

Nanowire metamaterials with extreme optical anisotropy

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The authors study perspectives of nanowire metamaterials for negative-refraction waveguides, high-performance polarizers, and polarization-sensitive biosensors. They demonstrate that the behavior of these composites is strongly influenced by the concentration, distribution, and geometry of the nanowires, derive an analytical description of electromagnetism in anisotropic nanowire-based metamaterials, and explore the limitations of their approach via three-dimensional numerical simulations. Finally, they illustrate the developed approach on the examples of nanowire-based high-energy-density waveguides and nonmagnetic negative-index imaging systems with far-field resolution of one-sixth of vacuum wavelength. © 2006 American Institute of Physics. [DOI: 10.1063/1.2422893]

The anisotropy of effective dielectric permittivity is widely used in optical, infrared (IR), terahertz and gigahertz sensings, spectroscopy, and microscopy.^{1–4} Strongly anisotropic optical materials can be utilized in nonmagnetic, non-resonant optical media with negative index of refraction and have the potential to perform subdiffraction imaging and to compress the radiation to subwavelength areas.^{2,5–7} The performance of these polarization-sensitive applications can be related to the relative difference of the dielectric constant along the different directions. In the majority of natural anisotropic crystals this parameter is below 30%.⁸ While it may be sufficient for some applications, a number of exciting phenomena ranging from high-performance polarization control⁴ to subwavelength light guiding^{2,5,6} to planar imaging⁷ require different components of a permittivity tensor to be of *different signs*.

In this letter we study the perspectives of using nanowire composites as *metamaterials* with extreme optical anisotropy. We demonstrate that even 10% stretching/compression of the nanowire structures *change* the sign of components of the permittivity tensor. We present an analytical description of wave propagation in anisotropic nanowire composites, generalized Maxwell-Garnett (GMG) approach, and verify our technique via three-dimensional (3D) numerical simulations. Finally, we illustrate our approach on the examples of several nanowire-based systems for light compression below the diffraction limit and negative-refraction imaging with far-field resolution of $\lambda_0/6$ (with λ_0 being free-space wavelength).

The use of metallic wire mesh as anisotropic low-frequency plasma has been proposed in Ref. 9 and experimentally realized for normal light incidence in Ref. 4 and 10. However, the applicability of these nanowire-based materials for any nontrivial geometry involving oblique light incidence or waveguiding is still considered to be questionable due to strong nonlocal interactions,¹¹ that may potentially result in *positive* components of the permittivity tensor. Furthermore, the majority of existing effective-medium theories (EMTs) [Refs. 11–14] are limited to the optical response of nanowires that are isotropically distributed in the host material. The predicted response of these systems is almost indepen-

dent of nanowire distribution and is described by a single parameter—nanowire concentration. These existing techniques are therefore not applicable for practical composites where the geometry is anisotropic due to fabrication process or as a result of a controlled mechanical deformation.¹⁵ Understanding the optical behavior of nanowire structures beyond one-parameter EMT is the main purpose of this letter.

The geometry of the nanowire composites considered in this work is shown in Fig. 1. The nanowires with permittivity ϵ^{in} are embedded into a host material with permittivity ϵ^{out} . The nanowires are aligned along the z direction of Cartesian coordinate system. We assume that the nanowires have elliptic crosssections with the semiaxes r_x and r_y directed along the x and y coordinate axes, respectively. We further assume that the homogeneous nanowire composite may be compressed or stretched, leading to the anisotropic distribution of individual nanowires. The typical separations between the

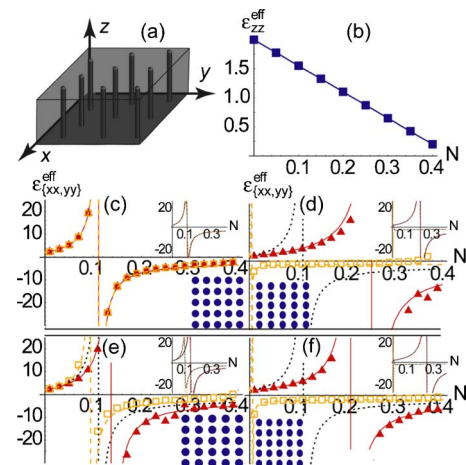


FIG. 1. (Color online) (a) Geometry of a nanowire composite. (b) $\epsilon_{zz}^{\text{eff}}$ for $\epsilon^{\text{in}} = -2.5$, $\epsilon^{\text{out}} = 2$ (Ag nanowires in a polymer for $\lambda_0 \approx 360$ nm). [(c)–(f)] $\epsilon_{xx}^{\text{eff}}$ (red triangles, solid lines) and $\epsilon_{yy}^{\text{eff}}$ (orange rectangles, dashed lines) for the composite in (a), with $\Lambda_x = \Omega_x = 0$ (c), $\Lambda_x = 0.2$; $\Omega_x = -0.2$ (d), $\Lambda_x = 0.2$; $\Omega_x = 0$ (e), $\Lambda_x = 0$; $\Omega_x = -0.2$ (f); quasistatic numerical calculations (symbols) and GMG (lines); dotted lines in (d)–(f) are identical to lines in (c). Bottom insets: cross sections of composites for $N = 0.35$. Black dashed lines in top insets: losses in nanowires ($\epsilon^{\text{in}} = -2.5 + 0.04i$). The breakdown of GMG occurs when the local field becomes inhomogeneous on the scale of r_x .

nanowires along x and y directions are denoted by l_x and l_y .¹⁶ In this work we focus on the case of “homogeneous metamaterial,” $r_\alpha, l_\alpha \ll \lambda_0$ and $N \ll 1$ (for the case of $\epsilon^{\text{in}} < 0$ additional requirement $r_\alpha \lesssim \sigma$, with σ being skin depth in wires must be fulfilled). Under these conditions, Maxwell equations have solutions that can be represented as a series of plane electromagnetic waves propagating inside a material with some effective dielectric permittivity¹⁷ ϵ^{eff} ,

$$\langle D_\alpha \rangle = \epsilon_{\alpha\beta}^{\text{eff}} \langle E_\beta \rangle. \quad (1)$$

The angular brackets in Eq. (1) denote the average over microscopically large (multiwire), macroscopically small (sub-wavelength) region of the space, with Greek indices corresponding to Cartesian components, and assumed summation over the repeated indices. If both ϵ^{in} and ϵ^{out} are isotropic, the permittivity tensor becomes diagonal, $\epsilon_{\alpha\beta}^{\text{eff}} = \delta_{\alpha\beta} \epsilon_{\beta\beta}^{\text{eff}}$, with $\delta_{\alpha\beta}$ being the Kronecker delta function.

We now derive the expressions for the components of the effective permittivities $\epsilon_{xx}^{\text{eff}}$, $\epsilon_{yy}^{\text{eff}}$, and $\epsilon_{zz}^{\text{eff}}$. Using the continuity of the E_z component, Eq. (1) yields

$$\epsilon_{zz}^{\text{eff}} = N \epsilon^{\text{in}} + (1 - N) \epsilon^{\text{out}}. \quad (2)$$

To find (x, y) components of the ϵ^{eff} we use the Maxwell-Garnett (MG) technique.^{12–14} This approach assumes $N \ll 1$ so that the local field in the composite is homogeneous across a nanowire. The fields D and E are then averaged over a typical nanowire cell, and Eq. (1) is used to extract the effective permittivity of a material. Naturally, average fields will have two contributions: one coming from the fields *inside* nanowires E^{in} , and the second one coming from the fields *between* nanowires E^{out} . The derivation of an EMT is therefore equivalent to understanding the relationship between E^{in} , E^{out} , and the *external* field acting on the system E^0 . Conventional MG approach assumes that $E^{\text{out}} = E^0$,^{12,13} which is true only for the case of isotropic nanowire distributions. In fact, the typical excitation field acting on a nanowire in the sample will contain the major contribution from external field E^0 and the feedback field scattered by all other nanowires in the structure $\hat{\chi} E^0$, resulting in the effective excitation $E^0 + \sum_j \hat{\chi}^j E^0 = [\delta_{\alpha\beta} - \chi_{\alpha\beta}]^{-1} E_\beta^0$. For rectangular, triangular, and other highly symmetrical lattices, as well as for a wide class of random nanowire microarrangements, the feedback tensor becomes diagonal,¹⁸ with the effective field acting on a nanowire being $[1 - \chi_{\alpha\alpha}]^{-1} E_\alpha^0$.¹⁹

Using the dimensionless function $S(\xi) = \sum_{ij} i^j j^i / (i^2 + \xi^2 j^2)^2$ with summation going over all pairs of i, j except coordinate origin, the summation of 2D dipole fields over rectangular lattice shown in Fig. 1(a) yields²¹

$$\chi_{\alpha\alpha} \approx -0.16 N \Lambda_\alpha P_\alpha (\epsilon^{\text{in}} - \epsilon^{\text{out}}), \quad (3)$$

where we introduced the lattice distortion vector $\{\Lambda_x, \Lambda_y\} = \{l_x/l_y - 1, l_y/l_x - 1\}$ and polarization term $P_\alpha = 1/[\epsilon^{\text{out}} + n_\alpha(\epsilon^{\text{in}} - \epsilon^{\text{out}})]$, with $\{n_x, n_y\} = \{r_y/(r_x + r_y), r_x/(r_x + r_y)\}$ being the depolarization factors.^{14,17} Note that $\chi_{\alpha\alpha} = 0$ only for $l_x = l_y$, corresponding to the well-known MG result.^{9,11–14}

This interwire interaction changes the “microscopic” field acting on the individual nanowires, and thus it directly affects both (homogeneous) field inside the nanowire E^{in} ,¹⁷

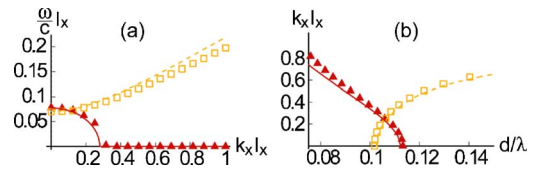


FIG. 2. (Color online) (a) Dispersion of the fundamental TM (red triangles, solid lines) and TE (orange squares, dashed lines) modes in a waveguide with $d=400$ nm with nanowire composite core; $\epsilon^{\text{in}}=13$; $\epsilon^{\text{out}}=-120$; $\Lambda_x=0.2$; $\Omega_x=-0.2$; $l_x=40$ nm; $r_x=10$ nm. Note the negative-refraction mode, predicted in Ref. 7. (b) Modal propagation constant for $\lambda_0=1.5$ μm as a function of d ; numerical solutions of 3D Maxwell equations (symbols); Eqs. (2), (6), and (7) (lines). The breakdown of GMG correspond to $|k_\alpha l_\alpha| \sim 1$.

$$E_\alpha^{\text{in}} = \frac{\epsilon^{\text{out}} P_\alpha}{1 - \chi_{\alpha\alpha}} E_\alpha^0, \quad (4)$$

and the average (dipole)¹⁷ field in between the nanowires E^{out}

$$E_\alpha^{\text{out}} \approx \left[1 + \frac{NP_\alpha(\epsilon^{\text{in}} - \epsilon^{\text{out}})(Q(N)(\Omega_\alpha + \Lambda_\alpha) - \pi\Omega_\alpha)}{2\pi(1-N)(1-\chi_{\alpha\alpha})} \right] E_\alpha^0, \quad (5)$$

with $Q(N) = \pi - 1 - N(\pi - 2)$ and shape vector $\{\Omega_x, \Omega_y\} = \{r_x/r_y - 1, r_y/r_x - 1\}$.

Combining Eqs. (1), (4), and (5) we arrive at the following expression for the in-plane components of permittivity in GMG approach:

$$\epsilon_{\alpha\alpha}^{\text{eff}} = \frac{N \epsilon^{\text{in}} E_\alpha^{\text{in}} + (1 - N) \epsilon^{\text{out}} E_\alpha^{\text{out}}}{N E_\alpha^{\text{in}} + (1 - N) E_\alpha^{\text{out}}}. \quad (6)$$

To verify the accuracy of the developed GMG technique, we generate a set of nanowire composites with given values of N , ϵ^{in} , ϵ^{out} , Λ , and Ω , excite each composite with a homogeneous field, and use the commercial finite-element partial differential equations solver, COMSOL MULTIPHYSICS 3.2,²² to solve Maxwell equations, and extract ϵ^{eff} via Eq. (1). In the simulations we used both random and periodic nanowire composites; the number of nanowires was sufficient ($>10^2$) to eliminate the dependence of ϵ^{eff} on the sample size. Figure 1 shows the excellent agreement between GMG approach presented in this work and numerical solution of Maxwell equations in quasistatic limit for $N, |\Omega_\alpha|, |\Lambda_\alpha| \lesssim 0.3$. The quasistatic material properties are fully described by *average* parameters (N , l_α , and r_α). This particular property of the effective-medium composites indicates high tolerance of anisotropic metamaterials to possible fabrication defects.

As expected, the field distribution across the nanowire structure and ϵ^{eff} are strongly affected by N , as well as Λ and Ω . Thus, even 10% anisotropy in inclusion shape or distribution may result in change of sign of dielectric permittivity.

As it has been noted for gigahertz systems in Ref. 11, the components of ϵ^{eff} may be strongly affected by the spatial dispersion. To clarify these effects we used COMSOL package to identify the eigenwaves propagating in x direction through a planar waveguide with a composite core consisting of a rectangular array of 10% Ag nanowires in Si host, extending from $z=0$ to $z=d$ [see Fig. 1(a)], bounded by perfectly conducting walls (see Ref. 7 for the detailed explanation of the effects of waveguide walls and material absorption on the mode propagation). In Fig. 2(a) we show the agreement of the results of numerical solutions of 3D wave equations with AIP license or copyright; see <http://apl.aip.org/apl/copyright.jsp>

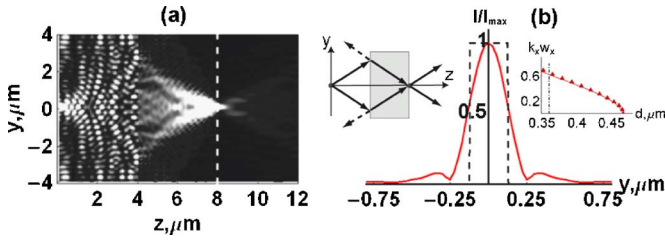


FIG. 3. (Color online) Planar waveguide imaging via nanowire materials $\lambda_0 = 1.5 \mu\text{m}$; $d = 360 \text{ nm}$; $n > 0$ material: $\epsilon = 13$; nanowire composite ($4 < z \leq 8$): $r_x = r_y = 10 \text{ nm}$; $l_x = l_y = 50 \text{ nm}$; $\epsilon^{\text{in}} = -120$; $\epsilon^{\text{out}} = 2$. (a) Intensity across the system; (b) intensity distribution across the focal plane; insets show planar-lens geometry and dispersion of a negative-index mode; dash-dotted line corresponds to $d = 360 \text{ nm}$ (a).

the EMT dynamics of TE and TM modes propagating in a waveguide with homogeneous anisotropic core, described by

$$\frac{\pi^2}{\epsilon_{yy}^{\text{eff}} d^2} + \frac{k_x^{(\text{TE})2}}{\epsilon_{yy}^{\text{eff}}} = \frac{\omega^2}{c^2}, \quad \frac{\pi^2}{\epsilon_{xx}^{\text{eff}} d^2} + \frac{k_x^{(\text{TM})2}}{\epsilon_{xx}^{\text{eff}}} = \frac{\omega^2}{c^2}, \quad (7)$$

with $\omega = 2\pi/\lambda_0$ and k_x , c , and d being the modal wave vector, speed of light in the vacuum, and waveguide thickness, respectively. Note that this system does not support TEM modes.⁷

Figure 2(b) illustrates one of the applications of nanowire-based optical composites, *high-energy-density waveguide*—a subwavelength structure supporting propagating volume modes. It is important to point out that in contrast to uniaxial media, anisotropic ($\epsilon_{xx}^{\text{eff}} \neq \epsilon_{yy}^{\text{eff}}$) nanowire composites can simultaneously support both $n > 0$ -TE and $n < 0$ -TM waves ($n = k_x c/\omega$). Moreover, the in-plane anisotropy (induced, for example, by deformation) can be used as a controlling mechanism in nanoscale nanowire-based pulse-management devices.

It is clearly seen that the propagation of these modes is adequately described by GMG technique when $|k_\alpha l_\alpha| \ll 1$. Note that the real requirement for EMT applicability, $|k_\alpha l_\alpha| \ll 1$, is different from the commonly used criterion $l_\alpha \ll \lambda_0$. Indeed, our simulations show that the spatial dispersion leads to cutoff of the modes with $|k_\alpha l_\alpha| \geq 1$, similar to gigahertz wire systems¹¹ and nanolayer-based photonic funnels.⁶

Another application of nanowire structure, nonmagnetic negative-index materials⁷ is illustrated in Fig. 3. It is seen that the nanowire materials may be used to achieve sub-diffraction ($\lambda_0/6$) far-field resolution in the planar-lens geometry.

In conclusion, we have developed the effective-medium theory (GMG) that adequately describes the optical properties of nanowire composites with anisotropic cross sections and arrangements. Limitations of the proposed approach have been studied via numerical modeling. We demonstrated that the nanowire composites can be used to achieve extreme anisotropy at optical and IR frequencies, with controlled effective permittivity ranging from $\epsilon \ll -1$ to $\epsilon \approx 0$ to $\epsilon \gg 1$ —thus leading to practical implementations of high-energy-density waveguides,^{5,6} novel polarization-sensitive

detectors, and recently proposed nonmagnetic negative-index systems.⁷ Finally, we note that the technique presented here can be readily applied to dielectric, plasmonic, and polar-wire composites at optical, IR, and terahertz frequencies, and can be further extended to the cases of nonaligned inclusions, anisotropic ϵ^{in} and ϵ^{out} , and 3D composites similar to what have been done for isotropic-arrangement cases in Refs. 13 and 14

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