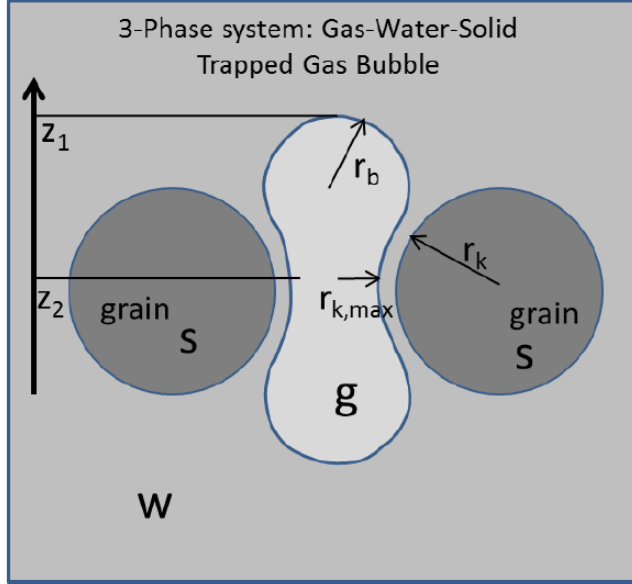


## Supplementary Material

### S1: Thermodynamical argument:

#### Gas bubble surrounded by intergranular capillary-held water and a thick water film



**Figure S1** Trapped gas bubble surrounded by intergranular capillary-held water and a thick water film.

(i) Assumption: The glass beads sediment is completely surrounded by intergranular capillary-held water and a thick, coherent (= continuous) water film (normal water phase with same density and viscosity as the bulk water phase).

(ii) For a stable trapped gas bubble shown in Fig. S1 the gas pressure inside the bubble has to be constant:

$$p_g(z_1) = p_g(z_2) . \quad (S1)$$

With

$$p_g(z) = p_c(z) + \rho_w g \cdot z, \quad (S2)$$

one obtains the *thermodynamic stability condition*:

$$p_c(z_2) - p_c(z_1) = p_c(z) + \rho_w g(z_1 - z_2) \cong \rho_w g \cdot r_k \geq 0, \quad (S3)$$

where the equality sign stands for  $g = 0$ , i.e. for a horizontal gas bubble and  $r_k$  denotes the grain radius.

(iii) Calculation of the capillary pressure by the Young-Laplace equation yields:

$$p_c(z_1) = 2\gamma_{g,w}/r_b \cong 2\gamma_{g,w}/r_{k,max} \quad (S4a)$$

$$p_c(z_2) = \gamma_{g,w} (1/r_{k,max} - 1/r_k) \quad (S4b)$$

( $r_b$  – bubble radius,  $\gamma_{g,w}$  – surface tension or excess free energy).

(iii) Inserting (S4) into (S3) yields a negative expression for the difference of the capillary pressures and therefore a contradiction to assumption (i), namely:

$$p_c(z_2) - p_c(z_1) = -\gamma_{g,w}/r_k (1 + 1/\xi_{max}) < 0 \quad (S5)$$

with  $r_{k,max} = \xi_{max} \cdot r_k$ .

(iv) Conclusion: The result (S5) can be interpreted in two ways: (i) If there exists a *stable* trapped gas bubble with  $r_b > r_{k,max}$  a surrounding thick water film is thermodynamically not possible. (ii) If there exists a thick water film, then trapped gas bubbles with  $r_b > r_{k,max}$  are thermodynamically *unstable*. Since about 50% of all trapped gas bubbles (see Table S1) have a radius larger than  $r_{k,max}$  and the trapped gas bubbles exhibit a negative curvature shown in Fig. 4, a complete wetting of the whole sediment by intergranular capillary-held water and thick water films is thermodynamical not possible.

(v) Disjoining pressure and augmented Young-Laplace equation

If we add an additional repulsive disjoining pressure to the capillary pressure at  $z_2$  we obtain the augmented Young-Laplace equation:

$$\tilde{p}_c(z_2) = p_c(z_2) + \Pi(h), \quad (S6)$$

where  $\Pi(h)$  denotes the short-ranged disjoining pressure, and  $h$  the film thickness. Inserting (S6) into (S3) yields:

$$\Pi(h_{equ}) = \frac{\gamma_{g,w}}{r_k} \left(1 + \frac{1}{\xi_{max}}\right) + \rho_w g r_k \cong 400 \text{ Pa} , \quad (S7)$$

with  $\gamma_{g,w} = 73 \text{ mN/m}$ ,  $r_k = 0.5 \text{ mm}$ , and  $\xi_{max} = 0.6$  (see Geistlinger et al., 2006). Physically, (S7) means that a new mechanical equilibrium has been established at the gas-water interface for a disjoining pressure of about 400 Pa (see Fig. 3 Disjoining pressure isotherm). In order to obtain a rough estimate of the relevant scale of the equilibrium film thickness  $h_{equ}$  we calculate the disjoining pressure by van der Waals forces only (for details see Safran, 1997):

$$\Pi_{vdW}(h) = \frac{-A_{123}}{6\pi h^3} , \quad (S8)$$

with the Hamaker constant  $A_{123} = -1.3 \times 10^{-20} \text{ J}$  (French, 2000). Inserting (S8) into (S7) yields the relevant scale for the equilibrium film thickness of about 12 nm, i.e. the new equilibrium leads to a stable thin adsorbed water film.

(viii) What about incoherent, *discontinuous thick water films*? They are thermodynamically possible?

According to the *Second Law of Thermodynamics* the system at thermodynamic equilibrium tries always to find it minimal *Free Energy*. We compare the *Free Energy* of a thick film (thickness =  $\delta$ ) that covers a grain and a triangular pendular ring (inner radius = 0, outer radius =  $r_a$ ). The boundary condition of equal phase volume yields:

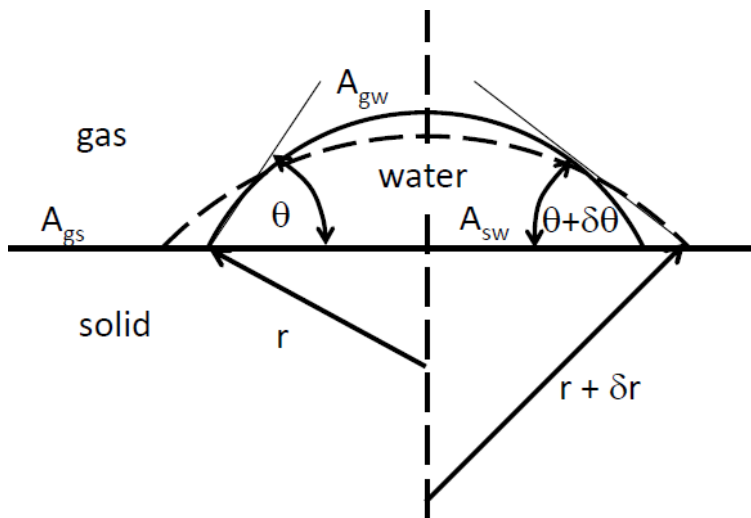
$$r_a(\delta) = \sqrt[3]{\frac{4}{\sqrt{3}} \cdot \{(r_k + \delta)^3 - r_k^3\}} \quad (\text{S6})$$

The difference of the *Free Energy* considering only the gas-water *Excess Free Energy* is

$$\Delta F = \gamma_{g,w} \cdot 4\pi \{(r_k + \delta)^2 - r_a^2(\delta)/\sqrt{3}\}. \quad (\text{S7})$$

Calculating  $\Delta F$  for  $r_k = 0.5$  mm (1mm-GBS), yields for film thicknesses  $\delta < r_k$  positive values for  $\Delta F$ . Hence, the thick film will draw back to a pendular ring, since its *Free energy* is smaller, i.e. incoherent thick films that cover a grain are thermodynamically not stable!

## S2: Thermodynamics of Interfaces: Calculation of the Free Energy



**Figure S2** Spreading of a thick water film (circular cap) from contact angle  $\theta$  to  $\theta + \delta\theta$ .

(i) We consider a spherical curved water film with a circular-cap geometry shown in Fig. S2 with the following boundary lines (or 2D-interfaces):

$$A_{g,w} = 2r\theta, \quad (\text{S9})$$

$$A_{s,w} = 2r \cdot \sin(\theta), \quad (\text{S10})$$

and the area or 2D-volume of the water phase:

$$V_w = r^2(\theta - \sin(2\theta)/2), \quad (\text{S11})$$

(ii) An increase of the g-w-interface by  $dA_{g,w}$ , will increase the *Free Energy* of the system by

$$dF_{g,w} = \gamma_{g,w} \cdot dA_{g,w}$$

and

$$dF_{s,w} = \gamma_{s,w} \cdot dA_{s,w},$$

where  $\gamma$  [Nm/m] denotes the *Excess Free Energy*. Physically, the increase is caused by the loss of binding energy, i.e. water molecules from the phase volume (binding energy  $\sim 12 \text{ } \epsilon$  for face-centered coordination) lose  $\sim 6 \text{ } \epsilon$  of their binding energy (= negative energy!), if they reach the surface.

(iii) The system wins binding energy, if the g-s-interface  $dA_{s,g}$  is decreased, since water molecules in general are stronger bounded at the solid surface than gas molecules, i.e.:

$$dF_{s,g} = -\gamma_{s,g} \cdot |dA_{s,g}|. \quad (\text{S13})$$

(iv) The system at thermodynamic equilibrium possesses a minimal *Free Energy*, therefore holds:

$$dF = \gamma_{g,w} \cdot dA_{g,w} + \gamma_{s,w} \cdot dA_{s,w} - \gamma_{s,g} \cdot |dA_{s,g}| = 0. \quad (\text{S14})$$

(v) Boundary condition: The volume of the water phase,  $V$ , do not change.

$$dV = 0. \quad (\text{S15})$$

With (S11) and (S15) we obtain:

$$\delta\theta = -2/3 \cdot \theta/r \cdot \delta r. \quad (\text{S16})$$

(vi) We consider the geometry of a 2D-circular cap and calculate the changes of the interfaces (z-dimension is not considered, i.e. one has to multiply each expression by  $z_0$  to obtain the right dimension):

$$dA_{g,w} = 2/3 \cdot \theta \cdot \delta r,$$

$$dA_{s,w} = (2 \cdot \sin(\theta) - 4/3 \cdot \theta \cdot \cos(\theta)) \cdot \delta r = B(\theta) \cdot \delta r. \quad (\text{S17})$$

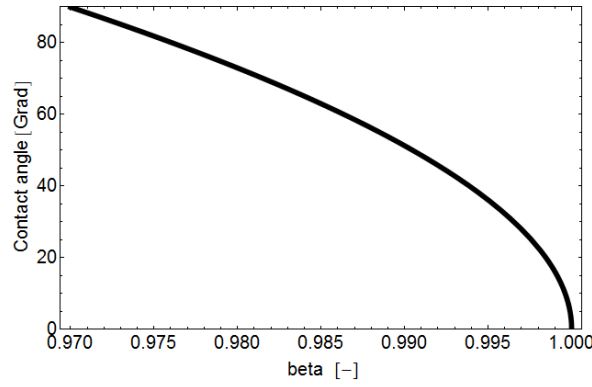
(vii) Inserting of (S17) into (S14) yields the following implicate equation for the contact angle in thermodynamic equilibrium:

$$\theta - \frac{3}{2} \cdot \beta \cdot B(\theta) = 0, \quad (\text{S18})$$

where  $B(\theta)$  is defined in Eq.(S17) and where we have introduced the wetting parameter

$$\beta = \frac{\omega}{\gamma_{g,w}}, \quad (\text{S19})$$

with  $\omega = \gamma_{s,g} - \gamma_{sw}$ . In Fig. S3 we show the sensitive dependency of the contact angle on the wetting parameter  $\beta$  for partial wetting, i.e. for  $0 \leq \theta \leq 90^\circ$ .



**Figure S3** Contact angle versus wetting parameter  $\beta$ .

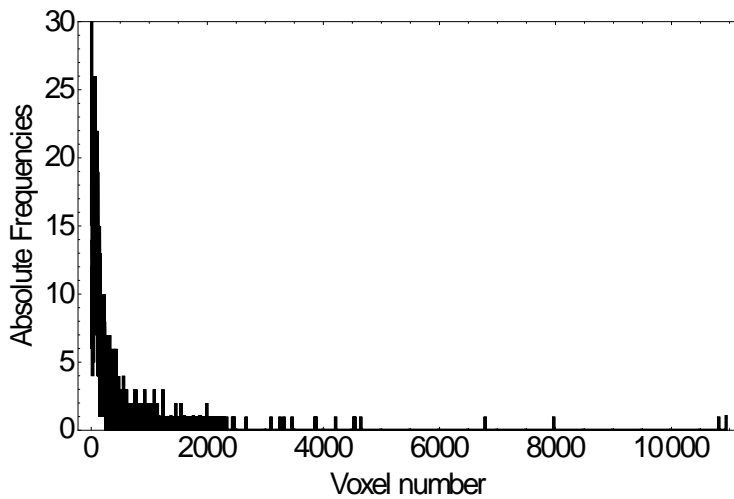
Complete wetting occurs, if  $\beta \geq 1$ , i.e. the radius tends to infinity according to

$$r(\theta) = \sqrt{\frac{r_0^2}{(2\theta - \sin(2\theta))}}, \quad (\text{S20})$$

with  $r_0 = r(\pi/2)$ .

(viii) Under the assumption that the interaction of gas molecules with the solid surface is of similar order of magnitude as the interaction of NAPL-molecules (like Toluene; see Pan et al., 2007) with the solid surface, we can consider  $\omega$  as constant or at least as a small increasing function compared to  $\gamma_{\text{NAPL},w} = \gamma_{g,w} - \gamma_{g,\text{NAPL}} \approx (73 - 29) \text{ mN/m}$ . Therefore, we obtain a larger  $\beta$ -value and according to Fig. S3 a smaller contact angle. Since the area of the fluid-fluid interface is inverse proportional to the contact angle, we anticipate a larger interfacial area for the gas-water system as for the NAPL-water system, i.e. the NAPL-w-interface will extend more than the g-w-interface in thermodynamic equilibrium.

**S3: Complete histogram with noisy voxels (Voxel-Nr: 1 -10) for experiment 7.**



**Figure S4** Histogram of unique objects (gas cluster with a certain voxel number) for experiment 7.

**S4 Cluster statistics, bubble-size distribution, and pore-size distribution for 2<sup>nd</sup> series of experiments (3 experiments under same WT-rise)**

**Cluster statistics**

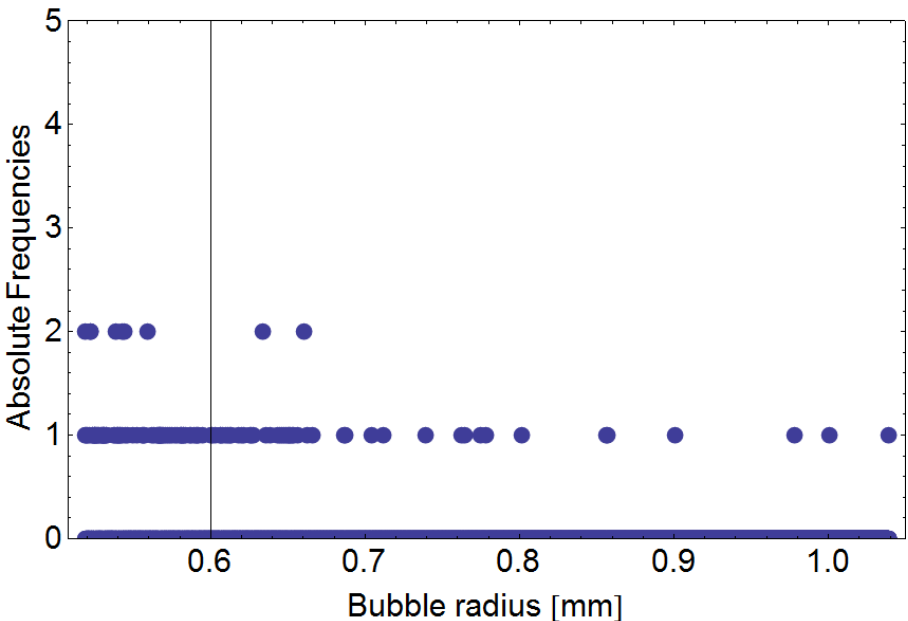
**Table S1** Cluster statistics (sp – single-pore trapped gas bubbles with  $r_b < r_{k,max}$ ; mp – multipore-trapped gas bubbles with  $r_{k,max} < r_b < r_k$ ; and l – large trapped gas bubbles; N – number of bubbles; V – gas volume).

Experiment	N <sub>tot</sub>	N <sub>sp</sub> [%]	N <sub>mp</sub> [%]	N <sub>l</sub> [%]	V <sub>sp</sub> [%]	V <sub>mp</sub> [%]	V <sub>l</sub> [%]
7	3695	53	37	10	16	40	44
8	3687	51	38	11	16	42	42
9	4445	50	38	12	12	35	53

**Bubble-size distribution**

**Table S2** LogNormal-Bubble-size distribution: Mean bubble radius and SDV.

Experiment	Mean radius [mm]	SDV [mm]
7	0.24	0.07
8	0.24	0.07
9	0.23	0.08



**Figure S5** Bubble-size distribution for  $r_b > r_k$  (experiment 7).

In Figure S5 the bubble-size distribution is shown for larger bubble radii  $r_b > r_k$ . Up to  $r_b = 0.65\text{mm}$  the distribution is nearly uniform; and then rather sparse with only 14 trapped gas bubbles.

## Pore-size distribution

**Table S3** Pore-size distribution. Mean radius and SDV for the Normal (column 2 and 3) and the LogNormal (column 4 and 5) pore-size distribution.

Experiment	Mean [mm]	SDV [mm]	Mean [mm]	SDV [mm]
7	0.162	0.057	0.175	0.063
8	0.167	0.060	0.181	0.063
9	0.170	0.060	0.181	0.063

## S5 Experimental verification of static bubble distribution

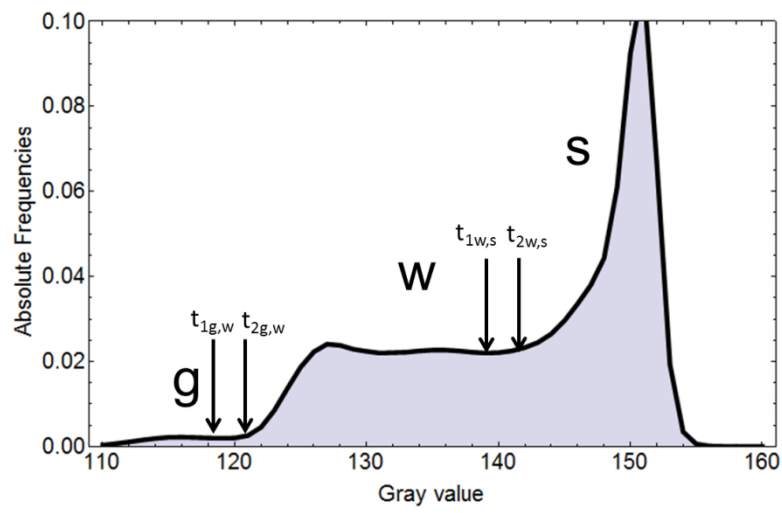
In order to proof that the trapped gas phase is static and will not dissolved during the experiment, we conduct an experiment for a 0.7mm-GBS ( $d_{50} = 0.7\text{mm}$ , packing density 1.56 g/mL, porosity = 0.37) for a WT-velocity of 0.5 cm/min that is equal to that of the second experimental series (exp. 7 -9). The CT-images were taken after 3 different times, 20 min, 3h, and 24 h. The evaluated quantities are listed in Table S4.

**Table S4** Porosity, volumetric gas content, total surface and gas-water for 3 different times after WT-rise.

Time	Porosity [ - ]	Error <sup>#</sup> [ % ]	Gas content [ - ]	$a_g$ [ 1/mm ]	$a_{gw}$ [ 1/mm ]
20 min	0.386	4	0.0136	0.170	0.161
3 h	0.387	5	0.0138	0.165	0.156
24 h	0.385	4	0.0136	0.171	0.161

## S6 Histogram of the whole original image of experiment 7.

Fig. S5 shows the complete tri-modal histogram of the original image of experiment 7 indicating the different phases and the threshold pairs  $(t_{1g,w}, t_{2g,w})$  and  $(t_{1w,s}, t_{2w,s})$  for segmentation of the gas phase and water phase and the water phase and the solid phase, respectively.



**Figure S6** Histogram of the complete CT-image of experiment 7.