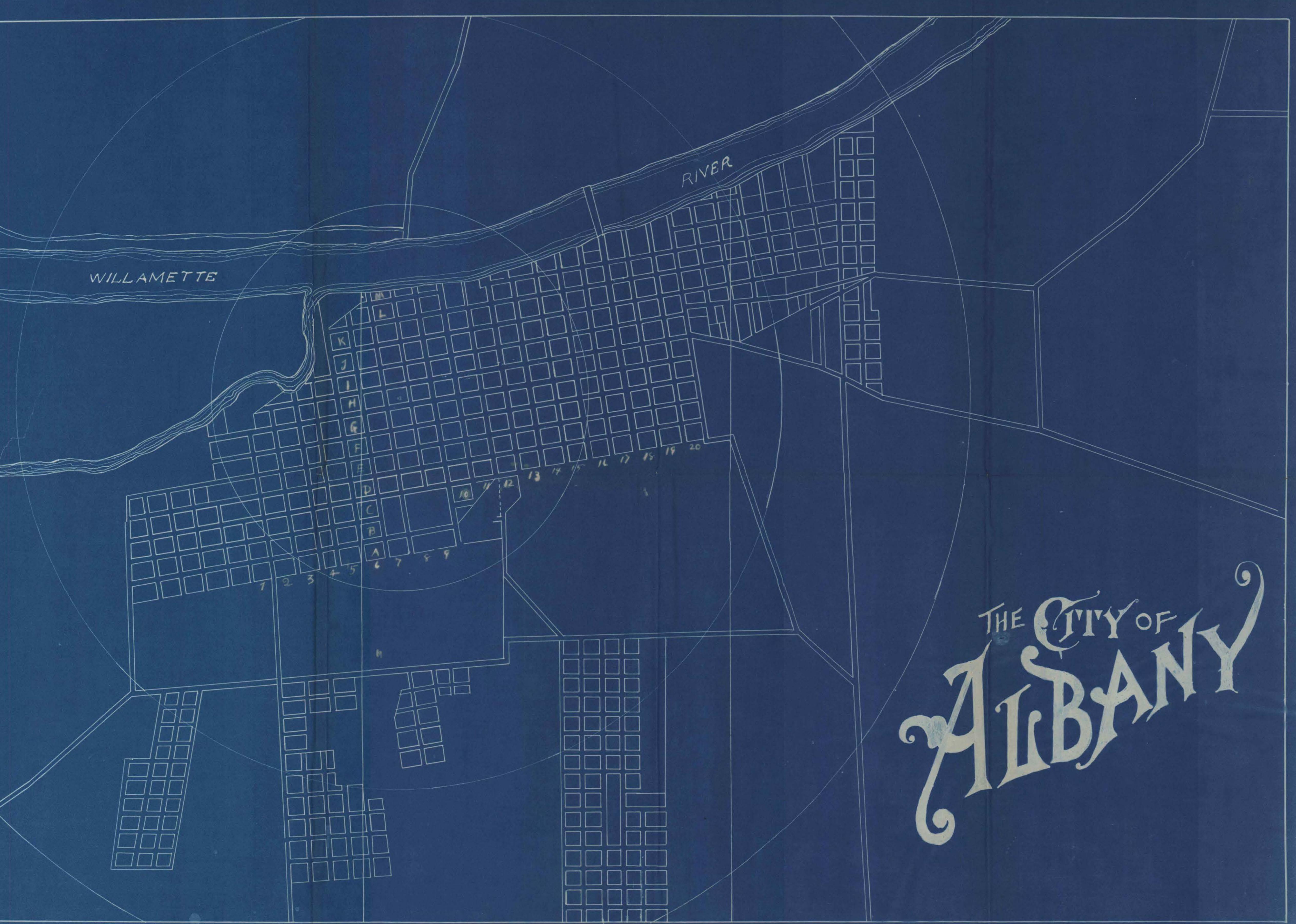
I	2	3	4	5	6
I.9	I.25	I.8	3.1	.62	8.3
I.7	I.25	.88	I.25	.31	.7
I.8	I.25	.88	I.8	.99	5.6
I.87	.94	.88	.64	.36	I.56
.94	.87	.88	I.25	.9	.99
.62	.62	.64	.88	I.2	.99
.62	.62	.64	.88	I.25	.62
	.62	.31	.62	I.25	.99
				I.25	.99
				.99	.18
				.77	.31
					.31

7 &	8	9	10	11	12	13	14	15
6.3	5.6	9.8	9.9	5.4	3.1	.99	.99	.99
I.12	II.4	II.2	6.3	6.3	6.3	.6	.99	I.09
6.3	9.4	II.8	6.3	5.6	3.1	.99	.99	I.25
I.25	.6	I.25						
I.25	I.35	.99	I.25	.99	.99	I.25	.62	I.25
.99	.99	.99	I.25	I.09	.99	.99	.62	.99
.99	I.25	I.09	I.25	.36	.62	.99	.62	.62
.62	I.9	.62	.99	.36	.62	.62	.62	.62
.62	.99	.62	.62	.3	.3	.62	.62	.62
I.56	I.25			.62	.94			.99
					I.85			
.31	.31	.31	I.8					

.....

I6	I7	I8	I9	20
.99	.6	.99	.6	.6
.99	.6	.99	.77	.37
.62	1.25	.99	.79	.6
.62	1.25	.99	.99	.6
.62	1.25	.99	.99	.3
.62	.99	.62	.62	.3
.3	.62	.77	.6	.3
.3	.6	.3	.6	.3
.3	.3	.3	.6	.3

.....



# THE CITY OF ALBANY





Drawn by Grace M. Profst.  
C. A. Sonnen, No. 3.



THESIS

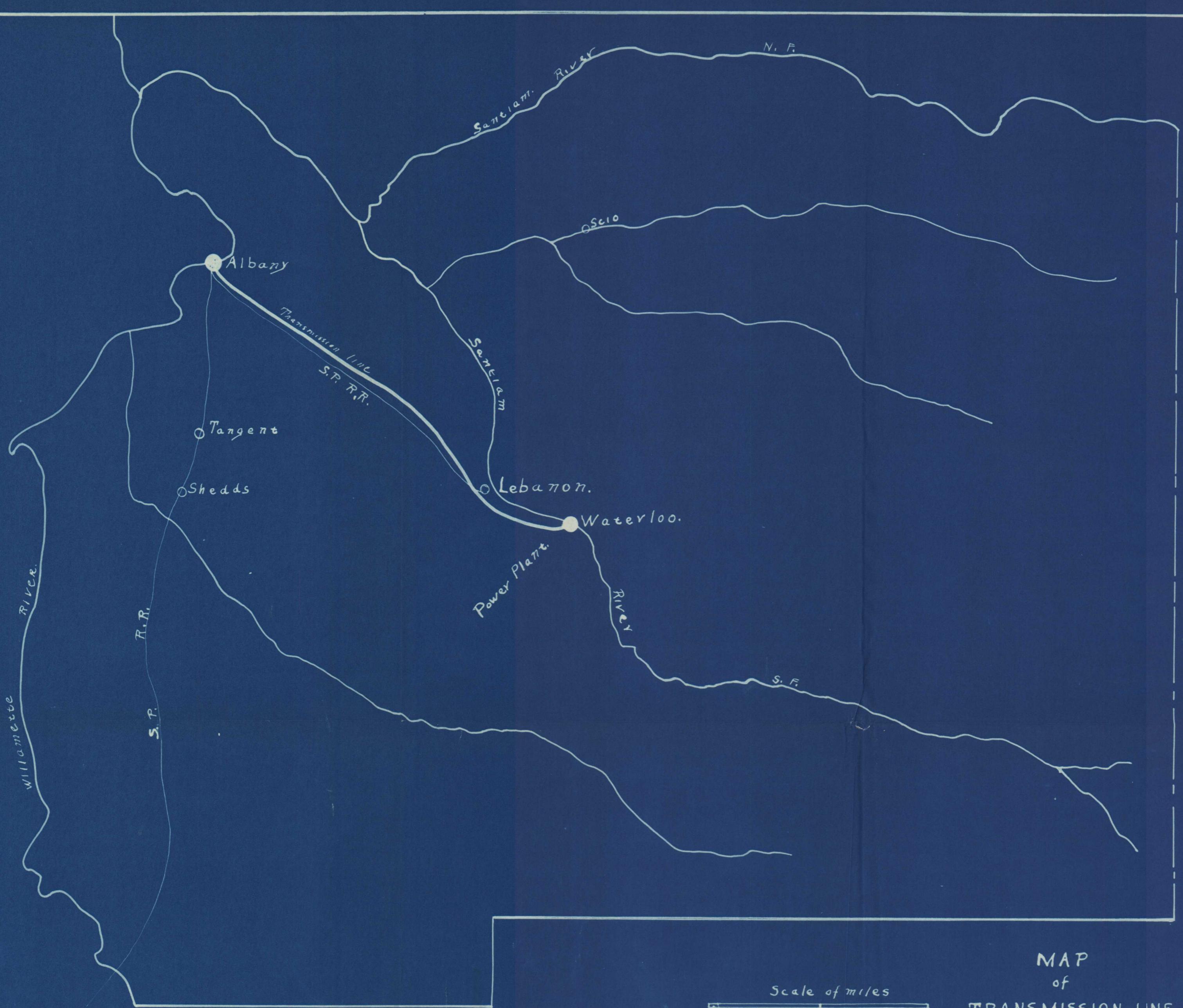
PRIMARY CIRCUITS.

SECONDARY CIRCUITS.

Drawn by Harry H. Profet  
E. A. Sorenson.

Serial No.

Place No. 4.



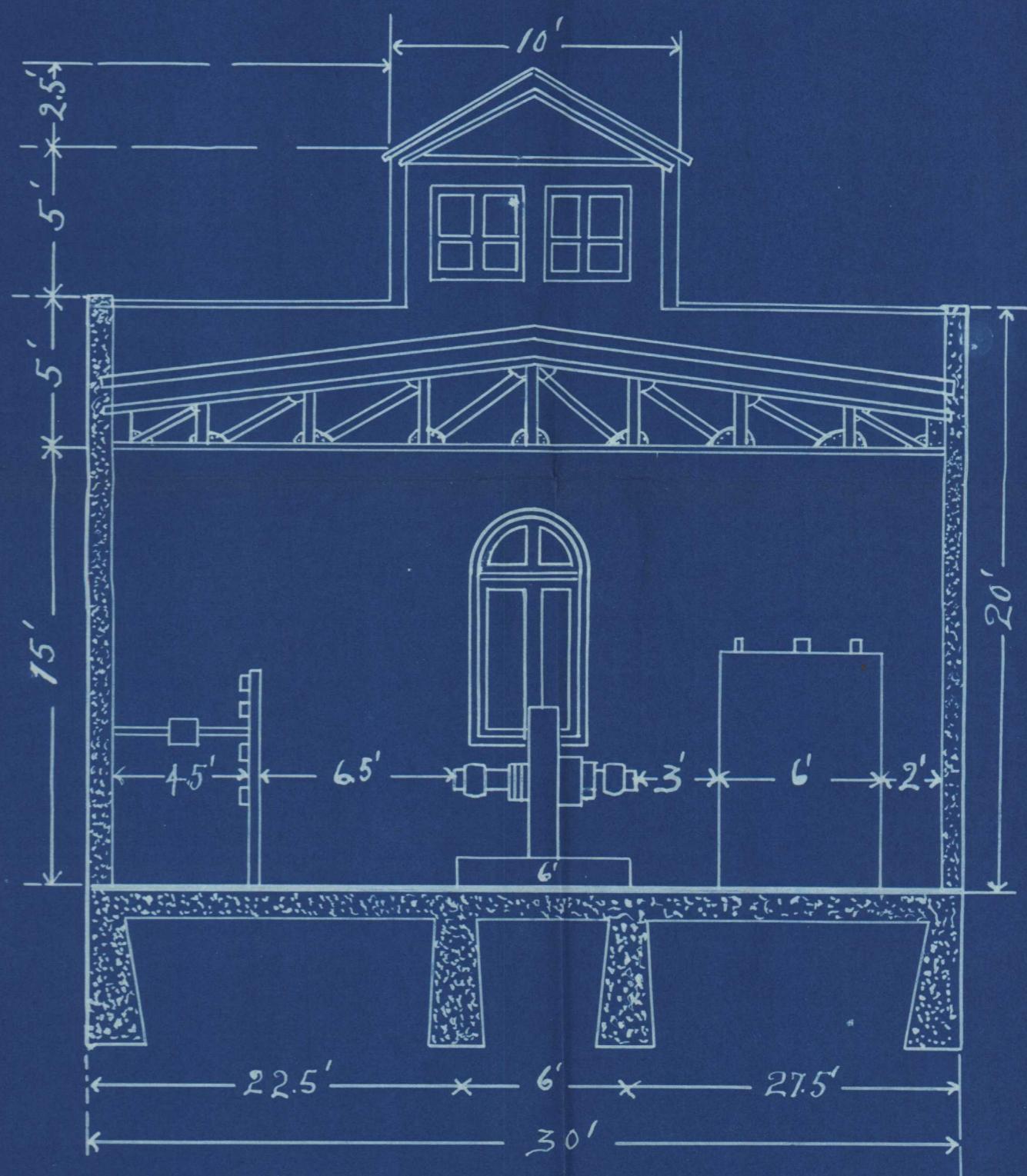
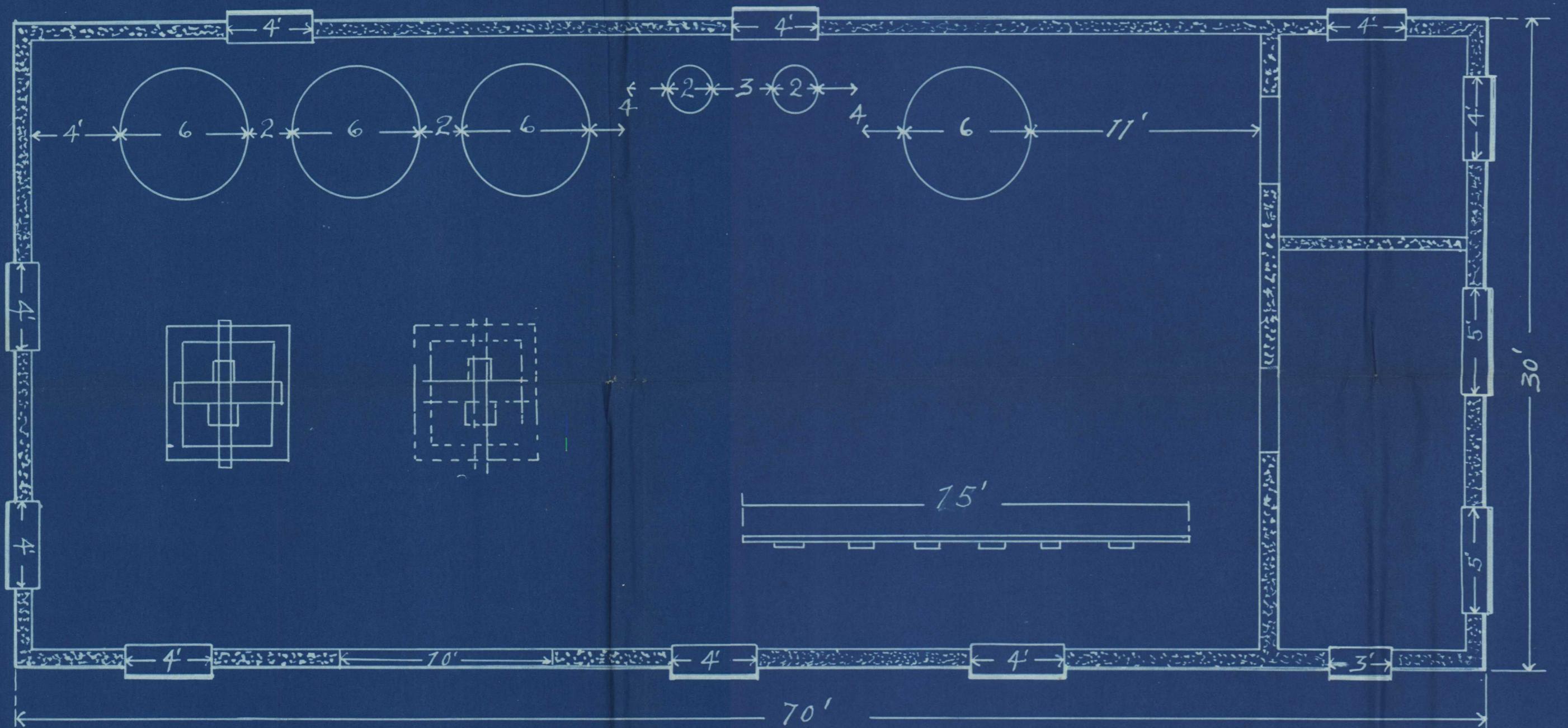
Scale of miles

0 5 10

MAP  
of  
TRANSMISSION LINE.

Serial no.

Plat & no. 6



THESES

SUB STATION

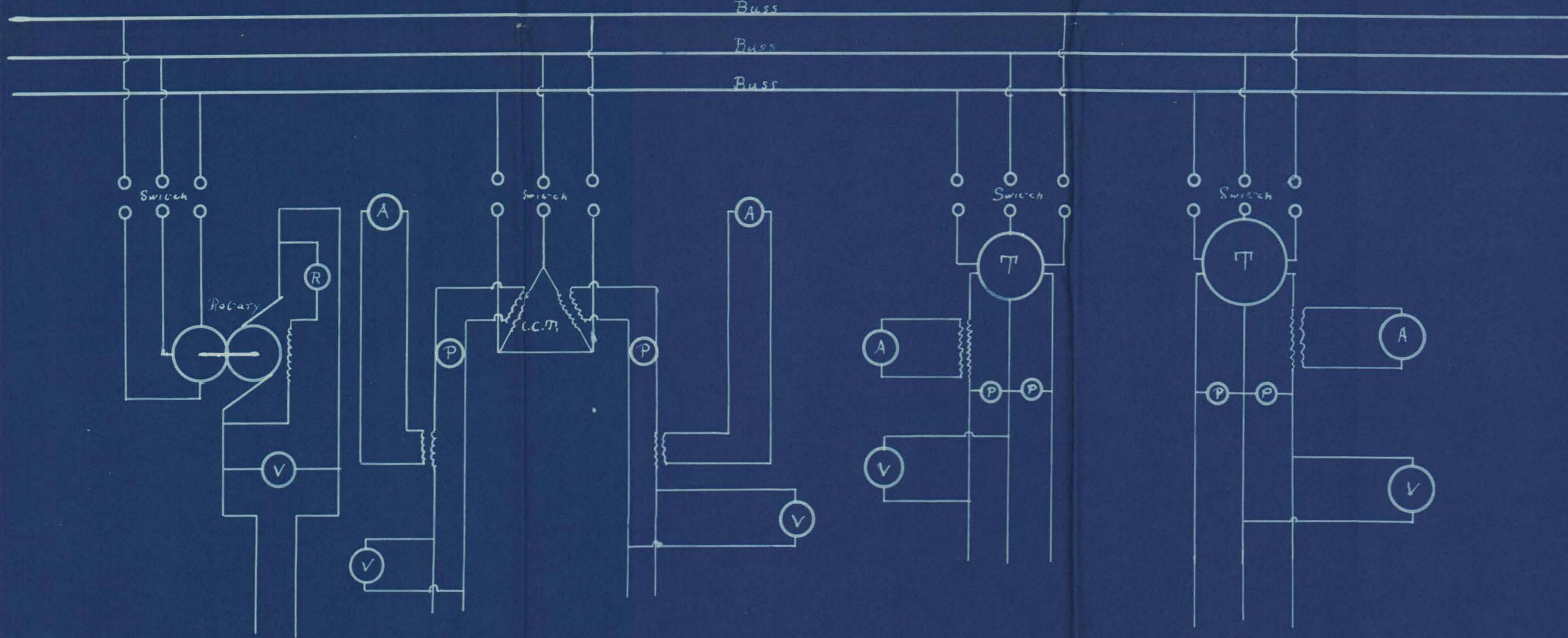
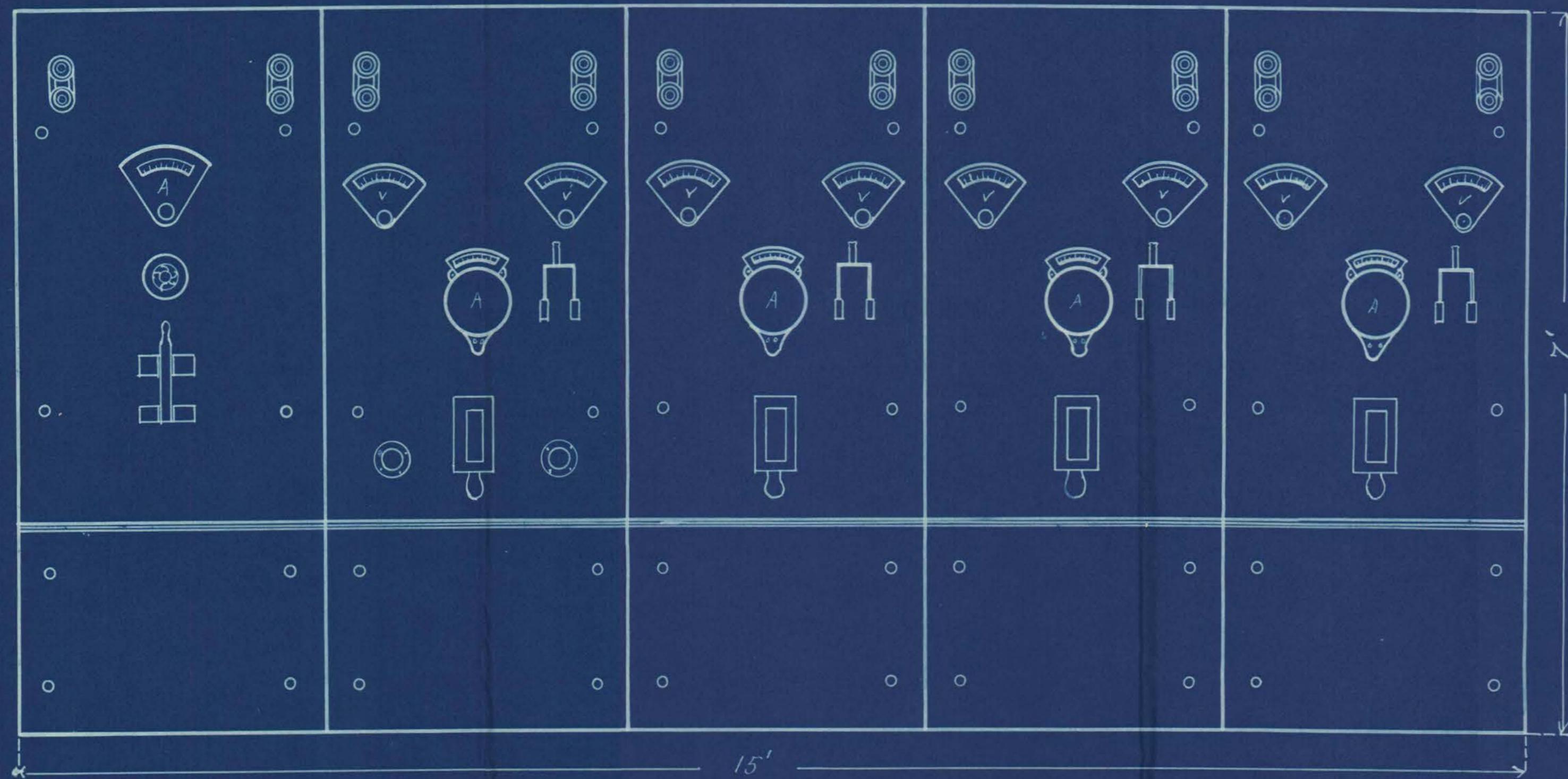
Drawn by

Grace M. Ropke  
C. A. Sonnen

Serial No.

Place No.

Scale one inch = five feet.



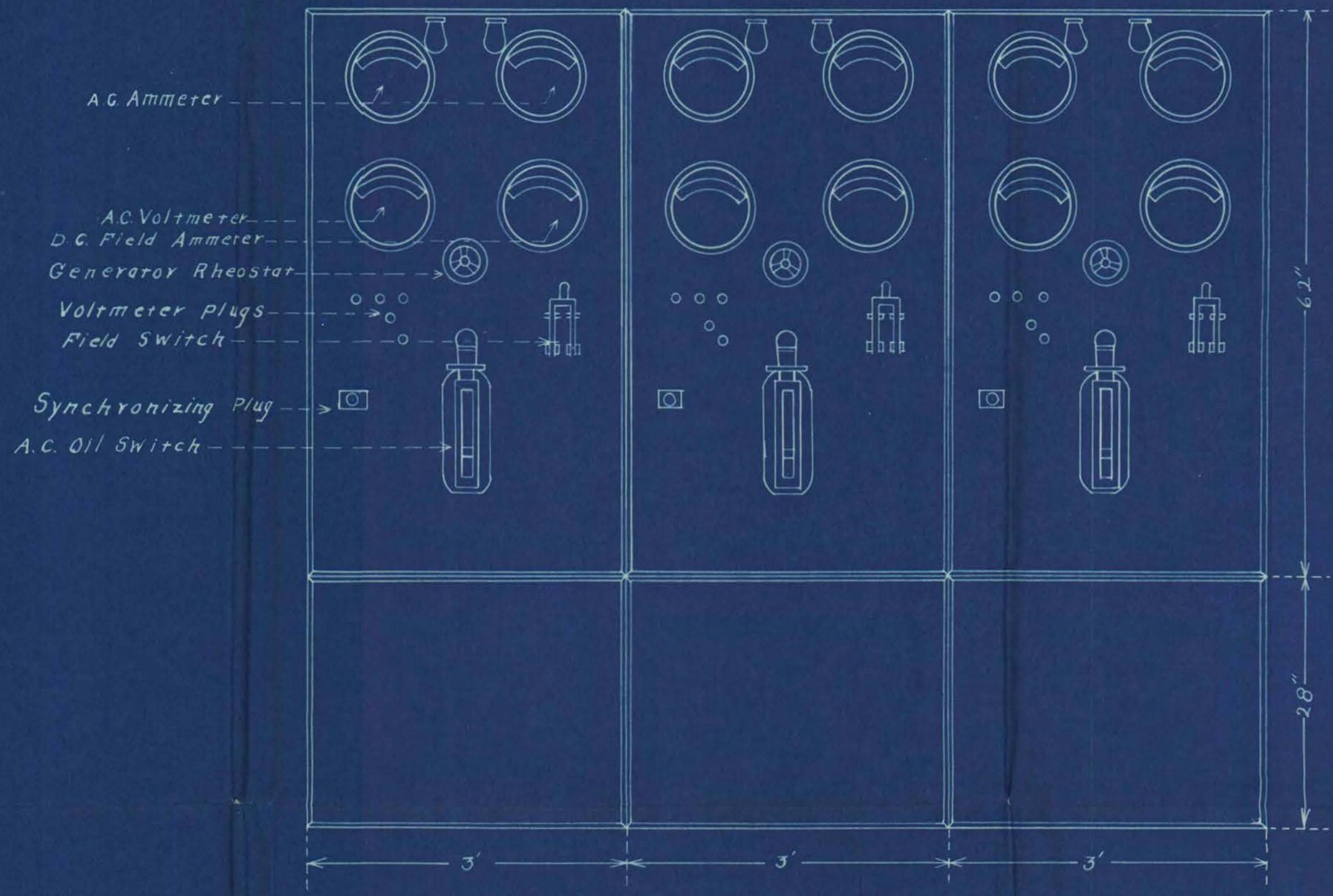
THESES  
SUB STATION.

Designed by H. M. Projst  
Ed. Saemson

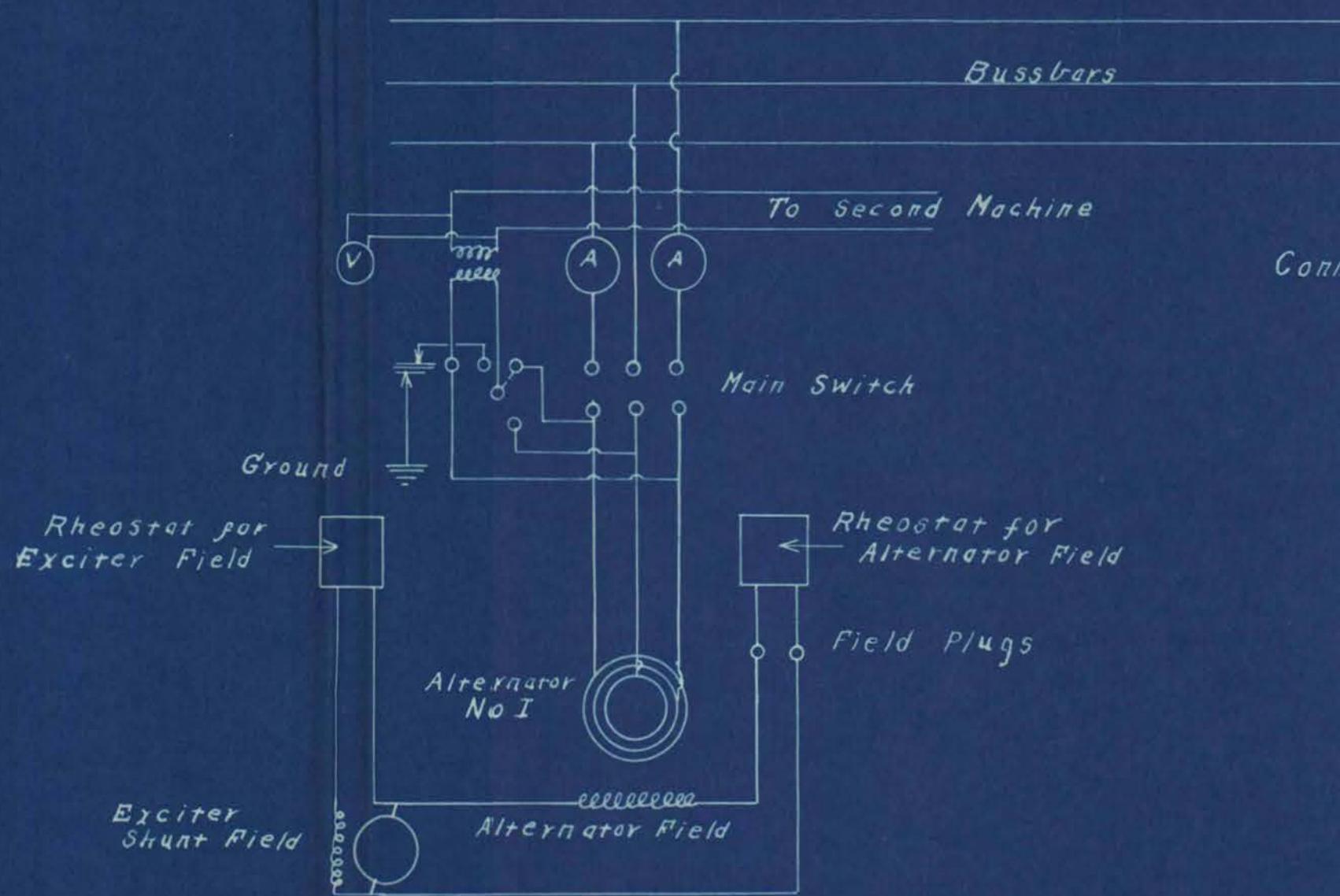
Drawn by H. M. Projst

Sixty

Place No 7

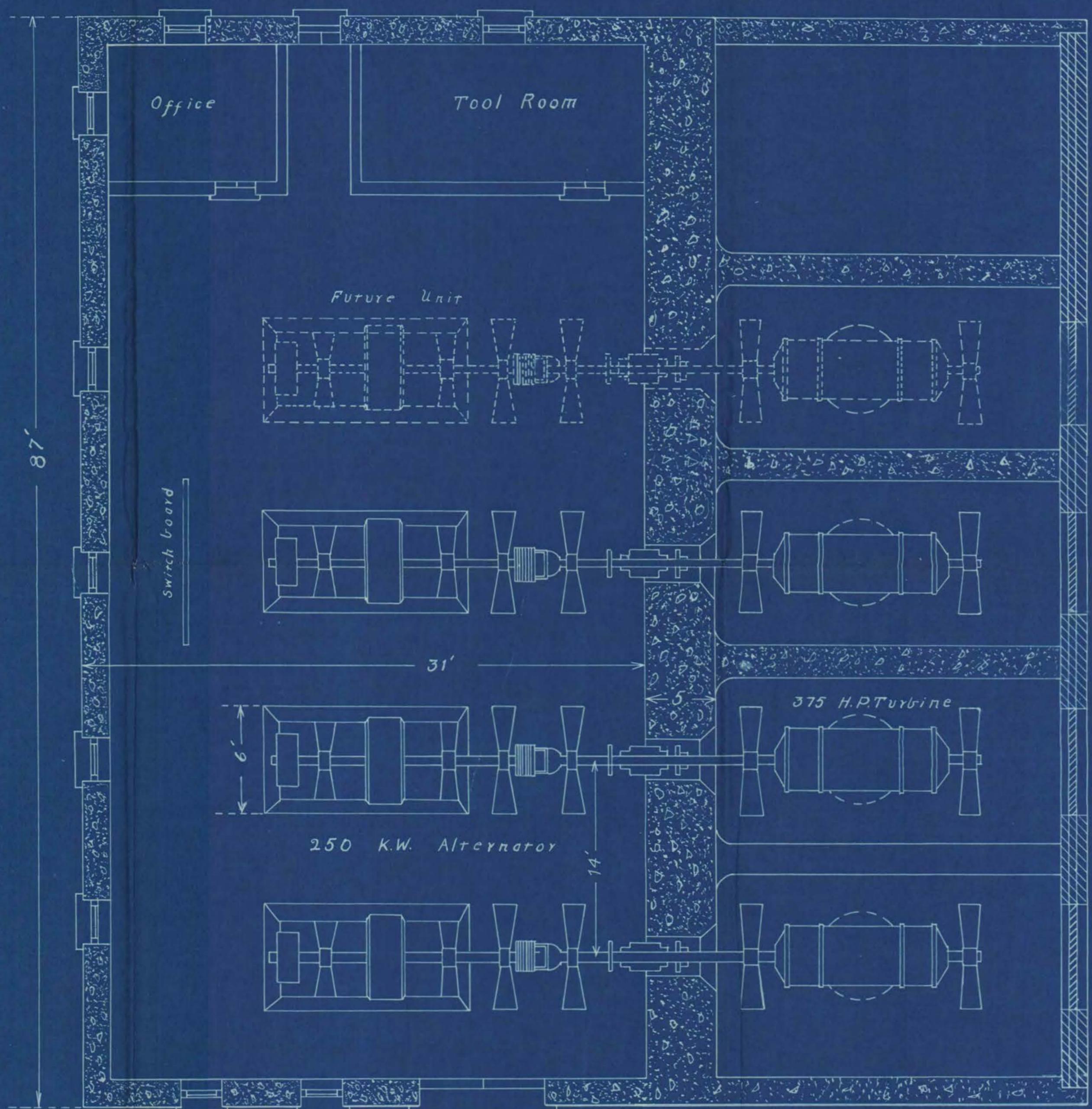


SWITCHBOARD  
 And  
 SWITCHBOARD CONNECTIONS



POWER PLANT  
 FOR  
 ALBANY OREGON

Designed by H.M. Propst  
 E.A. Sorenson  
 Drawn by G.A. Sorenson  
 Serial No. Plate No. 8



POWER PLANT  
FOR  
ALBANY OREGON

Designed by H.M. Propst  
EA Soverson  
Drawn by EA Soverson  
Serial No. Plate No. 9

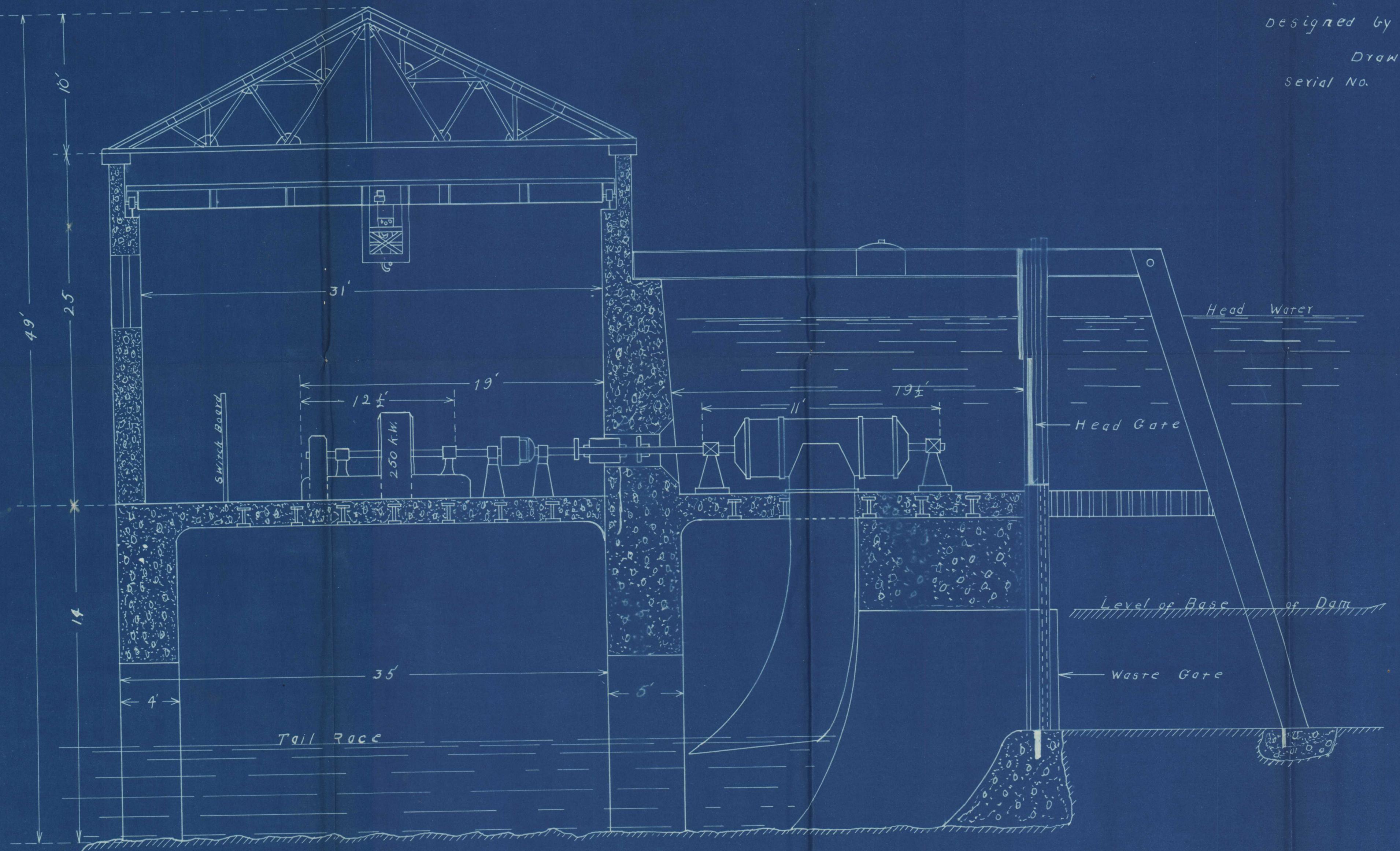
PLAN

POWER PLANT  
FOR  
ALBANY OREGON

Designed by H.M. Pyopst  
E.A. Sorenson

Drawn by C.A. Sorenson

Serial No. Plate No. 10



TRANSVERSE CROSS-SECTIONAL ELEVATION