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The characteristic of the subthreshold current in a GaAs MESFET exhibits a negative exponential function with V_{gs} . After studying the behavior of this current in this region over a range of temperature and drain bias voltages, a subthreshold current model was developed. The model was implemented in a circuit simulation program called VREFSIM. An arbitrary reference voltage is obtained by a simple selection of different component values. In this project, 2.56 volt and 1.28 volt references were designed and simulated. The simulated temperature coefficients of these two voltage references over a temperature range of -55 to 125 degrees Celsius were 7 and 26 parts-per-million (PPM)/Kelvin, respectively.

Modeling of Subthreshold Current in GaAs MESFET and
the Design of Voltage Reference Circuit

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Modeling of Subthreshold Current in GaAs MESFET and the Design of Voltage Reference Circuit

1. INTRODUCTION

As gallium arsenide (GaAs) integrated circuit (IC) technology matures, high-speed logic and memory applications of GaAs circuits are receiving more attention [1,2]. The inherent high electron mobility makes GaAs Metal Semiconductor Field Effect Transistors (MESFETs) an attractive technology over silicon based technologies. However, leakage currents in GaAs MESFETs due to backgating [3,4] and subthreshold conduction have impeded large scale integration of GaAs circuits.

In section 2 of this report, subthreshold current for a quarter micron gate length depletion-mode buried-channel GaAs MESFET is characterized. Two of the subthreshold models that were introduced in recent publications are discussed. Section 3 explores different possibilities of generating a temperature independent voltage reference. Finally, section 4 describes the circuit design implementation, simulation program VREFSIM, and gives design equations for generating other reference voltages using the same topology.

2. SUBTHRESHOLD CURRENT MODELING

2.1 Subthreshold Current Models

There are several approaches to model drain current behavior in MESFETs. These approaches vary from the physical models which involve a two-dimensional simulation [5,6] to a heuristic model [7]. Though it is insightful to do a comprehensive physical model, such a model obscures the necessary I-V relationship for circuit design and simulation. Therefore, the approach taken herein to model the subthreshold current is a compromise between understanding the first-order device physics, that is, relating device parameters to different drain voltage biases and temperature variations, and at the same time having an I-V relationship that is easily applied to circuit design and simulation.

Even though there are several sophisticated above-threshold MESFET models for circuit simulation [8,9], little work has been done in subthreshold modeling. The MESFET model that is presently implemented in SPICE2 is the Curtice MESFET model [10]. The Curtice model, as represented in Equation (1), is fairly accurate for V_{gs} values above the pinch-off voltage:

$$I_{ds} = \beta (V_{gs} - V_t)^2 (1 + \alpha V_{ds}) \tanh(\sigma V_{ds}), \quad (1)$$

where,

β is the transconductance,
 V_t is the threshold voltage,
 α is an empirical parameter that accounts for
 the output conductance, and
 σ is the channel conductance modeled at low V_{ds} .

Unfortunately, this model only represents the current in the square-law region, that is, above threshold voltage. When the gate to source voltage, V_{gs} , is equal to the threshold voltage, V_t , the model erroneously predicts zero current flow. The understanding of the drain current in the subthreshold region is critical to circuit design. One limitation to large-scale circuit integration in GaAs technology is the subthreshold leakage current. However, in this project the subthreshold current, which exhibits a linear exponential function is used to advantage in the design of a temperature insensitive voltage reference circuit.

Several subthreshold models have been introduced in recent publications. The McKinley model [11] is similar to the Curtice model with an added subthreshold term. The Chang model [12] specifically models the subthreshold conduction region. In the following, we discuss the McKinley and Chang models.

2.1.1 McKinley Drain Current Model [11]

The DC model Equation (2) for the drain to source

current is implemented by McKinley as :

$$I_{ds} = \beta (V_{gs} - V_{to})^2 (1 + \alpha V_{ds}) \tanh(\delta V_{ds}) + V_{ds}/R_{sh}, \quad (2)$$

and

$$R_{sh} = R_{sho}/2 [\exp (V_{to} - V_{gs}/STF * kT/q) + 1], \quad (3)$$

where,

R_{sho} is the parasitic drain to source shunt resistance at $V_{gs} = V_{to}$, and
 STF is an empirical parameter.

Equation (2) is similar to Curtice model except that McKinley uses R_{sh} in Equation (2) to empirically model the subthreshold current. The subthreshold current is given as :

$$I_{sub} = 2V_{ds}/R_{sho} * [\exp(V_{to} - V_{gs}/STF * kT/q) + 1]. \quad (4)$$

This equation was not implemented in this project because it lacks a description of the subthreshold current for V_{ds} at different temperatures. As was observed from the experimental data, drain voltage bias at different temperatures plays a significant role in the subthreshold current. Furthermore, the coefficient of the exponential term, $I_o = 2V_{ds}/R_{sho}$, is not a constant. As shown in section 2.2, a device is defined to enter the subthreshold region when $I_{sub} = I_o$, which is a constant.

2.1.2 Chang Subthreshold Current Model [12]

Chang specifically looks at the subthreshold region of MESFET drain current. He observed a linear exponential drain current in the subthreshold region and a monotonic increase

of this current at a more negative V_{gs} due to leakage current through the gate. Figure 1 represents a typical subthreshold current characteristic. The semi-empirical expression is:

$$I_{sub} = WJ \exp\left[\frac{q}{kT} N_s (1 - \Gamma V_{ds})(V_{gs} - V_{to} + \Phi V_{ds})\right], \quad (5)$$

for $V_{gs} < V_{to}$,

where,

- J current for low drain voltage at $V_{gs} = V_{to}$ in ampere/unit width,
- N_s Schottky ideality factor,
- Γ related mainly to the lowering of the Schottky barrier in volt⁻¹,
- Φ revealed mainly in the change of the subthreshold current slope, and
- W device width in microns.

This closed form of I-V relationship is relatively simple to implement in a voltage reference circuit design and simulation. The Chang model is therefore more appropriate to develop for this project than the McKinley model. The Chang model is implemented for a buried-channel depletion-mode GaAs MESFET in the next section.

2.2 Device for Model Implementation

The model developed in this project uses several definitions that differ from those of Chang. These modified definitions are necessary in order to relate first-order physics to the model and to set a convention for terms used in the rest of this thesis.

2.2.1 Buried-Channel GaAs MESFET

The device that is characterized and used in the circuit design has a 0.25 micron gate length and 50 micron gate width. It is a depletion-mode buried-channel GaAs MESFET. This device is well described in [13]. Figure 2 shows a side profile and energy band diagram and Figure 3 shows a impurity doping profile of the device.

The device is fabricated on a semi-insulating GaAs substrate. The active channel is silicon doped to a concentration of about $8E17$ dopant/cm³. This channel is "buried" between two p-type layers doped with beryllium. The top p-layer is shallow and highly doped, while the bottom p-layer is deep and lightly doped. The thickness of the active channel is defined as the distance from the gate depletion region to the channel-substrate depletion layer at zero gate bias. From Figure 3, the depth is about $6.6E-2$ microns.

2.2.2 Subthreshold Leakage Current Mechanism

For above threshold voltage analysis, the channel under the gate region provides a conduit for free carriers to drift from the source to the drain under the influence of an electric field. The number of available free carriers is assumed to be proportional to the constant doping profile, N_c . The free carriers at the fringing edges is assumed to have little contribution to the drain current conduction as

shown in Figure 5. The fringing edge effect is due to the probability of finding carriers a distance away from the edges. The assumption of a constant doping profile is valid only when $V_{gs} > V_t$ since the total number of free carriers in the constant doping profile dominates over the total number of free carriers in the edges.

However, the carriers at the edges will play a significant role in drain current conduction when V_{gs} is equal or less than V_t . Under this condition, the doping profile concentration became a exponential term :

$$\text{Doping Concentration} \propto N_c \exp[q(V_{gs} - V_t)/kT]. \quad (6)$$

The edge effect is modeled as :

$$\text{Edge Effect} \propto \exp[-t/L_D], \quad (7)$$

where,

L_D is the Debye length, and
 t channel thickness.

Therefore, the drain current density, J_n , and the total number of free carriers in the profile shown in Figure 5 is represented as:

$$J_n \propto \text{Number of free carriers},$$

$$J_n \propto 2 \int N_c \exp[q(V_{gs} - V_t)/kT] \exp[-t/L_D] dt, \quad (8)$$

for $V_{gs} \leq V_t$.

This first order analysis shows the exponential characteristic of the subthreshold current.

2.2.3 Development of Subthreshold Current Model in Buried-Channel GaAs MESFET

In this project the subthreshold current is modeled as :

$$I_{sub} = I_o \exp[(q/kTN_s)(1 - \Gamma V_{ds})(V_{gs} - V_{to} + \Phi V_{ds})], \quad (9)$$

where,

I_o current when the device enters subthreshold region,
 N_s, Γ parameters that model changes in the slope, and
 Φ is related to barrier lowering associated with changes in V_{ds} .

The approach to this model is semi-empirical. For this particular technology a set of empirical values for N_s, Γ and Φ have been determined from experimental data. N_s and Γ are obtained from a curve fitting program (see Appendix 7.4).

Because of the steep slope of the subthreshold characteristic, it is more appropriate to define a constant current when the device enters subthreshold region rather than a constant voltage. When the drain bias voltage, V_{ds} , and/or the temperature is increased, at constant V_{gs} , the active channel thickness is increased from t to t' [14] as shown in Figure 6a. Thus, more current flow through the channel. Graphical representation of the experimental data in Figure 6b illustrates the physical behavior of the drain current in Figure 6a. A more negative V_{gs} is needed to deplete the channel from t' back to t . A constant I_o

provides a consistent measure of the subthreshold region of operation. I_o is derived from Equation (2) :

$$I_{ds} = \beta (V_{gs} - V_t)^2 (1 + \alpha V_{ds}) \tanh(\sigma V_{ds}).$$

When V_{gs} is equal to the subthreshold voltage, V_{ts} (see Equation (11)), $I_{ds} = I_o$. Since I_o is independent of V_{ds} (see Figure 7), I_o is expressed as :

$$I_o = \beta (V_{ts} - V_t)^2, \quad (10)$$

For the device under study, I_o is taken as 0.1 milliamperes for all V_{ds} values and at all temperatures. Figure 7 shows I_o as defined on the data plots, and Figure 8 shows that I_o as expressed in Equation (10) is constant for the temperature range of interest.

At the threshold voltage, the channel is not fully depleted as predicted in the abrupt transition case. The voltage at which the device enters the subthreshold region, V_{ts} , is defined as the gate-source voltage for which the gate-channel depletion region and the channel-substrate depletion region are γ Debye lengths apart [15] :

$$V_{ts} = V_t + (2V_p \gamma L_D / t) (1 - \gamma L_D / 2t), \quad (11)$$

From Sze [16], the definitions of transconductance, β , pinch-off current, I_p , and threshold voltage with $V_{ds} = 0$, V_{to} , are used:

$$I_p = (W/L) U_q^2 N_c^2 t^3 / 6 \epsilon_s, \quad (12)$$

$$V_{to} = V_{bi} - V_p, \quad (13)$$

$$V_{bi} = kT/q \ln[N_c/n_i], \quad (14)$$

$$V_p = \frac{qN_c t}{2\epsilon_s} - \frac{T}{292}, \quad (15)$$

where,

N_c is the impurity doping concentration in dopant/cm³,
 U bulk carrier mobility in volt/cm²-second.

From equations (12) and (15), β is simplified to :

$$\beta = \frac{2}{3} \frac{W}{L} \frac{U_c \epsilon_s}{t} \frac{292^2}{T^2}. \quad (16)$$

It is observed that β is similar to the k' in a MOSFET, except it has an explicit temperature dependent term.

2.3 Experimental Procedure

A work station based on the Tektronix 4054A controller was set up to take measurements. A controller program was written in BASIC to interface various measuring instruments with the controller. A plotting program was also written to plot the experimental data. The large signals V_{ds} , V_{gs} , V_p and I_{ds} , for the device under investigation are first examined using a Tektronix 576 curve tracer. The data is stored on a magnetic tape for later analysis. An example of the measured data for the buried-channel MESFET is presented in Appendix 7.3.

2.3.1 Work Station SetUp

The equipment used in this project is listed in

Appendix 7.2. Figure 9 shows a schematic of the work station setup. Communication between instruments was based on HP-IB protocol. A closed system helium refrigeration unit and cold head allowed low temperature measurements to be taken. Also listed in Appendices 7.4 and 7.5 are the program listings for the controller and plotter.

2.3.2 Initial Determination of Large Signal I-V Behavior

Before the measurement sequence began, it was imperative that the large signal characteristics of the device be examined. This is to assure that the data gathered is valid within the range of useful V_{ds} , V_{gs} and I_{ds} values.

Two parasitic effects in some MESFETs are kinking [17] and looping [18]. To avoid kinking effect, V_{ds} is ramped up to a maximum of 3.0 volts. And to avoid looping, measurements were taken at DC. The pinch-off voltage is also determined experimentally using the curve tracer.

2.4 Subthreshold Current Model

The subthreshold current model developed in the previous three sections is implemented in this section. The implementation starts with the interpretation of data. The two empirical parameters N_s and Γ are extracted through a least-square method of curve-fitting.

2.4.1 Data Interpretation

The data acquired for the buried-channel MESFET is plotted as drain current, I_{ds} , versus gate-source voltage, V_{gs} . To observe the influence of the drain bias voltage, V_{ds} , a set of plots are made with constant temperature but varying V_{ds} as shown in Appendix 7.3.1. Conversely, the effect of temperature is studied by keeping the V_{ds} constant and varying the temperature as in Appendix 7.3.2.

The pinch-off voltage for this device at room temperature is approximately -0.75 volt. In the subthreshold region, the drain current varies exponentially in the region of $-0.75 \text{ V} < V_{gs} < -1.0 \text{ V}$. Also observed was a gradual monotonic increase of drain current for $V_{gs} < -1.0 \text{ V}$. This increase was principally due to the gate conduction through the reverse-biased gate-to-drain diode.

Since I_0 is constant, the voltage in which the device enters subthreshold region will vary with temperature and V_{ds} as modeled by the Φ parameter. From both representations of data in Appendix 7.3, the slope of the exponential curve decreases with increasing temperature and V_{ds} . The changes in the slope are modeled by the N_s and Γ parameters.

2.4.2 Parameters Extraction

Two of the three parameters (N_s and Γ) that modeled the

changes in temperature and V_{ds} are extracted from a curve fitting program (Appendix 7.5). From the data plots, the changes in $V_{gs}(I_{sub} = I_o)$, Φ , are consistent, and can be measured directly from the plot as shown in Figure 7.

The parameter values extracted by the methods described above for the device characterized are :

$$N_s = 1.671$$

$$\Gamma = 0.046 \text{ Volt}^{-1}, \text{ and}$$

$$\Phi = 0.07.$$

Implementing these parameters, and letting I_o equal 0.1 milliamperes in Equation (10), the current model agrees with the subthreshold current data with the experimental error as shown in Figure 10.

3. VOLTAGE REFERENCE

3.1 Generation of V_{ref}

Voltage references find useful applications both in analog and digital circuits. In analog ICs, voltage references are found in operational amplifiers and analog-to-digital converters. In digital ICs, a temperature insensitive voltage reference is required for biasing circuits such as ECL gates. In all applications, the sensitivity of the voltage reference to temperature is a critical issue.

On a GaAs IC, the two devices that are available to generate a DC voltage reference are a thin-film resistor and MESFET a transistor. These two devices have one or more temperature dependent term in their current expressions. Therefore, the strategy was to find a positive and a negative temperature drift component. To obtain a minimum temperature dependence of the voltage reference, the scaled sum of these two components must give an overall change in current over temperature to be approximately equal to zero. Figure 11 shows a schematic of a voltage reference design by the technique of drain current summation. The next two sections examine the available components and how to make use of their temperature variation properties.

3.2 Negative Temperature Coefficient Component

The first-order temperature dependence of resistance of a resistor is represented by :

$$R(T) = R_0 + \alpha_t (T - T_{273}), \quad (17)$$

where,

R_0 resistance at 273 Kelvin,
 α_t resistance coefficient of resistor in ohm/Kelvin,
 T operational temperature, and
 T_{273} is 273 Kelvin.

The current through the resistor and the derivative of the current with respect to the temperature are given by :

$$I_R = V/R(T), \quad (18)$$

$$dI_R/dT = -(\alpha_t V)/[R_0 + \alpha_t (T - T_{273})]^2, \quad (19)$$

where, V is assumed to be a constant with temperature.

Assuming α_t is positive, the dI_R/dT is a negative quantity. Thus, resistors provide a negative temperature drift component of current.

The MESFET operating in the square-law saturation region also exhibits a negative temperature drift coefficient of current as the shown below :

$$I_{ds} = \beta (V_{gs} - V_t)^2 (1 + \alpha V_{ds}) \tanh(\alpha V_{ds}), \quad (20)$$

From Appendix 7.1.1, Equation (18) is recast as :

$$I_{ds} = (A/T^3)(C - BT)^2 D, \quad (20a)$$

where,

A , B , C , D are positive temperature independent variables, and $(C - BT) > 0$.

Therefore, the derivative of Equation (20a) with respect to temperature is :

$$\begin{aligned} dI_{ds}/dT &= -(2AD/T^3)(C - BT)(B + 2/T*(C - BT)) \quad (21) \\ &= \text{Negative Quantity.} \end{aligned}$$

Thus, the resistor and the MESFET operating in the square-law saturation region are both used in the design to provide current component with negative temperature drift.

Next, a positive temperature drift component of current with predictable behavior must be implemented in the circuit. When these two temperature components are appropriately combined, the resulting dI/dT is ideally zero.

3.3 Positive Temperature Coefficient Component

The other region of MESFET operation, the subthreshold region is now examined closely.

Though the subthreshold current is usually undesirable in a circuit design, its predictable behavior is advantageously made use of in this design. Interestingly, when the device operates in the subthreshold region, its subthreshold current increases with temperature, as shown in the following equations and derivative:

$$I_{dsub} = I_o \exp[(q/kTn_s)(1 - \Gamma V_{ds})(V_{gs} - V_{to} + \phi V_{ds})]. \quad (22)$$

From Appendix 7.1.2, Equation (22) is recast as :

$$I_{sub} = I_o \text{Exp}[-AB] \text{Exp}[AC/T], \quad (22a)$$

where,

A and B are positive temperature independent variables.
C is negative temperature independent variable.

Therefore, the derivative of Equation (23a) with respect to temperature is :

$$\begin{aligned} dI_{sub}/dT &= -I_o \text{EXP}[-AB] (AC/T^2) \text{exp}[AC/T] & (23) \\ &= \text{Positive Quantity.} \end{aligned}$$

This current provides the positive temperature drift component for the voltage reference circuit design. This positive quantity is predicable by the current model. These quantities are further emphasized by the design curves generated from VREFSIM program in the next section.

4. VOLTAGE REFERENCE CIRCUIT DESIGN

4.1 Circuit Implementation

The voltage reference implementation technique with GaAs MESFETs deviates from that of the bipolar voltage reference [20]. As the name implies, the bipolar bandgap reference circuit is only referenced at one voltage, that is at the silicon bandgap voltage of 1.12 volt at room temperature. The technique deployed is a voltage summation [19] as shown in Figure 12.

Conversely, using GaAs MESFETs and current summation, any reference voltage is realizable so long as the reference voltage is within the power supply limits and all devices operate in saturation. The technique of current summation is illustrated in Figure 13.

From section 3, the schematic in Figure 11 has been realized with two MESFETs, one operating in the square-law saturation region and the other operating in the subthreshold saturation region. Figure 13 shows the transistor-level schematic of the circuit. The idea behind drain current summation is that the negative temperature coefficient of the drain current of device M2 will cancel the positive temperature coefficient of the drain current of

the subthreshold device M1. Ideally, the current through the resistor R₀ is constant with temperature. Thus, a voltage is generated by the constant current flowing through the resistor R₀. This is almost the case in the circuit simulation except that the thin-film resistor has a small positive temperature coefficient. For the worst case, the temperature coefficient of the resistance is 100 PPM/Kelvin. The resistor R₁ biases M1 in the subthreshold region, and R₃ holds the node voltage V₁ to a variation of only q0.1 V. Without R₁, V₁ will vary in a range of q0.3V. This is undesirable because the device M1 may exit the the subthreshold region. The resistor R₂ biases M2 in the square-law saturation region.

4.2 Square-Law Device in Saturation

In Section 2, the first-order subthreshold device physics were discussed. In this section, the first-order physics of the device operating in square-law saturation region are analyzed.

The doping concentration in the channel, N_c, is assumed to have a uniform profile. The electron mobility is inversely proportional to temperature and thus, mobility at different temperatures is calculated as :

$$\frac{U_{300}}{T_{300}} = \frac{U_T}{T}, \quad (24)$$

where,

μ_{300} bulk mobility at room temperature,
 T_{300} room temperature = 300 Kelvin,
 μ_T mobility at temperature T, and
 T temperature of interest.

The device operating in square-law saturation region has a gate length of 0.25 micron and a gate width of 5 micron. The I-V equation for this region is given from the Curtice model as:

$$I_{ds} = \beta (V_{gs} - V_t)^2 (1 + \alpha V_{ds}) \tanh(\kappa V_{ds}),$$

where,

$$\begin{aligned} \alpha &= 0.05 \text{ volt}^{-1}, \\ \kappa &= 2.2 \text{ volt}^{-1}, \text{ and} \\ V_{gs}(T=300) &= 0.0 \text{ volt.} \end{aligned}$$

The variables that change with temperature are β and V_t . These variations are analyzed in the next two sections.

4.2.1 V_p Variations with Temperature

The pinch-off voltage here assumes a channel pinch-off rather than saturated velocity pinch-off. The pinch-off voltage term used in this project has a slightly different definition from that of Sze. From Equation (15) :

$$V_p = \frac{qN_c t^2}{2\epsilon_s} \frac{T}{292}.$$

With the assumption that the doping profile is a constant, V_p varies linearly with temperature. The derivative of $(V_p)^2$ with temperature is a positive term :

$$\frac{dV_p}{dT} = \frac{2T}{292^2} \frac{qN_c t^2}{2\epsilon_s}. \quad (25)$$

4.2.2 Beta Variations with Temperature

From Equations (16), the transconductance, β , is represented as :

$$\beta = \frac{2}{3} \frac{W}{L} \frac{U_c \epsilon_s}{t_c} \frac{292^2}{T^2}.$$

The implicit temperature dependent term is mobility. The bulk mobility varies as T^{-1} . The derivative of β with respect to temperature is a negative term :

$$\frac{d\beta}{dT} = -\left(\frac{4}{3} \frac{W}{L} \frac{U_c \epsilon_s}{t_c} \frac{292^2}{T^3}\right). \quad (26)$$

Therefore,

$$\frac{dI_{ds}}{dT} = \frac{d\beta}{dT} * \frac{dV_p}{dT} * C, \quad (27)$$

where,

$$C = (1 + \alpha V_{ds}) \tanh(\delta V_{ds}).$$

4.3 VREFSIM Circuit Simulation Program

The MESFET model that is available in SPICE2 does not model the subthreshold behavior. A simulation program that implements the DC behavior of the MESFET, including the subthreshold region was implemented in Pascal. In the following sections, the basic programming technique, user interface, and generation of design curves are discussed.

4.3.1 Programming Technique

The VREFSIM program consists of four subroutines. Three of these subroutines generate design curves and one simulates the circuit. The purpose of these different subroutines is explained fully in section 4.3.3. The required algorithms are simplified since only the DC analysis of the circuit is of interest for DC voltage references. The programming techniques for these programs are similar, with the basic idea being to establish a continuity of current at a node.

A node is the point where two or more devices are connected together as illustrated in Figure 14. An initial guess of the node voltage, V_n , is made. For the example shown in the Figure 14, the resistor current, I_r , is calculated using Ohm's law and the current for the MESFET, I_m , is found using Equation (2). The relative ratio of I_m/I_r indicates the continuity of current through the node. The

ratio is recast as $(I_m/I_r - 1)$. For the implemented program, the error tolerance was set at 0.5 percent. When the ratio is less than or equal to the tolerance, the continuity of current at that node is established. Otherwise the node voltage is either increased or decreased so that the ratio will approach the tolerance level.

4.3.2 Generating Design Curves

There are three subroutines in VREFSIM that generate design curves for a particular subthreshold device and a square-law device. These subroutines generate the design curves that give the designer a choice of different square-law device gate width for a given gate length, and the subthreshold biasing current for a given V_{gs} . With this information the designer is able to optimize the design. The generation and explanation of these design curves are given in the following sub-sections.

4.3.2.1 Square-Law Device

The square-law device is simulated by the subroutine called NORMAL. For a given gate width, the current-temperature slope is calculated and plotted in Figure 15.

4.3.2.2 Subthreshold Device

There are two subroutines that simulate the device in subthreshold saturation region. One subroutine, SUB_DEV,

generates a plot of dI/dT versus the bias current, I_{bias} , for a given V_{gs} , as shown in Figure 16. The purpose of this design curve is to give the designer a view of different dI/dT values that are obtainable with different V_{gs} and bias current values.

The second subroutine, SUB_R1R3 calculates the values of R1 and R3 for the given bias current. Since nickel-chrome thin-film resistors are used in this GaAs process, the values of resistance have a resolution of 1 ohm. Therefore, R1 and R3 are accurately adjusted to give the desired bias current and dI/dT to compensate the dI/dT of the square-law device.

4.3.3 Design Procedure

Since the generated voltage is based on the principal of current summation, the dI/dT 's of the square-law device and the subthreshold device must add up to approximately zero. By using the design curves, one can determine the range of dI/dT 's that are suitable for these devices to compensate each other.

The program NORMAL provides the appropriate width W for the square-law device and SUB_R1R3 gives the values of R1 and R3. These data are then input into the full circuit simulation subroutine called CKTSIM. The output gives the voltage reference value over the desired range of

temperatures. The temperature coefficient of the reference is determined as :

$$\text{PPM} = \frac{(\text{Vhi} - \text{Vnom}) * 1\text{E}6}{\text{Vhi} * (\text{TempHi} - \text{TempLo})}. \quad (28)$$

4.2.6 Simulated Output

Two voltage reference circuits were designed. Both used the same number of circuit devices. The circuits were simulated over the temperature range of -55 to 125 degrees Celsius. Figure 17 shows the negative temperature drift component of the square-law device, and Figure 18 shows the positive temperature drift component of the subthreshold device. One reference is at 2.56 volts with a temperature variation of 6.5 PPM/Kelvin. The second reference is at 1.28 volt with a temperature variation of 26 PPM/Kelvin. Figures 19 and 20 show the simulated output of these two circuits.

5. CONCLUSION

The advantages of this voltage reference over a bipolar bandgap reference [20] are very significant. A typical temperature sensitivity for a bipolar bandgap circuit is in a range of 30 - 60 PPM/Kelvin, whereas, for this MESFET circuit, the voltage variation over temperature is about 6.5 PPM/Kelvin for the 2.56 volt reference.

The differences in performance are due to the basic technique of generating the voltage reference. In bipolar technology, the reference voltage is generated by summing V_{be} and ΔV_{be} . The derivative of this sum with temperature determines the performance of the circuit with temperature. In GaAs MESFET technology, the reference voltage is generated by summing the derivative of current components with temperature :

$$dI/dT = dI_{sub}/dT + dI_{ds}/dT. \quad (28)$$

The dI/dT is typically in the range of $1E-6$ ampere/Kelvin, whereas, dV/dT is typically in the range of $1E-3$ volt/Kelvin. The resolution of the current summation technique is three orders of magnitude better than the voltage summation technique.

One important advantage of this MESFET circuit is that

it requires no amplification. In this project, 2.56 volt and 1.28 volt references are realized using the same circuit without any additional components. In other words, any voltage reference is realizable using this circuit as long as the devices are kept in saturation. This is also an important advantage over other voltage reference techniques. For example, in a bipolar bandgap reference, the 1.12 volt reference is not generally very useful. This voltage must be amplified by an external gain circuit to a more practical voltage. The additional devices in the amplification circuit not only increase the cost, but also degrade the performance. Figure 21 shows a comparison between the two voltage reference schemes.

Finally, it was observed that the subthreshold behavior in a MESFET is similar to a MOSFET. Therefore, it may be possible to transfer the design technique from GaAs MESFETs to silicon MOSFETs.

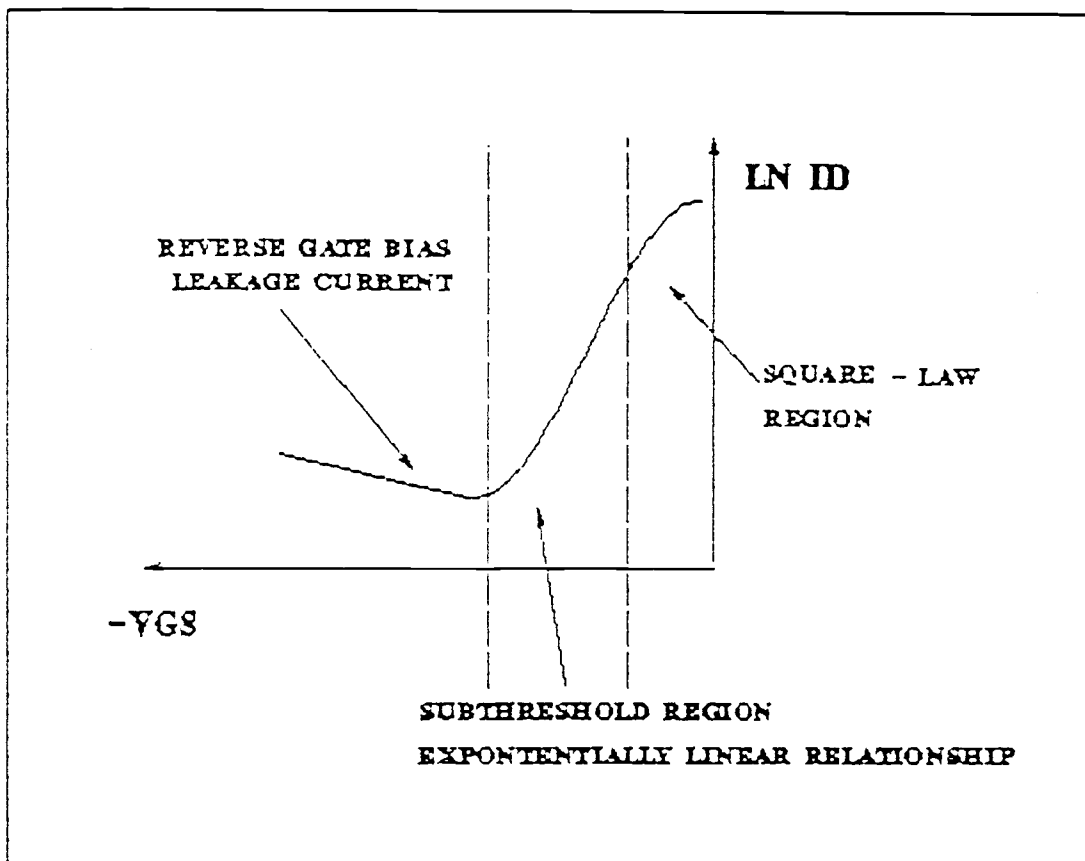


Figure 1. MESFET in Subthreshold Current Region

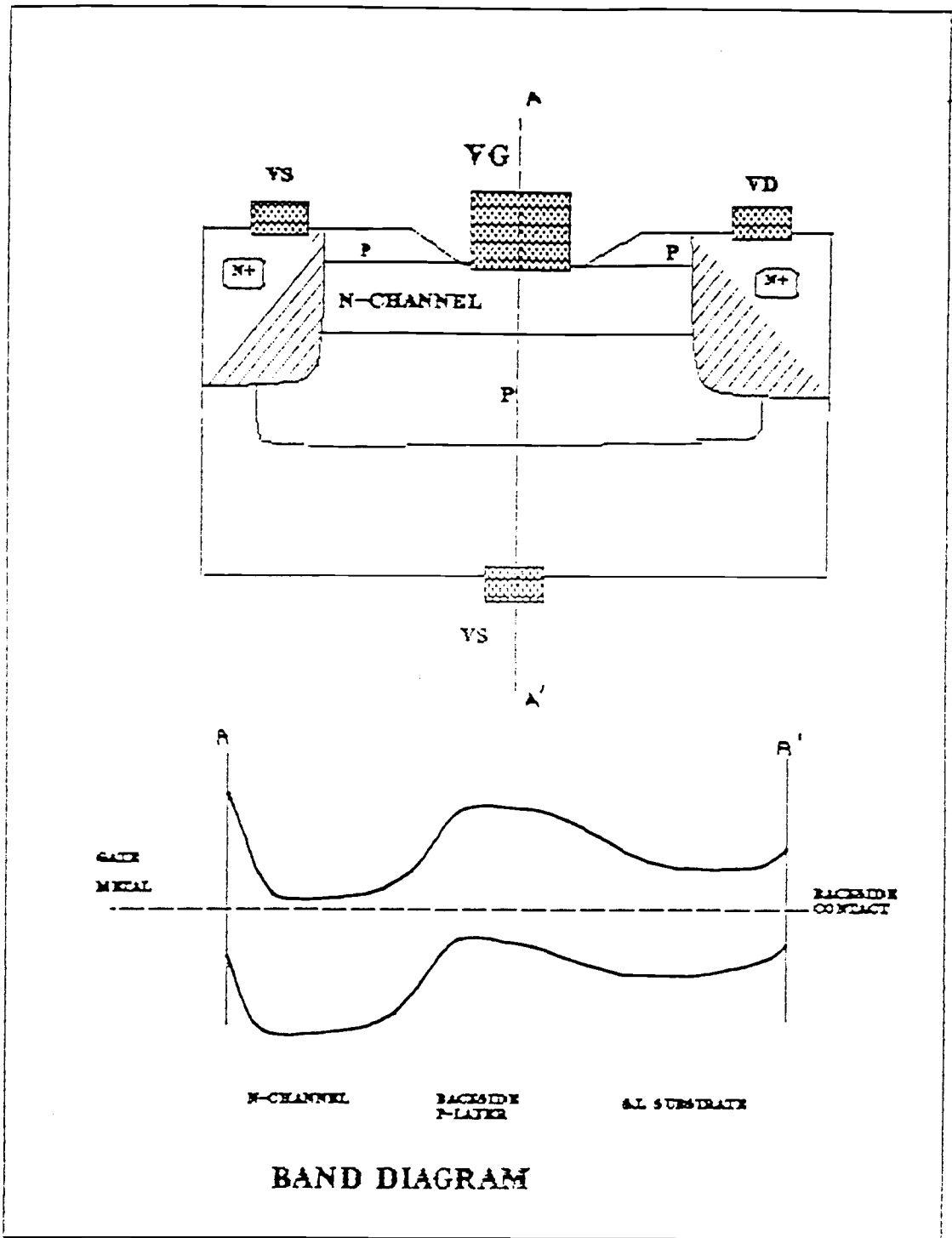


Figure 2. Buried-Channel GaAs MESFET

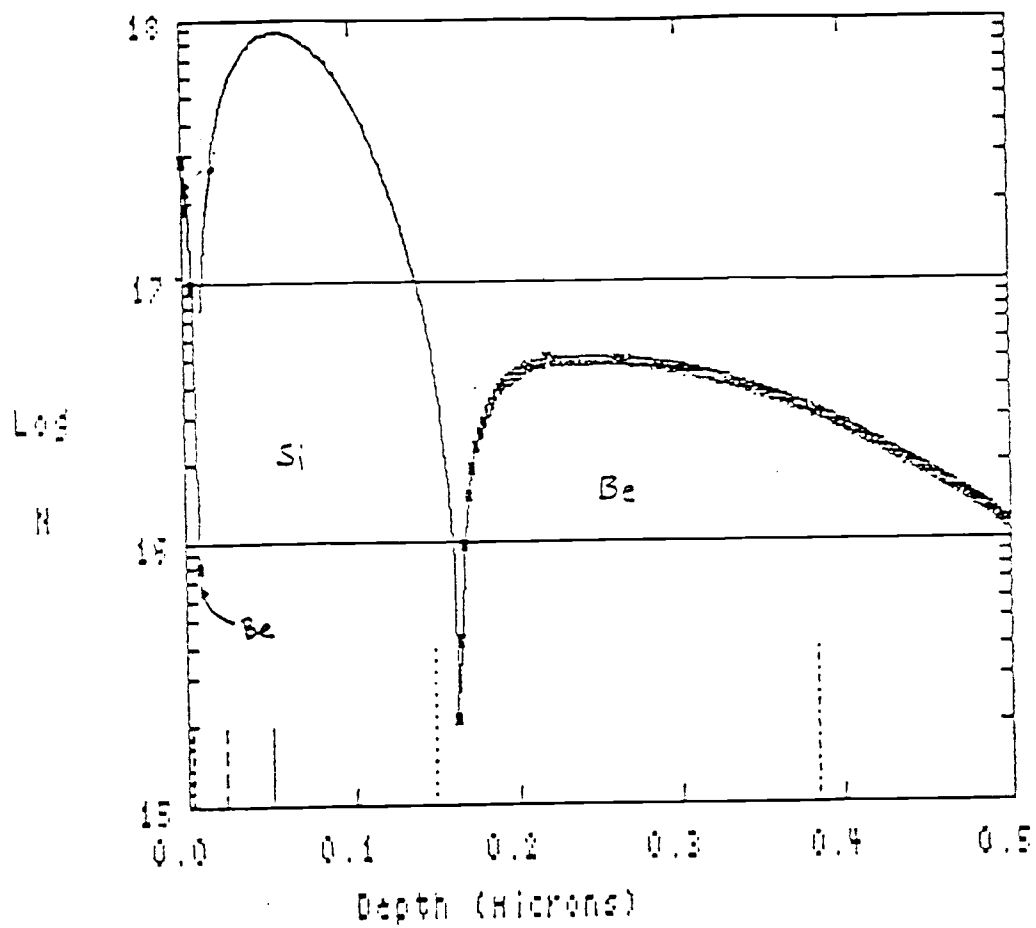


Figure 3. Impurity Doping Profile

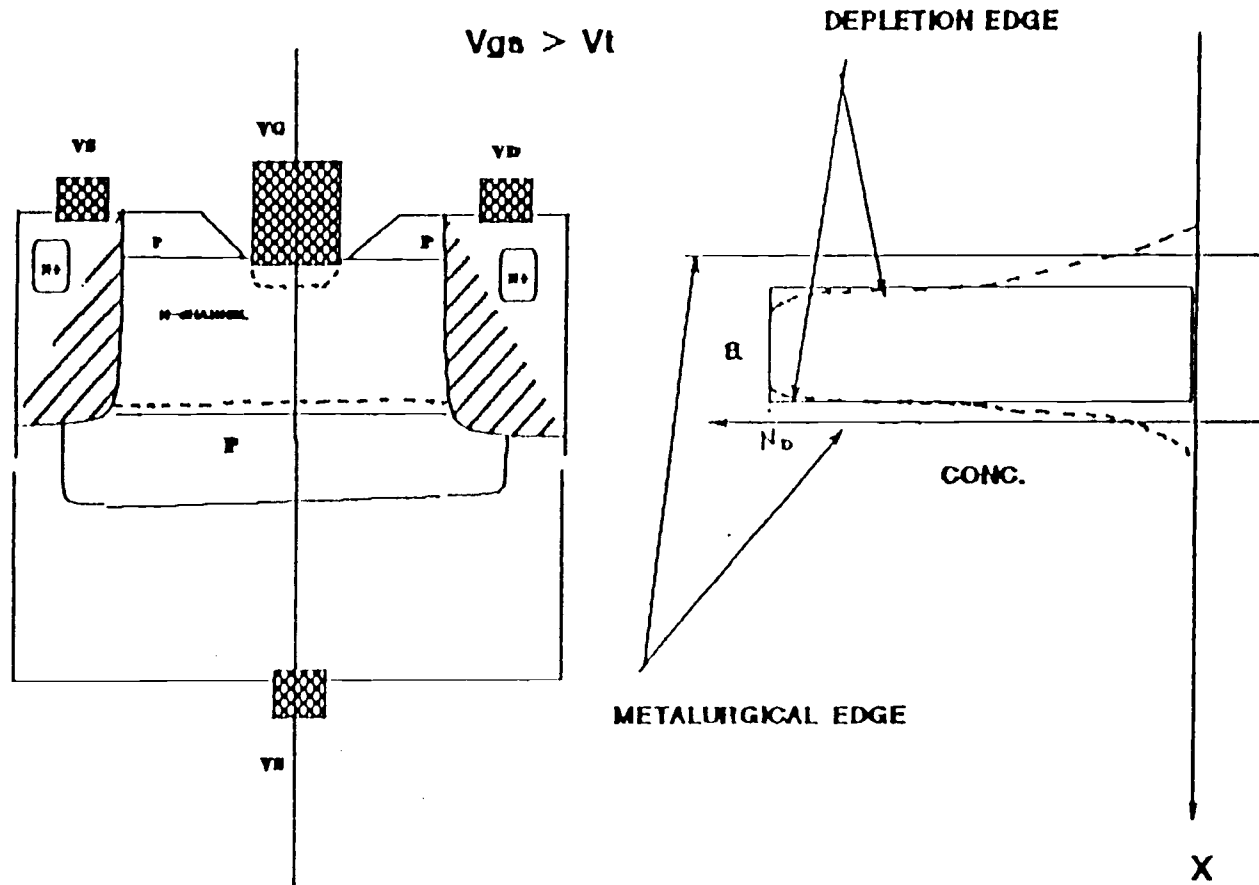


Figure 4. Above Threshold Drain Current Conduction

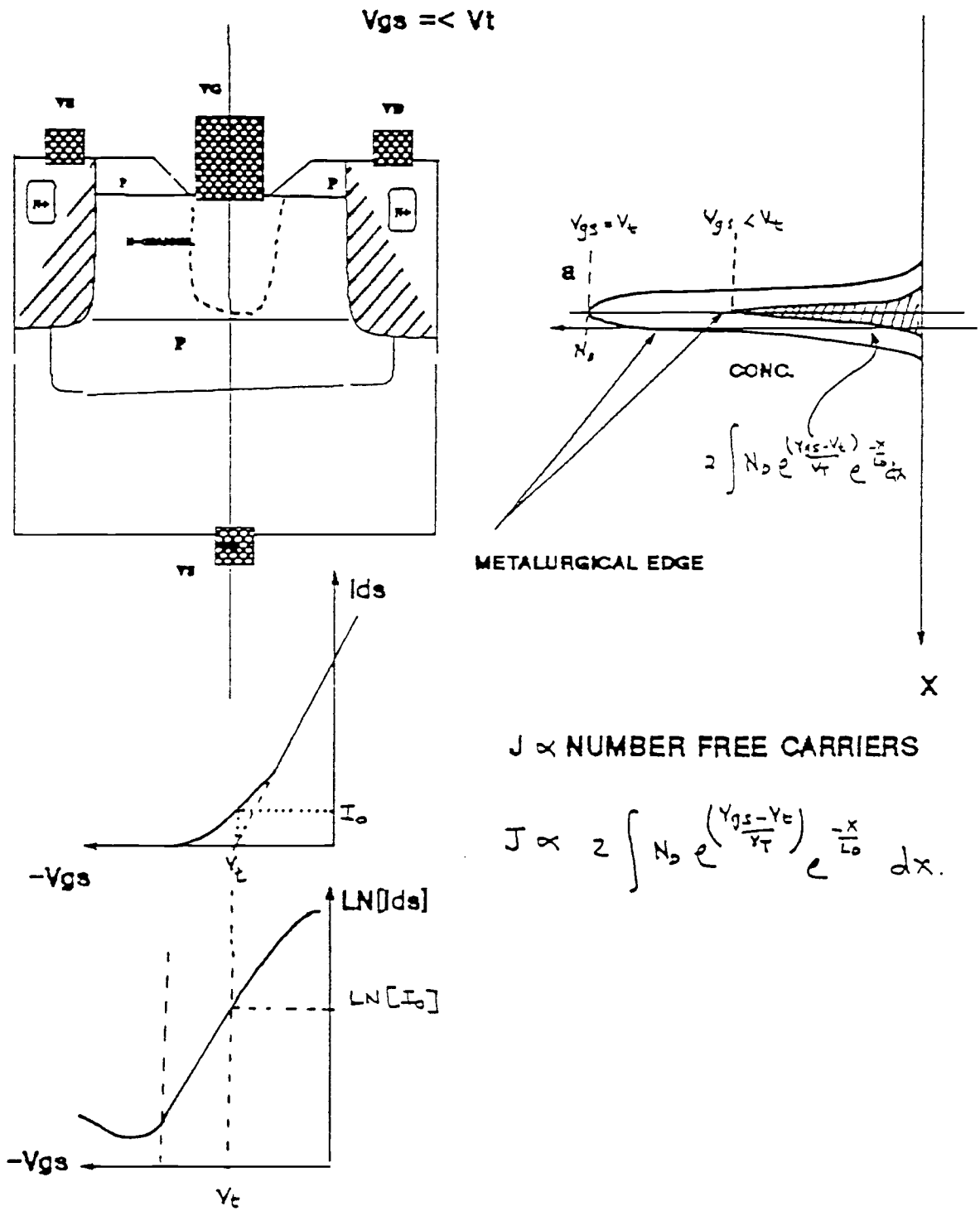


Figure 5. Below Threshold Drain Current Conduction

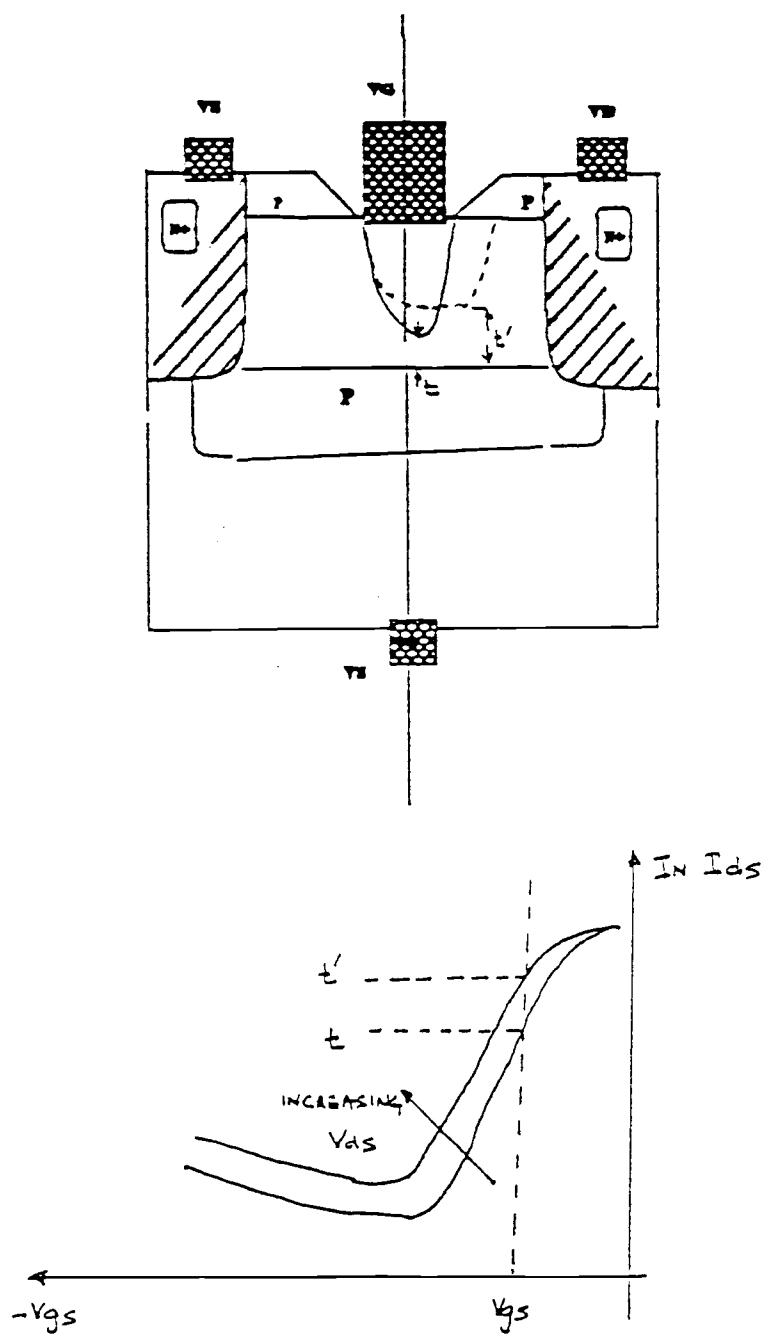


Figure 6. Changes in Channel Thickness Due to V_{DS} change

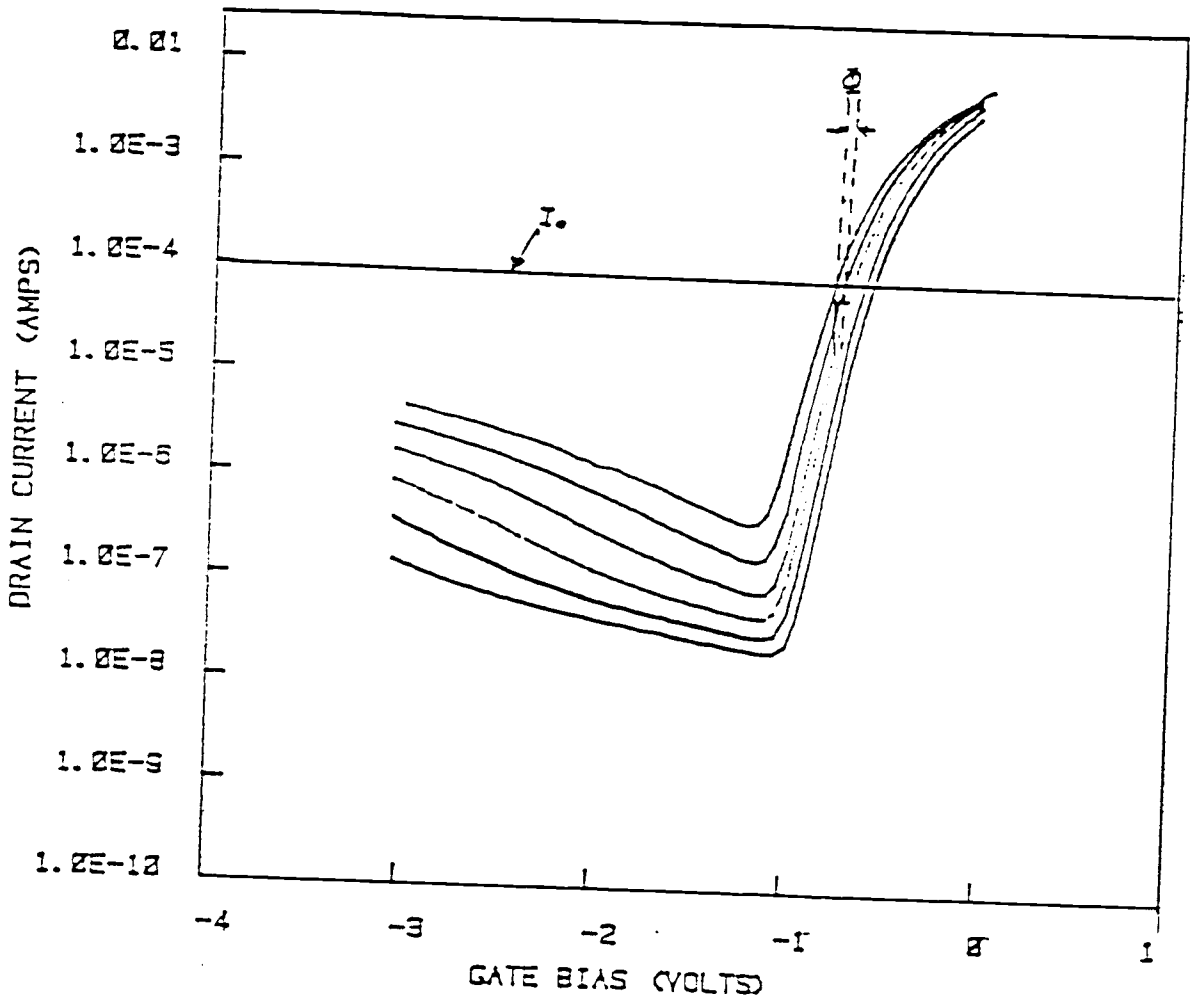


Figure 7. I_0 as defined on Data Plot

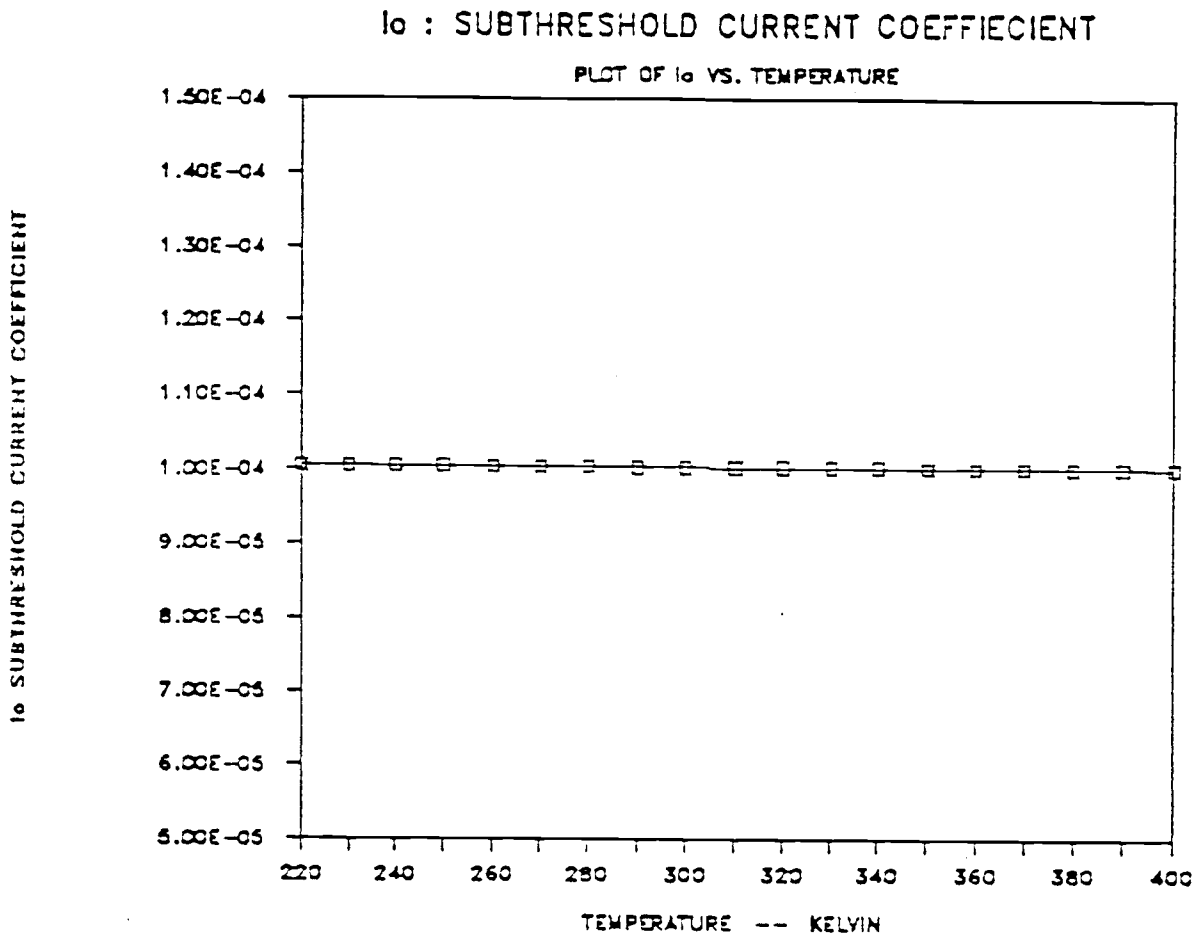


Figure 8. I_0 as expressed by Eqn. (10)

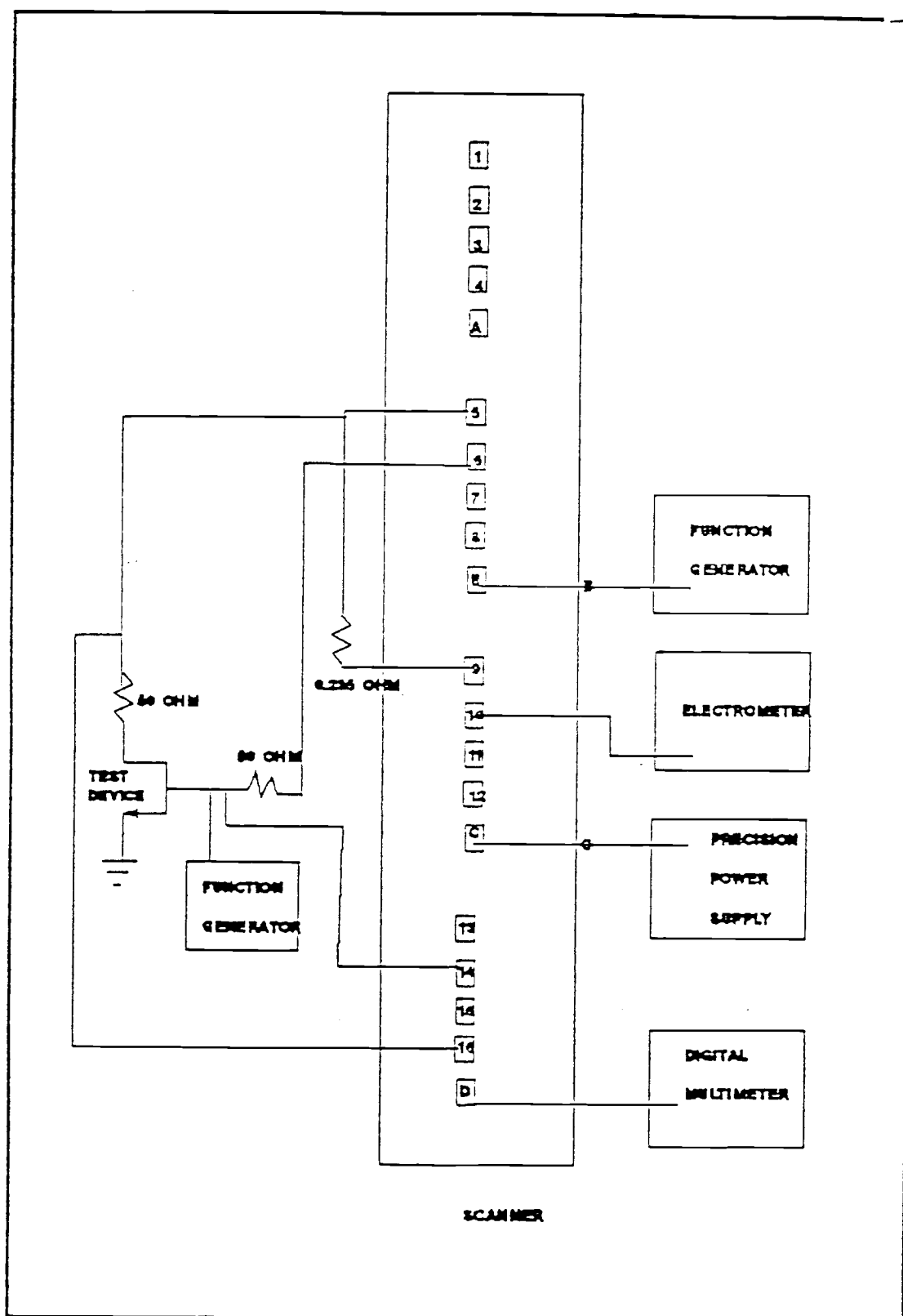


Figure 9. Schematic of Work Station Setup

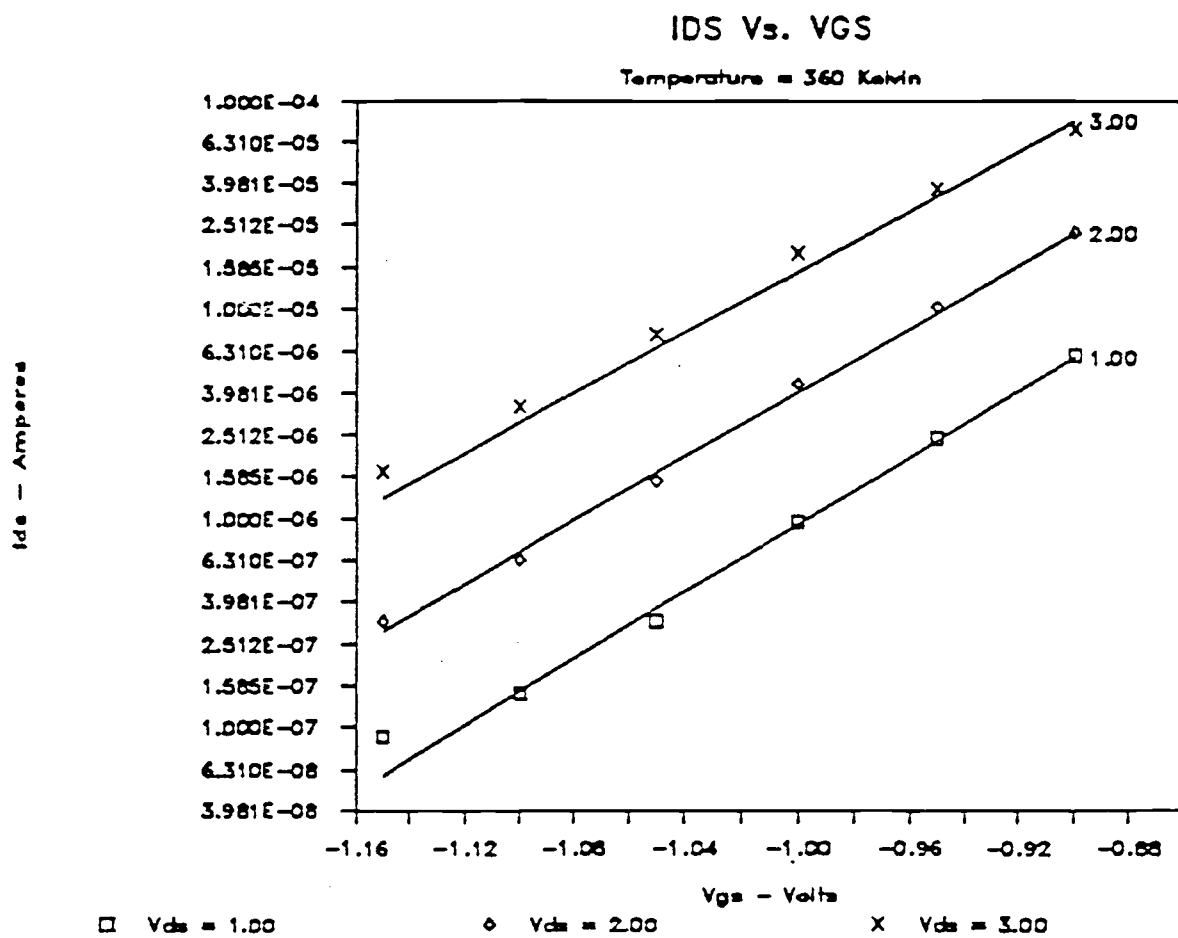


Figure 10a. Theoretical Data and Experimental Data Plots

IDS Vs. VGS

Temperature = 310 Kelm

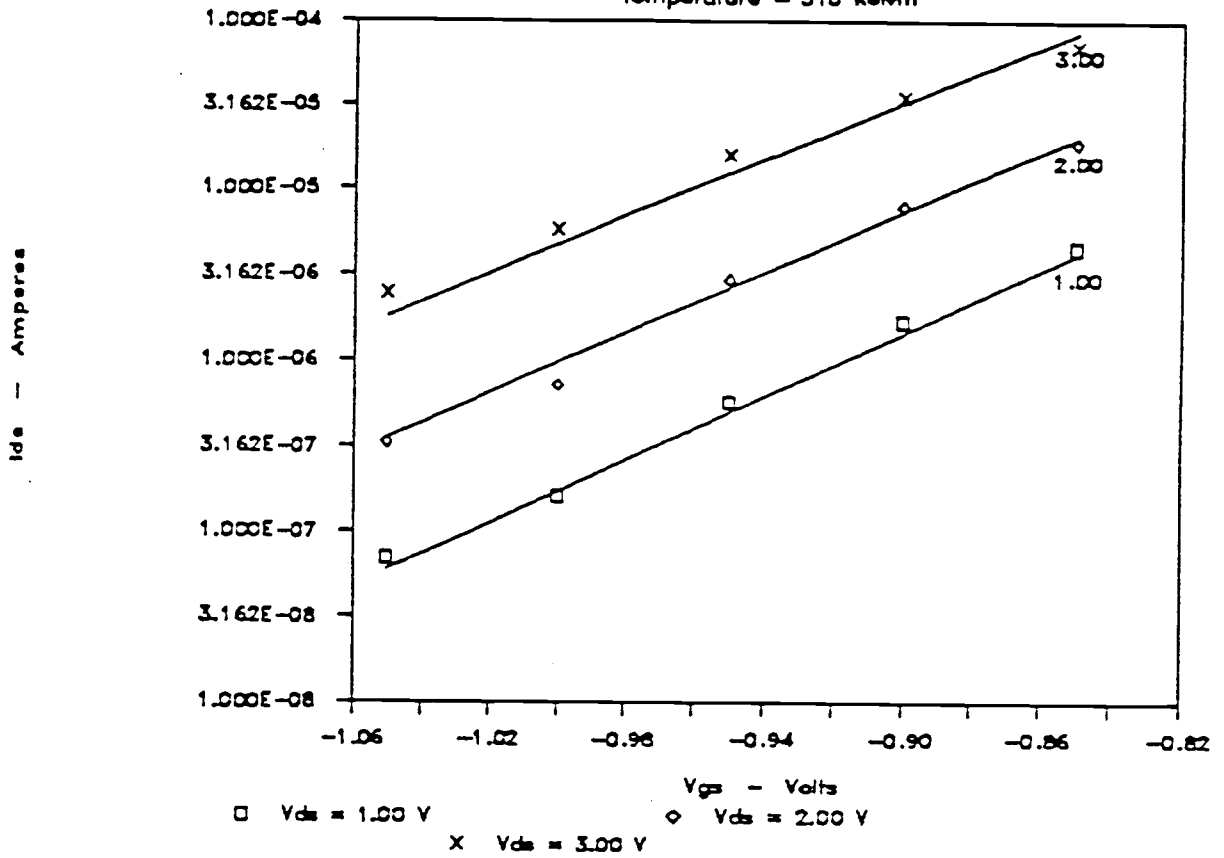


Figure 10b. Theoretical Data and Experimental Data Plots

IDS Vs. VGS

Temperature = 303 Kelvin

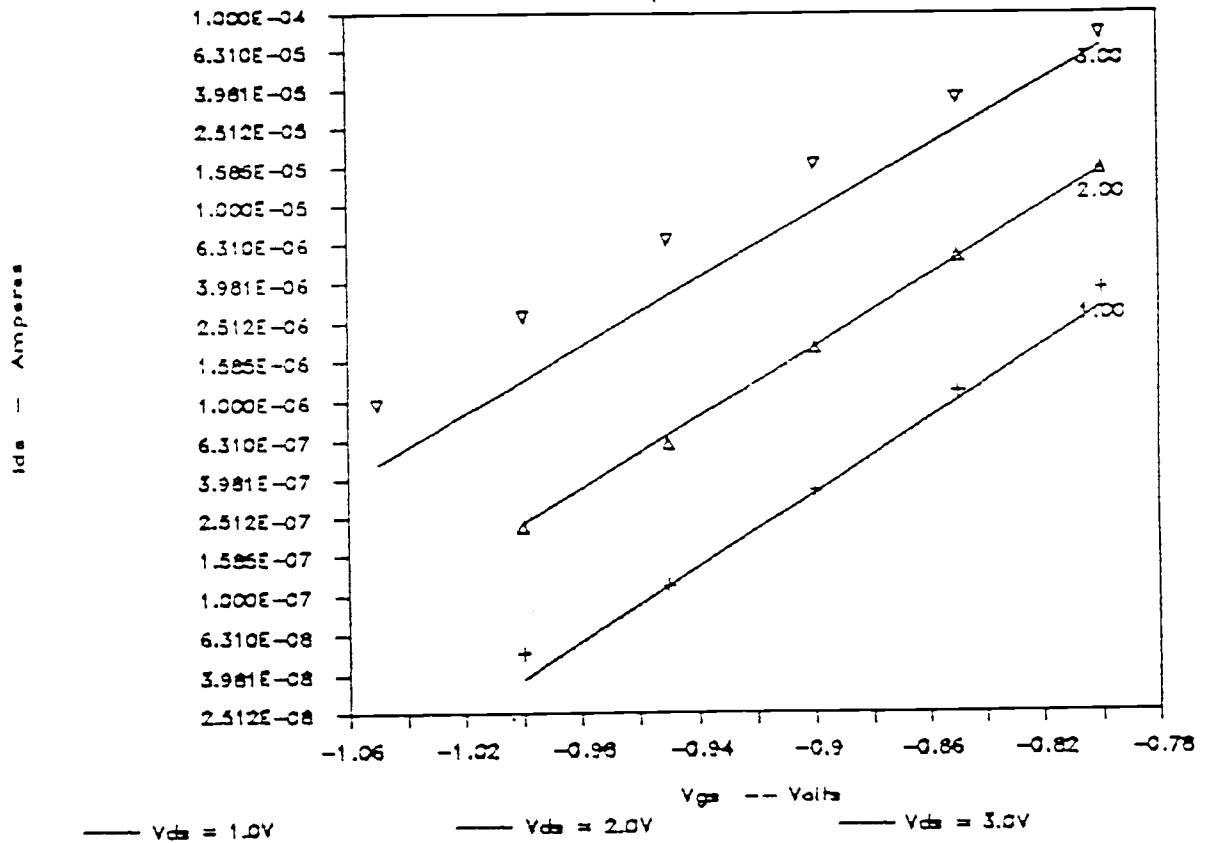


Figure 10c. Theoretical Data and Experimental Data Plots

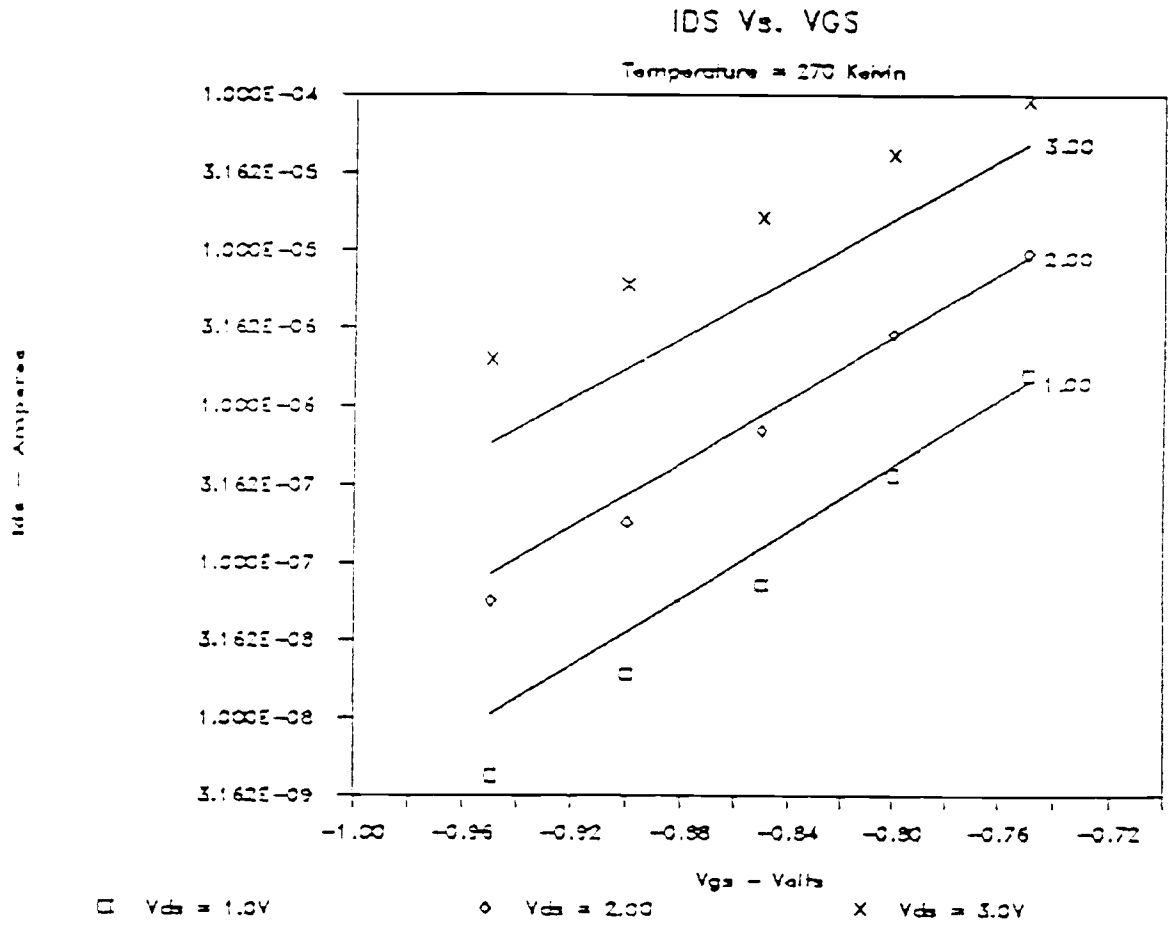


Figure 10d. Theoretical Data and Experimental Data Plots

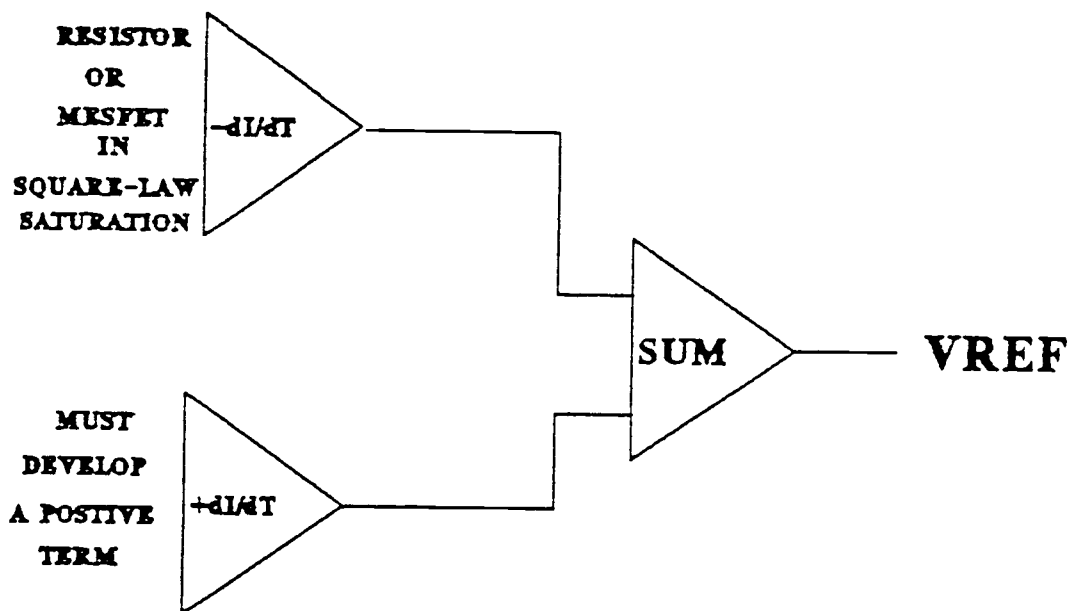


Figure 11. MESFET Voltage Reference Schematic

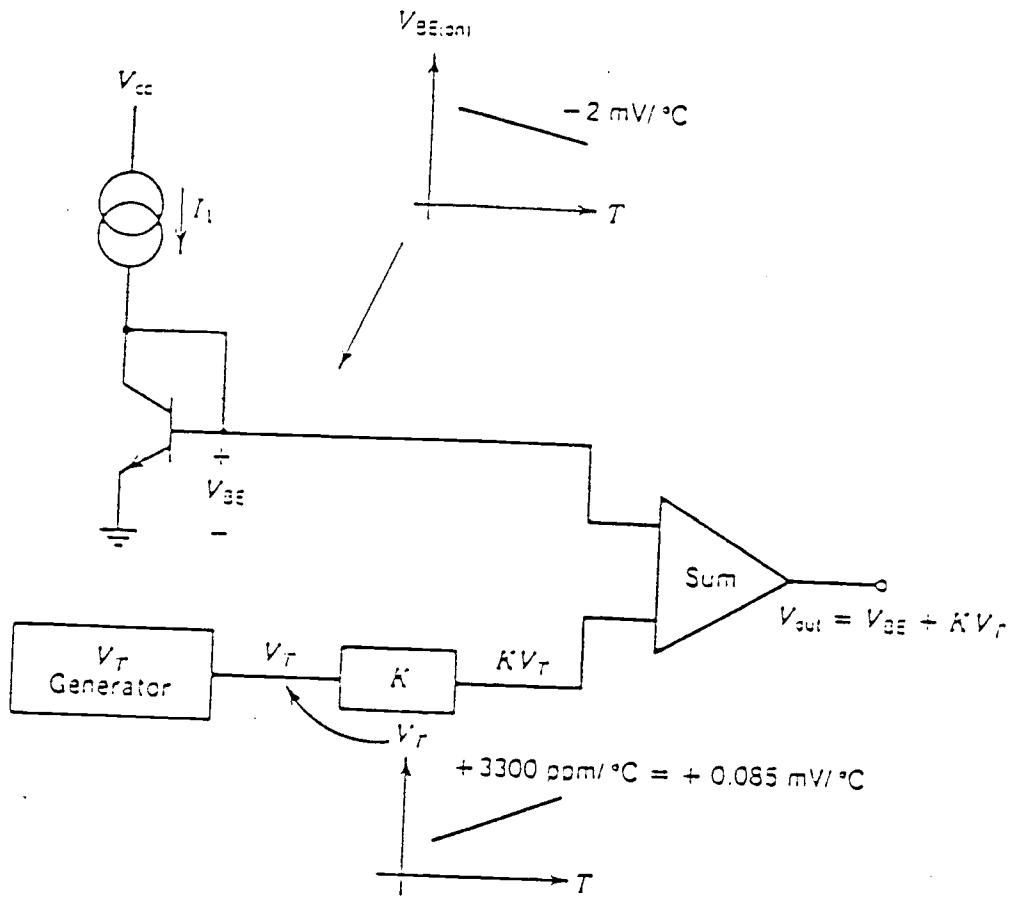


Figure 12. Bipolar Bandgap Voltage Reference Schematic
 [After A. L. Grebene, pp 206-209]

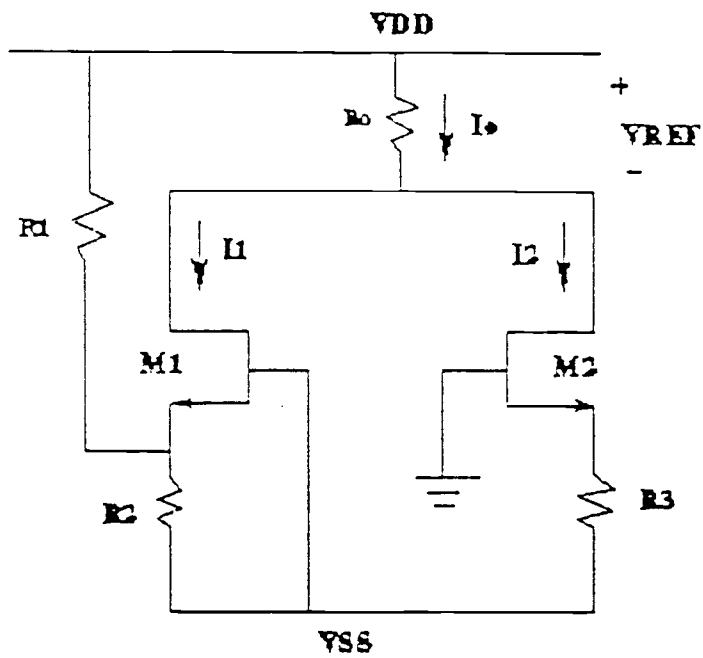
CIRCUIT

Figure 13. Circuit Implementation

VREFSIM

SIMPLE EXAMPLE

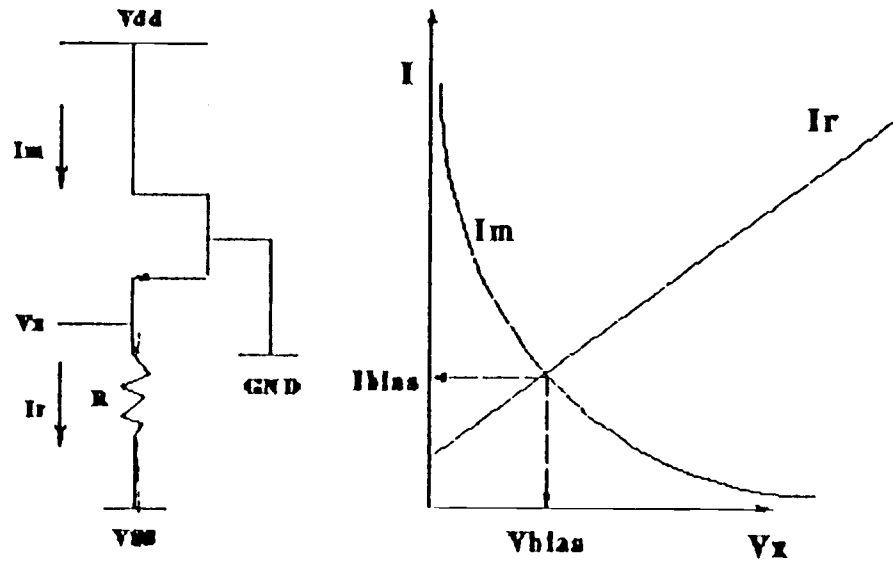


Figure 14. VREFSIM Iteration Technique

Square-Law Scaling by Width

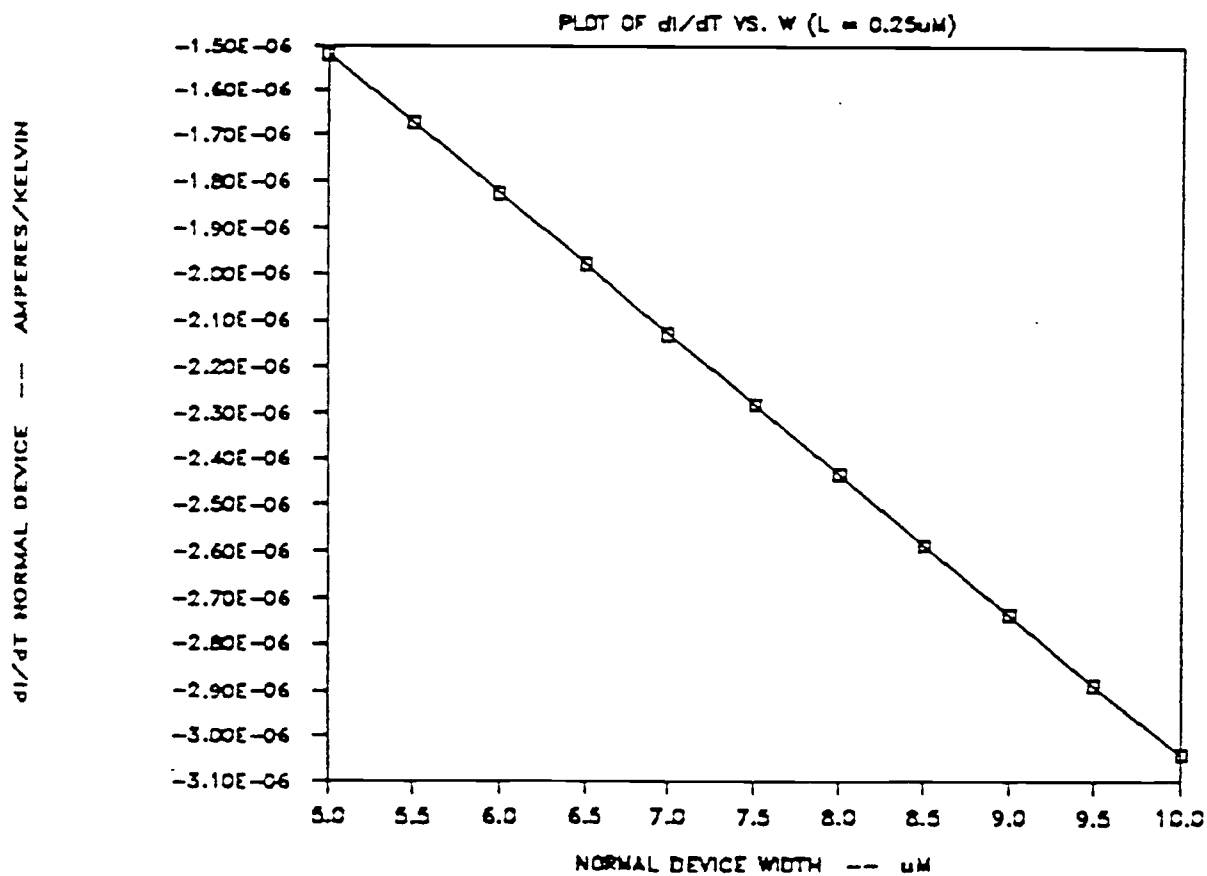


Figure 15. Square-Law Device Design Curve

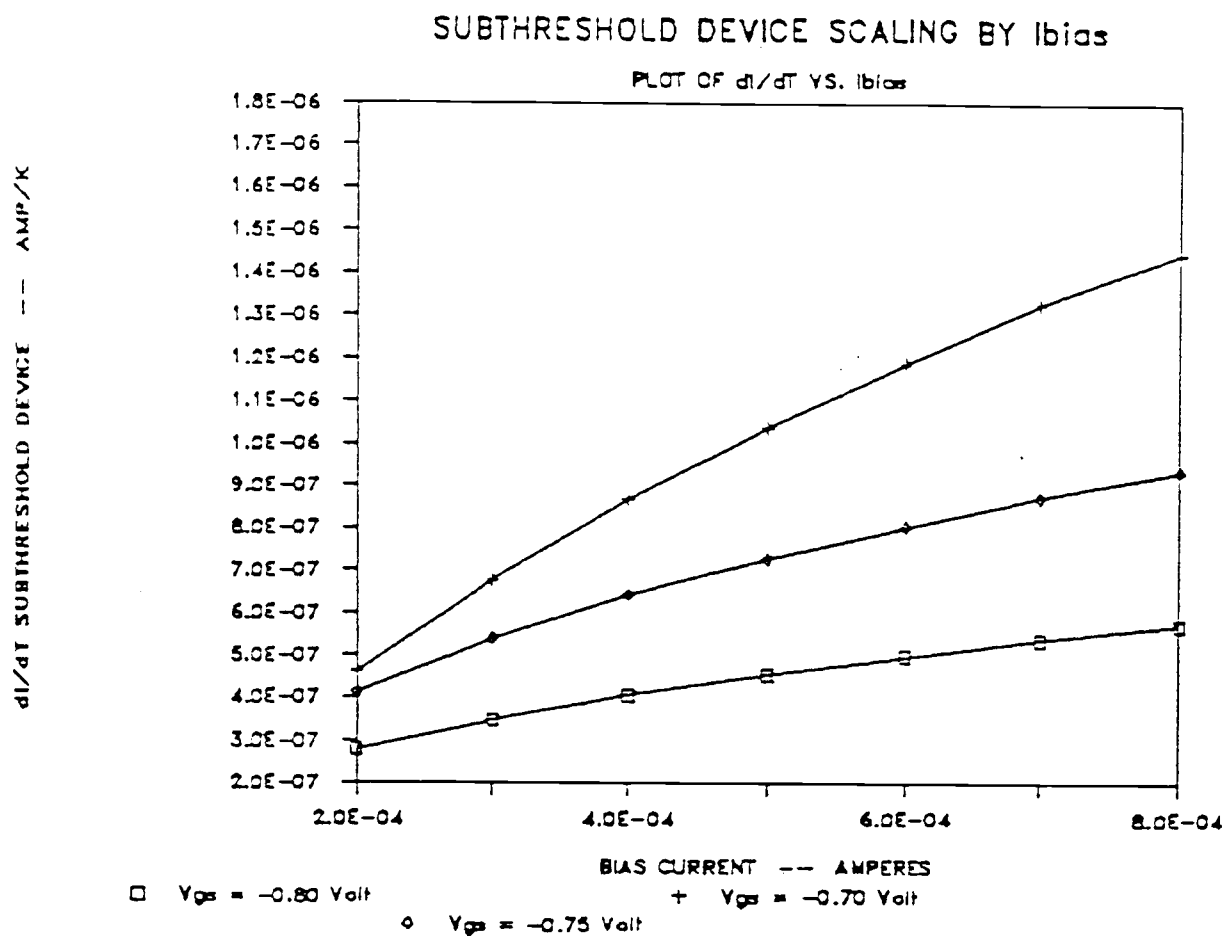


Figure 16. Subthreshold Device Design Curve

dI / dT OF SQUARE-LAW DEVICE

PLT OF I VS. TEMP (W=6.0uM, L=0.25uM)

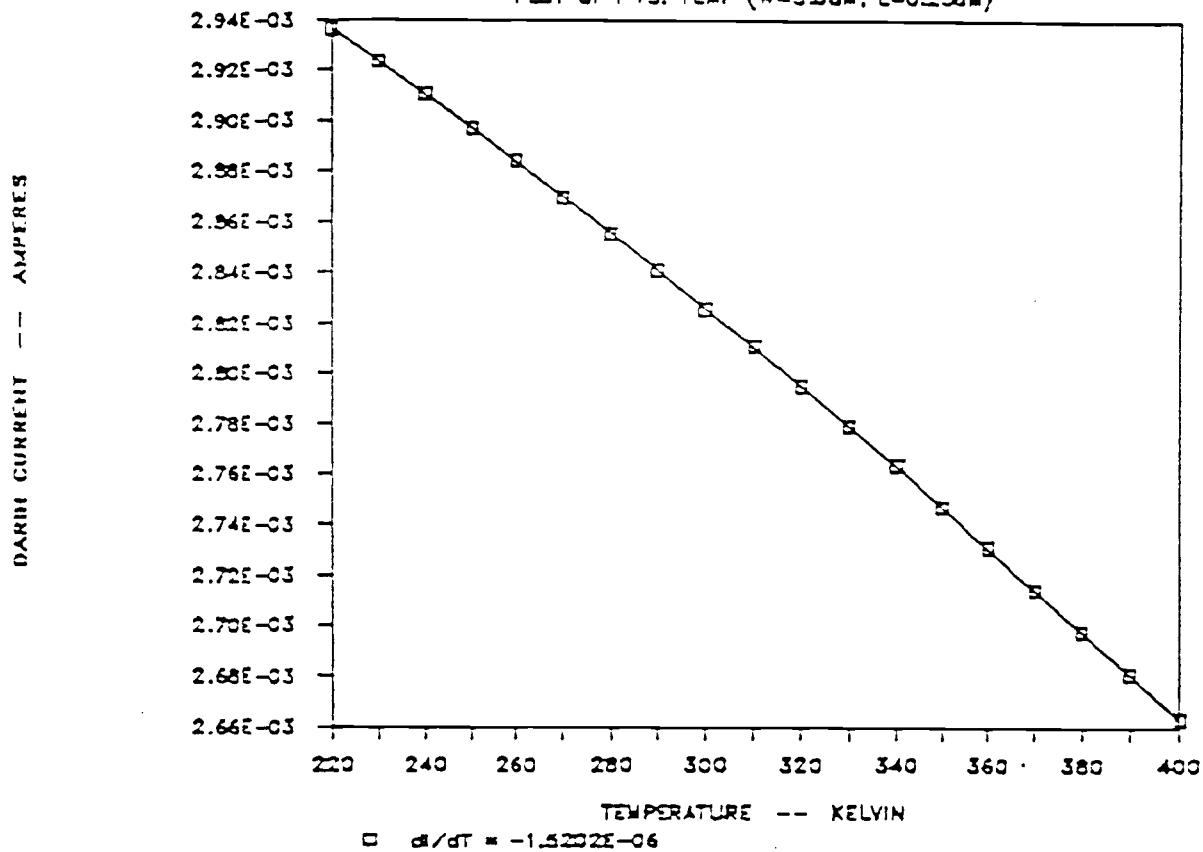


Figure 17. Square-Law Device Negative Temperature Drift Component

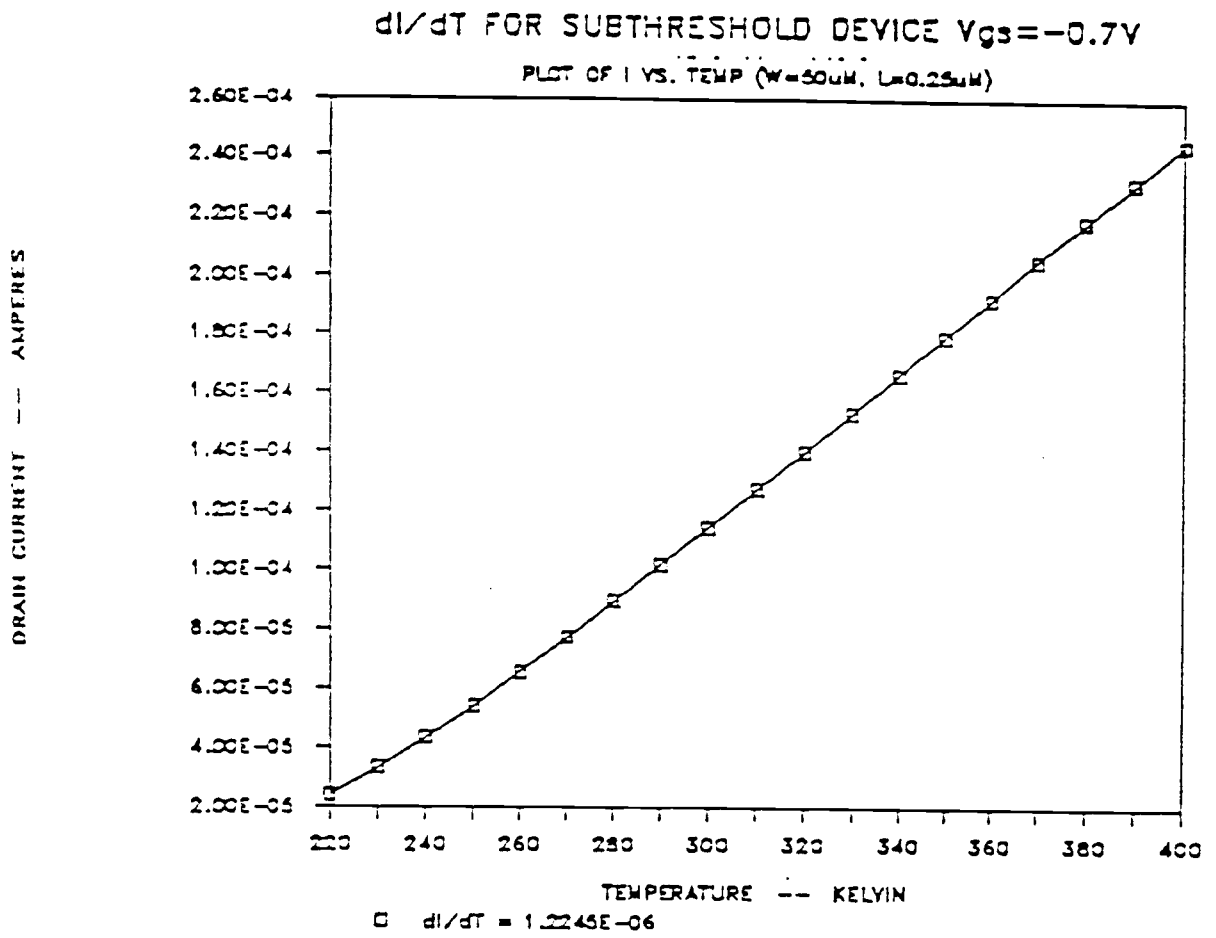


Figure 18. Subthreshold Device Positive Temperature Drift Component

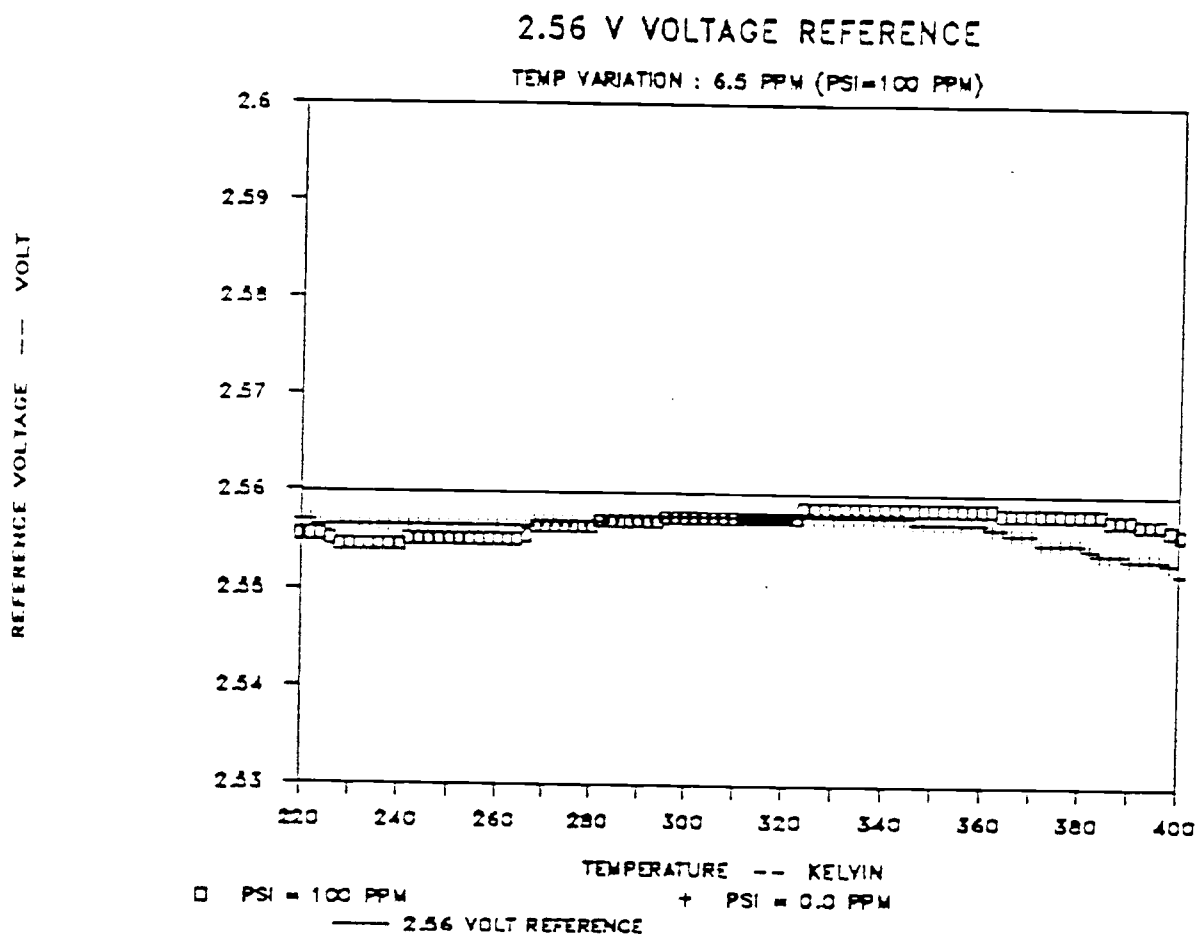


Figure 19. A 2.56 Volt Simulated Output

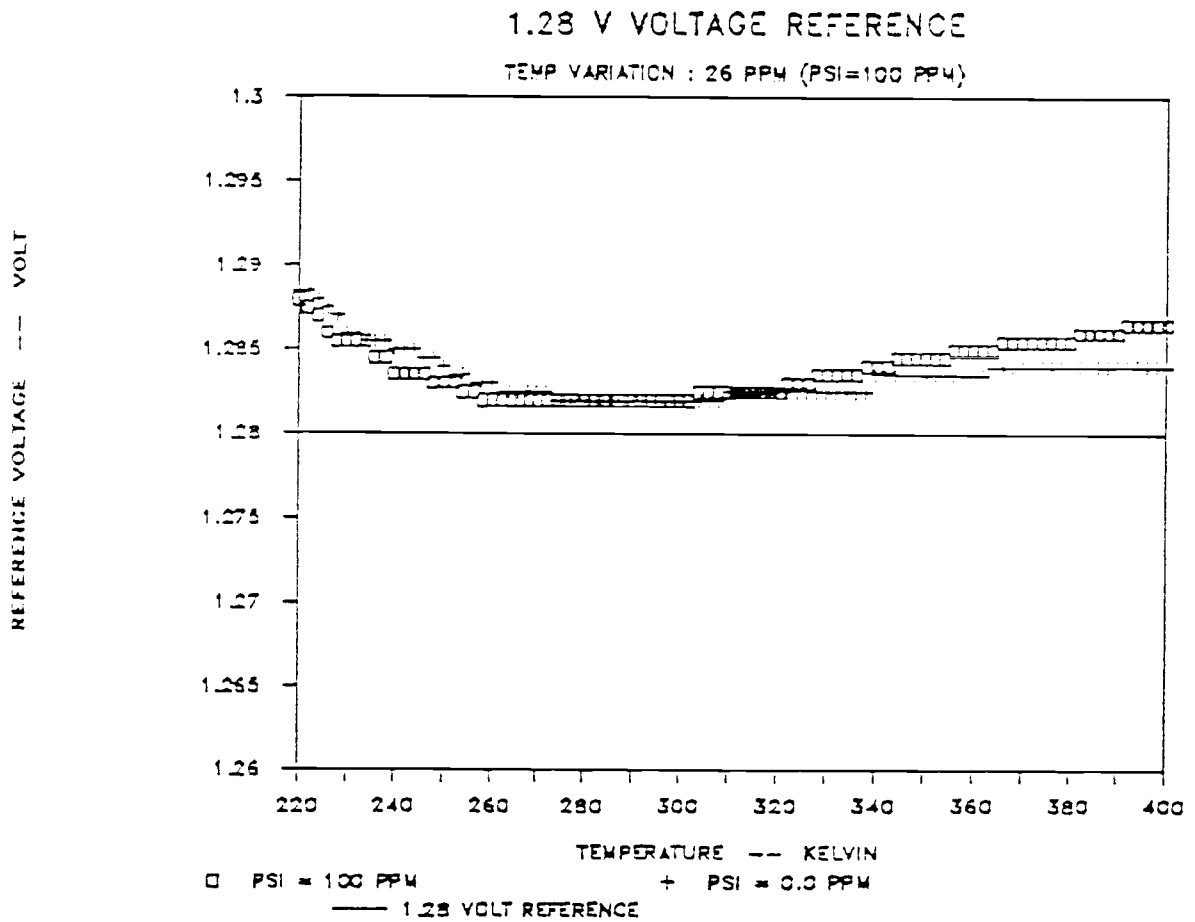
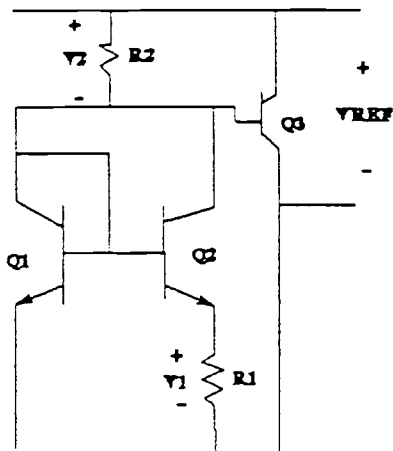


Figure 20. A 1.28 Volt Simulated Output

A. BIPOLAR TECHNOLOGY

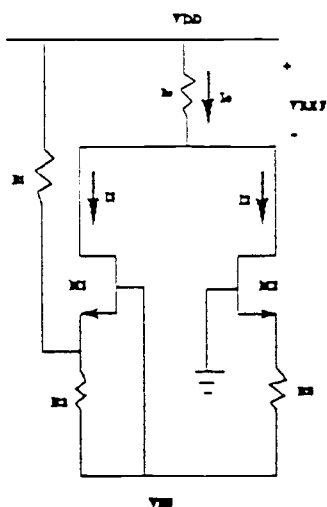


TECHNIQUE : VOLTAGE SUMMATION

PERFORMANCE : FOR TEMP : -66K TO 125K
 VOLTAGE VARIATION = 0.0000036 / KELVIN
 OR 36 PPM / KELVIN

LIMITATIONS : FIXED REFERENCE AT 1.14V
 NEED AMPLIFICATION CIRCUITRY,
 DEGRADE PERFORMANCE
 VOLTAGE DIVISION ON EXTERNAL RESISTOR STRING

B. MESFET TECHNOLOGY



TECHNIQUE : CURRENT SUMMATION

PERFORMANCE : FOR TEMP = -66K TO 125K
 VOLTAGE VARIATION = 0.0000065 / KELVIN
 OR 6.5 PPM / KELVIN
 AT 2.56 VOLTS

ADVANTAGES : VREF CAN BE CHOSEN WITHOUT
 ANY ADDITIONAL COMPONENT COST
 BUILT-IN AMPLIFICATION
 INTERNAL VOLTAGE DIVISION - SAVE CHIP SPACE

Figure 21. Bipolar Versus MESFET Technology

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APPENDICES

7. APPENDICES

7.1 Equation Derivations

7.1.1 Equation (20a)

The Curtice model was used to implement the square-law device in saturation region. From Equation (21),

$$I_{ds} = \beta (V_{gs} - V_t)^2 (1 + \alpha V_{ds}) \tanh(\sigma V_{ds}). \quad (20.0)$$

From Equation (16),

$$\beta = \left(\frac{2 W U_c \epsilon_s 292^2}{3 L t T^2} \right) \quad (20.1)$$

The mobility, U_c , as expressed in Equation (24) is inserted into the above equation. Beta is expressed as,

$$\beta = \left(\frac{2 U_{300} * T_{300} \epsilon_s 292^2}{3 T t T^2} \right) = \frac{A}{T^3}, \quad (20.2)$$

where,

$$A = \left(\frac{2 U_{300} * T_{300} \epsilon_s 292^2}{3 t} \right). \quad (20.3)$$

The threshold voltage is :

$$V_t = V_{to} - \Phi V_{ds}, \quad (20.4)$$

and from Equation (13),

$$V_{to} = V_{bi} - V_p. \quad (20.5)$$

Equation (15) gives V_p as:

$$V_p = \frac{qN_c t}{2 \epsilon_s} \frac{T}{292}. \quad (20.6)$$

Combining Equation (20.4), (20.5), and (20.6) :

$$\begin{aligned}
 V_t &= V_{bi} - V_p - \Phi V_{ds} \\
 &= kT/q \cdot \ln(N_c/n_i) - (qN_c t^2 / 2 \epsilon_s) (T/292) - \Phi V_{ds} \\
 &= T[(k/q \cdot \ln(N_c/n_i) - (qN_c t^2 / 2 \epsilon_s 292))] - \Phi V_{ds} \\
 &= BT - \Phi V_{ds}, \tag{20.7}
 \end{aligned}$$

where,

$$B = T[(k/q \cdot \ln(N_c/n_i) - (qN_c t^2 / 2 \epsilon_s 292))]. \tag{20.8}$$

Finally, inserting Equation (20.7) :

$$\begin{aligned}
 (V_{gs} - V_t)^2 &= (V_{gs} - BT + \Phi V_{ds}) \\
 &= (C - BT), \tag{20.9}
 \end{aligned}$$

where,

$$C = (V_{gs} - \Phi V_{ds}) \tag{20.10}$$

$$(1 + \alpha V_{ds}) \tanh(\sigma V_{ds}) = D \tag{20.11}$$

Expressing Equation (21) in terms of the temperature independent variables A, B, and C we have,

$$I_{ds} = (A/T^3)(C - BT)^2 D. \tag{20a}$$

7.1.2 Equation (23a)

For the subthreshold device, the current model is :

$$I_{dsub} = I_o \exp[(q/kTN_s)(1 - \Gamma V_{ds})(V_{gs} - V_{to} + \Phi V_{ds})] \tag{23.0}$$

The exponential term is expressed as,

$$(q/kTN_s)(1 - \Gamma V_{ds}) = A/T, \tag{23.1}$$

and,

$$(V_{gs} - V_{to} + \Phi V_{ds}) = (B - V_{to}). \tag{23.2}$$

Where,

$$A = (q/kN_s)(1 - \Gamma V_{ds}), \tag{23.3}$$

$$B = (V_{gs} + \Phi V_{ds}). \tag{23.4}$$

Inserting Equations (14) and (15) into V_{to} , we have an explicit temperature term:

$$V_{to} = T(k/q \ln[N_c/n_i] + qN_c t^2 / 584 \epsilon_s). \quad (23.5)$$

Letting the term in Equation (23.5) equal C , Equation (23.0) is expressed in terms of the temperature independent variables A , B , and C as,

$$I_{dsub} = I_o \text{Exp}[A/T*(B - CT)]. \quad (23.6)$$

Finally, rearranging the exponential terms in Equation (23.6) :

$$I_{dsub} = I_o \text{Exp}[-AB] \text{Exp}[AC/T] \quad (23a)$$

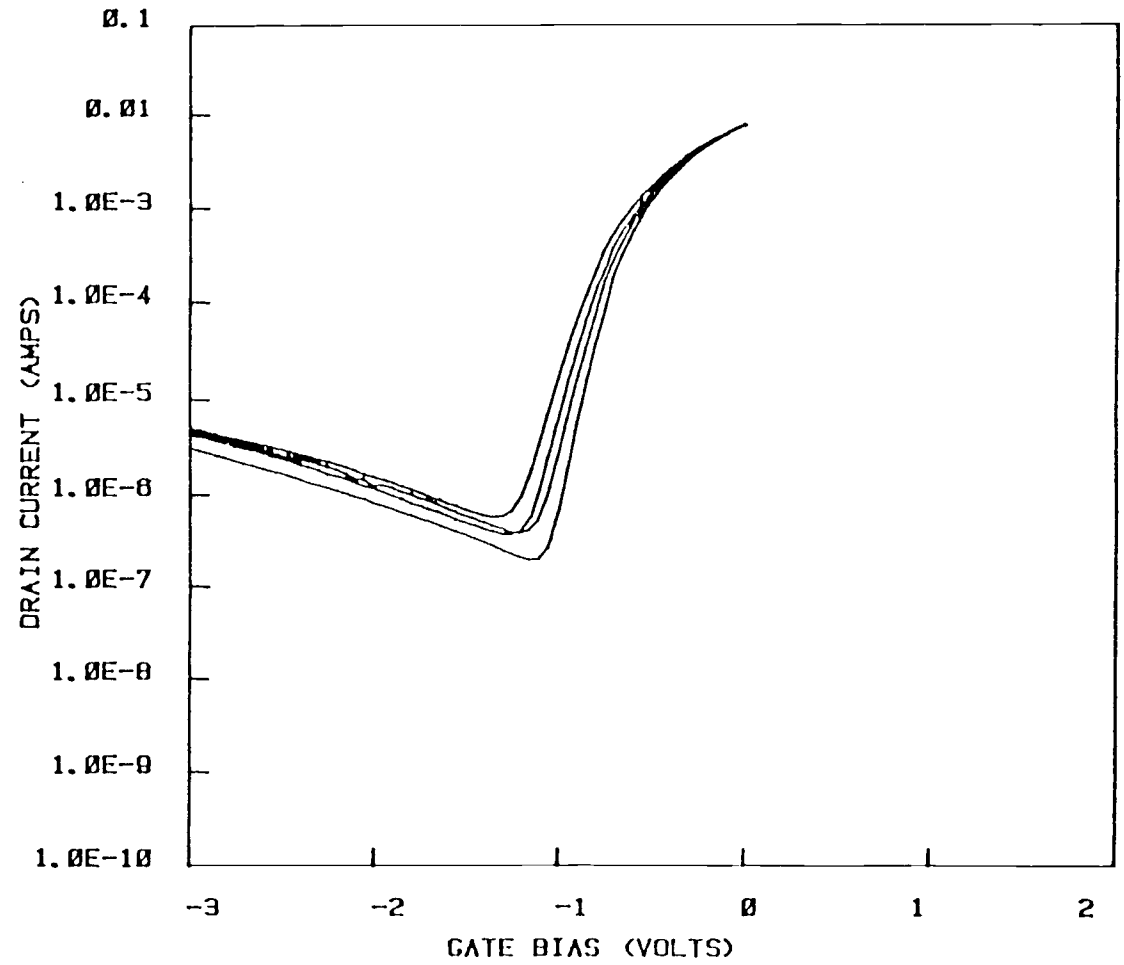
7.2 List of Equipment

The work station consists of a Tektronix 4054A computer, Keithley 192 electrometer, two Tektronix PS 5004 programmable precision power supply, a Tektronix FG 5010 Programmable 20MHz Function Generator, a Tektronix DM 5010 Programmable Digital Multimeter, a Tektronix SI 5010 Programmer Scanner, a Air Product Temperature controller, and a Helium closed cycle refrigeration unit. Figure 9 shows the experimental work station set up in the laboratory.

8-11-1987
G558A-D8 33400 PKG. #2
LG=0.25u, Z=50u, 1010A
BURIED CHANNEL

VDS= 3 VOLTS

TEMP (K)	TAPE&FILE (T, F)
.380	(4, 2)
.310	(4, 3)
300	(4, 1)
270	(4, 8)

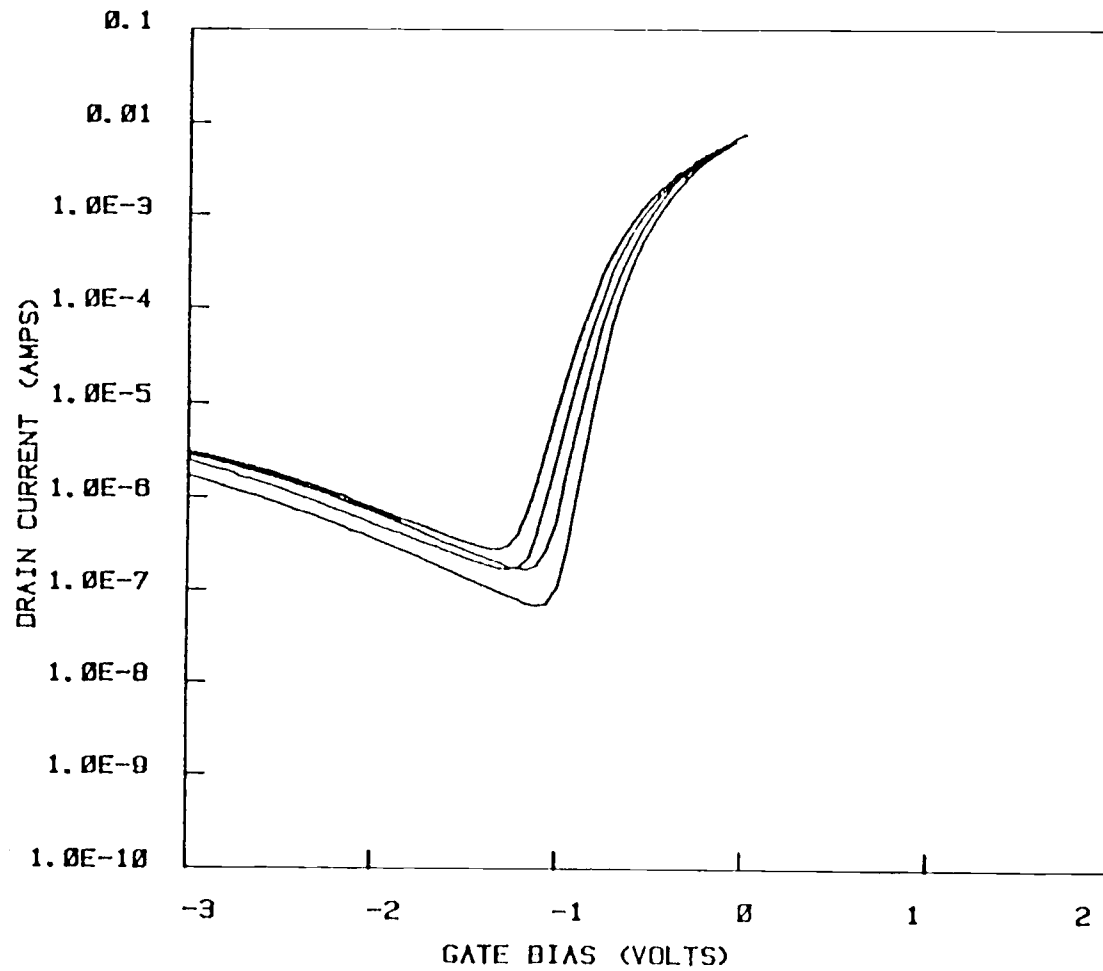


7.3 List of Experimental data

8-11-1007
G550A-00 33400 PKG. #2
LG=0.25u, Z=50u, 1010A
BURIED CHANNEL

VDS= 2.5 VOLTS

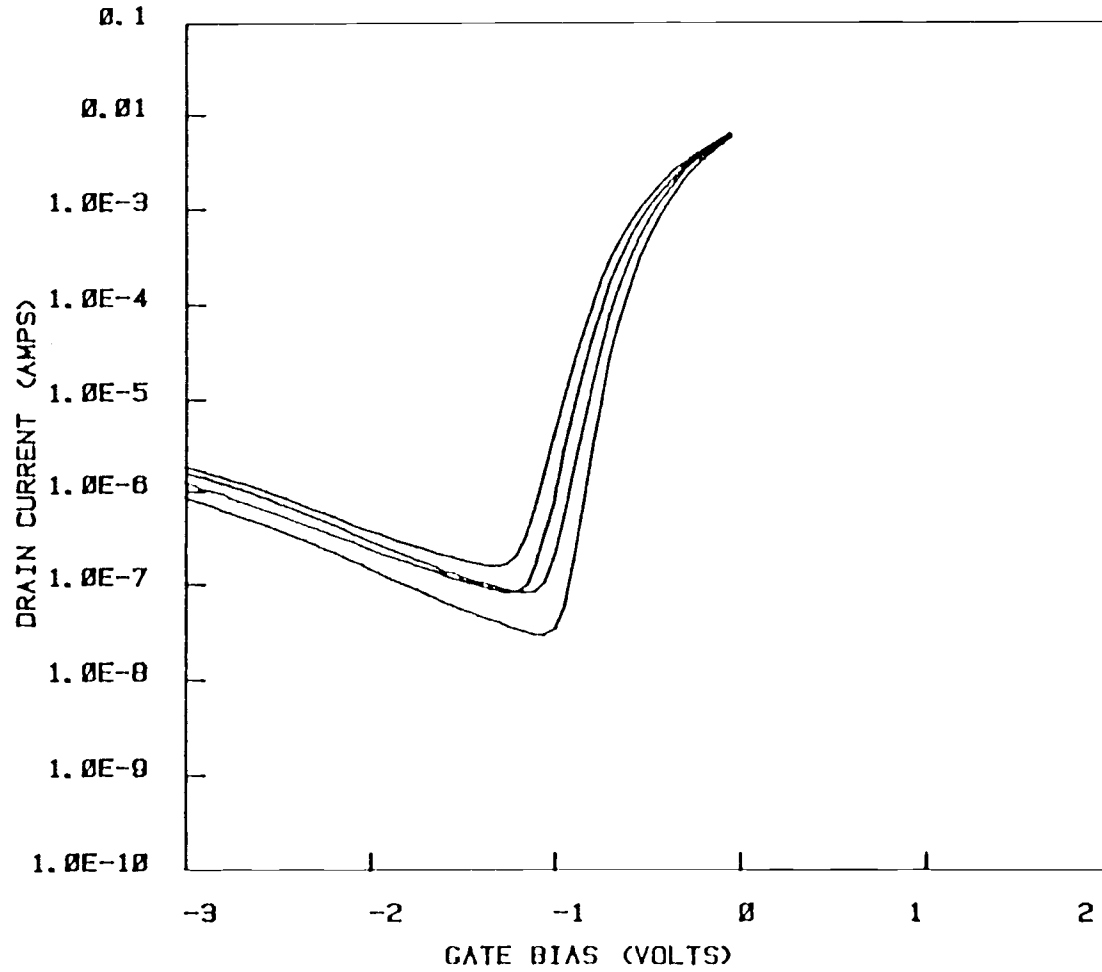
TEMP (K)	TAPE&FILE (T, F)
360	(4, 2)
310	(4, 3)
300	(4, 1)
270	(4, 8)



8-11-1987
G558A-D8 39400 PKG. #2
LG=0.25u, Z=50u, 1010A
BURIED CHANNEL

VDS= 2 VOLTS

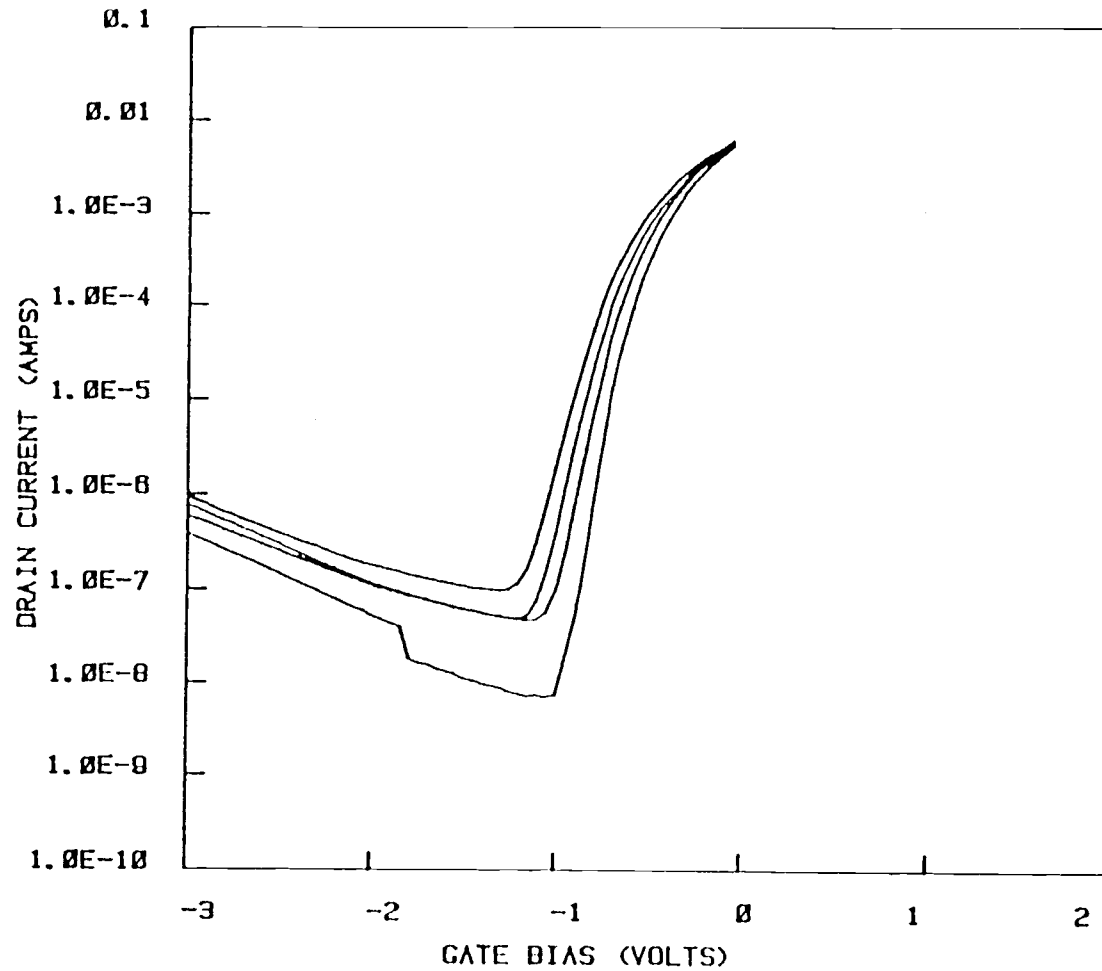
TEMP (K)	TAPE&FILE (T, F)
360	(4, 2)
310	(4, 3)
300	(4, 1)
270	(4, 8)



8-11-1987
G550A-D0 33400 PKG. #2
LG=0.25u, Z=50u, 1010A
BURIED CHANNEL

VDS= 1.5 VOLTS

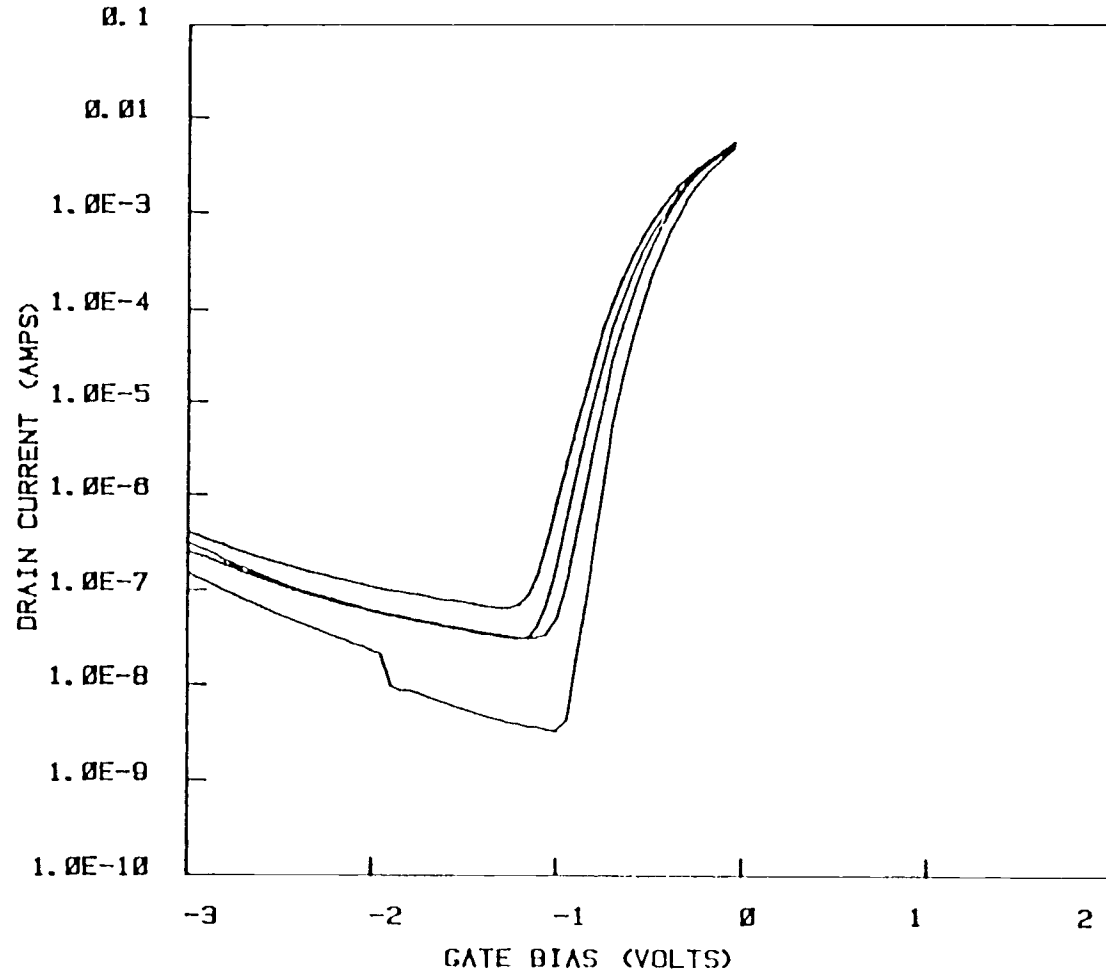
TEMP (K)	TAPE&FILE (T, F)
360	(4, 2)
310	(4, 3)
300	(4, 1)
270	(4, 8)



8-11-1987
C550A-D8 33400 PKG. #2
LG=0.25u, Z=50u, 1010A
BURIED CHANNEL

VDS= 1 VOLTS

TEMP (K)	TAPE&FILE (T, F)
300	(4, 2)
310	(4, 3)
300	(4, 1)
270	(4, 8)



8-11-1987

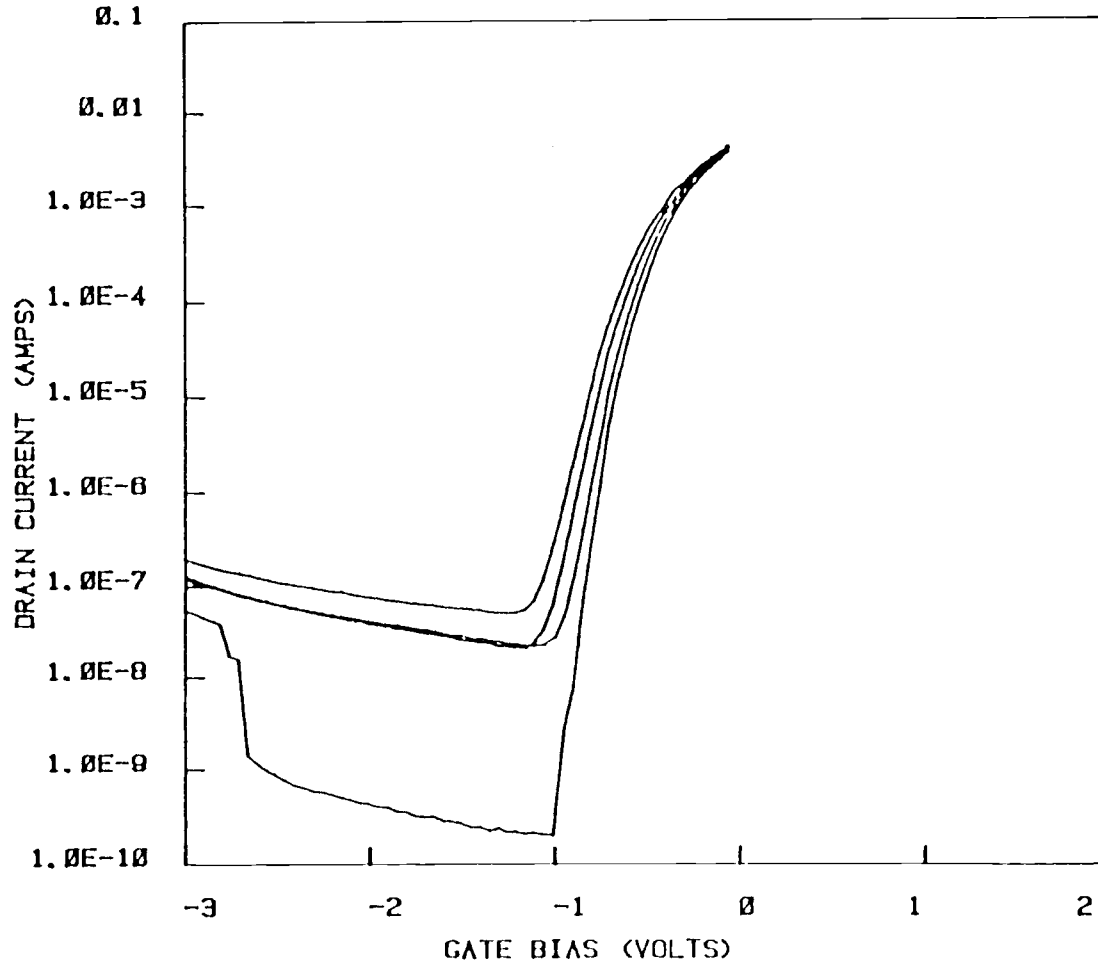
VDS= 0.5 VOLTS

G550A-D8 33400 PKG. #2

LG=0.25u, Z=50u, 1010A

BURIED CHANNEL

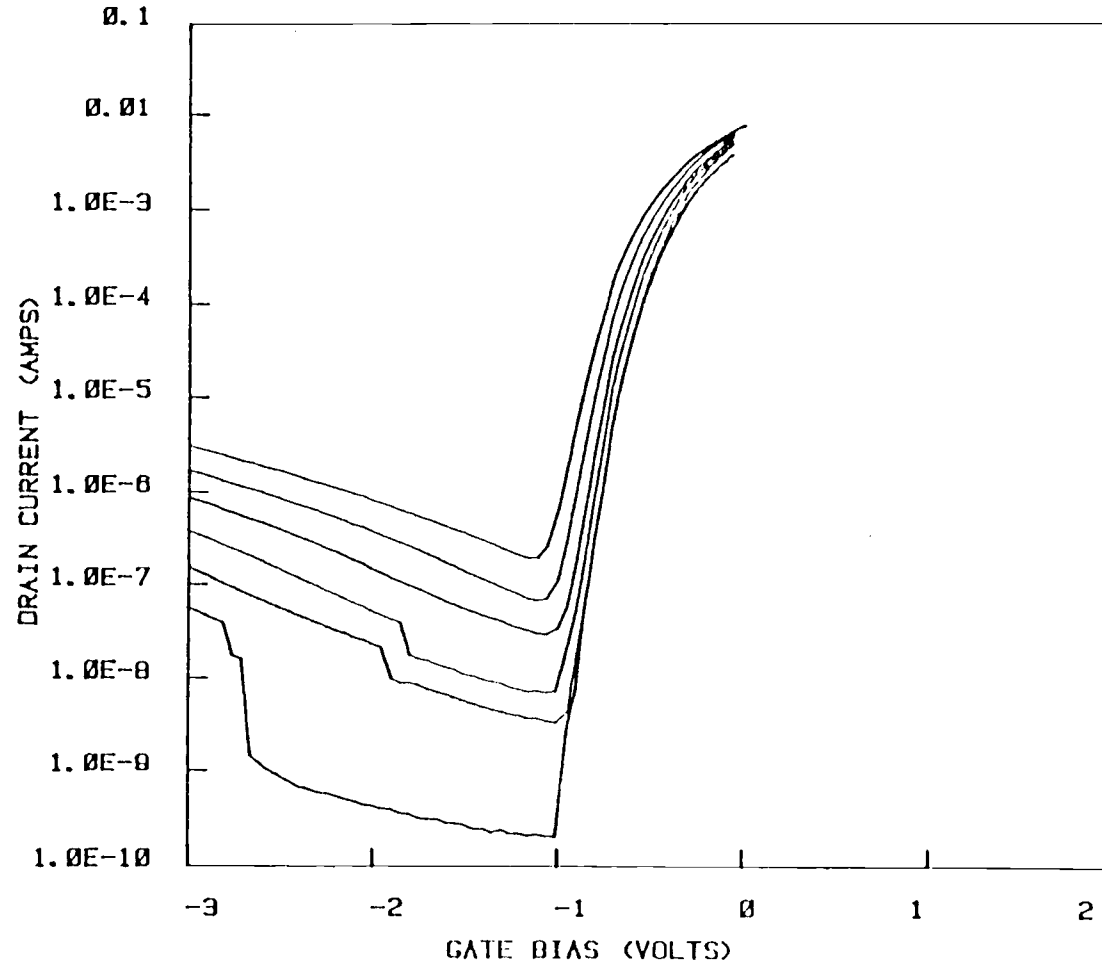
TEMP (K)	TAPE&FILE (T, F)
360	(4, 2)
310	(4, 3)
300	(4, 1)
270	(4, 8)



8-14-1987
G558A-D8 33400 PKG. #2
LG=0.25 μ , Z=50 μ , 1010A
BURIED CHANNEL

TEMP= 270 K

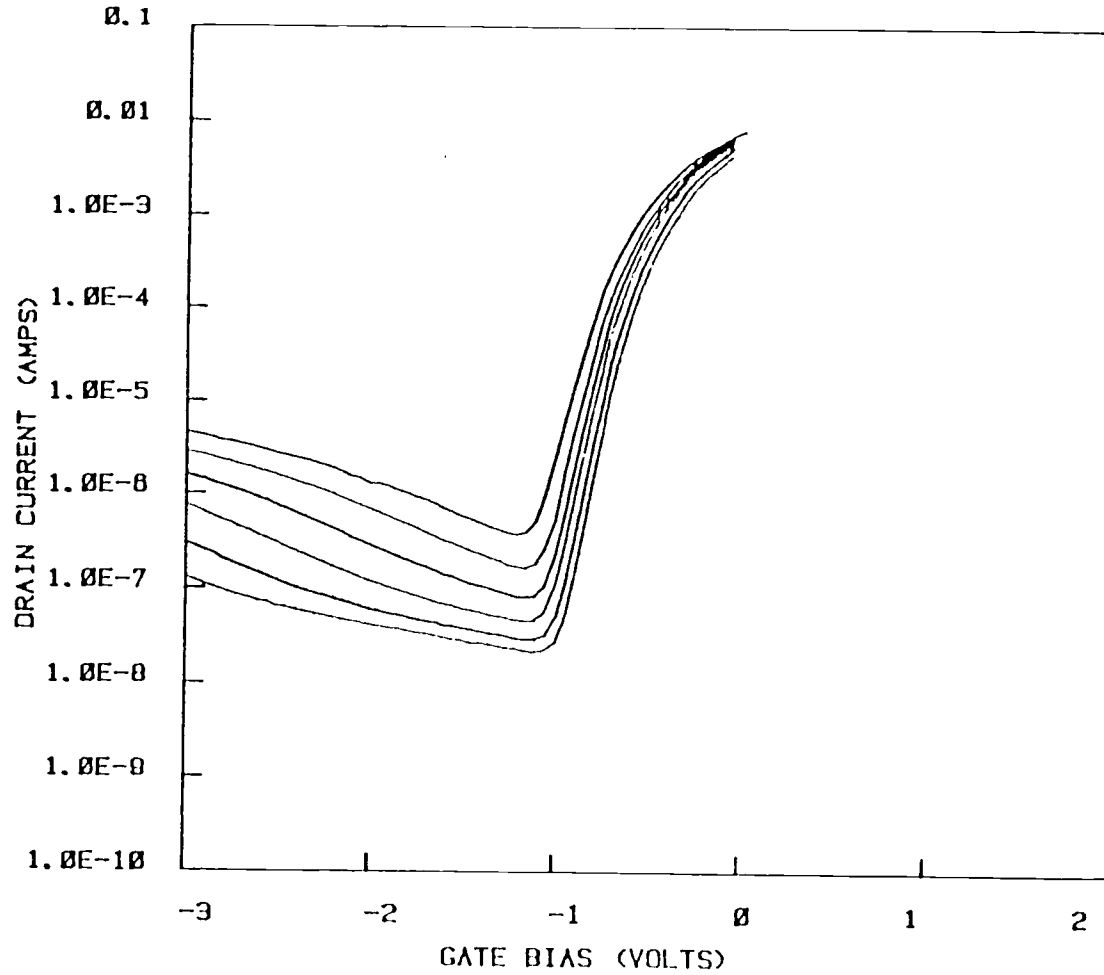
VDS (VOLTS)	TAPE&FILE (T, F)
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1	(4, 8)
1.5	(4, 6)
2	(4, 8)
2.5	(4, 6)
3	(4, 6)



8-11-1987
G558A-08 33400 PKG. #2
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BURIED CHANNEL

TEMP= 300 K

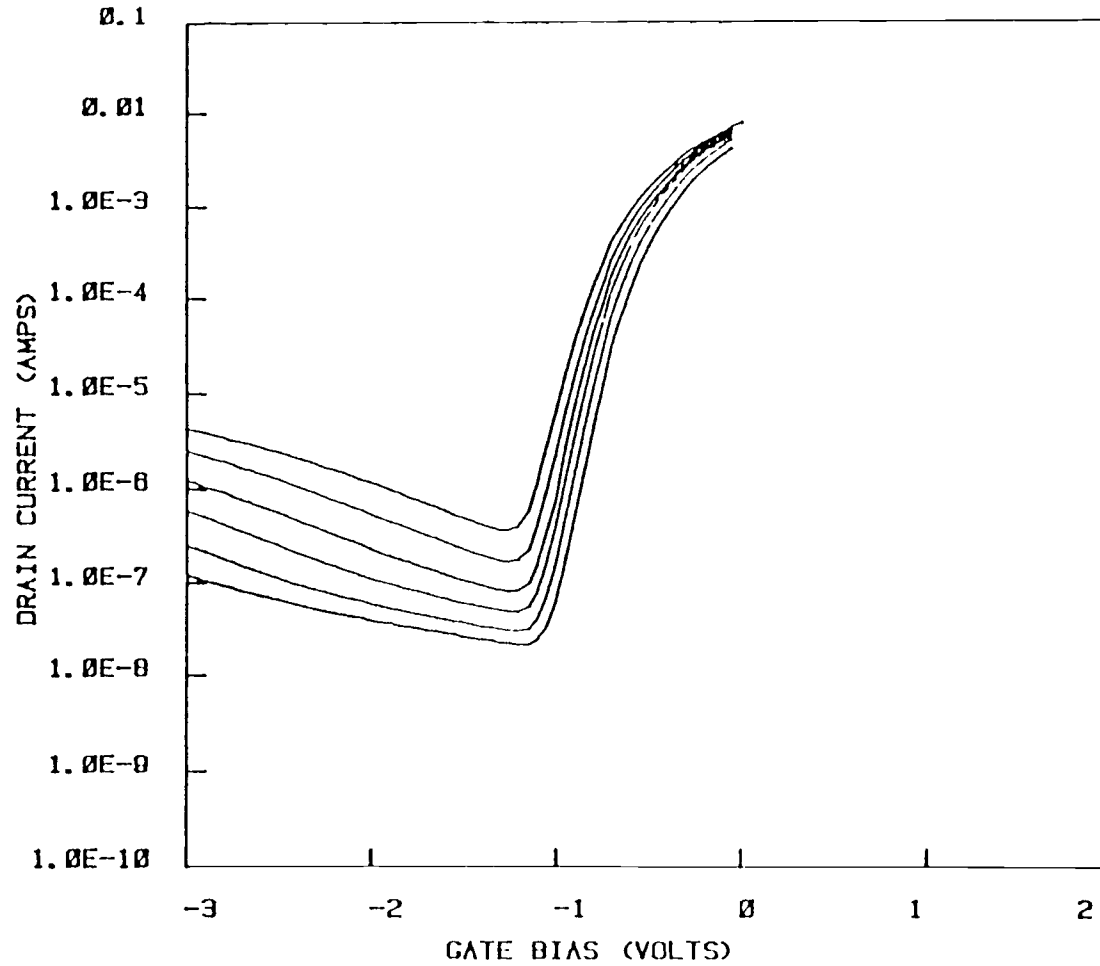
VDS (VOLTS)	TAPE&FILE (T, F)
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1	(4, 1)
1.5	(4, 1)
2	(4, 1)
2.5	(4, 1)
3	(4, 1)



8-12-87
G550A-D8 33400 PKG. #2
LG=0.25u Z=50u 1010A
BURIED CHANNEL

TEMP= 310 K

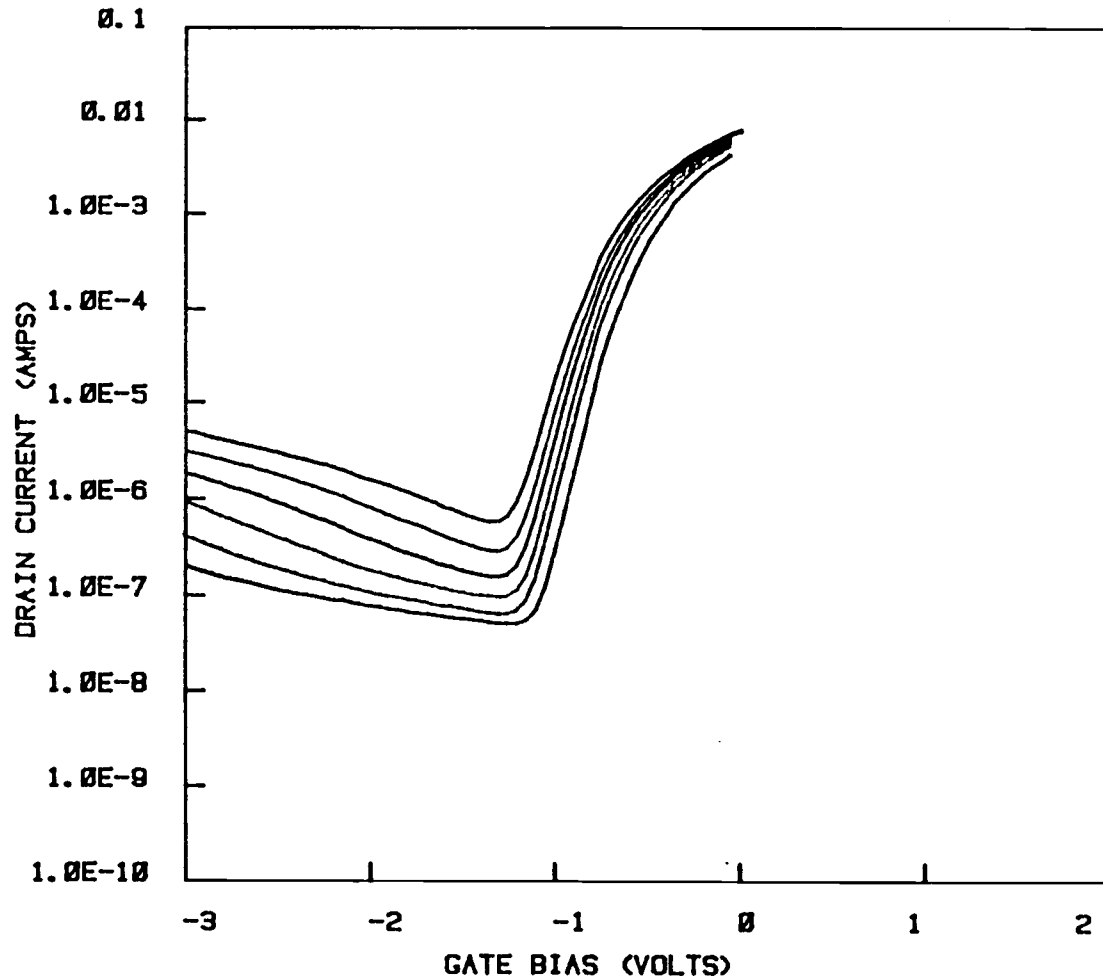
VDS (VOLTS)	TAPE&FILE (T, F)
0.5	(4, 3)
1	(4, 3)
1.5	(4, 3)
2	(4, 3)
2.5	(4, 3)
3	(4, 3)



6-11-1987
G558A-DB 33400 PKG. #2
LG=0.25 μ , Z=50 μ , 1010A
BURIED CHANNEL

TEMP= 360 K

VDS (VOLTS)	TAPE&FILE (T, F)
0.5	(4, 2)
1	(4, 2)
1.5	(4, 2)
2	(4, 2)
2.5	(4, 2)
3	(4, 2)



7.4 Controller and Plotter Program Listings

```

100 REM *****5-13-1987 ***** FILE 6 *****
110 REM *
120 REM * Author      : Philip C. Canfield
130 REM * Update      : P. K. Or
140 REM * Date        : July 15, 1987 (Last Update)
150 REM * Implement    : BASIC on Tektronix 4054A
160 REM *
170 REM * Purpose     : To issue communication protocol to various
180 REM *                 measuring equipments, sequence the measurement
190 REM *                 procedure and store data in tape.
200 REM *
210 REM *****|
220 REM *****
    **
230 CALL Start
240 END
250 CALL Ndev
260 END
270 CALL Tempset
280 END
290 CALL Bias
300 END
310 CALL Idsvgs
320 END
330 CALL Vdsswp
340 END
350 CALL Sbtshhd
360 END
370 REM *****
380 REM ***                                     ***
390 REM *** PROGRAM: MEASURES Ids vs Vgs ***
400 REM ***                                     ***
410 REM *****
420 !
430 !
440 REM
450 REM
460 REM INITIALIZE THE SYSTEM AND IDENTIFY THE DEVICE TO BE MEASURED
470 REM
480 REM
490 REM *****
500 REM
510 REM
520 SUB Start
530 PAGE
540 INIT
550 PRINT @26:"init"
560 PRINT @16:"init"
570 PRINT @24:"init"
580 PRINT @20:"IN"
590 PRINT @25:"INit"
600 PRINT @25:"freq 20E5;ampl 0.0;offs 0.0"
610 Rsen=50
620 Ids=" "

```

```

630 Devcom$=" "
640 Com$=" "
650 Dte$=" "
660 Temp=300
670 Lz=300
680 Crntlm$="0.1"
690 J=1
700 Relec=0.235
710 PRINT @26:"clo 9,10"
720 PRINT "Check the resistance used to measure the current by the"
730 PRINT "electrometer when the drain current is out of range."
740 R$=STR(Relec)
750 ALTER R$,R$
760 Relec=VAL(R$)
770 PRINT @26:"ope 9,10"
780 PRINT @37,0:10,255,13
790 PRINT "IF THE ELECTROMETER 'ZERO CHECK' LIGHT IS ON, TURN IT OFF"
800 PRINT "AND PRESS 'RETURN' TO CONTINUE"
810 INPUT C$
820 File=1
830 Tape=1
840 END SUB
850 !
860 !
870 ! -----
880 !
890 ! RECORD NEW DEVICE IDENTIFICATION
900 !
910 ! -----
920 !
930 !
940 SUB Ndev
950 Thrshld$="N"
960 Ovrrng$="N"
970 PRINT "ENTER DEVICE I.D. NUMBER"
980 ALTER Id$,Id$
990 PRINT "ENTER DEVICE SPECIFICS AND/OR PECULIARITIES"
1000 ALTER Devcom$,Devcom$
1010 Lz$=STR(Lz)
1020 PRINT "Enter the device gate width."
1030 ALTER Lz$,Lz$
1040 Lz=VAL(Lz$)
1050 Rsen$=STR(Rsen)
1060 PRINT "THE VALUE OF THE DRAIN SENSE RESISTOR=? "
1070 ALTER Rsen$,Rsen$
1080 Rsen=VAL(Rsen$)
1090 PRINT "CURRENT LIMIT FOR THE DRAIN CURRENT SOURCE=? (AMPS)"
1100 ALTER Crntlm$,Crntlm$
1110 C1$="CU "
1120 C1$=C1$&Crntlm$
1130 PRINT @23:C1$
1140 ALTER Dte$,Dte$
1150 END SUB
1160 !

```

```

1170  !
1180  ! -----
1190  !
1200  ! RECORD TEMPERATURE OF THE MEASUREMENT
1210  !
1220  ! -----
1230  !
1240  !
1250  SUB Tempset
1260    Temp$=STR(Temp)
1270    PRINT "Enter temperature of the measurement."
1280    ALTER Temp$,Temp$
1290    Temp=VAL(Temp$)
1300  END SUB
1310  !
1320  !
1330  REM
1340  REM
1350  REM *****
1360  REM
1370  REM
1380  REM SET VARIOUS BIASES AND DIMENSION ARRAYS
1390  REM
1400  REM
1410  REM *****
1420  REM
1430  REM
1440  SUB Bias
1450    PRINT "ENTER MOST NEGATIVE GATE BIAS"
1460    INPUT Negvgs
1470    PRINT "ENTER MOST POSITIVE GATE BIAS"
1480    INPUT Plsvgs
1490    PRINT "ENTER GATE BIAS INCREMENT"
1500    INPUT Vgsincr
1510    M=INT(1+(Plsvgs-Negvgs)/Vgsincr)
1520    PRINT "ENTER ADDITIONAL IMPORTANT INFORMATION"
1530    ALTER Com$,Com$
1540    IF Thrshld$="Y" THEN 1560
1550    DIM Gds(M),Vgsgo(M+1),Gm(M),Vgsgm(M+1)
1560  END SUB
1570  REM
1580  REM
1590  REM *****
1600  REM
1610  REM
1620  REM MEASURE DRAIN CURRENT VS VGS
1630  REM
1640  REM
1650  REM *****
1660  REM
1670  REM
1680  SUB Idsvgs
1690    Vgs=Plsvgs
1700    Vds4=Vds

```

```

1710 Vgs4=Vgs
1720 PRINT @16:"dcv"
1730 Ovrngs="N"
1740 Xd$="V0 "
1750 Xg$="offs "
1760 Y$=STR(Vds)
1770 Zd$=Xd$&Y$
1780 PRINT @20:Zd$
1790 PRINT @37,26:1
1800 PRINT @6,1:"F1R9T4X" !put electrometer on the 2A scale.
1810 PRINT @37,26:0
1820 CALL "wait",4
1830 PRINT @20:"OUT ON" !turn on the drain power supply
1840 Vgg=Vgs
1850 Gps=25
1860 Y$=STR(Vgs)
1870 Zg$=Xg$&Y$
1880 PRINT @6ps:Zg$
1890 PRINT @6ps:"OUT ON" !turn on the gate power supply
1900 Dps=20
1910 PRINT @26:"clo 14,10" !measure Vgs DVM; connect the elect.
1920 CALL "WAIT",2
1930 CALL Adjvgs
1940 PRINT @26:"ope 14;clo 15" !measure Vds with the DVM
1950 CALL "wait",2
1960 CALL Adjvds
1970 PRINT @26:"ope 15;clo 14" !measure Vgs with the DVM
1980 IF Ovrngs="Y" THEN 2050
1990 CALL "wait",2
2000 PRINT @16:"SEN"
2010 INPUT @16:Vgsid(K,1)
2020 Vdif=Vgsid(K,1)-Vgs
2030 IF ABS(Vdif)>0.01 THEN 1930
2040 PRINT @26:"ope 14;clo 15" !measure Vds with the DVM
2050 PRINT "Check the electrometer666666"
2060 P=1
2070 CALL "wait",4
2080 PRINT @37,26:1
2090 INPUT %5,1:Ids(K,P)
2100 PRINT @37,26:0
2110 IF ABS(Ids(K,P))<0.01 THEN 2130
2120 GO TO 2470
2130 PRINT @37,26:1
2140 PRINT @6,1:"F1R8T4X" !set the electrometer to the 20mA scale
2150 CALL "wait",2
2160 PRINT @6,1:"F1R0T4X" !set the electrometer to autoranging
2170 PRINT @37,26:0
2180 Vgs=Vgs-Vgsincr
2190 Y$=STR(Vgs)
2200 Zg$=Xg$&Y$
2210 P1=P
2220 FOR P=P1 TO M
2230 PRINT @26:"ope 15;clo 14" !measure Vgs with the DVM
2240 CALL "wait",2

```

```

2250     CALL Adjvgs
2260     PRINT @26:"ope 14;clo 15" !measure Vds with the DVM
2270     CALL "wait",2
2280     CALL Adjvds
2290     PRINT @26:"ope 15;clo 14" !measure Vgs with the DVM
2300     CALL "wait",2
2310     PRINT @16:"SEN"
2320     INPUT @16:Vgsid(K,P)
2330     Vdif=Vgsid(K,P)-Vgs
2340     IF ABS(Vdif)>0.01 THEN 2250
2350     PRINT @26:"ope 14;clo 15" !measure Vds with the DVM
2360     CALL "WAIT",2
2370     PRINT @37,26:1
2380     INPUT %6,1:Ids(K,P)
2390     PRINT @37,26:0
2400     Vgs=Vgs-Vgsincr
2410     Y$=STR(Vgs)
2420     Zg$=Xg$&Y$
2430     PRINT @6ps:Zg$
2440     CALL "wait",1
2450     NEXT P
2460     GO TO 2830
2470     PRINT @26:"clo 9" !connect resistor across inputs of electr.
2480     PRINT @37,26:1
2490     PRINT @6,1:"F0R0T4X" !SET ELECTROMETER TO MEASURE VOLTAGE
2500     PRINT @37,26:0
2510     PRINT @26:"ope 15;clo 14" !MEASURE Vgs with the DVM
2520     CALL "Wait",2
2530     CALL Adjvgs
2540     PRINT @26:"ope 14;clo 15" !measure Vds with the DVM
2550     CALL "Wait",2
2560     CALL Adjvds
2570     PRINT @26:"ope 15;clo 14" !measure Vds with the DVM
2580     CALL "wait",2
2590     PRINT @16:"SEN"
2600     INPUT @16:Vgsid(K,P)
2610     Vdif=Vgsid(K,P)-Vgs
2620     IF ABS(Vdif)>0.01 THEN 2520
2630     PRINT @26:"ope 14;clo 15" !measur Vds with the DVM
2640     CALL "WAIT",3
2650     PRINT @37,26:1
2660     INPUT %6,1:V8
2670     PRINT @37,26:0
2680     Ids(K,P)=V8/Relec
2690     P=P+1
2700     Vgs=Vgs-Vgsincr
2710     Y$=STR(Vgs)
2720     Zg$=Xg$&Y$
2730     PRINT @6ps:Zg$
2740     CALL "wait",1
2750     IF P>M THEN 2830
2760     IF ABS(Ids(K,P-1))=>0.01 THEN 2510
2770     P1=P
2780     PRINT @26:"ope 9"

```

```

2790 PRINT @37,26:1
2800 PRINT @6,1:"F1R0T4X" !set the electrometer to autorange current
2810 PRINT @37,26:0
2820 GO TO 2220
2830 PRINT @6ps:"OUT OFF"
2840 PRINT @20:"OUT OFF"
2850 PRINT @26:"ope all"
2860 END SUB
2870 |
2880 |
2890 | -----
2900 |
2910 | ADJUST VDS TO THE DESIRED VALUE
2920 |
2930 | -----
2940 |
2950 |
2960 SUB Adjvds
2970 Vdd=Vds4
2980 PRINT @16:"sen"
2990 INPUT @16:Vds4
3000 Udif=Vds-Vds4
3010 IF ABS(Udif)<0.01 THEN 3130
3020 Vdd=Vdd+Udif
3030 IF Dps<>24 THEN 3050
3040 IF Vdd>7.5 THEN 3120
3050 IF Vdd<0 THEN 2970
3060 IF Vdd>10 THEN 3130
3070 Y$=STR(Vdd)
3080 Zd$=Xd$&Y$
3090 PRINT @Dps:Zd$
3100 CALL "wait",2
3110 GO TO 2980
3120 Ovrrng$="Y"
3130 END SUB
3140 |
3150 |
3160 | -----
3170 |
3180 | ADJUST THE GATE BIAS TO THE DESIRED VALUE
3190 |
3200 | -----
3210 |
3220 |
3230 SUB Adjvgs
3240 Vgg=Vgs
3250 PRINT @16:"sen"
3260 INPUT @16:Vgs4
3270 Udif=Vgs-Vgs4
3280 IF ABS(Udif)<0.01 THEN 3380
3290 Vgg=Vgg+Udif
3300 IF Vgg<-7.5 THEN
3310 Vgg=Vgs
3320 END IF

```



```

3330   Y$=STP(Vgg)
3340   Zg$=Xg$&Y$
3350   PRINT @Gps:Zg$
3360   CALL "wait",2
3370   GO TO 3250
3380 END SUB
3390   !
3400   !
3410   ! -----
3420   !
3430   ! SUBROUTINE FOR MEASUREING SUBTHRESHOLD CURRENTS
3440   !
3450   ! -----
3460   !
3470   !
3480 SUB Sbtshsd
3490   PRINT @26:"OPE ALL"
3500   Thrshld$="Y"
3510   PRINT "Enter Vds max."
3520   INPUT Vdsmax
3530   PRINT "Enter Vds min."
3540   INPUT Vdsmin
3550   PRINT "Enter the step size for Vds."
3560   INPUT Vdsstp
3570   J=INT((Vdsmax-Vdsmin)/Vdsstp+1.001)
3580   DIM Sbvds(J+1)
3590   PRINT "Enter the data tape number and be sure that"
3600   PRINT "it is in the computer.666"
3610   INPUT Tape
3620   PRINT "Enter the starting data file #."
3630   INPUT File
3640   CALL Bias
3650   CALL Tempset
3660   Sbvds(1)=Vdsmin
3670   DIM Ids(J,M),Vgsid(J,M)
3680   FOR K=1 TO J
3690     Vds=Sbvds(K)
3700     CALL Idsvgs
3710     IF K=>J THEN 3730
3720     Sbvds(K+1)=Vdsmin+Vdsstp*K
3730   NEXT K
3740   CALL Sbtstr
3750   J=1
3760   Thrshld$="N"
3770 END SUB
3780   !
3790   !
3800   ! -----
3810   !
3820   ! STORE THE SUBTHRESHOLD CURRENT DATA
3830   !
3840   ! -----
3850   !
3860   !

```

```
3870 SUB Sbthstr
3880   FIND File
3890   WRITE @33:Ids,Devcom$,Dtes$,Com$
3900   WRITE @33:Tape,File,J,M,Temp,Negvgs,Plsvgs,Udsmax,Udsmin
3910   FOR Ks=1 TO J
3920     WRITE @33:Sbvds(Ks)
3930     FOR Ps=1 TO M
3940       WRITE @33:Ids(Ks,Ps),Ugsid(Ks,Ps)
3950     NEXT Ps
3960   NEXT Ks
3970 END SUB
```

```

100  |*****6-29-1987*****FILE 7*****
110 REM *
120 REM * Author   : P. K. Or, Philip C. Canfield
130 REM * Update   : P. K. Or
140 REM * Date     : July 30, 1987 (Last update)
150 REM * Implement: BASIC on Tektronix 4054A
160 REM * Plotter  : HP 7225A
170 REM *
180 REM * Purpose  : To plot data stored on magnetic tapes. Four
190 REM *             forms of data : Ids vs Vgs, Igs vs Vgs, Iss vs
200 REM *             Vgs and Isb vs Vgs for different temperature
210 REM *             ranges. The data are presented in linear or
220 REM *             log current plot with normalized or non-
230 REM *             normalized Y-axis. These choices are presented in
240 REM *             the main menu.
250 REM *
260 REM *
270  |*****BACKUP FILE 6*****
280 CALL Main
290  |
300  |
310  |-----
320  |
330  | SUBROUTINE TO DRAW AND LABEL THE AXIS
340  |
350  |-----
360  |
370  |
380 SUB Pltaxis
390   Prt=5
400   PRINT @37,26:1
410   PRINT @Prt:"IN"
420   HS=CHR(3)
430   PRINT @Prt:"PA 9800,6500;PD;"
440   PRINT @Prt:"PA 9800,900;"
450   PRINT @Prt:"PA 3800,900;"
460   PRINT @Prt:"PA 3800,6500;"
470   PRINT @Prt:"PA 9800,6500;PU;"
480   PRINT @Prt:"PA 3800,6500;"
490   PRINT @Prt:"TL 2.0;"
500   PRINT @Prt:"IP 3800,900,9800,6500;"
510   PRINT @Prt:"SC";Xlo;"",Xhi;"",Ylo;"",Yhi;"";
520   FOR I=1 TO Nydiv-1
530     PRINT @Prt:"PR 0,";-Ty;"";YT;"
540   NEXT I
550   PRINT @Prt:"PA";Xlo;"",Ylo;"";
560   FOR I=1 TO Nxdiv-1
570     PRINT @Prt:"PR";Tx;"",0;XT;"
580   NEXT I
590   PRINT @Prt:"PA";Xlo;"",Ylo;"";
600   PRINT @Prt:"SI;"
610   Xdvlb$=STR(Xdivlb(1))
620   PRINT @Prt:"CP -1,-1.5;LB";Xdvlb$;HS;"";
630   FOR I=2 TO Nxdiv+1

```

```

640     Xdvlb$=STR(Xdivlb(I))
650     PRINT @Prt:"PR";Tx;",";0;CP-3,0;LB";Xdvlb$;H$;";"
660     NEXT I
670     PRINT @Prt:"PA";Xlo;",";Ylo;";CP -2,0;"
680     FOR I=1 TO Nydiv+1
690         Ydvlb$=STR(Ydivlb(I))
700         PRINT @Prt:"CP";-LEN(Ydvlb$);",";0;"
710         PRINT @Prt:"LB";Ydvlb$;H$;";PR 0,";Ty;";"
720     NEXT I
730     PRINT @Prt:"IP;SC;"
740     PRINT @Prt:"PA 5500,300;"
750     PRINT @Prt:"LB";Xlable$;H$;";"
760     IF Nrmal$="Y" THEN
770         PRINT @Prt:"PA 2700,1700;"
780     ELSE
790         PRINT @Prt:"PA 2700,2500;"
800     END IF
810     PRINT @Prt:"DI 0,1;"
820     PRINT @Prt:"LB";Ylable$;H$;";"
830     PRINT @Prt:"DI 1,0;"
840     PRINT @Prt:"PA 3900,7800;"
850     PRINT @Prt:"LB";Header1$;H$;";CP;"
860     PRINT @Prt:"LB";Header2$;H$;";CP;"
870     PRINT @Prt:"LB";Header3$;H$;";CP;"
880     PRINT @Prt:"LB";Header4$;H$;";"
890     PRINT @Prt:"PA 7000,7800;"
900     PRINT @Prt:"LB";Var1$;H$;";CP;"
910     PRINT @Prt:"LB";Var2$;H$;";"
920     PRINT @Prt:"PA 50,7000;LB";Var3$;H$;";"
930     PRINT @Prt:"PA 1500,7000;LB TAPE&FILE";H$;";"
940     PRINT @Prt:"PA 50,7000;CP;"
950     PRINT @Prt:"OA;"
960     INPUT @Prt:Lx,Ly,St
970     PRINT @Prt:"LB";Unt$;H$;";"
980     PRINT @Prt:"PA 1500,";Ly;";"
990     PRINT @Prt:"LB (T,F)";H$;";"
1000    PRINT @Prt:"PA 50,";Ly;";CP 0,-2;OA;"
1010    INPUT @Prt:Lx,Ly,St
1020    PRINT @37,26:0
1030 END SUB
1040 !
1050 !
1060 ! -----
1070 !
1080 ! SUBROUTINE TO PLOT THE DATA AT THE PLOTTER
1090 !
1100 ! -----
1110 !
1120 !
1130 SUB Pltdta
1140     PRINT @37,26:1
1150     PRINT @Prt:"IP 3800,900,9800,5500;"
1160     PRINT @Prt:"IW 3800,900,9800,5500;"
1170     PRINT @Prt:"SC";Xlo;",";Xhi;",";Ylo;",";Yhi;";"

```

```

1180 PRINT @Prt:"PA";X(1);", ";Y(1);";PD;"
1190 FOR I=1 TO Numpts
1200 PRINT @Prt:"PA";X(I);", ";Y(I);";"
1210 NEXT I
1220 PRINT @Prt:"IP;IW;SC;"
1230 PRINT @Prt:"PU;PA";Lx; ", ";Ly;";"
1240 PRINT @Prt:"LB";Crntdta$;H$;";"
1250 PRINT @Prt:"CP 2,0.5;PD;PR 300,0;PU;"
1260 PRINT @Prt:"PA 1500,";Ly;";LB (";Tape; ", ";File;")";H$;";"
1270 PRINT @Prt:"PA";Lx; ", ";Ly;";CP;CP;OA;"
1280 INPUT @Prt:Lx,Ly,St
1290 PRINT @37,26:0
1300 END SUB
1310 !
1320 !
1330 !-----
1340 !
1350 !SUBROUTINE TO READ THE SUBTHRESHOLD CURRENT DATA
1360 !
1370 !-----
1380 !
1390 !
1400 SUB Ridsdta
1410 PRINT "Check to be sure that data tape #";Tape;" is instaled"
1420 INPUT Cs
1430 FIND File
1440 READ @33:Id$,Devcom$,Dtes$,Com$
1450 READ @33:Tape,File,J,M,Temp,Negvgs,Plsvgs,Udsmax,Udsmin,Lg,Lz
1460 DIM Sbvds(J),Ids(J,M),Ugsid(J,M),Igs(J,M),Iss(J,M),Isb(J,M)
1470 FOR Ks=1 TO J
1480 READ @33:Sbvds(Ks)
1490 FOR Ps=1 TO M
1500 READ @33:Ids(Ks,Ps),Ugsid(Ks,Ps),Igs(Ks,Ps),Iss(Ks,Ps),Isb
(Ks,Ps)
1510 NEXT Ps
1520 NEXT Ks
1530 END SUB
1540 !
1550 !
1560 !-----
1570 !
1580 ! SUBROUTINE TO PUT THE SUBTHRESHOLD DATA IN THE PROPER
1590 ! FORMAT FOR PLOTTING AND THEN TO PLOT IT.
1600 !
1610 !-----
1620 !
1630 !
1640 SUB Indcrnt
1650 Pass$="N"
1660 PAGE
1670 PRINT "CHOOSE CURRENT VERSUS Vgs PLOT WANTED::"
1680 PRINT
1690 PRINT "1.....DRAIN CURRENT"
1700 PRINT "2.....GATE CURRENT"

```

```

1710 PRINT "3.....SOURCE CURRENT"
1720 PRINT "4.....SUBSTRATE CURRENT"
1730 PRINT "5.....RETURN TO MAIN MENU"
1740 INPUT Ipt
1750 IF Pass$="Y" THEN 1830
1760 PRINT "SELECT THE DATA TAPE AND FILE NUMBER TO BE PLOTTED."
1770 PRINT "TAPE?   ";
1780 INPUT Tape
1790 PRINT "FILE?   ";
1800 INPUT File
1810 CALL Ridsdta
1820 DIM Sbipt(J,M)
1830 IF Ipt=1 THEN
1840   Crnt$="DRAIN"
1850   FOR Ks=1 TO J
1860     FOR Ps=1 TO M
1870       Sbipt(Ks,Ps)=Ids(Ks,Ps)
1880     NEXT Ps
1890   NEXT Ks
1900 ELSE
1910   IF Ipt=2 THEN
1920     Crnt$="GATE"
1930     FOR Ks=1 TO J
1940       FOR Ps=1 TO M
1950         Sbipt(Ks,Ps)=Igs(Ks,Ps)
1960       NEXT Ps
1970     NEXT Ks
1980   ELSE
1990     IF Ipt=3 THEN
2000       Crnt$="SOURCE"
2010       FOR Ks=1 TO J
2020         FOR Ps=1 TO M
2030           Sbipt(Ks,Ps)=Iss(Ks,Ps)
2040         NEXT Ps
2050       NEXT Ks
2060     ELSE
2070       IF Ipt=4 THEN
2080         Crnt$="SUBSTRATE"
2090         FOR Ks=1 TO J
2100           FOR Ps=1 TO M
2110             Sbipt(Ks,Ps)=Isb(Ks,Ps)
2120           NEXT Ps
2130         NEXT Ks
2140       ELSE
2150         IF Ipt=5 THEN 2410
2160         PRINT "INVALID SELECTION. TRY AGAIN";
2170         GO TO 1740
2180       END IF
2190     END IF
2200   END IF
2210 END IF
2220 Scl$="0"
2230 IF Ipt=1 THEN
2240   PRINT "PLOT DRAIN CURRENT ON LOG(O) OR LINEAR(I) SCALE?   ";

```

```

2250     ALTER Scle$,Scle$
2260     ELSE
2270     PRINT "CURRENT IS PLOTTED ON LOG SCALE"
2280     END IF
2290     PRINT "CHOOSE TEMPERATURE(T) OR Vds(V).  ";
2300     Choice$="V"
2310     ALTER Choice$,Choice$
2320     PRINT "NORMALIZE PLOT WITH GATE WIDTH (Y/N)?  ";
2330     Nrmal$="N"
2340     ALTER Nrmal$,Nrmal$
2350     CALL Label
2360     CALL Xyaxis
2370     CALL Pltaxis
2380     CALL Frmdta
2390     Pass$="Y"
2400     GO TO 1660
2410 END SUB
2420 !
2430 SUB Label
2440     Header1$=Dte$
2450     Header2$=Id$
2460     Header3$=Devcom$
2470     Header4$=Com$
2480     Var2$=" "
2490     IF Ipt=1 THEN
2500         IF Scle$="0" THEN
2510             IF Nrmal$="Y" THEN
2520                 Ylable$="DRAIN CURRENT (AMPS) / GATE WIDTH (uM)"
2530             ELSE
2540                 Ylable$="DRAIN CURRENT (AMPS)"
2550             END IF
2560         ELSE
2570             IF Nrmal$="Y" THEN
2580                 Ylable$="DRAIN CURRENT (MILLIAMPS) / GATE WIDTH (uM)"
2590             ELSE
2600                 Ylable$="DRAIN CURRENT (MILLIAMPS)"
2610             END IF
2620         END IF
2630     ELSE
2640         IF Nrmal$="Y" THEN
2650             Ylable$=Crnt$&" CURRENT (AMPS) / GATE WIDTH (uM)"
2660         ELSE
2670             Ylable$=Crnt$&" CURRENT (AMPS)"
2680         END IF
2690     END IF
2700     Xlable$="GATE BIAS (VOLTS)"
2710     IF Choice$="T" THEN
2720         Var1$="VDS="
2730         FOR K=1 TO J
2740             PRINT K;".....VDS(";K;")=";Sbvds(K)
2750         NEXT K
2760     PRINT "CHOOSE THE VDS TO PLOT BY #"
2770     INPUT K
2780     IF K<1 THEN

```

```

2790         PRINT "INVALID CHOICE TRY AGAIN"
2800         GO TO 2770
2810     END IF
2820     IF K>J THEN
2830         PRINT "INVALID CHOICE TRY AGAIN"
2840         GO TO 2770
2850     END IF
2860     Vds$=STR(Sbvds(K))
2870     Vdsunt$=" VOLTS"
2880     Var1$=Var1$&Vds$&Vdsunt$
2890     Var3$="TEMP"
2900     Unt$="(K)"
2910 ELSE
2920     Var1$="TEMP="
2930     Temp$=STR(Temp)
2940     Tunt$=" K"
2950     Var1$=Var1$&Temp$&Tunt$
2960     Var3$=" VDS"
2970     Unt$="(VOLTS)"
2980 END IF
2990 END SUB
3000 !
3010 !
3020 SUB Xyaxis
3030 !
3040     ! X-AXIS DIVISIONS
3050     !
3060     Xlo=-4
3070     Xhi=1
3080     Nxdiv=Xhi-Xlo
3090     DIM Xdivlb(Nxdiv+1)
3100     Xdivlb(1)=Xlo
3110     FOR Ix=2 TO Nxdiv+1
3120         Xdivlb(Ix)=INT(Xdivlb(Ix-1)+1.001)
3130     NEXT Ix
3140     Xlo=INT(100*Xlo+1.0E-3)
3150     Xhi=INT(100*Xhi+1.0E-3)
3160     Tx=100
3170     !
3180     ! Y-AXIS DIVISIONS
3190     !
3200     IF Scl$="I" THEN
3210         Ylo=0
3220         IF Ids(J,1)<0.025 THEN
3230             Yhi=25
3240             Nydiv=5
3250         ELSE
3260             IF Ids(J,1)<0.05 THEN
3270                 Yhi=50
3280                 Nydiv=5
3290             ELSE
3300                 IF Ids(J,1)<0.1 THEN
3310                     Yhi=100
3320                     Nydiv=5

```



```

4410         IF Nrmals$="Y" THEN
4420             FOR P=1 TO M
4430                 Y(P)=INT(10000*Sbipt(Udv(K),P)/Lz+1.0E-3)
4440             NEXT P
4450         ELSE
4460             FOR P=1 TO M
4470                 CALL Pdata
4480             NEXT P
4490         END IF
4500     ELSE
4510         IF Nrmals$="Y" THEN
4520             FOR P=1 TO M
4530                 Y(P)=INT(LGT(ABS(Sbipt(Udv(K),P)/Lz))*100+1.0E-33
4540                 )
4550             NEXT P
4560         ELSE
4570             FOR P=1 TO M
4580                 Y(P)=INT(LGT(ABS(Sbipt(Udv(K),P)))*100+1.0E-3)
4590             NEXT P
4600         END IF
4610     END IF
4620     PRINT "INSERT A DIFFERENT COLORED PEN IN THE PLOTTER"
4630     PRINT "AND PRESS RETURN."
4640     INPUT C$
4650     CALL Pltdta
4660     NEXT K
4670 END IF
4680 !
4690 !
4700 SUB Pdata
4710     PAGE
4720     Pnt=1
4730     PRINT "SELECT DATA TAPE & FILE TO BE PRINTED"
4740     PRINT "TAPE= ";
4750     INPUT Tape
4760     PRINT "FILE= ";
4770     INPUT File
4780     CALL Ridsdata
4790     PRINT @37,26:1
4800     PRINT @Pnt:Id$
4810     PRINT @Pnt:Devcom$
4820     PRINT @Pnt:Com$
4830     PRINT @Pnt:"TAPE: ",Tape,"          FILE: ",File
4840     PRINT @Pnt:"TEMP=",Temp
4850     PRINT @Pnt:"LG= ",Lg,"          LZ= ",Lz
4860     FOR Ks=1 TO J
4870         PRINT @Pnt:"Uds=",Sbvds(Ks)
4880         FOR Ps=1 TO M
4890             PRINT @Pnt:"Ugs=",Ugsid(Ks,Ps),"          Ids=",Ids(Ks,Ps)
4900         NEXT Ps
4910     NEXT Ks
4920     PRINT @37,26:0
4930 END SUB

```

```

3870         NEXT P
3880     END IF
3890 ELSE
3900     IF Nrmal$="Y" THEN
3910         FOR P=1 TO M
3920             Y(P)=INT(LGT(Sbipt(K,P)/Lz)*100+1.0E-3)
3930         NEXT P
3940     ELSE
3950         FOR P=1 TO M
3960         END IF
3970         PRINT "CHOOSE A DIFFERENT COLORED PEN FOR THE"
3980         PRINT "PLOTTER AND PRESS RETURN ."
3990         INPUT Cs
4000         CALL Pltdta
4010         PRINT "PLOT ANOTHER TEMPERATURE? (Y/N)"
4020         Y(P)=INT(LGT(Sbipt(K,P))*100+1.0E-3)
4030     NEXT P
4040 END IF
4050 INPUT Anthrts$
4060 IF Anthrts$="N" THEN 4670
4070 PRINT "DATA TAPE #?"
4080 INPUT Tape
4090 PRINT "FILE #?"
4100 INPUT File
4110 CALL Ridsdta
4120 GO TO 3690
4130 ELSE
4140 PAGE
4150 PRINT "DO YOU WISH TO PLOT THE DATA FOR ALL OF THE"
4160 PRINT "VDS VALUES LISTED BELOW? (Y/N)"
4170 Slvdvlu$="Y"
4180 DIM Vdv(J+1)
4190 FOR Ki=1 TO J
4200     PRINT Ki;".....VDS(";Ki;")=";Sbvds(Ki)
4210     Vdv(Ki)=Ki
4220 NEXT Ki
4230 J1=J
4240 ALTER Slvdvlu$,Slvdvlu$
4250 IF Slvdvlu$="Y" THEN 4340
4260 PRINT "SELECT THE #'S CORRESPONDING TO THE VDS VALUES"
4270 PRINT "YOU WANT TO PLOT ONE AT A TIME FOLLOWED BY A <CR>."
4280 PRINT "ENTER A 0 TO QUIT"
4290 Kc=0
4300 Kc=Kc+1
4310 INPUT Vdv(Kc)
4320 IF Vdv(Kc)<>0 THEN 4300
4330 J1=Kc-1
4340 Numpts=M
4350 FOR K=1 TO J1
4360     Crntdta$=STR(Sbvds(Vdv(K)))
4370     FOR P=1 TO M
4380         X(P)=INT(100*Vgsid(Vdv(K),P)+1.0E-3)
4390     NEXT P
4400     IF Scle$="I" THEN

```

```
4940  !
4950  !
4960  !
4970  SUB Main
4980    Tape$="1"
4990    File$="1"
5000    PAGE
5010    CHARSIZE 3
5020    PRINT "*****"
5030    PRINT
5040    PRINT
5050    PRINT "                MAIN MENU "
5060    PRINT
5070    PRINT
5080    PRINT "*****"
5090    PRINT
5100    PRINT
5110    PRINT "1.....INDIVIDUAL COMPONENT OF CURRENT"
5120    PRINT "2.....PRINT DATA FROM DATA TAPE"
5130    PRINT "3.....QUIT"
5140    INPUT Slct
5150    IF Slct=1 THEN
5160      CALL Indcrnt
5170    ELSE
5180      IF Slct=2 THEN
5190        CALL Pdata
5200      ELSE
5210        IF Slct=3 THEN 5270
5220        PRINT "INVALID CHOICE. CHOOSE AGAIN.";
5230        GO TO 5140
5240      END IF
5250    END IF
5260    GO TO 5000
5270  END SUB
```



```

        Readln (DataFile);
    End;
2    : Begin
        ClrScr;
        Repeat
            Write ('Which Data File to be processed =
? ');
            Readln (DataFile);
            StoDataFile := DataFile + '.Dat';
            Assign (Data, StoDataFile);
            ($I-) Reset (Data) ($I+);
            OK := (IOresult = 0);
            If Not OK then
                Writeln ('Cannot find file
',StoDataFile);
            Until OK;
            ProcessFile := DataFile + '_';
            Readln (Data, DeviceID);
            Readln (Data, Lg, Lz, Temp, Vto, Vpts);
            Writeln;
            Write ('Alpha = ? ');           Readln
(Alpha);
            Write ('Ns      = ? ');           Readln (Ns);
            Sequence := 0;
            SequenceNum := '0';
        End;
3    : Exit;
End;
End;

```

```

(*****
*****
)
(
)
(           M A I N       P R O G R A M
)
(
)
(*****
*****
)

```

```

Begin
    Select := 1;
    Repeat
        SetUp (Select);
        ClrScr;
        Case Select Of
            1    : DiskStorage;
            2    : Begin
                    Set Vthv (Vthv, Temp);
                    For I := 1 To Vpts Do

```

```

Begin
  Readln (Data, Vds[I], DataPts);
  Get_Data(X, Y, DataPts, Vds[I]);
  Nlin (X, Y, Y Calc, DataPts);
  Print_Data(Vds[I], DataPts);
  Write('Store Data on Disk? (y/n) ');
  Readln (Store);
  If Store = 'y' then
    Store_Data(Vds[I], DataPts);
  End;
  Close (Data);
End;
3 : ;
End;
Until Select = 3;
End.

```

7.6 VREFSIM Program Listing

```

1/2      )
(  N O R M A L      )
(      )
(Circuit1 is the program to simulate the normal device
operation. It runs )
(From a temperature of 400K to 220K. The user has to change
the lambda and )
(and Alpha manually in the constant declaration. The (W/L)
scale the Tempe )
(coefficient of the device. The minimum current must be
greater than 1mA. )
(      INPUT  : TEMP HIGH, TEMP LOW, TEMP STEP, RS
)
(      OUTPUT : VOUT, IM
)

```

Program Circuit1;

Const

```

Es      = 1.1599E-12;
Q       = 1.60218E-19;
K       = 1.3806E-23;
t       = 6.6E-6;
Nc      = 4.0E17;
ni      = 2.0E6;
U300    = 3500;
T300    = 300;
Vdd     = 0.74;
Vss     = -2.0;
Lambda  = 0.05;
Alpha   = 2.2;

```

Type

```
Element = Array[1..25] of Real;
```

Var

```

Vds, Vgs      : Real;
Vthv, Vto, Vp : Real;
Vout, Vt, Vr, Vdif : Real;
Temp, Vg      : Real;
W, L, Psi     : Real;
Beta          : Real;
Rs, Rsi       : Real;
Im, Ir, Ilast : Real;
TempHi, TempLow, TempStep : Real;
I, P, LastElem : Integer;
Okay, FirstPass : Boolean;
Data          : Text;
DataFile     : String[12];
StoDataFile  : String[16];

```



```

    IBias                               : Element;

Procedure SetUp;

Begin
  ClrScr;
  ( Write ('High Temperature = ? ');      Readln (TempHi);
    Write ('Low  Temperatute = ? ');      Readln (TempLow);
    Write ('Temperature Step = ? ');      Readln
(TempStep);)
  TempHi := 400;    TempLow := 220;  TempStep :=10;
  Write ('DataFile = ? ');              Readln
(DataFile);

  Vout := 0.0;
  Vg := 0.0;
  Write ('W = ?');    Readln(W);
  L := 0.25;
  Rs := 2/(1.4129E-4*(W/L));           Writeln('Rs =
',Rs:1:0);
  Psi := 0.0001;
  Rsi := Rs/(1+Psi*(T300-273));
End;

Function Tanh (X : Real): Real;

Var
  A, B : Real;

Begin
  A := Exp(X);
  B := Exp(-X);
  Tanh := (A-B)/(A+B);
End;

Procedure Im_Solve;

Begin
  Beta := (2*W*U300*T300*Es*Sqr(292/Temp))/(3*L*Temp*t);
  Vds := Vdd - Vout;
  Vgs := Vg - Vout;
  Vp := (Q*Nc*Sqr(t)/(2*Es))*(Temp/292);
  Vthv := (K/Q)*Temp;
  Vto := Vthv*Ln(Nc/ni)-Vp;
  Vt := Vto-0.07*Vds;
  Im := Beta*Sqr(Vgs-Vt)*(1+Lambda*Vds)*Tanh(Alpha*Vds);
  (writeln('Beta=',Beta:6:5,' Vp=',Vp:4:3,'
Vthv=',Vthv:4:3,' Vto=',Vto:4:3,' Vt=',Vt:4:3);)
End;

Procedure Ir_Solve;

```

```

Begin
  Vr := Vout - Vss;
  Rs := Rsi*(1+Psi*(Temp-273));
  Ir := (Vr)/Rs;
End;

Procedure Test_Bias (Var OKAY : Boolean);

Const
  Tol = 0.0001;

Var
  Itest : Real;

Begin
  Itest := Im/Ir - 1;
  If ABS(Itest) <= Tol Then
    OKAY := True
  Else
    Begin (ABS)
      If FirstPass Then
        Begin (FirstPass)
          Vdif := 0.0005;
          If Itest > 0 then
            Vout := Vout + Vdif
          Else
            Vout := Vout - Vdif;
          FirstPass := False;
        End (FirstPass)
      Else
        Begin (Subsequent Passes)
          If Itest > 0 then
            Begin
              If Ilast < 0 then Vdif := Vdif*0.5;
              Vout := Vout + Vdif;
            End
          Else
            Begin
              If Ilast > 0 then Vdif := Vdif*0.5;
              Vout := Vout - Vdif;
            End;
          End; (Subsequent Passes)
        End; (ABS)
      Ilast := Itest;
    End;

Procedure Store_Data (Ibias : Element; LastElem: integer);
Var
  J : Integer;

Begin
  StoDataFile := DataFile+'.Dat';

```

```

Rs := Rsi*(1 + Psi*(300-273));
Assign (Data, StoDataFile);
Rewrite (Data);
Writeln (Data, 'W :',W:1:1);
Writeln (Data, 'Rs :',Rs:1:0);
For J := 1 to LastElem Do
  Writeln (Data, Ibias[J]);
Flush (Data);
Close (Data);
End;

Begin
  SetUp;
  Temp := TempLow;
  P := 0;
  Writeln ('Temp   Vg       Vout       Vgs       Im
Ir');
  Repeat
    OKAY := False;
    P := P + 1;
    FirstPass := True;
    I := 0;
    Repeat
      I := I + 1;
      Im Solve;
      Ir Solve;
      Test Bias (OKAY);
      If Keypressed then exit;
    Until (OKAY = True) OR (I > 1000);
    If I >= 1000 then
      Begin
        Writeln ('No convergence. Program terminated. ');
        Exit
      End;
    Ibias[P] := Im;
    If (Vg-Vout)<0 then
      Writeln (Temp:0:0,'   ',Vg:5:3,'   ', Vout:5:3,'
',(Vg-Vout):3:3,'   ',Im:10,'   ',Ir:10)
    Else
      Writeln (Temp:0:0,'   ',Vg:5:3,'   ', Vout:5:3,'
',(Vg-Vout):3:3,'   ',Im:10,'   ',Ir:10);
    Temp := Temp + TempStep;
    Until Temp >= TempHi + Tempstep;
    LastElem := P;
    Store_Data(Ibias, LastElem);
  End.

```

```

(
( SUB _ DEV
(
(THE PROGRAM SIMULATE THE POSITIVE TEMPERATURE DRIFT
COMPONENT PARTOF THE
(CIRCUIT. IT CONSISTS OF A TRANSISTOR IN SUBTRESHOLD REGION,
AND TWO RESISTOR.)
( INPUT : temp high, Temp low, Rs, R2
)
( OUTPUT : IM
)

```

```
Program SUB_DEV;
```

```
Const
```

```

Es      = 1.1599E-12;
Q       = 1.60218E-19;
K       = 1.3806E-23;
t       = 6.6E-6;
Nc      = 4.0E17;
ni      = 2.0E6;
U300   = 3500;
T300   = 300;
Vdd    = 0.74;
Vss    = -2.0;
Gamma  = 0.07;
Alpha  = 0.046;
Ns     = 1.671;

```

```
Var
```

```

Vthv, Vto, Vp      : Real;
Vout, Vdif         : Real;
Temp, Vg           : Real;
W, L, Rs, Rsi, Psi, R2, R2i : Real;
Im, Ir, Ir2, Ilast, Io : Real;
TempHi, TempLow, TempStep : Real;
I                  : Integer;
Okay, FirstPass   : Boolean;

```

```
Procedure SetUp;
```

```
Begin
```

```

  ClrScr;
  Write ('High Temperature = ? ');      Readln (TempHi);
  Write ('Low Temperatute = ? ');      Readln (TempLow);
  Write ('Temperature Step = ? ');      Readln
(TempStep);
  Write ('Rs = ? ');                    Readln (Rs);
  Write ('R2 = ? ');                    Readln (R2);
  Vout := -1.25;
  Vg := -2.0;
  W := 50;

```

```

    L := 0.25;
    Psi := 0.0001;
    Rsi := Rs/(1+Psi*(T300-273));
    R2i := R2/(1+Psi*(T300-273));
    Io := 1.0E-4;
End;
```

```
Procedure Calc_TempVar;
```

```

Begin
    Vp := (Q*Nc*Sqr(t)/(2*Es))*(Temp/292);
    Vthv := (K/Q)*Temp;
    Vto := Vthv*Ln(Nc/ni)-Vp;
    Rs := Rsi*(1+Psi*(Temp-273));
    R2 := R2i*(1+Psi*(Temp-273));
End;
```

```
Procedure Im_Solve;
```

```

Var
    Vds, Vgs, Vt :Real;
```

```

Begin
    Vds := Vdd - Vout;
    Vgs := Vss - Vout;
    Im := Io*Exp(((1-Alpha*Vds)/(Ns*Vthv))*(Vgs-
Vto+Gamma*Vds));
End;
```

```
Procedure Ir_Solve;
```

```

Var
    Vr, Vr2 : Real;
Begin
    Vr := Vout-Vss;
    Ir := Vr/Rs;
    Vr2 := 3.3 - Vout;
    Ir2 := Vr2/R2
End;
```

```
Procedure Test_Bias (Var OKAY : Boolean);
```

```

Const
    Tol = 0.0001;
```

```

Var
    Itest : Real;
```

```

Begin
    Itest := Im/(Ir - Ir2) - 1;
```

```

If ABS(Itest) <= Tol Then
  OKAY := True
Else
  Begin (ABS)
    If FirstPass Then
      Begin (FirstPass)
        Vdif := 0.0005;
        If Itest > 0 then
          Vout := Vout + Vdif
        Else
          Vout := Vout - Vdif;
        FirstPass := False;
      End (FirstPass)
    Else
      Begin (Subsequent Passes)
        If Itest > 0 then
          Begin
            If Ilast < 0 then Vdif := Vdif*0.5;
            Vout := Vout + Vdif;
          End
        Else
          Begin
            If Ilast > 0 then Vdif := Vdif*0.5;
            Vout := Vout - Vdif;
          End;
        End; (Subsequent Passes)
      End; (ABS)
      Ilast := Itest;
    End;

Begin
  SetUp;
  Temp := TempLow;
  Writeln ('Temp  Vref      Vout      Vgs      Im
Ir          Ir2');
  Repeat
    OKAY := False;
    FirstPass := True;
    I := 0;
    Calc TempVar;
    Repeat
      I := I + 1;
      Im Solve;
      Ir Solve;
      ( Writeln('Vout=',Vout:5:4,' Im=',Im:8,' Id=',(Ir-
Ir2):8,' Ir=',Ir:8,' Ir2=',Ir2:8);
      If I mod 20 = 0 Then Repeat Until KeyPressed;
      Test Bias (OKAY);
      If KeyPressed then Exit;
    Until (OKAY = True) OR (I > 10000);
    If I > 10000 then
      Begin
        Writeln ('No convergence. Program terminated.');
```

```
        Exit
    End;
    Writeln (Temp:0:0,' ',(Vdd-Vout):5:3,'
',Vout:5:3,' ',(Vg-Vout):4:3,
',Im:10,' ',Ir:10,' ',Ir2:10);
    Temp := Temp+TempStep;
    Until Temp >= TempHi + Tempstep
End.
```

```

(
( SUB _ R 1 R 3 )
(
(
(simulate the subthreshold device, the positive temperature
drift portion)
(of the vref circuit. The program step through a given range
of desire )
(bias current. Temp high, temp low and temp Step are preset
)
( input : Desire Vgs
)
( output: R1, R3, Icoeff, Im
)

```

```
($F20)
```

```
Program SUB_R1R3;
```

```
Const
```

```

Es      = 1.1599E-12;
Q       = 1.60218E-19;
K       = 1.3806E-23;
t       = 6.6E-6;
Nc      = 4.0E17;
ni      = 2.0E6;
U300    = 3500;
T300    = 300;
Vdd     = 0.74;
Vss     = -2.0;
Gamma   = 0.07;
Alpha   = 0.046;
Ns      = 1.671;

```

```
Var
```

```

Vthv, Vto, Vp      : Real;
Vout, Vdif         : Real;
Temp, Vgs          : Real;
W, L, R1, R1i, Psi, R2, R2i : Real;
IMin, IMax, IStep  : Real;
Im, I1, I2, Ilast, Io, I : Real;
TempHi, TempLow, TempStep : Real;
J, Last, P         : Integer;
Okay, FirstPass, Init, Skip : Boolean;
Ij                 : Array[1..20] of real;
Data               : Text;
DataFile           : String[14];
StoDataFile        : String[14];
Sequence           : Integer;
SequenceNum        : String[2];

```

```
Label
```

```
Next;
```



```
Procedure SetUp;
```

```
Begin
```

```
  ClrScr;
```

```
  TempHi := 400;   TempLow := 220;   TempStep := 10;
```

```
  IMin   := 1.6E-3;   Imax    := 2.1E-3;   IStep    := 5E-5;
```

```
  Write ('Vgs (must be -ve number) = ?');   Readln
```

```
(Vgs);
```

```
  Write ('Data File Name = ? ');           Readln
```

```
(DataFile);
```

```
  Sequence :=0;
```

```
  SequenceNum := '0';
```

```
  W := 50;
```

```
  L := 0.25;
```

```
  Psi := 0.0001;
```

```
  Io := 1.0E-4;
```

```
End;
```

```
Procedure Temp_300Var;
```

```
Var
```

```
  Vds : Real;
```

```
Begin
```

```
  Vout := Vss - Vgs;
```

```
  Vds := Vdd - Vout;
```

```
  R1 := (Vout-Vss)/I1;
```

```
  R1i := R1/(1 + Psi*(300-273));
```

```
  Im := Io*Exp((1-Alpha*Vds)/(Ns*Vthv)*(Vgs - Vto +  
Gamma*Vds));
```

```
  I2 := (I1-Im);
```

```
  R2 := (3.3-Vout)/I2;
```

```
  R2i := R2/(1+Psi*(300-273));
```

```
End;
```

```
Procedure Calc_TempVar;
```

```
Begin
```

```
  Vp := (Q*Nc*Sqr(t)/(2*Es))*(Temp/292);
```

```
  Vthv := (K/Q)*Temp;
```

```
  Vto := Vthv*Ln(Nc/ni)-Vp;
```

```
  If Not Init Then
```

```
  Begin
```

```
    R2 := R2i*(1+Psi*(Temp-273));
```

```
    R1 := R1i*(1+Psi*(Temp-273));
```

```
  End
```

```
End;
```

```
Procedure Im_Solve;
```

```
Var
```

```
  Vds, Vgs, Vt :Real;
```

```

Begin
  Vds := Vdd - Vout;
  Vgs := Vss - Vout;
  Im := Io*Exp(((1-Alpha*Vds)/(Ns*Vthv))*(Vgs-
Vto+Gamma*Vds));

```

```
End;
```

```
Procedure Ir_Solve;
```

```

Var
  V1, V2 : Real;
Begin
  V1 := Vout - Vss;
  I1 := V1/R1;
  V2 := 3.3 - Vout;
  I2 := V2/R2;
End;
```

```
(*Procedure Test_Bias (Var OKAY : Boolean);
```

```

Const
  Tol = 0.001;
```

```

Var
  Itest : Real;
```

```

Begin
  Itest := Im/(I1 - I2) -1;
  If ABS(Itest) <= Tol Then OKAY := True
  Else
    Begin
      OKAY := False;
      If (ABS(Itest) > 1) Then
Vdif := 0.05;
      If (ABS(Itest) < 1) And (ABS(Itest) >= 0.9) Then
Vdif := 0.01;
      If (ABS(Itest) < 0.9) And (ABS(Itest) >= 0.8) Then
Vdif := 0.005;
      If (ABS(Itest) < 0.8) And (ABS(Itest) >= 0.7) Then
Vdif := 0.001;
      If (ABS(Itest) < 0.7) And (ABS(Itest) >= 0.6) Then
Vdif := 5e-4;
      If (ABS(Itest) < 0.6) And (ABS(Itest) >= 0.5) Then
Vdif := 1e-4;
      If (ABS(Itest) < 0.5) And (ABS(Itest) >= 0.4) Then
Vdif := 5e-5;
      If (ABS(Itest) < 0.4) And (ABS(Itest) >= 0.3) Then
Vdif := 1e-5;
      If (ABS(Itest) < 0.3) And (ABS(Itest) >= 0.2) Then
Vdif := 5e-6;

```

```

      If (ABS(Itest) < 0.2) And (ABS(Itest) >= 0.1) Then
Vdif := 1e-6;
      If (ABS(Itest) < 0.1) And (ABS(Itest) >= 0.05) Then
Vdif := 5e-7;
      If (ABS(Itest) < 0.05) And (ABS(Itest) >= 0.01) Then
Vdif := 1e-7;
      If (ABS(Itest) < 0.01) Then
Vdif := 5e-8;
      If Itest > 0 then
        Vout := Vout + Vdif
      Else
        Vout := Vout - Vdif;
      End;
      Writeln ('Itest=',Itest:10,' Im= ',Im:10,' I1-I2=',(I1-
I2):10,
              ' Vdif= ',Vdif:10,' Vout=',Vout:4:3);
End;*)

```

```

Procedure Test_Bias (Var OKAY : Boolean);

```

```

Const

```

```

  Tol = 0.001;

```

```

Var

```

```

  Itest : Real;

```

```

Begin

```

```

  Itest := Im/(I1 - I2) - 1;

```

```

  If ABS(Itest) <= Tol Then

```

```

    OKAY := True

```

```

  Else

```

```

    Begin (ABS)

```

```

      If FirstPass Then

```

```

        Begin (FirstPass)

```

```

          Vdif := 0.0001;

```

```

          If Itest > 0 then

```

```

            Vout := Vout + Vdif

```

```

          Else

```

```

            Vout := Vout - Vdif;

```

```

            FirstPass := False;

```

```

          End (FirstPass)

```

```

        Else

```

```

          Begin (Subsequent Passes)

```

```

            If Itest > 0 then

```

```

              Begin

```

```

                If Ilast < 0 then Vdif := Vdif*0.5;

```

```

                Vout := Vout + Vdif

```

```

              End

```

```

            Else

```

```

              Begin

```

```

                If Ilast > 0 then Vdif := Vdif*0.5;

```

```

        Vout := Vout - Vdif
    End;
End; (Subsequent Passes)
End; (ABS)
Ilast := Itest;
( Writeln ('Itest= ',Itest:10,' Im= ',Im:10,' I1-I2=
',(I1-I2):10,' I= ',I:4);)
End;

Procedure Store_Data;

Var
    J : Integer;

Begin;
    StoDataFile := DataFile+' '+SequenceNum+'.Dat';
    Assign (Data, StoDataFile);
    Rewrite (Data);
    For J := 1 to Last do
        Writeln(Data, Ij[J]);
    Flush (Data);
    Close (Data);
    Sequence := Sequence + 1;
    Str(Sequence, SequenceNum);
End;

Begin
    SetUp;
    I := Imin;
    Repeat
        Temp := 300;
        I1 := I;
        Init := True;
        Calc TempVar;
        Init := False;
        Temp_300Var;
        Skip := False;
        Temp := TempLow;
        P := 0;
        Write ('I= ',I:8,' Im= ',Im:10,' Vgs= ',Vgs:1:3,' R1=
',R1:4:0,' R2= ',R2:5:0);
        ( Writeln ('Temp  Vref  Vout  Vgs  Im
I1-I2')));
        Repeat
            P := P+1;
            OKAY := False;
            FirstPass := True;
            J := 0;
            Calc TempVar;
            Repeat
                J := J + 1;
                Im Solve;
                Ir Solve;
                Test_Bias (OKAY);

```

```

    If KeyPressed then exit;
Until (OKAY = True) OR (J > 2000);
If J > 2000 then
  Begin
    Writeln (' No convergence. ');
    Temp := TempHi + TempStep;
    Skip := true;
    Goto Next;
  End;
  ( Writeln (Temp:0:0,' ',(Vdd-Vout):5:3,'
',Vout:5:3,' ',(Vss-Vout):4:3,
',Im:10,' ',(I1-I2):10);)
  Ij[P] := Im;
Next:   Temp := Temp+TempStep;
  Until Temp >= TempHi + Tempstep;
  Last := P;
  ( Store Data;)
  If not Skip then
    Writeln ( ' Icoef = ',(Abs(Ij[1]-Ij[Last])/180):10);
    I := I + Istep;
  Until I >= Imax + Istep;
End.

```

```

(
(          C K T S I M          )
(          )
(          )
(          )
Program Circuit3;

Const
  K    = 1.3806E-23;
  Q    = 1.60218E-19;
  Es   = 1.1599E-12;
  Nc   = 4.0E17;
  ni   = 2.0E6;
  t    = 6.6E-6;
  Ido  = 1.0E-4;
  Vdd  = 3.3;
  Vss  = -2.0;
  W1   = 50;
  L1   = 0.25;      L2 = 0.25;
  Alpha = 0.046;
  Ns   = 1.671;
  Gamma = 0.07;      (Vds Coefficient of Isub)
  Lambda = 0.05;
  Theta = 2.2;
  Psi  = 0.0001;      (Temperature Coefficient of
resistor)
  T300 = 300;
  U300 = 3500;

Var
  Vo, V1, V2          : Real;
  Io, I1, I2, I3     : Real;
  Ro, R1, R2, R3     : Real;
  Vthv, Vbi, Vp, Vto, Vt : Real;
  Roi, R1i, R2i, R3i : Real;
  Ilast, Ibias, Vbias : Real;
  Vdif, Idummy       : Real;
  Temp, TempHi, TempLo, TempStep : Real;
  Beta, W2           : Real;
  FirstPass, Okay    : Boolean;
  Pass, Dummy, Converge : Boolean;
  C, Last            : Integer;
  Data               : Text;
  DataFile           : String[12];
  StoDataFile        : String[16];
  Vref               : Array [1..200] of
Real;

Procedure SetUp;

Begin
  ClrScr;
  ( Write ('High Temperature = ? ');      Readln
(TempHi);

```

```

    Write ('Low Temperature = ? ');           Readln
(TempLo);
    Write ('Temperature Step = ? ');         Readln
(TempStep);)
    TempHi := 400; TempLo := 220; TempStep := 10;
    Write ('Ro      = ? ');                   Readln
(Ro);
    Write ('R1      = ? ');                   Readln
(R1);
    Write ('R2      = ? ');                   Readln
(R2);
    Write ('R3      = ? ');                   Readln
(R3);
    Write ('W2      = ? ');                   Readln
(W2);
    Write ('DataFile = ? ');                 Readln
(DataFile);

```

```

    Roi := Ro/(1 + Psi*(T300-273));
    R1i := R1/(1 + Psi*(T300-273));
    R2i := R2/(1 + Psi*(T300-273));
    R3i := R3/(1 + Psi*(T300-273));
End;

```

```

Procedure Initial_Guess;

```

```

Begin
    Vo := 0.74;
    V1 := -1.25;
    V2 := 0.0;
End;

```

```

Procedure Calc_TempVar (Var Vthv, Vto      : Real;
                        Var Ro, R1, R2, R3 : Real);

```

```

Begin
    Vthv := (K/Q)*Temp;
    Vbi  := Vthv*Ln(Nc/ni);
    Vp   := ((Q*Nc*Sqr(t)/(2*Es))*(Temp/292));
    Vto  := Vbi - Vp;

    Ro   := Roi*(1 + Psi*(Temp-273));
    R1   := R1i*(1 + Psi*(Temp-273));
    R2   := R2i*(1 + Psi*(Temp-273));
    R3   := R3i*(1 + Psi*(Temp-273));
End;

```

```

Function Tanh (X : Real) : Real;

```

```

Var
    A, B : Real;

```

```

Begin
  A := Exp(X);
  B := Exp(-X);
  Tanh := (A-B)/(A+B);
End;

```

```

Procedure Calc_Ibias ( Branch : Integer;
                      Var Ir, Im : Real;
                      V : Real);

```

```

Var
  Vds, Vgs : Real;
  Ip, I1, I3 : Real;

```

```

Begin
  Case Branch of
    0 : Begin
          Ir := (Vdd - V)/Ro;
          Im := 0.0;
        End;
    1 : Begin
          Vds := Vo - V;
          Vgs := Vss - V;
          Im := Ido*Exp((1-Alpha*Vds)/(Ns*Vthv)*(Vgs-
Vto+Gamma*Vds));
          I1 := (V - Vss)/R1;
          I3 := (Vdd - V)/R3;
          Ir := (I1 - I3);
        End;
    2 : Begin
          Vgs := 0.0 - V;
          Vds := Vo - V;
          Ip :=
(W2/L2)*(Sqr(Q*Nc*t)*t*U300*T300/Temp)/(6*Es);
          Beta := Ip/Sqr(Vp);
          Vt := Vto - Gamma*Vds;
          Im := Beta*Sqr(Vgs-
Vt)*(1+Lambda*Vds)*Tanh(Theta*Vds);
          Ir := (V-Vss)/R2;
        End;
  End;
End;

```

```

Procedure Test_Bias ( Ir, Im : Real;
                    Var Vbias : Real;
                    Var Okay : Boolean);

```

```

Const
  Tol = 0.0005;

```



```

Var
  Itest : Real;

Begin
  Itest := Abs(Ir/Im) - 1;
  If Abs(Itest) <= Tol Then
    Okay := True
  Else
    Begin
      If FirstPass then
        Begin (FirstPass)
          Vdif := 0.0005;
          If Itest > 0 then
            Vbias := Vbias - Vdif
          Else
            Vbias := Vbias + Vdif;
          FirstPass := False;
        End (FirstPass)
      Else
        Begin (Subsequent Passes)
          If Itest > 0 then
            Begin
              If Ilast < 0 then Vdif := Vdif*0.5;
              Vbias := Vbias - Vdif;
            End
          Else
            Begin
              If Ilast > 0 then Vdif := Vdif*0.5;
              Vbias := Vbias + Vdif;
            End;
          End; (Subsequent Passes)
        End; (Abs(Itest))
      Ilast := Itest;
    End;
  End;

```

```

Procedure Set_Bias (Branch : Integer;
  Var I, V : Real;
  Var Converge : Boolean;
  Var Flag : Boolean);

```

```

Var
  Im, Ir, Io : Real;
  J : Integer;

```

```

Begin
  Vbias := V;
  Ibias := I;
  Okay := False;
  FirstPass := True;
  J := 0;
  Repeat
    J := J + 1;

```

```

Case Branch of
  0 :   Begin
        Calc_IBias (0, Io, Idummy, Vbias);
        Test_Bias ((I1+I2), Io, Vbias, Okay);
        Ibias := Io;
      End;
  1 :   Begin
        Calc_IBias (Branch, Ir, Im, Vbias);
        Test_Bias (Ir, Im, Vbias, Okay);
        Ibias := Im;
      End;
  2 :   Begin
        Calc_IBias (2, Ir, Im, Vbias);
        Test_Bias (Ir, Im, Vbias, Okay);
        Ibias := Im;
      End;
End;
Until (Okay) Or (J >10000);
If J > 10000 then
  Begin
    Writeln ('No Convergence in branch ',Branch:2, '.
Program Terminated');
    Converge := False;
  End;
  If J = 1 then Flag := True;
  I := Ibias;
  V := Vbias;
End;

Procedure Store_Data;
Var
  I : Integer;

Begin
  StoDataFile := DataFile+'.Dat';
  Assign(Data, StoDataFile);
  Rewrite(Data);
  For I := 1 to Last Do
    Writeln (Data, Vref[I]);
  Flush (Data);
  Close (Data);
End;

Begin
  SetUp;
  Initial_Guess;
  Writeln('Temp  Vref  Vo      V1      V2      Io
I1      I2');
  Temp := TempLo;
  Pass := False;
  Converge := True;
  C := 0;
  Repeat (Temperature loop)

```

```

    Calc TempVar (Vthv, Vto, Ro, R1, R2, R3);
    C:=C+ 1;
    Repeat      (Bias Setting Loop)
      Set Bias (1, I1, V1, Converge, Dummy);  If Not
Converge then Exit;
      Set Bias (2, I2, V2, Converge, Dummy);  If Not
Converge then Exit;
      Set Bias (0, Io, Vo, Converge, Pass);    If Not
Converge then Exit;
      If KeyPressed then exit;
      Until Pass = True;
      Vref[C] := (Vdd-Vo);
      If V2 > 0 Then
        Writeln(Temp:0:0,' ', (Vdd-Vo):5:4,' ', Vo:4:3,'
',
                V1:4:3,' ', V2:4:3,' ', Io:10,' ',
I1:10,' ', I2:10)
      Else
        Writeln(Temp:0:0,' ', (Vdd-Vo):5:4,' ', Vo:4:3,'
',
                V1:4:3,' ', V2:4:3,' ', Io:10,' ',
I1:10,' ', I2:10);
      Temp := Temp + TempStep;
      Until Temp >= TempHi + TempStep;
      Last := C;
      Store_Data;
End.

```