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Uncertainty to Uncertainty in Calculated Reactor

Decay Power

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Abstract approved:

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The uncertainty in decay energy for those fission products which contribute significantly to reactor shutdown power was evaluated. The methodology used assigned significantly larger uncertainties for data which were theoretically predicted than it did for experimentally determined data. The uncertainty was modeled as an increasing function of distance from beta stability for both theoretical and experimental data.

The evaluated data were used in the ROPEY summation code to estimate the uncertainty in reactor decay heat due to the fission product decay energies. The uncertainty in reactor shutdown power after a 100-day irradiation was found to be about 8% immediately after shutdown. This uncertainty decreases to about 2% at shutdown times greater

than 100 seconds. This is in substantial agreement with results of Schmittroth and Schenter.<sup>(5)</sup> The decay energy uncertainty for short cooling times is dominated by uncertainty in the theoretically predicted data.

The Contribution of Fission Product  
Decay Energy Uncertainty to Uncertainty  
in Calculated Reactor Decay Power

by

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THE CONTRIBUTION OF FISSION PRODUCT  
DECAY ENERGY UNCERTAINTY TO UNCERTAINTY  
IN CALCULATED REACTOR DECAY POWER

I. INTRODUCTION

1.1 The After-Heat Problem

Many heavy elements fission when they are bombarded with neutrons, releasing a relatively large amount of energy essentially immediately after each fission event occurs. Each fission also produces two (or sometimes three) fission fragments (or fission products) and several neutrons. The fission fragments are produced in a "spectrum" which includes over 800 nuclides, i.e., the mass and charge numbers of the fission fragments and their nuclear states can be predicted by a probability density function. Most of the fission products are radioactive with half lives ranging from milliseconds to months (seven fission products have half lives greater than one year and none of large yield have half lives greater than 100 years). It is the energy released by radioactive decay of the fission products (referred to here as "decay heat") which causes a nuclear (fission) reactor to continue to produce power after it has been shut-down. It is necessary to predict accurately the amount of decay heat produced by a particular reactor with a given power history in order to conduct safety analyses

for that reactor. One method of predicting this decay heat is the "summation method" in which the power being produced by decay of each fission product at time  $t$  after shut-down is calculated, and the reactor shut-down power being produced at time  $t$  is obtained by summing over all of the fission products. The evaluated nuclear data file, ENDF/B-IV, supplies the nuclear decay data which are recommended for use in these calculations. The following paragraphs define the functions which are of interest in decay heat discussions.

If a burst of fission occurs in a reactor at time  $t = 0$ , then the number of atoms of each fission product can be calculated<sup>(1)</sup> as a function of time after the fission burst. Let  $N_i(t)$  be the number of atoms per fission of the  $i^{\text{th}}$  fission product present at time  $t$  after the burst where  $1 \leq i \leq n$ , and  $n$  is the number of fission products which contribute significantly to decay. If  $\lambda_i$  is the decay constant (in  $\text{sec}^{-1}$ ), and  $E_i$  is the average sensible energy of decay for the  $i^{\text{th}}$  fission product (in Mev per decay), then reactor decay power per fission at time  $t$  after a fission burst is given (in MeV/sec-fission) by:

$$H_0(t) = \sum_{i=1}^n \lambda_i N_i(t) E_i \quad (1-1)$$

If the reactor is operated at a steady power of  $P$  fissions/second from time  $t = -T$  to  $t = 0$  and then shutdown,

then for  $t \geq 0$ , reactor shut-down power in MeV/second shut-down power per fission/second operating power is approximated by:

$$H_1(t, T) \approx \int_{-T}^0 H_0(t - t') dt' \quad (1-2)$$

The  $H_1$  function can be expressed as a sum of integrals:

$$H_1(t, T) = \sum_{i=1}^n \lambda_i E_i \int_{-T}^0 N_i(t - t') dt' \quad (1-3)$$

It is useful to define a third function,  $H_2(t, T)$ , which is the decay energy released between time  $t = 0$  and time  $t$ :

$$\begin{aligned} H_2(t, T) &= \int_0^t H_1(t, T) dt \\ &= \sum_{i=1}^n \lambda_i E_i \int_0^t \int_{-T}^0 N_i(t - t') dt' dt \end{aligned} \quad (1-4)$$

$H_2$  has units of MeV shutdown energy per fission/second of operating power. The  $H_2$  function represents the amount of energy available to increase fuel temperature in a loss of coolant situation.

The functions  $N_i$  can be written in a form which can be integrated analytically so that one can define a  $3 \times n$  matrix,  $A(t, T)$ , of functions of  $t$  and  $T$  by:

$$\begin{aligned} A_{0j}(t) &= \lambda_j N_j(t), \\ A_{1j}(t, T) &= \int_{-T}^0 \lambda_j N_j(t - t') dt' \\ A_{2j}(t, T) &= \int_0^t \int_{-T}^0 \lambda_j N_j(t - t') dt' dt \end{aligned} \quad (1-5)$$

If  $A_i$ ,  $1 \leq i \leq 3$  is defined to be the  $i^{\text{th}}$  row of the matrix  $A$ , and the vector  $E$  is defined by  $(E)_j = E_j$ , then the  $H$  functions can be expressed as the vector dot products:

$$H_i(t, T) = \sum_{j=1}^n A_{ij}(t, T) E_j \quad \text{for } 0 \leq i \leq 2 \quad (1-6)$$

## 1.2 Energy Uncertainty Propagation

The data used in summation calculations are evaluated experimental data, or data which are predicted by theoretical models. In either case, some uncertainty as to the exact value of each datum must exist. If one is not certain that the data which he uses are absolutely correct, then there must be uncertainty in any computational result which is obtained using that data. Thus there are two (fairly vague) problems associated with performing calculations which use physical data: the uncertainties in the data must be discovered, and the effect that these uncertainties have on the computational results must be determined. The usual method of handling these problems is to assume that each datum is the mean of a random variable (Appendix I) which has the datum uncertainty for its standard deviation. Once the mean, standard deviation and probability density function are assigned for each datum, then the question of uncertainty propagation through a calculation (in this case the calculation is the computation

of the after-heat functions,  $H_0$ ,  $H_1$  and  $H_2$ ) becomes a simple and well defined mathematical problem: the calculation becomes a function of several random variables, and any such function determines a new random variable which shall be referred to as the "derived" random variable. The result of the calculation can then be defined to be the mean of the derived random variable, and the uncertainty in the answer can be defined to be the standard deviation of the derived random variable. Since the mean of the derived random variable is usually quite well approximated by performing the calculation using the means of the data random variables (this latter quantity is sometimes referred to as the "point value")<sup>(2)</sup> the distinction between the two quantities is usually ignored. When the uncertainty problem is interpreted as above, the techniques of Appendix I can be applied. If one assumes that the random variables describing the average sensible decay energy for each nuclide are normal and independent, then the uncertainty,  $\delta H_i$ , for the after-heat functions is given by:

$$(\delta H_i)^2 = \sum_{j=1}^n [A_{ij}(t, T)]^2 (\delta E_j)^2 \quad (1-7)$$

where  $\delta E_j$  is the standard deviation for the random variable  $E_j$  (this follows from equation 4 of Appendix I). If the energy uncertainties are assumed to be 100% correlated, then the after-heat uncertainty is given by:

$$\delta H_i = \sum_{j=1}^n A_{ij}(t, T) \delta E_j \quad (1-8)$$

Usually the mean and standard deviation of the derived random variable are the only parameters considered in uncertainty analysis; however much more information is available: given any interval of real numbers,  $(a, b)$ , one can determine the probability that the result of the calculation is between  $a$  and  $b$ .

In determining the probability density function for the derived random variable, it may be necessary to use probabilistic techniques (Appendix I). Thus, two problems arise in determining the uncertainty in a specific calculation:

1. determination of reasonable probability density functions for the data, and
2. calculation of an approximation to the probability density function of the derived random variable which is accurate enough to be satisfactory, without requiring an unreasonable amount of computer time.

This thesis provides a methodology which can be used to approach these two tasks, and applies the methodology to the specific problem of determining the uncertainty in the decay heat functions due to uncertainties in average sensible decay energy of the fission products. The next section

reviews an earlier estimate of these uncertainties, Chapter II presents a method for estimating decay energy uncertainties for each fission product (the uncertainties obtained are tabulated in Appendix III), and Chapter III applies the techniques given in Appendix I to the uncertainties of Appendix III to give uncertainty estimates for the after-heat functions.

### 1.3 Other Uncertainty Analyses

Two studies, one by Schmittroth<sup>(4)</sup> and the other by Schmittroth and Schenter,<sup>(5)</sup> have produced estimates of uncertainty in summation decay energy calculations due to uncertainties in the various input parameters.

Schmittroth's study is essentially a sensitivity analysis. For example, if  $\epsilon_i$  are the average energies of decay for the fission product and  $\sigma_i$  are the uncertainties in those decay energies, then the relative uncertainties,  $r_i$ , are defined by:  $r_i = \sigma_i/\epsilon_i$ . In order to determine the sensitivity of the decay energy calculation to energy uncertainties, Schmittroth assumes that the relative energy uncertainties are the same for all fission products (i.e.,  $r_i$  is constant with respect to  $i$ ). He then calculates the relative uncertainty in decay heat due to energy uncertainties,  $R_\epsilon(t) = \sigma_\epsilon(t)/H_0(t)$ , where  $t$  is the time after reactor shutdown,  $H_0$  is the fission burst decay heat function defined in equation (1-1), and  $\sigma_\epsilon$  is the uncertainty in  $H_0$ .

which is due to decay energy uncertainties. Let the subscripts,  $x$  and  $T$ , be used so that  $x$  indicates that the subscripted parameter is due to nuclides for which decay energy data are experimentally determined and  $T$  refers to those nuclides for which decay energy is predicted by theoretical models. Schmittroth assumed that uncertainties due to experimental nuclides are completely uncorrelated, and theoretical uncertainties are completely correlated. He then observed that (due to the linear nature of the summation calculation)  $R_{\varepsilon x}(t)/r_{\varepsilon x}$  is constant with respect to  $r_{\varepsilon x}$  and  $R_{\varepsilon T}(t) = r_{\varepsilon T}$ . The parameters  $R_{\varepsilon}(t)/r_{\varepsilon x}$ ,  $R_{\varepsilon}(t)/r_{\varepsilon T}$ , and  $R_{\varepsilon}(t)/r_{\varepsilon}$  describe the sensitivity of  $H_0(t)$  to uncertainties in fission product decay energies (assuming that all relative average decay energy uncertainties are the same). Schmittroth plots these ratios for cooling times less than  $10^8$  seconds; for these times the ratios are 0.10 or less (e.g., a relative uncertainty in fission product decay energy of 50% would result in an uncertainty of  $H_0(t)$  of 5% or less). Arbitrarily assuming  $r_{\varepsilon} = 0.5$ , Schmittroth calculated uncertainty in  $H_0(t)$  for  $t$  less than  $10^8$  seconds. He concluded that the uncertainty in  $H_0$  due to energy uncertainties is about 6% at  $t = 10$  seconds, greater at shorter cooling times and less at longer cooling times. Uncertainty in  $H_0$  is dominated by theoretical decay energy uncertainties at times less than 100 seconds. Theoretical energy uncertainties become unimportant at

decay times greater than  $10^3$  or  $10^4$  seconds (at longer decay times more of the contributing nuclides have been measured experimentally). At longer decay times, Schmittroth calculated that yield, half life and experimental energy uncertainties contribute about equally to a total  $H_0$  uncertainty of about 1-2%.

The study by Schmittroth and Schenter<sup>(5)</sup> examines fission product decay energy uncertainty directly. The nuclides were divided into three classes:

1. those whose average decay energies are based on detailed photon and beta spectra,
2. those whose Q-value is known but where the split between beta, gamma, and neutrino energy must be estimated, and
3. those whose Q-value must be estimated from nuclear mass systematics.

They then analyzed the data in each class in order to obtain uncertainty estimates.

Uncertainty estimates for the data in class 1 were made by comparing the ENDF/B-IV Q-values with those published by Tobias<sup>(5)</sup> and with the Q-value obtained by adding the average neutrino energy to the average beta and gamma energies. (A procedure for calculating the latter three quantities from spectral data is given in section 2.1.)

The energy split estimate for nuclides in classes 2 and 3 was made by using the formula:

$$\bar{E}_0 = Q[a_0 + b_0 A + C_0 (N-Z) + d_0 P] \quad (1-9)$$

where  $Q$  is the decay  $Q$ -value,  $0$  denotes either beta or gamma,  $A$  is the mass number,  $Z$  is the charge number,  $N$  is the neutron number,  $P$  is the nuclear pairing energy, and the coefficients were determined by a least-squares fit to known data. Schmittroth and Schenter used the RMS deviations from these fits to obtain beta and gamma decay energy uncertainties due to uncertainty in the coefficients of:  $\sigma_\beta = 0.35$  MeV, and  $\sigma_\gamma = 0.70$  MeV. Early calculations used to obtain these values yielded values of  $\sigma_\beta = 0.32$  MeV and  $\sigma_\gamma = 0.65$  MeV. Schmittroth made these early results available and they have been used in Oregon State University after-heat reports<sup>(6)</sup> and in Chapter II of this thesis.

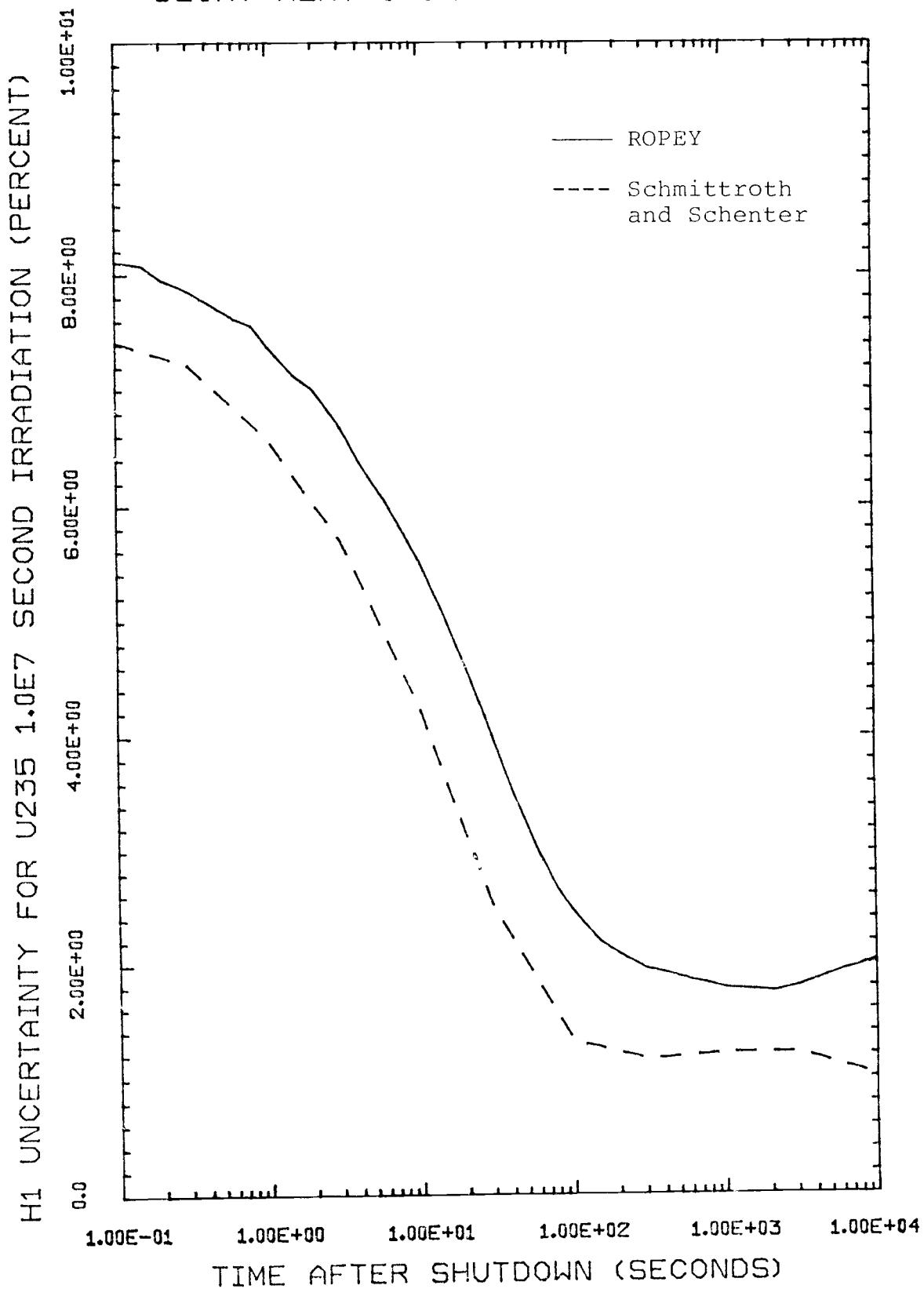
Uncertainty in  $Q$ -value must also be considered in estimating decay energy uncertainty. In order to obtain uncertainty estimates for  $Q$ -values, Schmittroth and Schenter used results from Janecke and Eynon.<sup>(5)</sup> These results indicate that the uncertainty in  $Q$ -value for a nuclide which has the most probable charge number for its mass chain should be about one MeV. Schmittroth and Schenter then reason that since a typical  $Q$ -value near the most probable charge number is about 4.3 MeV, class 3 nuclides should have a relative uncertainty of  $100(1/4.3) = 23\%$ .

They consider these uncertainties to be completely correlated.

Figure 1-1 shows relative uncertainties in the  $H_1$  function as a function of shutdown time for a U-235 reactor after a  $10^7$  second irradiation as calculated by Schmittroth and Schenter. Results obtained at Oregon State University using the program, ROPEY, are shown for comparison.

Schmittroth and Schenter also investigated the contribution to the decay heat uncertainties of the yields and decay constants. Their estimate of yield uncertainty is consistant with Spinrad's.<sup>(1)</sup> They also conclude that, for short cooling times, decay heat uncertainty due to decay constant data is small compared to that of either energy or yield uncertainties.

FIGURE 1-1  
DECAY HEAT UNCERTAINTY COMPARISON



## II. ENERGY UNCERTAINTY DATA

The evaluated nuclear data file, ENDF/B-IV, gives the average sensible energy released per decay for the fission products which contribute significantly to reactor decay heat; however, this file does not list decay energy uncertainties. C. W. Reich of Aerojet Nuclear Company (now EG&G, Idaho) has supplied a source document<sup>(3)</sup> which tabulated experimentally derived nuclear data for many fission products. Using the data in the Reich file it is possible to infer decay energy uncertainties for many (but not all) of the fission products for which experimental data is available. Thus, the fission products of interest can be divided into three groups:

- A. Nuclides for which experimental data and evaluated uncertainties are available.
- B. Nuclides for which experimental data are available but evaluated uncertainties are not available.
- C. Nuclides for which decay energy data are predicted from theoretical models.

The uncertainty in each decay heat function will, therefore, have a component for each of the above groups. A further complication arises because it is possible for a theoretical model to give decay energy predictions which are biased away from the true values with a high degree of correlation. The effect of this possible bias on the decay

energy functions is estimated by postulating an additional "correlated" uncertainty for each nuclide in group C, and propagating that uncertainty through the after-heat calculations along with the "uncorrelated" uncertainties. The problem, then, is to evaluate uncorrelated uncertainties for nuclides in groups B and C, and to evaluate a correlated uncertainty for nuclides in group C.

Section 2.1 shows how group A uncertainties are obtained from the Reich data, sections 2.2 and 2.3 give procedures for evaluating uncertainties for nuclides in groups B and C respectively; section 2.3 also gives a method for evaluating the correlated uncertainties. Appendix II is a copy of the Reich data with estimates of spectral uncertainties, and average decay energy uncertainties inserted.

### 2.1 Energy Uncertainties Due to Evaluated Experimental Data

Table II-1 illustrates the format of the Reich nuclear data file. The entries in the right hand column are identifier numbers which identify the nuclide for which data is displayed and the type of data which is given on each line. Digits 2 through 4 give the atomic number of the nuclide, digits 5 through 7 give its atomic mass number, and the last digit indicates which metastable state is being considered (0 indicates the ground state). The first digit of the identifier is a code (or "card type") which tells what

Table II-1

42.990	MO		6	CWR	10420990	
PREPARED FOR FILE	10/73				20420990	
REFERENCES	Q- 1973 REVISION OF WAPSTRA-GOVE MASS TABLE				20420990	
	HALF-LIFE: N.E.HOLDEN, CHART OF THE NUCLIDES (1973),				20420990	
	AND PRIVATE COMMUNICATION (SEPT., 1973).				20420990	
	OTHER- M.J.MARTIN AND P.H.BLICHEFT-TGFT, NUCLEAR				20420990	
	DATA TABLES A 3, NOS.1-2, 1 (1970)				20420990	
58.02	0.01	H	2	2	30420990	
1	0	1356.6	1.0	13.7	1.0	40420990
1	1	1214.	1.0	86.3	1.0	40420990
584.74	0.0	186.06	0.0			50420990
1.0		7	1			60420990
215.	1.	0.11	0.01			70420990
352.	1.	0.14	0.01			70420990
476.	1.	18.6	0.6			70420990
596.	1.	0.024	0.014			70420990
685.	1.	0.054	0.006			70420990
94.8.	1.	1.44	0.03			70420990
1214.	1.	40.0	1.1			70420990
1.0		11	0			80420990
40.584	0.002	1.3	0.2	3.87		90420990
140.511	0.006	14.0	0.5	0.119	0.003	90420990
131.06	0.04	6.7	0.2	0.15		90420990
366.4	0.1	1.46	0.04			90420990
411.9	0.5	0.024	0.003			90420990
523.9	0.2	0.054	0.006			90420990
620.7	0.2	0.024	0.004			90420990
733.7	0.1	13.8	0.5			90420990
778.2	0.1	4.8	0.3			90420990
823.1	0.1	0.14	0.01			90420990
981.0	0.2	0.11	0.01			90420990

type of data is contained on the corresponding line.

The meaning of the codes is given in Table II-2 which is copied from reference (3). Notice that provisions are made to list uncertainties for average beta and average gamma energies although these uncertainties are not listed. Techniques for supplying those uncertainties are given in this chapter. The uncertainties obtained are given in Appendix II.

The beta decay energy listed in the first entry of the type 7 cards is the end point energy for each of the measured beta decay modes. The intensity listed in the third entry of the type 7 cards is (when normalized by the first entry in the type 6 card) the percentage of the total decays which should decay with the corresponding end point energy. If the energies are denoted by  $E_{\beta i}$  and the intensities are denoted by  $I_{\beta i}$  where  $1 \leq i \leq n$  and  $n$  is the number of type 7 cards (i.e., the number of beta decay modes measured), and if the normalization factor is denoted by  $F_{\beta}$ , then the average beta energy of decay for the nuclide under consideration,  $E_{\beta}$ , is given by (reference 3, pp. 13-14):

$$E_{\beta} = \frac{1}{100} F_{\beta} \sum_{i=1}^n E_{\beta i} I_{\beta i} f(E_{\beta i}), \quad (2-1)$$

where

$$f(E_{\beta i}) = \frac{1}{4} \frac{10 + 8x + 2x^2}{10 + 5x + x^2} \quad \text{and} \quad x = E_{\beta i}/511$$

The function,  $f$ , estimates the fraction of decay energy not carried away by neutrinos (the neutrino energy does not stay

Table II-2

## Card Format for Input to the Nuclear Decay-Data File

(All energy values are given in keV and all intensities are given in percent of decays.)

CARD TYPE

## 1 NUCLIDE IDENTIFICATION (one card)

*column(s) description*  
 1-3.....Z (Atomic Number) (Right Adjusted)  
 4-6.....A (Mass Number) (Right Adjusted)  
 7.....Isomer tag:  
     Blank (or zero) indicates the ground state;  
     1 indicates the first isomeric state;  
     2 indicates the second isomeric state; etc.  
 31-40.....Number of comment cards to follow (Right Adjusted)

## 2 COMMENT CARDS (any number of cards)

*column(s) description*  
 1-66.....These include any desired comments on the decay information. They should contain the month/year the information was prepared and the references from which it was obtained.

## 3 HALF-LIFE (one card)

*column(s) description*  
 1-10.....Half-life  
 11-20.....Its uncertainty  
 20.....Units for half-life (one letter: S, M, H, D, Y)  
 40.....Number of decay modes of the parent state. [This is equal to the number of decay-mode cards (type 4).]  
 50.....Number of "spectra", or data lists, to follow. (E.g., 0 indicates no data lists, 2 indicates two such lists, etc.)

## 4 DECAY MODES (one card for each mode; any number of cards)

*column(s) description*  
 10.....Mode of decay:  
     1 =  $\beta^-$   
     2 =  $\beta^+$   
     3 = Isomeric transition  
     4 = alpha particle  
     5 = delayed neutron  
     6 = spontaneous fission  
 20.....Is an isomeric state in the daughter nucleus fed?  
     0 = no  
     1 = first isomeric state in daughter is fed  
     2 = second isomeric state in daughter is fed  
     etc.  
 21-30.....Q-value of the decay. For isomeric-transition decay, this will be the energy of the isomeric state.  
 31-40.....Uncertainty (in keV) in this Q-value  
 41-50.....Percentage branching of this decay mode  
 51-60.....Uncertainty in this branching

Note: If both an isomeric state and the ground state in the daughter nucleus are fed in the decay, separate cards for each should be prepared.

CARD TYPE

- 5 AVERAGE ENERGY (one card)
- column(s) description*
- 1-10.....Average beta energy  
 11-20.....Its uncertainty  
 21-30.....Average gamma energy  
 31-40.....Its uncertainty  
 41-50.....Average alpha energy  
 51-60.....Its uncertainty
- 6 INTENSITY NORMALIZATION (one type-6 card to be followed by any number of type-7 cards; any number of such groups)
- column(s) description*
- 1-10.....Normalization factor (absolute intensity / relative intensity) for the list to follow in type-7 cards  
 11-20.....Uncertainty in the normalization factor  
 21-30.....Number of transitions of this type to be listed (right adjusted)  
 40.....Radiation type (same numerical designation as in column 10 of card 4)
- 7 ENERGY AND INTENSITY (one per card in order of increasing energy of each individual transition of the radiation type given on card 6; any number of cards)
- column(s) description*
- 1-10.....Energy of transition (gamma radiation excluded)  
 11-20.....Uncertainty (in keV) of the energy  
 21-30.....Intensity of this transition  
 31-40.....Uncertainty in this intensity value
- 8 GAMMA-RAY DATA (one type-8 card followed by any number of type-9 cards)
- column(s) description*
- 1-10.....Normalization factor (absolute intensity / relative intensity) for the gamma rays listed on the type-9 cards to follow  
 11-20.....Uncertainty in the normalization factor  
 21-30.....Number of gamma rays included in the list. This is equal to the number of type-9 cards to follow. (right adjusted)  
 40.....0, radiation-type designation for gamma radiation
- 9 GAMMA-RAY ENERGY AND INTENSITY DATA (any number of cards, in order of increasing gamma-ray energy)
- column(s) description*
- 1-10.....Gamma-ray energy ( $E_\gamma$ )  
 11-20.....Uncertainty in  $E_\gamma$   
 21-30.....Gamma-ray intensity ( $I_\gamma$ )  
 31-40.....Uncertainty in  $I_\gamma$   
 41-50.....Internal-conversion coefficient, ICC. (Generally given only for isomeric transitions or for highly converted gamma rays.)  
 51-60.....Uncertainty in ICC
- Note: If an isomeric state in the daughter nucleus is fed, do not include in this list any transitions which result from the decay of this daughter isomer.

in the vicinity of the reactor, thus it does not contribute to sensible decay heat).

Thus, if one has uncertainties,  $\delta E_{\beta i}$  and  $\delta I_{\beta i}$ , for all of the end point energies and intensities, and if each end point energy is assumed to be the mean of a random variable with standard deviation the listed uncertainty, then the standard deviation,  $\sigma_{\beta}$ , of the derived random variable (Appendix I) can be approximated by:

$$\sigma_{\beta}^2 \approx \frac{1}{10,000} F_{\beta}^2 \sum_{i=1}^n f^2(E_{\beta i}) [I_{\beta i}^2 \delta E_{\beta i}^2 + E_{\beta i}^2 \delta I_{\beta i}^2] \quad (2-2)$$

The above approximation assumes that the function,  $f$ , is not a strongly varying function of  $E_{\beta i}$ . Probabilistic techniques can also be used to find  $\sigma_{\beta}$  (Appendix I) without making the above assumption. Appendix II includes values of  $\sigma_{\beta}$  obtained using both of the above methods; the agreement between the two methods is quite good.

An analogous calculation is used to find average gamma energy of decay,  $E_{\gamma}$ , and its uncertainty  $\sigma_{\gamma}$ . Let  $E_{\gamma i}$  and  $\delta E_{\gamma i}$  be the gamma decay mode energies and their uncertainties where  $1 \leq i \leq m$  and  $m$  is the number of type 9 cards (i.e.,  $m$  is the number of measured gamma decay modes). If  $F_{\gamma}$  is the normalization constant,  $IC_i$  are the internal conversion coefficients, and  $I_{\gamma i}$  and  $\delta I_{\gamma i}$  relative intensities and intensity uncertainties, then

$$E_{\gamma} = \frac{1}{100} F_{\gamma} \sum_{i=1}^m E_{\gamma i} I_{\gamma i} (1 + IC_i) \quad (2-3)$$

and

$$\sigma_{\gamma}^2 = \frac{1}{10000} F_{\gamma}^2 \sum_{i=1}^m (1 + IC_i)^2 [I_{\gamma i}^2 \delta E_{\gamma i}^2 + E_{\gamma i}^2 \delta I_{\gamma i}^2] \quad (2-4)$$

Appendix II includes the results of these calculations together with probabilistic estimates of  $\sigma_{\gamma}$  for the various nuclides.

## 2.2 Energy Uncertainties Due to Unevaluated Experimental Data

Energy and intensity uncertainties are listed for all of the spectral data for the nuclide illustrated in Table II-1. This uncertainty data is not complete for many of the nuclides listed in the Reich data file (cf. Table II-3). This section gives a method for analyzing the existing uncertainty data and using the results of the analysis to supply estimates for the missing uncertainty data. Tables II-4 through II-7 list various sortings of the uncertainty data which are used to make the estimates. Table II-8 gives the algorithm used to supply the estimates, and Table II-9 lists the decay data for the nuclide of Table II-3 with estimates for the missing uncertainties included. The uncertainties which were supplied by the methods described below are labeled with "\*".

Table II-4 lists the 25 largest relative and absolute uncertainties found in spectral energy or intensity for all spectral lines listed in the Reich file. For example, the

Table II-3

441030	PU	12	RES (GULF)	10441030
PREPARED FOR FILE # 9/73				
REFERENCE# H. FETTERSON ET AL., Z. PHYSIK 233, 260 (1970)				
HALF-LIFE- N.E.HOLDEN, CHART OF THE NUCLIDES (1973) +				
AND PRIVATE COMMUNICATION(SEPT., 1973).				
Q VALUE IS FROM 1973 REVISION OF WAPSTRA-GOVE MASS TABLES.				
GAMMA-RAY ENERGIES ARE WEIGHTED AVERAGE ENERGIES FROM				
TABLE 2 OF REF.				
GAMMA-RAY INTENSITIES AND INTENSITY UNCERTAINTIES ARE TAKEN				
FROM TABLE 1 OF REF., EXCEPT FOR 610.24-KEV GAMMA RAYS, FOR				
THESE GAMMA RAYS, INTENSITY DATA FROM FIG. 4 WERE ALSO USED.				
INTERNAL CONVERSION COEFFICIENTS WERE OBTAINED FROM DATA IN REF.				
BETA-RAY DATA WERE TAKEN FROM FIG. 4 OF REF.				
39.6	0.2	0	1	2
1	1	722.0	3.6	100.
67.53	0.0	490.02	0.0	
1.0		6	1	
111.		0.4		
112.		0.2		
225.		90.		
405.		0.01		
467.		0.25		
722.		3.5		
0.30		10	0	
53.274	0.010	0.384	0.020	2.18
114.65	0.05	0.012	0.005	0.21
241.82	0.13	0.014	0.004	
294.88	0.06	0.284	0.015	
357.27	0.13	0.007		
443.82	0.07	0.402	0.018	
497.080	0.013	100.		
557.09	0.09	0.893	0.035	
618.29	0.19	5.96		
611.53	0.25	0.44		

Table II-4

THE 25 LARGEST RELATIVE AND ABSOLUTE UNCERTAINTIES LISTED  
IN THE AEROJET FILE

UNCERTAINTIES							
BETA				GAMMA			
ENERGY	INTENSITY	ENERGY	INTENSITY	KEV	PERCENT	KEV	PERCENT
400.00	36.70	5.00	200.00	10.00	1.43	37.76	216.30
400.00	23.70	5.00	200.00	8.00	1.42	13.83	142.86
400.00	24.34	3.70	160.87	5.00	1.40	10.00	111.11
400.00	24.59	3.10	180.00	5.00	1.39	7.20	100.00
400.00	24.27	3.00	100.00	5.00	1.22	7.00	100.00
400.00	23.53	3.00	100.00	5.00	1.14	6.50	100.00
400.00	22.46	3.00	100.00	5.00	1.04	6.00	100.00
400.00	21.13	2.20	100.00	3.00	.93	6.00	100.00
400.00	20.65	2.20	100.00	3.00	.87	5.00	100.00
400.00	20.97	2.00	100.00	3.00	.86	5.00	100.00
300.00	18.37	2.00	100.00	3.00	.84	5.00	100.00
300.00	18.52	2.00	100.00	3.00	.73	5.00	100.00
300.00	18.40	2.00	80.00	3.00	.79	+.2+	100.00
200.00	18.38	1.80	80.00	2.00	.73	+.33	100.00
200.00	17.64	1.60	70.41	2.00	.77	+.37	100.00
200.00	17.41	1.60	75.32	2.00	.71	+.26	100.00
200.00	16.50	1.60	65.67	2.00	.66	+.00	100.00
200.00	16.23	1.40	65.67	2.00	.66	3.60	100.00
200.00	16.06	1.30	51.52	2.00	.64	3.46	100.00
200.00	15.56	1.20	50.00	2.00	.64	3.20	100.00
200.00	14.83	1.10	50.00	2.00	.62	3.03	100.00
200.00	14.11	1.10	50.00	2.00	.61	3.05	100.00
200.00	13.57	1.10	50.00	2.00	.60	2.83	100.00
100.00	13.43	1.10	50.00	2.00	.60	2.32	100.00
100.00	13.45	.90	50.00	2.00	.60	2.83	100.00

Table II-5

THE 25 LARGEST RELATIVE AND ABSOLUTE UNCERTAINTIES WITH  
SPECTRAL LINE INTENSITY LESS THAN OR EQUAL TO ONE PERCENT OF  
TOTAL INTENSITY

UNCERTAINTIES					
BETA			GAMMA		
ENERGY KEV	PERCENT PERCENT	INTENSITY	ENERGY KEV	PERCENT PERCENT	INTENSITY
100.00	23.70	.80	200.00	1.43	1.60
100.00	24.34	.80	200.00	1.42	142.80
100.00	24.53	.27	100.00	1.40	111.11
100.00	24.27	.20	100.00	1.39	100.00
100.00	23.53	.20	100.00	1.22	100.00
100.00	23.05	.20	100.00	1.14	100.00
100.00	20.37	.20	100.00	.87	100.00
100.00	13.37	.20	100.00	.86	100.00
100.00	13.52	.17	100.00	.84	100.00
100.00	13.40	.11	80.00	.79	100.00
100.00	17.34	.11	60.00	.73	100.00
100.00	17.41	.10	73.41	.72	100.00
100.00	15.50	.10	75.02	.73	100.00
100.00	16.06	.10	65.87	.68	100.00
100.00	15.56	.10	65.67	.64	100.00
100.00	14.33	.10	51.52	.64	100.00
100.00	13.57	.10	50.00	.62	100.00
100.00	13.49	.10	50.00	.61	100.00
100.00	13.45	.10	50.00	.60	100.00
100.00	13.44	.10	50.00	.60	100.00
100.00	13.27	.10	50.00	.58	100.00
100.00	13.22	.10	50.00	.57	100.00
100.00	12.61	.10	50.00	.56	100.00
100.00	12.37	.10	50.00	.55	100.00
100.00	12.01	.10	50.00	.53	100.00

Table II-6

THE 25 LARGEST RELATIVE AND ABSOLUTE UNCERTAINTIES FOR  
SPECTRAL LINES WITH INTENSITY BETWEEN ONE AND TEN PERCENT OF  
TOTAL INTENSITY

UNCERTAINTIES					
BETA			GAMMA		
ENERGY	INTENSITY		ENERGY	INTENSITY	
KEV PERCENT	PERCENT	PERCENT	KEV PERCENT	PERCENT	PERCENT
400.00	36.70	3.70	160.07	2.00	.93
400.00	22.46	1.60	100.00	2.00	.86
400.00	21.13	1.40	100.00	2.00	.60
400.00	18.33	1.10	46.67	1.50	.39
400.00	16.23	1.10	36.77	1.20	.36
400.00	13.02	.80	24.44	1.10	.33
400.00	11.49	.70	26.13	1.10	.32
400.00	10.98	.70	22.71	1.10	.29
200.00	10.73	.57	16.38	1.00	.28
200.00	3.52	.60	13.92	1.00	.27
200.00	3.14	.41	11.52	1.00	.26
200.00	3.09	.40	11.51	1.00	.26
100.00	3.46	.43	10.07	1.00	.22
100.00	3.03	.40	9.30	1.00	.22
100.00	7.35	.40	8.33	1.00	.22
100.00	7.63	.50	8.33	1.00	.18
100.00	7.52	.37	7.58	1.00	.17
100.00	7.51	.30	7.49	1.00	.15
100.00	7.34	.70	7.22	1.00	.15
100.00	5.97	.30	7.14	1.00	.15
100.00	6.13	.23	7.14	1.00	.15
100.00	6.08	.20	7.14	1.00	.15
100.00	5.45	.19	7.04	1.00	.14
100.00	5.66	.19	6.35	1.00	.14
100.00	5.63	.15	6.67	1.00	.14

Table II-7

THE 25 LARGEST RELATIVE AND ABSOLUTE UNCERTAINTIES FOR  
SPECTRAL LINES WITH RELATIVE INTENSITY GREATER THAN TEN  
PERCENT

UNCERTAINTIES					
BETA			GAMMA		
ENERGY	INTENSITY	PERCENT	ENERGY	INTENSITY	PERCENT
KEV	PERCENT	PERCENT	KEV	PERCENT	PERCENT
400.00	14.11	6.00	27.27	5.00	1.04
400.00	13.43	6.00	13.60	1.00	.71
300.00	13.40	3.10	11.76	1.00	.56
300.00	11.79	3.10	11.70	.80	.40
300.00	10.64	3.00	3.63	.50	.32
200.00	3.95	3.00	2.40	.50	.20
200.00	9.07	2.20	9.20	.50	.23
200.00	8.92	2.20	3.77	.50	.24
200.00	5.93	2.00	3.33	.50	.18
200.00	5.67	2.00	7.21	.50	.17
200.00	5.53	2.00	7.14	.50	.16
100.00	5.43	2.00	5.77	.50	.16
100.00	5.35	1.80	4.66	.50	.15
100.00	5.16	1.60	4.55	.40	.15
100.00	4.92	1.50	4.46	.40	.14
100.00	4.75	1.30	4.35	.40	.14
100.00	4.65	1.20	4.23	.40	.14
100.00	4.41	1.10	4.01	.40	.13
100.00	4.15	1.10	3.96	.30	.13
80.00	4.04	.90	3.61	.30	.13
80.00	3.82	.70	3.47	.30	.12
80.00	3.81	.70	3.23	.30	.12
80.00	3.62	.70	2.81	.30	.11
80.00	3.57	.60	2.44	.30	.11
80.00	3.55	.60	1.65	.30	.11

Table II-8  
Maximum Uncertainties for Spectral Decay Data

Intensity	B E T A		G A M M A	
	Energy keV or %	Intensity %(a) or %(b)	Energy keV or %	Intensity %(a) or %(b)
$I \geq 10\%$	400 or 15	6 or 30	5 or 1	10 or 70
$10\% \geq I \geq 1\%$	400 or 35	4 or 150	5 or 1	4 or 100
$1\% \geq I$	400 or 35	1 or 100	10 or 2	2 or 200

(a) of total intensity

(b) of line intensity

NOTE: The uncertainty to be supplied is either the first entry of the appropriate position or the second multiplied by the datum, whichever is smaller.

Table II-9

441030	RU		12	RES (GULF)	1	441030	
	PREPARED FOR FILE# 973				2	441030	
	REFERENCE# H. PETTERSON ET AL., Z. PHYSIK 233, 260 (1970)				2	441030	
	HALF-LIFE- N.E.HOLDEN, CHART OF THE NUCLIDES (1973) +				2	441030	
	AND PRIVATE COMMUNICATION (SEPT., 1973).				2	441030	
	Q VALUE IS FROM 1973 REVISION OF WAPSTRA-GOVE MASS TABLES.				2	441030	
	GAMMA-RAY ENERGIES ARE WEIGHTED AVERAGE ENERGIES FROM				2	441030	
	TABLE 2 OF REF.				2	441030	
	GAMMA-RAY INTENSITIES AND INTENSITY UNCERTAINTIES ARE TAKEN				2	441030	
	FROM TABLE 1 OF REF., EXCEPT FOR 610.29-KEV GAMMA RAYS, FOR				2	441030	
	THESE GAMMA RAYS, INTENSITY DATA FROM FIG. 4 WERE ALSO USED.				2	441030	
	INTERNAL CONVERSION COEFFICIENTS WERE OBTAINED FROM DATA IN REF.				2	441030	
	BETA-RAY DATA WERE TAKEN FROM FIG. 4 OF REF.				2	441030	
39.6	0.2	0	1	2	3	441030	
	1	1	722.0	3.6	100.	4	441030
67.53	0.0	490.02		0.0		5	441030
	1.0		6	1		6	441030
111.00	38.85 00*	.4000	.0000*			7	441030
112.00	39.20 00*	6.2000	4.0000*			7	441030
225.00	33.75 00*	90.0000	6.0000*			7	441030
405.00	141.75 00*	.0100	.0200*			7	441030
467.00	163.45 00*	.2500	.5000*			7	441030
722.00	252.70 00*	3.5000	4.0000*			7	441030
0.90		10	0			8	441030
53.27	.0100	.3840	.0200	2.1400		9	441030
114.65	.0500	.0120	.0050	.2100		9	441030
241.42	.1300	.0140	.0040			9	441030
284.88	.0600	.2840	.0150			9	441030
357.27	.1300	.0070	.0140*			9	441030
443.82	.0700	.4020	.0180			9	441030
497.08	.0130	100.0000	11.1111*			9	441030
557.09	.0900	.3930	.0350			9	441030
610.29	.1900	5.9600	4.4444*			9	441030
611.53	.2500	.4400	.3800*			9	441030

largest absolute beta endpoint energy uncertainty is 400 keV and the largest relative uncertainty in beta endpoint energy (i.e.,  $100\sigma_\beta/E_\beta$ ) is 36.7%. These maximum uncertainties need not correspond to the same spectral line or even the same nuclide. The largest absolute gamma intensity uncertainty is 37.76% of total intensity and the largest relative gamma intensity uncertainty (i.e.,  $100\sigma_\gamma/E_\gamma$ ) is 206.90%. Tables II-5, II-6, and II-7 are listings of the largest spectral uncertainty data found when attention is restricted to various subsets of the spectral data. Table II-5 lists the 25 largest uncertainties for spectral lines with intensity less than or equal to 1% of total intensity, Tables II-6 and II-7 list uncertainties for lines with relative intensities between 1 and 10%, and greater than or equal to 10% respectively. The expected pattern is found: the more intense spectral lines have been more accurately measured. Table II-8 summarizes this observation and gives an algorithm for estimating uncertainties for those spectral data which do not have evaluated uncertainties: for a given datum an uncertainty is assigned to be either the first entry in the appropriate position in Table II-8 or the second multiplied by the datum, whichever is smaller. Table II-9 shows the result of applying the algorithm to the Ruthenium-103 data given in the Reich file.

Once the spectral uncertainties are supplied for group B nuclides, average beta and gamma energies of decay can be

calculated as they were for group A nuclides. Many of the uncertainties supplied above are quite large compared to the corresponding data; some relative uncertainties are greater than 100%. This means that it is not reasonable to model these data as normal random variables since that model gives the data a high probability of being negative. It also suggests that the derived random variable might be strongly non-normal, in which case the standard deviation as estimated by equations (2-2) and (2-4) cannot be used to infer confidence information (this topic is discussed at the end of Appendix I).

In order to resolve the above questions, data with large relative uncertainties were modeled as beta distributions as described in section 2 of Appendix I. The probabilistic technique of Appendix I was then used to determine the derived density functions for average beta and gamma decay energies. Appendix II compares standard deviations obtained using probabilistic techniques with those obtained using equations (2-2) and (2-4). Agreement between these two methods is good for group B nuclides as it was for group A nuclides. Furthermore, the derived density functions turned out to be very nearly normal. This can be explained by noticing that the spectral data with large uncertainties have small yields. This means that the non-normal spectral data contribute little to average decay energy and have correspondingly little

effect on the derived density function.

### 2.3 Energy Uncertainties Due to Data from Theoretical Models

Most of the decay energy data used in afterheat summation calculations are predicted from theoretical models. In order to estimate the uncertainty in afterheat calculations due to uncertainty in decay energies, it is necessary to examine the possible sources of error in predicting these data. Two sources of error are considered here: a random or uncorrelated error in the decay energies predicted by the model, and a correlated error resulting from a bias in the model which systematically predicted energies too high or too low.

The decay energies listed in ENDF/B-IV were predicted by using nuclear systematics to obtain the atomic masses of the parent and daughter, and subtracting the masses to get the Q-value of the decay. This energy was then apportioned among the gamma, beta and neutrino radiation emitted from the decay according to formulae given by Schmittroth and Schenter (equation 1-9).

Several assumptions are made here in order to obtain uncertainty estimates for group C nuclides:

1. The uncertainty in Q-value,  $\delta Q$ , is assumed to be a function of the difference between the atomic number of the parent nuclide and the atomic

number of the first stable nuclide in the beta decay chain ( $\Delta z$ ).

2.  $\delta Q(0) = 0$  and  $\delta Q(2) \approx 1.3$  MeV [Schmittroth and Schenter,<sup>(5)</sup> and Liaw (reference 7, page 113) have independently concluded that this is a conservative assumption].
3. Correlated and uncorrelated Q-value uncertainties,  $\delta Q_c$  and  $\delta Q_u$ , apportion  $\delta Q(2)$  as follows:  $\delta Q_u(2) = 1.26$  MeV and  $\delta Q_c(2) = 0.26$  MeV.
4. Uncorrelated uncertainties in average beta and gamma decay energy,  $\delta E_\beta$  and  $\delta E_\gamma$ , are at least as large as those uncertainties, 0.32 MeV and 0.65 MeV, due to the least mean squares fitting process (section 1.3, page 9 of this thesis).
5.  $\delta Q_u$  increases linearly with  $\Delta z$ .
6. The predicted masses used in estimating Q-values are consistently in error by a term which is cubic in  $\Delta z$ .

Assumptions 1 and 5 reflect the trend that half life gets shorter as distance from beta stability increases. It is difficult to experimentally measure nuclear parameters for nuclides with short half lives, so as  $\Delta z$  increases there is less experimental verification for our evaluated nuclear data.

The assignment of about one MeV uncertainty for theoretically predicted Q-value was arrived at independently

by the researchers mentioned above by comparing evaluated data with predicted data (where the evaluated data is available). The value of 1.3 MeV used here is a conservative choice.

The uncertainties of assumption 3 apportion the total Q-value uncertainty between a correlated and an uncorrelated component  $[(1.26)^2 + (0.26)^2 = (1.3)^2]$ . The possibility of correlated Q-value uncertainty must be considered; however, the correlation cannot be too strong without showing up when predicted and observed data are compared. No such correlation has been observed. It is assumed here that a correlation would show if the correlated component were greater than 20% of the uncorrelated component.

Assumption 4 utilizes the statistical analysis that Schmittroth and Schenter have done on the evaluated beta decay data. As used here, this is a conservative assumption since it assigns finite uncertainties when  $\Delta z = 0$  and linearly increases uncertainties as  $\Delta z$  increases.

The semi-empirical mass formula, for constant atomic mass number, is essentially a quadratic in  $\Delta z$ , with even-odd correction terms. The addition of a cubic term with coefficient,  $k$ , provides a mechanism for considering bias in Q-value (which increases quadratically with  $\Delta z$ ). The coefficient,  $k$ , should be chosen large enough to accommodate any possible bias, but it cannot be so large that it would disturb the fit of the formula to known masses.

Assumption 3 imposes the appropriate limit on  $k$ . Conservation of mass and energy imposes further constraints on the size of  $k$ , but these constraints are less restrictive than assumption 3.

From assumptions 2, 3, and 5, a formula for  $\delta Q_u$  can be derived:

$$\delta Q_u(\Delta z) = \frac{1.26}{2} \Delta z = 0.63 \Delta z$$

Next, expressions for  $\delta E_\beta$  and  $\delta E_\gamma$  as functions of  $\Delta z$  can be derived. Since

$$E = E_\beta + E_\gamma = Q \left( \frac{E_\beta}{Q} + \frac{E_\gamma}{Q} \right)$$

$\delta E$  can be expressed in the following ways:

$$\begin{aligned} (\delta E)^2 &= (\delta E_\beta)^2 + (\delta E_\gamma)^2 \\ &= (\delta Q)^2 \left( \frac{E_\beta}{Q} + \frac{E_\gamma}{Q} \right)^2 + Q^2 \left[ \left( \frac{\delta E_\beta}{Q} \right)^2 + \left( \frac{\delta E_\gamma}{Q} \right)^2 \right] \\ &= E_\beta^2 \frac{(\delta Q)^2}{Q^2} \left( 1 + \frac{E_\gamma}{E_\beta} \right) + (\delta E_\beta)^2 + E_\gamma^2 \frac{(\delta Q)^2}{Q^2} \left( 1 + \frac{E_\beta}{E_\gamma} \right) + (\delta E_\gamma)^2 \\ &= E_\beta^2 \frac{0.4 \Delta z^2}{Q^2} \left( 1 + \frac{E_\gamma}{E_\beta} \right) + (0.32)^2 + E_\gamma^2 \frac{0.4 \Delta z^2}{Q^2} \left( 1 + \frac{E_\beta}{E_\gamma} \right) + (0.65)^2 \end{aligned}$$

$\delta E_\beta$  and  $\delta E_\gamma$  are defined by:

$$(\delta E_\beta)^2 = E_\beta^2 \frac{0.4 \Delta z^2}{Q^2} \left( 1 + \frac{E_\gamma}{E_\beta} \right) + (0.32)^2 \quad (2-5)$$

and

$$(\delta E_\gamma)^2 = E_\gamma^2 \frac{0.4 \Delta z^2}{Q^2} \left( 1 + \frac{E_\beta}{E_\gamma} \right) + (0.65)^2 \quad (2-6)$$

in order to satisfy  $\delta E^2 = \delta E_\beta^2 + \delta E_\gamma^2$ .

From assumption 6,

$$M(\Delta z) = M_s(\Delta z) + k\Delta z^3$$

where  $M(\Delta z)$  is the actual mass of the nuclide in a mass chain which is  $\Delta z$  charge units from beta stability,  $M_s$  is the predicted mass, and  $k$  is a constant. The  $Q$ -value can then be expressed:

$$Q(\Delta z) = M_s(\Delta z) - M_s(\Delta z - 1) + k[\Delta z^3 - (\Delta z - 1)^3]$$

and the correlated uncertainty in  $Q$ -value can be expressed as:

$$\delta Q_C(\Delta z) = k[\Delta z^3 - (\Delta z - 1)^3].$$

Since  $\delta Q_C(2) = 0.26$  MeV,

$$\delta Q_C(\Delta z) = 0.375[\Delta z^3 - (\Delta z - 1)^3]. \quad (2-7)$$

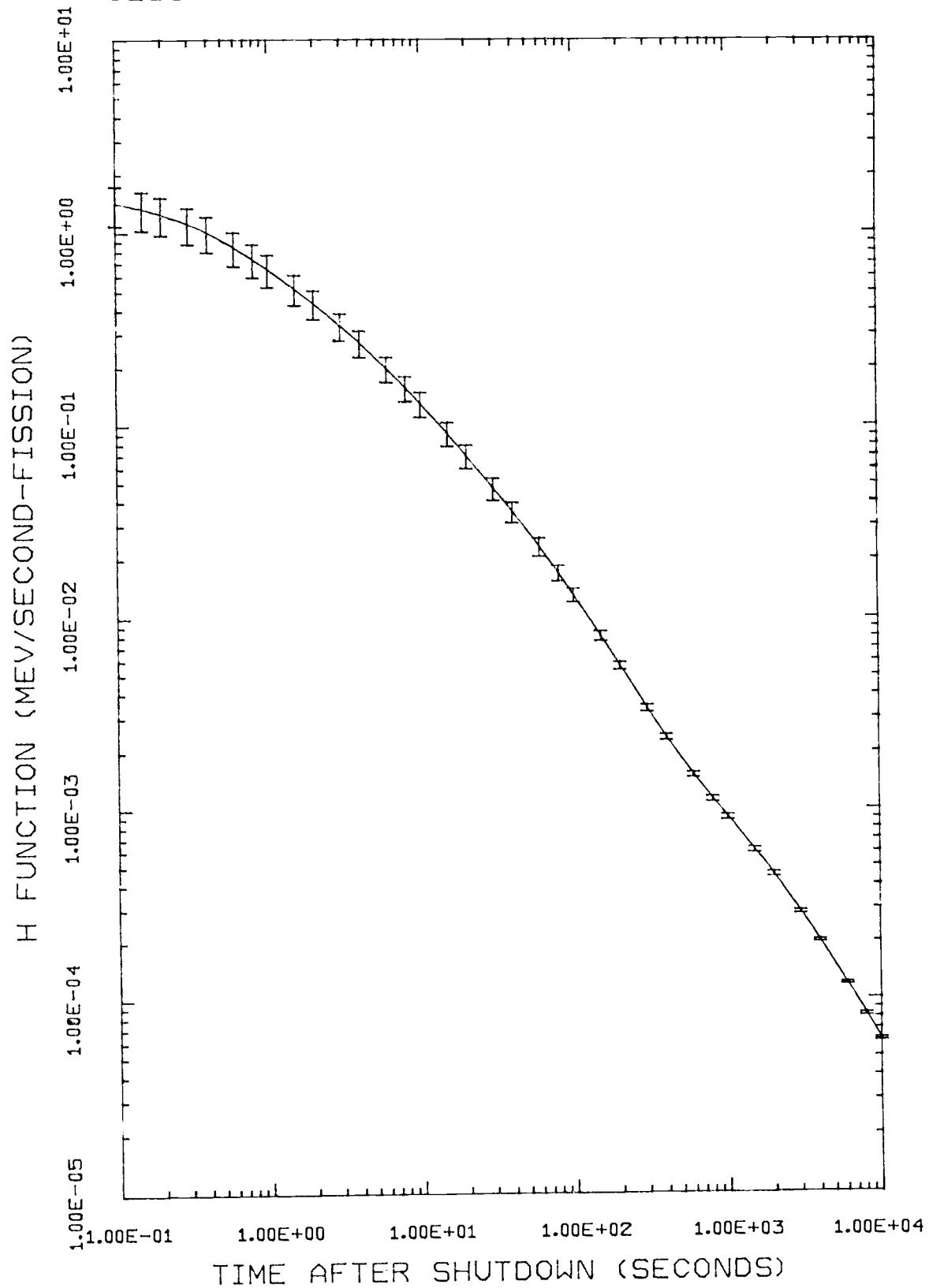
Equations 2-5, 2-6 and 2-7 were used to supply uncertainties for Appendix III when they were not available in Appendix II.

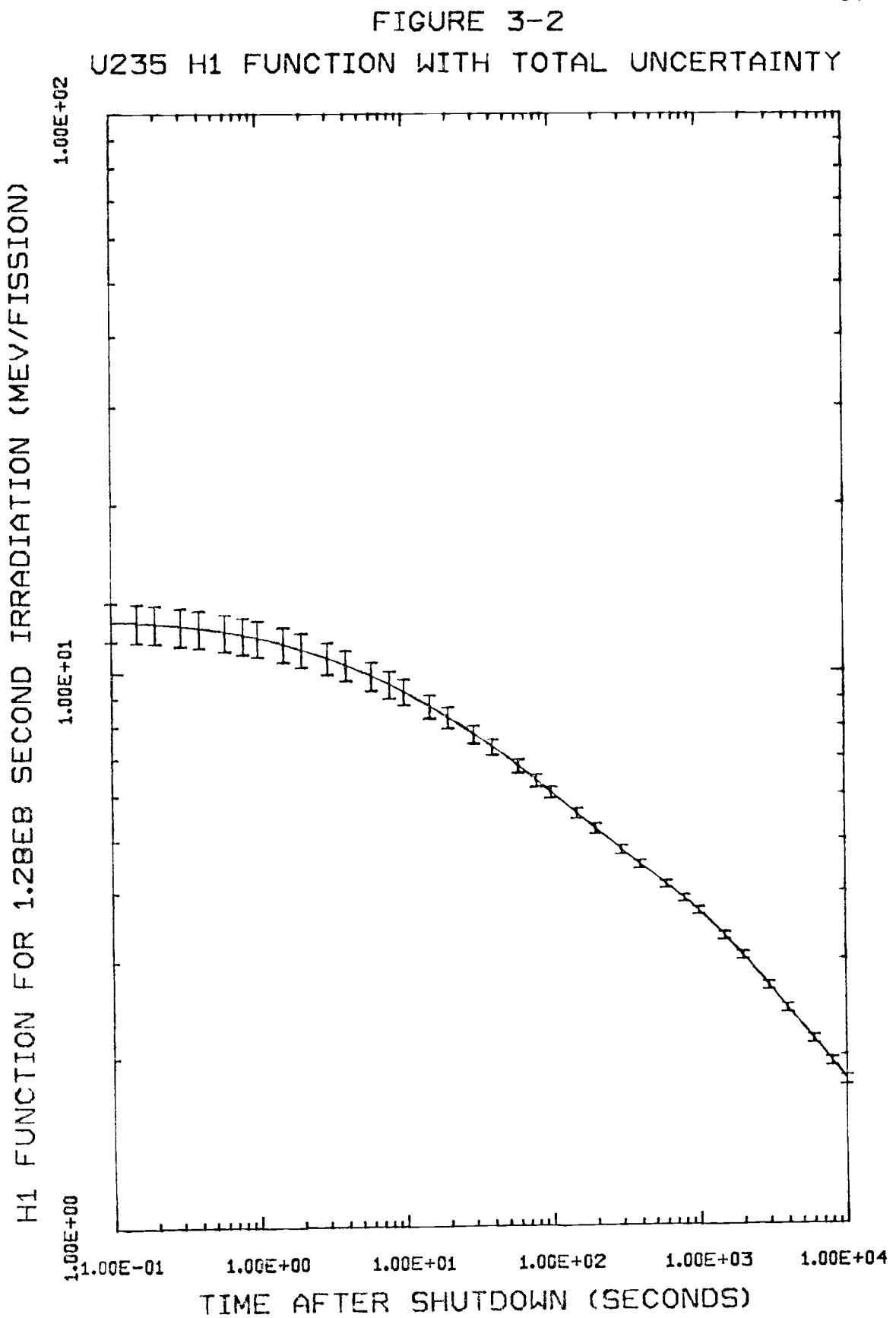
## III. CONCLUSIONS AND DISCUSSION

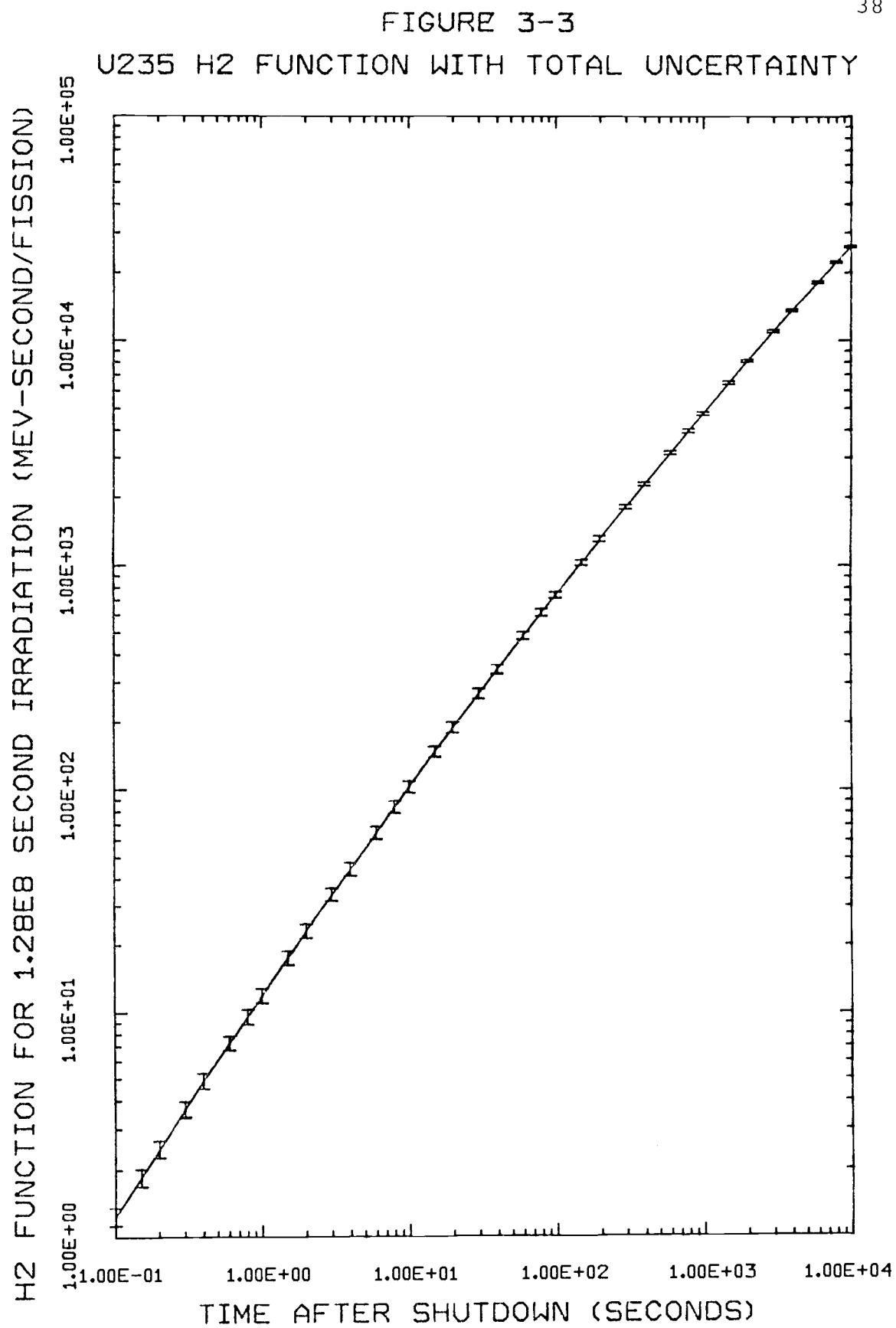
Appendix III is a listing of the nuclides used in after-heat calculations together with energy uncertainties obtained using the techniques of Chapter II. The coefficients  $A_{ij}(t,T)$  of equation 1-6 can be calculated using decay constant, yield, and branching ratios data. Appendix III data can then be used with equations 1-6, 1-7, and 1-8 to obtain the  $H$  functions as a function of irradiation time and shutdown time together with uncertainty in these functions due to decay energy uncertainties. Figures 3-1 through 3-6 display these functions and their uncertainties for a standard irradiation time of  $1.28 \times 10^8$  seconds at constant power and constant flux. The effect of neutron capture during the irradiation has been neglected in these calculations. Shay<sup>(8)</sup> has shown that these effects can be treated with a small correction for the conditions considered here. The graphs are plotted from calculations made with 37 decay times from zero to  $10^4$  seconds.

Figures 3-1 through 3-3 show log-log plots of  $H$ ,  $H_1$ , and  $H_2$  respectively with total uncertainty bars. The total uncertainties have both yield and energy components; the yield components were obtained using techniques described in reference 1, and the energy components were obtained using the techniques described in this paper. Each energy component has three subcomponents; a correlated component,

FIGURE 3-1  
U235 H FUNCTION WITH TOTAL UNCERTAINTY







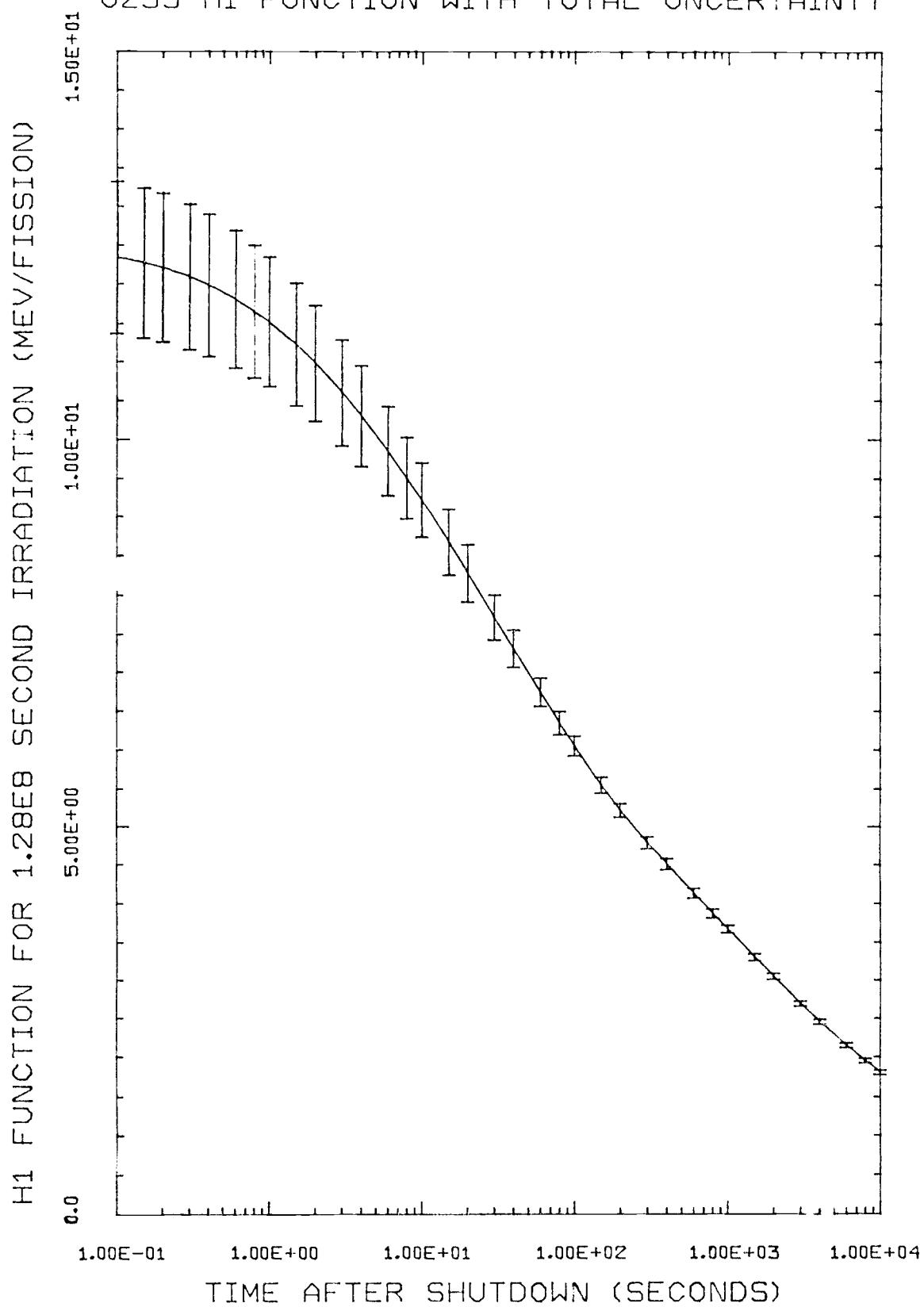
a component due to uncorrelated uncertainties in beta decay energies, and a component due to uncorrelated uncertainties in gamma decay energies. The total uncertainties are obtained by calculating the square root of the sum of the squares of the individual components.

Figure 3-4 is a semi-log plot of the  $H_1$  function with total uncertainty bars, and Figure 3-5 is a log-log plot of the  $H_1$  function with the uncertainty bars due to uncertainty in decay energy of the individual nuclides. Figure 3-6 compares the various energy uncertainty components.

Uncertainties are largest for short cooling times because most of the decay power immediately after shutdown comes from nuclides with short half lives. Decay data are not available for most of these nuclides since their short half lives make experimental observation difficult. Therefore, the data which contribute most to decay heat at short cooling times are predicted by nuclear chematics and have relatively large uncertainties; and these large uncertainties propagate to produce large uncertainties in the  $H$  functions.

The  $H_1$  function predicts the amount of power which must be removed from a reactor in event of a loss of coolant accident in order to prevent any increase in fuel temperature. The  $H_2$  function gives the amount of decay energy which has been released since the loss of coolant accident. The difference between the amount of energy removed by the

FIGURE 3-4  
U235 H1 FUNCTION WITH TOTAL UNCERTAINTY



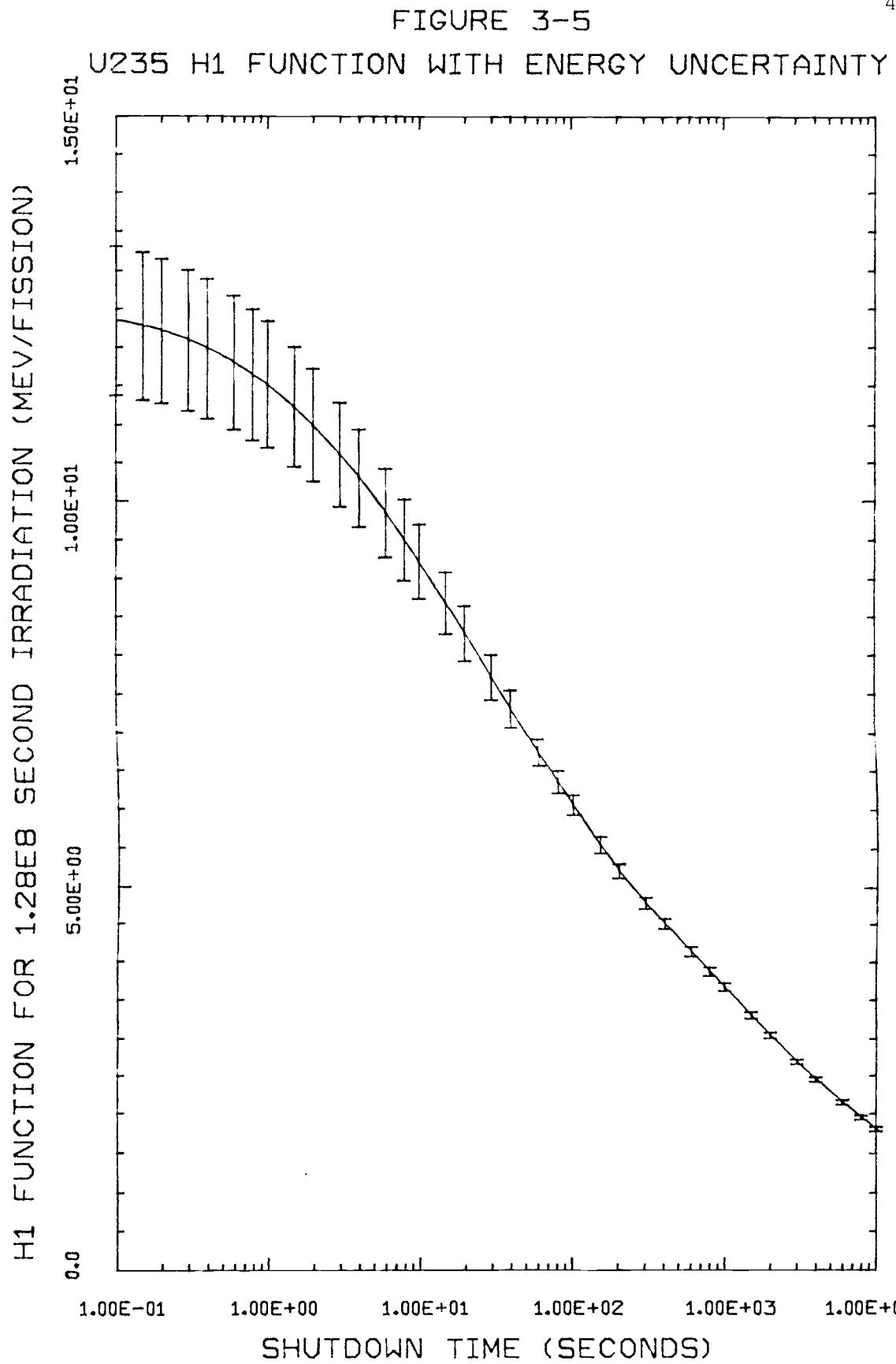
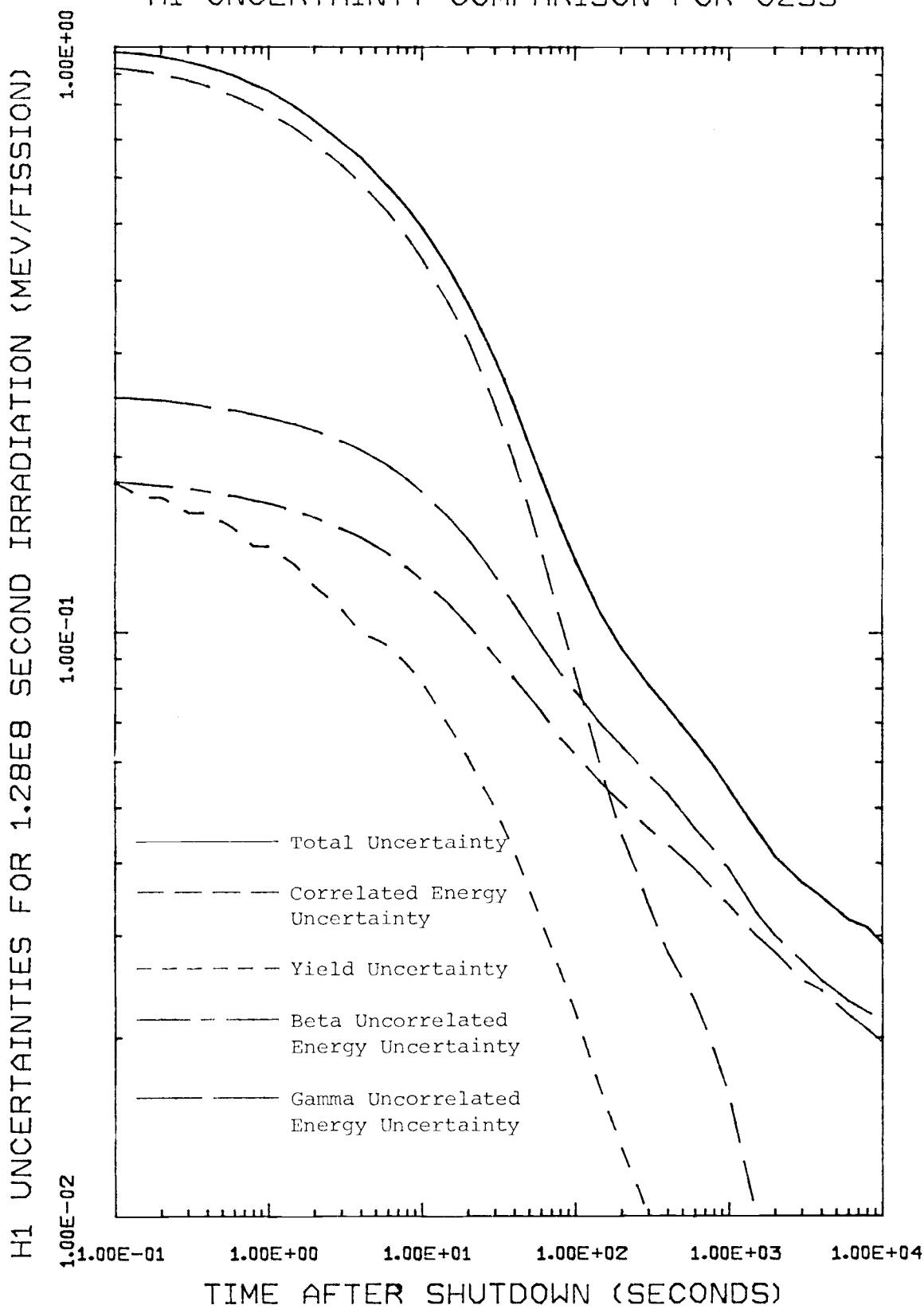


FIGURE 3-6  
H1 UNCERTAINTY COMPARISON FOR U235



emergency core cooling system and the  $H_2$  function is the energy which has produced a temperature change in the reactor fuel. The emergency core cooling systems must be designed so that fuel integrity is not damaged by this energy difference. It should be noted that the uncertainty bands for the  $H_2$  function are much smaller than the uncertainty bands for the  $H_1$  or  $H$  functions. This means that the amount of energy which must be removed can be calculated much more reliably than the instantaneous shutdown power.

The results presented here are intended to be used in the formulation of a new decay heat standard for the United States Regulatory Commission. The standard is used to determine adequacy of the emergency core cooling systems for commercial nuclear power plants. The emergency systems must be capable of removing the maximum amount of decay heat produced, so conservative engineering practice dictates that the emergency systems be capable of removing the maximum predicted heat plus enough extra heat that one can be confident that uncertainties in the computation will not cause reactor damage under any likely emergency condition.

The uncertainty bands given here are "one sigma" bands; i.e., the "confidence level" (Appendix I) which can be assigned to the calculation is 68%. If the emergency core cooling system is sized to remove the predicted heat plus

one sigma, then one can be 84% confident that it will be adequate.

The agreement between the results presented here and those of Schmittroth and Schenter<sup>(5)</sup> is a strong indication that these uncertainty calculations are reliable. Further comparisons should be made between these results and various integral experiments which are in progress.

There are a variety of ways in which these uncertainty calculations might be refined:

1. As evaluated data become available for more nuclides the calculations can be performed with the new data set. This might change the predicted decay power, and it should decrease the uncertainties.
2. Integral experiment data might be used to infer a correlation among the nuclides for which decay data is predicted by nuclear systematics; data for these nuclides could be modified according to the correlation, changing the predicted values of reactor heat.
3. The calculations could be performed again using the latest least-squares coefficient uncertainties (cf. section 1.3 of this thesis).
4. The methods presented here do not take advantage of the fact that the sum of the beta spectral line

intensities used in equation 2-1 add up to one  
(this is not true for gamma spectral intensities).  
This latter refinement should have little effect  
since the component of decay heat uncertainty due  
experimental data is small for most decay times.

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## APPENDICES

## Appendix I

## STATISTICAL PRELIMINARIES

Suppose that one is presented with a set of experimentally determined data,  $x_i$ ,  $1 \leq i \leq n$ , together with an estimate of the uncertainty,  $\sigma_i$ , in each  $x_i$ . Suppose further, that an arithmetic calculation is performed using the data. The question arises: "Given that there is uncertainty in the data base, how much confidence can one have in the result of the calculation?"

The above question is usually answered in terms of random variables (defined in section 1 of this appendix); it is assumed that each time a parameter,  $x_i$ , is measured, a different answer can be obtained. If a given parameter is measured many times, then an average value,  $\bar{x}_i$ , and a standard deviation  $\sigma_i$  can be determined. The average,  $\bar{x}_i$ , is an estimate of the "real" value of the parameter and the standard deviation,  $\sigma_i$ , is a measure of how well the various experimental observations agree. If a large enough number of observations have been made, then  $\bar{x}_i$  can be considered as the "best" estimate of the datum, and  $\sigma_i$  is a measure of the confidence that we can have in  $\bar{x}_i$ .

The arithmetic calculation referred to above is a continuous function of  $n$  variables,  $f(x_1, x_2, \dots, x_n) = f(\mathbf{x})$  (where  $\mathbf{x}$  is a real  $n$ -dimensional vector). Each time measurements

are taken to determine a complete set of data,  $(x_1, \dots, x_n)$ , a value of  $f$  can be determined. If several such sets of measurements are taken, then several values of  $f$  are available. These values of  $f$  can be averaged to determine  $\bar{f(x)}$ , and a standard deviation,  $\sigma$ , can also be determined. The average value,  $\bar{f(x)}$ , is the number which we expect to be the "real" result of the calculation, and  $\sigma$  is an indication of how much confidence we can have in  $\bar{f(x)}$ . In practice, the process of evaluating data is much more complex than the process described here, but this simple approach is used as a basis for estimating uncertainty propagation. When a datum is given with an uncertainty, it is assumed that the value given for the datum is the average value of a random variable and the uncertainty is the standard deviation.

Most physical parameters which are measured experimentally are not random variables; if successive measurements disagree, it is due to imperfections in our ability to observe physical phenomena (ignoring quantum mechanical effects). Sometimes, however, it is necessary to measure parameters which are random variables. For example consider the measurement of two parameters of a radionuclide which decays by beta emission. The two parameters to be measured are Q-value and kinetic energy of the beta particle. Every time a nuclide of the type being considered decays, the Q-value is the same; disagreement among observers is used to

determine "error bars" for the datum. The kinetic energy of the beta particle, however, varies widely from decay to decay. We say that the beta particles are produced in a "spectrum."

### 1. Random Variables

A "random variable"  $(x_i, p_i)$  is a function,  $x_i: S_i \rightarrow \mathbb{R}$ , from a set,  $S_i$ , to the real numbers, together with a "probability density function",  $p_i: \mathbb{R} \rightarrow \mathbb{R}^+$ , from the real numbers to the non-negative real numbers. The density function,  $p_i$ , has the properties:

1.  $p_i$  is Lebesgue integrable,
2.  $\int_{-\infty}^{\infty} p_i(x) dx = 1$ , and
3.  $p_i(x) \geq 0$  for all  $x$ .

This definition applies to the discussion above concerning experimental measurements. The set  $S$  is the set of all experimental observations of a particular phenomenon; for a particular observation,  $s \in S_i$ ,  $x_i(s)$  is the datum obtained. The integral,  $\int_b^a p_i(x) dx$ , is the probability that  $x_i(s)$  is in the interval  $[a, b]$ . If a finite number of observations  $(s_1, s_2, \dots, s_m)$  are made, then  $p_i$  can be approximated by approximating its integral between any two real numbers,  $a$  and  $b$ :

$$\int_a^b p_i(x) dx \approx \frac{1}{m} U(a, b)$$

where  $U(a, b)$  is the number of times that  $x_i(s_i)$  falls in

the interval  $[a, b]$ .

The mean,  $\bar{x}_i$ , and the standard deviation,  $\sigma_i$ , of the random variable,  $(x_i, p_i)$  (usually denoted simply by  $x_i$ ), are given by:

$$\bar{x}_i = \int_{-\infty}^{\infty} x p_i(x) dx, \text{ and}$$

$$\begin{aligned}\sigma_i^2 &= \int_{-\infty}^{\infty} (x - \bar{x}_i)^2 p_i(x) dx \\ &= \int_{-\infty}^{\infty} x^2 p_i(x) dx - 2\bar{x}_i \int_{-\infty}^{\infty} x p_i(x) dx + \bar{x}_i^2 \\ &= \bar{x}_i^2 - \bar{x}_i^2\end{aligned}$$

A probability density function,  $p_i$ , determines a "cumulative probability density function,"  $P_i$ , by the formula:

$$P_i(x) = \int_{-\infty}^x p_i(x) dx$$

Cumulative density functions are monotonically increasing, i.e., if  $x_1 < x_2$  then  $P_i(x_1) \leq P_i(x_2)$ . If a given cumulative density function is strictly increasing (i.e., if strict inequality holds above), then it has an inverse,  $P_i^{-1} : I \rightarrow R$ , where  $I$  is the unit interval of real numbers between zero and one.

Intuitively,  $P_i(x)$  is the probability that a given observation will give a result which is less than or equal to  $x$ .

## 2. The Normal and Beta Distributions

In order to exhibit a particular random variable,  $x_i$ , it is necessary to provide a prescription for its probability density function,  $p_i$ . The most commonly used random variable is the "normal distribution"; its density function is given by:

$$p_i(x) = \frac{1}{\sqrt{2\pi} \sigma_i} \exp\left(-\frac{(x - \bar{x}_i)^2}{2\pi \sigma_i^2}\right)$$

where  $\bar{x}_i$  and  $\sigma_i$  are the mean and standard deviation as defined above.

The "beta distribution" has been used in this thesis. Its density function is given by:

$$p_i(x) = \begin{cases} x^n (M - x)^m / N & \text{if } 0 \leq x \leq M \\ 0 & \text{otherwise} \end{cases}$$

where  $n$ ,  $m$  and  $M$  are positive real numbers, and  $N$  is chosen so that

$$\int_{-\infty}^{\infty} p_i(x) dx = 1$$

The parameters  $n$  and  $m$  are related to the mean and standard deviation of the random variable by:

$$\bar{x}_i = M \frac{n+1}{n+m+2} \quad \text{and}$$

$$\sigma_i^2 = M^2 \frac{(n+1)(m+1)}{(n+m+2)^2(n+m+3)}$$

Beta distributions are useful because they assign zero probability to values of the random variable which fall outside the range from zero to  $M$ . It is common for physical parameters to be confined to a finite range in this manner (e.g., the beta particle from a beta decay must have a kinetic energy which is greater than zero but less than the Q-value of the decay).

### 3. Sampling a Distribution

If the cumulative density function,  $P_i$ , for a random variable is strictly increasing (this is the case for most density functions including those for normal and beta distributions) then it has an inverse,  $P_i^{-1}$ , (as noted above). This distribution can then be "sampled" by choosing a number,  $r_j$ , at random from those real numbers between zero and one, and then calculating  $P_i^{-1}(r_j)$ . If  $m$  random numbers between zero and one are chosen, then a set of numbers  $P_i^{-1}(r_j)$ ,  $1 \leq j \leq m$  is determined. For any real number,  $x$ ,  $P(x)$  can be approximated by:

$$P(x) \approx \frac{1}{m} U(x)$$

where  $U(x)$  is the number of times that  $P_i^{-1}(r_j)$  falls in the interval from  $-\infty$  to  $x$ .

This sampling technique provides a method of converting a "uniform" random number into one which conforms to a given probability density function. The technique can be used to

model the situation described at the beginning of this appendix in which physical parameters are being measured. Selecting the random number,  $r_j$ , between zero and one corresponds to conducting an experimental measurement. The number,  $P_i^{-1}(r_j)$ , is modeled as the result of the experiment.

#### 4. Propagation of Uncertainties

Suppose that  $n$  uncorrelated physical parameters,  $x_1, x_2, \dots, x_n$ , are used in a calculation,  $f(x_1, x_2, \dots, x_n) = f(x)$ . The information about each parameter,  $x_i$ , comes as a random variable with density function,  $p_i$ , mean,  $\bar{x}_i$ , and standard deviation,  $\sigma_i$ . The mean,  $\bar{x}_i$  is modeled as the best estimate of the datum, and the standard deviation,  $\sigma_i$ , is modeled as a measure of the confidence in  $\bar{x}_i$ . Selection of  $n$  random numbers between zero and one,  $r_1, r_2, \dots, r_n$ , allows one to sample each random variable. The numbers obtained by sampling,  $P_1^{-1}(r_1), P_2^{-1}(r_2), \dots, P_n^{-1}(r_n)$ , can be interpreted as a set of measurements and, as such, they can be used to obtain a value of  $f$ . If the sampling process is repeated many times, then many values of  $f$  will be available and a probability density function,  $p(z)$ , for the calculation (the "derived" density function) can be approximated by:

$$p(z) \approx \frac{U(h)}{2mh}$$

where  $m$  is the number of sets of samples taken,  $U(h)$  is the

number of times that  $f(x)$  fell in the interval  $(z-h, z+h)$ , and  $h$  is some small positive number.

The derived density function is a complete measure of the reliability of the calculation. For example, if one wants to find an interval around  $\bar{f}(x)$  such that the probability of the "real" value of  $f(x)$  being in that interval is  $p\%$ , then one simply finds a number  $h$  such that

$$\int_{\frac{\bar{f}(x)-h}{\bar{f}(x)+h}}^{\bar{f}(x)+h} p(z) dz = \frac{p}{100}$$

The probabilistic techniques outlined above require a considerable amount of computer time, so techniques which give an indication of reliability for a calculation without sampling the density functions are very desirable. If the function,  $f$ , can be approximated by the first two Taylor terms,

$$f(x) \approx f(\bar{x}) + \sum_{i=1}^n f_i(\bar{x})(x_i - \bar{x}_i),$$

$$\text{then } \bar{f}(x) \approx f(\bar{x}) \quad \text{and } \sigma^2 \approx \sum_{i=1}^n f_i(\bar{x}) \sigma_i^2,$$

$$\text{where } \bar{x} = (\bar{x}_1, \bar{x}_2, \dots, \bar{x}_n)$$

$$\text{and } f_i(\bar{x}) = \frac{\partial}{\partial x_i} f(\bar{x})$$

In order to show the above, notice that

$$\begin{aligned} \bar{f}(x) &= \int f(x) p(x) dx \\ &\approx f(\bar{x}) \int p(x) dx + \int \left[ \sum_{i=1}^n f_i(\bar{x})(x_i - \bar{x}_i) \right] p(x) dx \end{aligned}$$

$$\begin{aligned}
 &= f(\bar{x}) + \sum_{i=1}^n f_i(\bar{x}) \int_{-\infty}^{\infty} (x_i - \bar{x}_i) p_i(x_i) dx_i \\
 &= f(\bar{x})
 \end{aligned} \tag{3}$$

where the integral sign without limits means the integral over all of n-dimensional Euclidean space and  $p(x)$  is the product of the  $p_i(x_i)$ .

The standard deviation can now be approximated by:

$$\begin{aligned}
 \sigma^2 &= \int [f(x) - \bar{f}(x)]^2 p(x) dx \\
 &\approx \int [f(x) - f(\bar{x})]^2 p(x) dx \\
 &\approx \int \left[ \sum_{i=1}^n f_i(\bar{x}) (x_i - \bar{x}_i) \right]^2 p(x) dx \\
 &= \int \sum_{i=1}^n f_i^2(\bar{x}) (x_i - \bar{x}_i)^2 p(x) dx \\
 &= \sum_i f_i^2(\bar{x}) \sigma_i^2
 \end{aligned} \tag{4}$$

Equations (3) and (4) both utilize the identity:

$$\int_{-\infty}^{\infty} (x_i - \bar{x}_i) p_i(x) dx = 0$$

##### 5. Standard Deviation as a Measure of Confidence

Standard deviation has been referred to (vaguely) in this appendix as a measure of the confidence that one can have in a datum. Specifically, if  $x_i$  is a normal random variable which describes a physical datum, then the probability that the "real" datum is within one standard deviation of the mean is 0.68. That is:

$$0.68 = \int_{\bar{x}_i - \sigma_i}^{\bar{x}_i + \sigma_i} p_i(x) dx$$

where  $p_i$  is the density function for  $p_i$  and  $\sigma_i$  is the standard deviation. The probability of being within two standard deviations is 95% and the probability of being within three is 99%.

These observations relating standard deviation and confidence do not apply if the random variable in question deviates much from the normal shape. For example, consider the "uniform" distribution determined by the following probability density function:

$$p(x) = \begin{cases} 1 & \text{if } 0 \leq x \leq 1 \\ 0 & \text{otherwise} \end{cases}$$

The mean of this random variable is 0.5 and the standard deviation is given by:

$$\sigma^2 = \int_0^1 x^2 dx - 0.25 = \frac{1}{12}$$

Thus the probability of being within one standard deviation of the mean is  $2/\sqrt{12} \approx 0.58$ , and one is certain to be within two standard deviations of the mean.

Non-normal random variables are commonly generated by normal ones; for example, if  $x$  is a normal random variable with  $\bar{x}=0$ , then the derived density function for  $x^2$  has a maximum at zero yet it is zero for all negative values. Thus  $x^2$  is a very "non-normal" random variable and it cannot

be expected that a "one sigma" band around the mean corresponds to a 0.68 confidence level. This is also an example where the approximation:

$$\bar{f(x)} \approx f(\bar{x})$$

is very poor.

Two methods for assessing the confidence that can be placed in a given calculation have been given here:

1. calculate the derived density function, and
2. approximate the first two moments of the derived density function.

The first method works in general but it takes significant amounts of computer time. The second method can be accomplished quickly and easily, but its results are valid only when the calculation can be approximated by the first two terms of its Taylor series, and the results (when valid) can be used to assess confidence levels only when the derived density function is approximately normal.

## Appendix II

ENERGY UNCERTAINTY EVALUATIONS FOR NUCLIDES  
LISTED IN THE REICH NUCLEAR DATA FILE

This file consists of the "5" cards of reference 3 (cf. Table II-3) together with two extra "5" cards generated as described in section 2.1 of this thesis. For each nuclide, the first "5" card is that of reference 3, the second "5" card lists energies and uncertainties calculated by equations 2-1 through 2-3, and the third "5" card lists energies and uncertainties obtained by using the probabilistic techniques of Appendix I.

The columns labeled "E BETA" and "E GAMMA" are average beta and gamma decay energies; the columns labeled "UNC BETA" and "UNC GAMMA" are "one sigma" uncertainties which are obtained from spectral uncertainty data assuming that the spectral uncertainties are completely uncorrelated. The column labeled "NUCLIDE" is an eight digit number which identifies the nuclide for which data is given. The first digit identifies the type of data presented (it is always "5" here). The next three digits give the atomic number of the nuclide, the following three digits give the atomic mass number of the nuclide, and the last digit indicates whether the data is for a metastable state or the ground state ("zero" indicates ground state and "one" indicates metastable state).

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L	S	JNC	DATA	E	54M14	UND	54M14	NUCL 10c
1332.64		21.8		251.36	0.1		532.790	
1332.65		217.38		251.77	74.53		532.790	
1332.66		217.32		277.11	74.97		532.790	
2322.67		6.1		515.50	0.3		533.800	
2322.68		271.10		615.53	117.59		533.800	
2322.69		264.50		527.47	165.32		533.800	
1333.68		6.0		3.0	0.3		533.810	
1333.69		128.27		3.0	0.30		533.810	
1333.70		281.93		3.0	0.30		533.810	
2211.71		6.0		233.03	0.0		533.820	
2211.72		244.89		233.03	84.57		533.820	
2211.73		247.74		234.70	71.47		533.820	
1319.73		6.0		2334.09	0.0		533.821	
1319.74		215.60		2334.09	705.38		533.821	
1322.74		215.43		2331.72	238.22		533.821	
4+1.75		6.0		2254.26	0.0		534.830	
4+1.76		161.26		2561.27	42.54		534.830	
4+1.77		6.0		2533.07	42.72		534.830	
1331.76		6.0		903.53	0.0		534.831	
1331.77		111.56		903.53	58.02		534.831	
1314.07		113.32		207.50	97.75		534.831	
530.84		6.0		407.70	0.0		534.840	
530.85		57.00		407.70	40.77		534.840	
531.07		57.10		413.23	40.77		534.840	
1251.74		6.0		1752.74	0.0		535.840	
1251.75		158.27		1752.74	101.54		535.840	
1254.59		158.49		1751.59	104.36		535.840	
338.59		6.0		2753.59	0.0		535.841	
345.59		67.01		2753.59	181.56		535.841	
381.73		61.05		2774.24	172.16		535.841	
384.71		6.0		54.53			535.850	
384.72		158.56		54.53	72.46		535.850	
384.74		158.56		54.53	27.31		535.850	
1775.29		6.0		3317.82	0.0		536.860	
1775.30		274.30		3317.82	143.52		536.860	
1775.31		257.53		3317.82	146.46		536.860	
2133.59		6.0		1720.23	0.0		536.870	
2133.60		221.31		1720.23	725.32		536.870	
2134.60		235.45		1713.37	301.24		536.870	
2251.59		6.0		2.25			536.880	
2251.60		6.0		2.25	1.56		536.880	
2251.61		6.0		2.25	0.00		536.880	
226.52		6.0		133.22	0.0		536.891	
226.53		3.77		133.22	4.74		536.891	
226.54		5.33		133.33	6.07		536.891	
1334.59		6.0		792.60	0.0		536.870	
1334.60		48.16		792.60	22.02		536.870	
1333.72		56.79		793.23	25.34		536.870	
248.68		6.0		2211.32	0.0		536.880	
248.69		63.40		2211.33	54.38		536.880	
255.77		6.0		2212.31	53.30		536.880	

| $\Delta E_{\text{PA}}$ |
|------------------------|------------------------|------------------------|------------------------|------------------------|------------------------|------------------------|------------------------|
| 1141.81                | 0.0                    | 2103.03                | 0.0                    | 5                      | 36                     | 840                    |                        |
| 1241.81                | 243.34                 | 2055.05                | 17.33                  | 5                      | 36                     | 840                    |                        |
| 1335.17                | 149.04                 | 2053.03                | 25.35                  | 5                      | 36                     | 840                    |                        |
| 1437.32                | 0.0                    | 1743.12                | 7.3                    | 5                      | 36                     | 840                    |                        |
| 1437.38                | 124.33                 | 1743.13                | 67.34                  | 5                      | 36                     | 840                    |                        |
| 1445.33                | 117.13                 | 1751.03                | 0.34                   | 5                      | 36                     | 840                    |                        |
| 2777.33                | 0.0                    | 723.73                 | 0.0                    | 5                      | 36                     | 310                    |                        |
| 2777.37                | 162.53                 | 723.73                 | 16.0.36                | 5                      | 36                     | 910                    |                        |
| 2777.41                | 200.51                 | 730.52                 | 161.36                 | 5                      | 36                     | 910                    |                        |
| 2777.45                | 0.0                    | 751.44                 | 0.0                    | 5                      | 36                     | 920                    |                        |
| 2813.21                | 203.24                 | 751.44                 | 20.44                  | 5                      | 36                     | 920                    |                        |
| 2835.72                | 245.23                 | 750.61                 | 20.35                  | 5                      | 36                     | 920                    |                        |
| 2837.51                | 0.0                    | 673.12                 | 0.0                    | 5                      | 37                     | 890                    |                        |
| 2832.67                | 162.73                 | 673.13                 | 1.34                   | 5                      | 37                     | 830                    |                        |
| 2833.27                | 151.33                 | 653.53                 | 0.36                   | 5                      | 37                     | 840                    |                        |
| 2844.34                | 0.0                    | 2233.43                | 0.0                    | 5                      | 37                     | 890                    |                        |
| 2846.34                | 131.73                 | 2233.43                | 84.34                  | 5                      | 37                     | 890                    |                        |
| 2847.32                | 126.14                 | 2237.07                | 87.14                  | 5                      | 37                     | 890                    |                        |
| 1458.02                | 2651.03                |                        |                        | 5                      | 37                     | 900                    |                        |
| 1458.03                | 243.77                 | 2650.42                | +16.42                 | 5                      | 37                     | 900                    |                        |
| 1477.64                | 230.03                 | 2313.27                | 345.36                 | 5                      | 37                     | 900                    |                        |
| 1480.53                |                        | 3613.31                |                        | 5                      | 37                     | 901                    |                        |
| 1480.57                | 176.73                 | 3615.31                | 374.57                 | 5                      | 37                     | 901                    |                        |
| 1484.21                | 167.56                 | 3650.33                | 309.53                 | 5                      | 37                     | 901                    |                        |
| 1484.18                | 0.0                    | 2737.13                | 0.0                    | 5                      | 37                     | 910                    |                        |
| 1484.17                | 223.22                 | 2733.13                | 460.15                 | 5                      | 37                     | 910                    |                        |
| 1478.16                | 184.54                 | 2335.53                | 361.52                 | 5                      | 37                     | 910                    |                        |
| 3459.27                | 0.0                    | 251.36                 | 0.0                    | 5                      | 37                     | 920                    |                        |
| 3459.27                | 203.23                 | 261.36                 | 16.32                  | 5                      | 37                     | 920                    |                        |
| 2604.13                | 271.27                 | 254.34                 | 0.30                   | 5                      | 37                     | 920                    |                        |
| 2832.62                | 0.0                    | 0.0                    | 0.0                    | 5                      | 33                     | 830                    |                        |
| 2867.46                | 34.01                  | 34.03                  | 0.30                   | 5                      | 33                     | 840                    |                        |
| 2869.46                | 34.37                  | 1.10                   | 0.31                   | 5                      | 33                     | 890                    |                        |
| 1495.06                | 0.0                    | 0.0                    | 0.0                    | 5                      | 33                     | 900                    |                        |
| 1722.50                | 27.37                  | 0.10                   | 0.30                   | 5                      | 33                     | 900                    |                        |
| 1633.57                | 31.16                  | 0.03                   | 0.00                   | 5                      | 33                     | 900                    |                        |
| 052.29                 | 0.0                    | 695.43                 | 0.0                    | 5                      | 33                     | 910                    |                        |
| 052.29                 | 90.10                  | 695.46                 | 102.33                 | 5                      | 33                     | 910                    |                        |
| 551.26                 | 93.31                  | 695.26                 | 124.71                 | 5                      | 33                     | 910                    |                        |
| 132.29                 | 0.0                    | 1333.34                | 0.0                    | 5                      | 33                     | 920                    |                        |
| 132.29                 | 41.43                  | 1333.34                | 46.30                  | 5                      | 33                     | 920                    |                        |
| 137.13                 | 35.51                  | 1342.35                | 45.37                  | 5                      | 33                     | 920                    |                        |
| 1161.05                | 0.0                    | 1335.33                | 0.0                    | 5                      | 33                     | 930                    |                        |
| 1161.05                | 128.32                 | 1235.33                | 193.52                 | 5                      | 33                     | 930                    |                        |
| 1170.36                | 169.53                 | 1513.23                | 128.19                 | 5                      | 33                     | 930                    |                        |
| 869.64                 | 0.0                    | 1242.43                | 0.0                    | 5                      | 33                     | 940                    |                        |
| 869.64                 | 34.43                  | 1242.43                | 142.36                 | 5                      | 33                     | 940                    |                        |
| 370.32                 | 95.29                  | 1244.43                | 146.33                 | 5                      | 33                     | 940                    |                        |
| 931.03                 |                        | 0.23                   |                        | 5                      | 33                     | 950                    |                        |
| 933.04                 | 56.31                  | 0.23                   | 0.20                   | 5                      | 33                     | 950                    |                        |
| 934.43                 | 56.15                  | 0.03                   | 0.30                   | 5                      | 33                     | 950                    |                        |

$\Delta E_{\text{FS}}$	$E_{\text{FS}}$	$\Delta E_{\text{PA}}$	$E_{\text{PA}}$	$\Delta E_{\text{PA}}$	$E_{\text{PA}}$	$\Delta E_{\text{PA}}$	$E_{\text{PA}}$	NUCLEUS
6.85			632.46		632.46		632.46	39 301
7.78		7.78	632.47	7.78	632.47	7.78	632.47	39 301
9.60		9.60	632.55	9.60	632.55	9.60	632.55	39 301
10.53		10.53	632.66	10.53	632.66	10.53	632.66	39 301
12.42		12.42	632.77	12.42	632.77	12.42	632.77	39 301
13.32		13.32	632.87	13.32	632.87	13.32	632.87	39 301
14.21		14.21	633.01	14.21	633.01	14.21	633.01	39 301
15.09		15.09	633.15	15.09	633.15	15.09	633.15	39 301
16.93		16.93	633.27	16.93	633.27	16.93	633.27	39 301
1454.23		1454.23	243.21	1454.23	243.21	1454.23	243.21	39 320
1454.24		1454.24	243.21	1454.24	243.21	1454.24	243.21	39 320
1477.23		1477.23	238.31	1477.23	238.31	1477.23	238.31	39 320
1484.63		1484.63	238.37	1484.63	238.37	1484.63	238.37	39 320
1484.69		1484.69	238.39	1484.69	238.39	1484.69	238.39	39 320
1484.70		1484.70	238.42	1484.70	238.42	1484.70	238.42	39 320
1717.4		1717.4	135.13	1717.4	135.13	1717.4	135.13	39 340
1727.24		1727.24	335.13	1727.24	335.13	1727.24	335.13	39 340
1746.25		1746.25	1003.43	1746.25	1003.43	1746.25	1003.43	39 340
1746.73		1746.73	633.31	1746.73	633.31	1746.73	633.31	39 340
1749.73		1749.73	433.52	1749.73	433.52	1749.73	433.52	39 340
1753.12		1753.12	204.71	1753.12	204.71	1753.12	204.71	39 340
2152.32		2152.32	335.35	2152.32	335.35	2152.32	335.35	39 370
2162.42		2162.42	332.21	2162.42	332.21	2162.42	332.21	39 370
2164.56		2164.56	437.53	2164.56	437.53	2164.56	437.53	39 370
6.82		6.82	231.31	6.82	231.31	6.82	231.31	40 901
7.72		7.72	231.31	7.72	231.31	7.72	231.31	40 901
8.60		8.60	231.33	8.60	231.33	8.60	231.33	40 901
116.29		116.29	735.03	116.29	735.03	116.29	735.03	40 960
116.29		116.29	735.03	116.29	735.03	116.29	735.03	40 960
116.81		116.81	735.75	116.81	735.75	116.81	735.75	40 960
707.12		707.12	131.73	707.12	131.73	707.12	131.73	40 970
707.12		707.12	131.75	707.12	131.75	707.12	131.75	40 970
712.67		712.67	101.74	712.67	101.74	712.67	101.74	40 970
1620.52		1620.52	793.70	1620.52	793.70	1620.52	793.70	40 990
1620.52		1620.52	793.71	1620.52	793.71	1620.52	793.71	40 990
1617.52		1617.52	791.37	1617.52	791.37	1617.52	791.37	40 990
43.56		43.56	765.34	43.56	765.34	43.56	765.34	41 950
43.56		43.56	765.34	43.56	765.34	43.56	765.34	41 950
43.57		43.57	763.91	43.57	763.91	43.57	763.91	41 950
6.02		6.02	235.46	6.02	235.46	6.02	235.46	41 951
8.00		8.00	235.47	8.00	235.47	8.00	235.47	41 951
9.00		9.00	151.52	9.00	151.52	9.00	151.52	41 951
107.34		107.34	677.03	107.34	677.03	107.34	677.03	41 970
167.94		167.94	677.03	167.94	677.03	167.94	677.03	41 970
43.53		43.53	630.34	43.53	630.34	43.53	630.34	41 970
6.00		6.00	742.70	6.00	742.70	6.00	742.70	41 971
8.00		8.00	742.70	8.00	742.70	8.00	742.70	41 971
9.00		9.00	743.63	9.00	743.63	9.00	743.63	41 971
1365.28		1365.28	142.23	1365.28	142.23	1365.28	142.23	41 980
1465.29		1465.29	214.47	1465.29	214.47	1465.29	214.47	41 980
1365.30		1365.30	205.37	1365.30	205.37	1365.30	205.37	41 980



E BETA	UNC BETA	E GAMMA	UNC GAMMA	NUCLEUS
470.06	0.0	45.20	6.0	5 441080
470.08	67.39	45.20	16.51	5 441080
458.36	31.53	30.67	14.30	5 441080
0.0	0.0	33.73	0.0	5 451031
0.00	0.00	33.73	4.00	5 451031
0.00	0.00	33.74	4.00	5 451031
1002.97	0.0	11.49	3.0	5 451040
1002.97	161.57	11.49	16.50	5 451040
1001.77	191.19	3.04	8.12	5 451040
0.53	0.0	132.2	0.0	5 451041
.53	.15	132.19	5.32	5 451041
0.00	0.00	135.20	13.40	5 451041
152.23	0.0	73.77	0.0	5 451050
152.23	28.59	73.77	2.02	5 451050
143.69	28.31	73.63	3.35	5 451050
0.0	0.0	129.70	0.0	5 451051
0.00	0.00	129.70	64.35	5 451051
0.00	0.00	35.30	47.79	5 451051
1449.66	0.0	199.44	0.0	5 451060
1445.67	175.73	199.44	68.86	5 451060
1438.84	186.23	203.23	60.20	5 451060
348.66	0.0	2645.23	0.0	5 451061
348.66	49.21	2645.24	187.52	5 451061
348.16	53.64	2673.23	179.34	5 451061
421.19	0.0	312.20	0.0	5 451070
421.19	62.40	312.25	43.11	5 451070
427.73	62.56	321.62	35.23	5 451070
1828.05	0.0	703.53	0.0	5 451080
1328.06	215.63	703.53	126.34	5 451080
1327.77	221.39	703.21	119.12	5 451080
864.06	0.0	2439.49	0.0	5 451081
864.06	136.63	2439.50	168.40	5 451081
796.63	139.40	2452.20	168.35	5 451081
1345.67	0.0	2257.63	0.0	5 451100
1345.68	192.56	2257.65	186.23	5 451100
1354.44	199.25	2274.00	194.38	5 451100
2481.22	0.0	56.07	0.0	5 451101
2481.22	241.66	56.07	37.38	5 451101
2478.34	246.48	34.95	26.16	5 451101
364.11	0.0	0.21	0.0	5 461090
364.11	58.82	0.21	0.16	5 461090
362.73	69.43	0.00	0.00	5 461090
0.0	0.0	183.00	0.0	5 461091
0.00	0.00	183.00	18.39	5 461091
0.00	0.00	183.47	19.36	5 461091
844.19	0.0	52.33	0.0	5 461110
844.19	57.55	52.88	3.87	5 461110
354.89	57.78	50.62	6.34	5 461110
167.11	0.0	421.39	0.0	5 461111
167.11	35.49	421.39	17.54	5 461111
176.79	29.74	419.13	14.50	5 461111

E	BETA	UNC	BETA	E	GAMMA	UNC	GAMMA	NUCLIDE
0.0	0.0			87.70	0.0			5 471091
0.00	0.00			87.70	0.31			5 471091
0.00	0.00			87.41	0.34			5 471091
354.76	0.0			26.97	0.0			5 471110
354.76	56.32			26.97	15.39			5 471110
342.52	71.31			26.01	10.38			5 471110
0.0	0.0			65.00	0.0			5 471111
0.00	0.00			65.00	0.53			5 471111
0.00	0.00			64.92	0.40			5 471111
1425.89	0.0			653.75	0.0			5 471120
1428.89	187.51			663.77	125.59			5 471120
1463.69	180.35			737.03	107.34			5 471120
629.46	0.0			2575.86	0.0			5 491180
629.46	87.54			2575.87	264.17			5 491180
636.42	91.36			2693.69	157.56			5 491180
1775.31	0.0			213.12	0.0			5 491181
1777.32	197.10			213.12	124.47			5 491181
1777.32	208.19			201.03	94.27			5 491181
1038.65	0.0			3058.71	0.0			5 491200
1038.65	146.76			3053.71	261.41			5 491200
1161.14	153.18			3103.34	221.44			5 491200
2471.42	0.0			175.74	0.0			5 491201
2471.42	237.36			175.74	117.16			5 491201
2480.77	220.12			112.93	54.34			5 491201
136.16	0.0			312.27	0.0			5 501250
936.16	135.59			312.27	67.25			5 501250
315.22	168.32			233.66	48.50			5 501250
798.01	0.0			345.86	0.0			5 501251
798.01	128.36			345.86	34.06			5 501251
807.32	146.29			346.02	34.66			5 501251
974.55	0.0			1434.31	0.0			5 501270
674.55	113.37			1434.31	52.37			5 501270
696.35	125.49			1435.21	51.47			5 501270
1134.21	0.0			434.03	0.0			5 501271
1134.21	181.29			494.00	49.65			5 501271
1140.61	210.49			494.61	47.12			5 501271
217.20	0.0			596.51	0.0			5 501280
217.20	31.34			596.51	38.73			5 501280
216.45	35.09			593.03	38.10			5 501280
660.29	0.0			1322.79	0.1			5 501320
660.30	87.33			1322.79	30.33			5 501320
662.31	100.14			1321.74	31.43			5 501320
36.86	0.0			452.07	0.0			5 511250
84.56	13.77			452.07	48.67			5 511250
84.83	19.46			450.10	45.61			5 511250
318.06	0.0			644.32	0.0			5 511270
318.06	52.48			644.32	125.50			5 511270
324.17	49.65			686.13	147.37			5 511270
418.49	0.0			3096.08	0.0			5 511280
418.49	76.76			3095.09	60.23			5 511280
424.06	73.20			3093.60	61.74			5 511280

E BETA	UNC BETA	E GAMMA	UNC GAMMA	NUCLIDE
947.26	0.0	1986.03	0.0	5 511251
947.26	147.07	1986.03	75.56	5 511251
945.84	159.31	1932.97	74.30	5 511281
359.11	0.0	1301.04	0.0	5 511290
359.11	79.17	1301.06	182.07	5 511290
381.17	54.83	1301.42	161.33	5 511290
1260.67	0.0	2140.33	6.0	5 511300
1260.67	176.52	2140.39	161.36	5 511300
1230.63	182.09	2143.02	145.26	5 511300
1093.22	0.0	2439.45	6.0	5 511301
1093.22	148.37	2439.46	163.37	5 511301
1199.59	192.78	2502.07	147.02	5 511301
713.69		1702.51		5 511310
713.69	126.22	1702.51	239.29	5 511310
742.56	98.47	1362.99	173.57	5 511310
1722.11	0.0	2036.60	0.0	5 511320
1722.11	213.22	2036.01	181.04	5 511320
1724.73	217.26	1933.51	173.29	5 511320
1695.53	0.0	2033.60	0.0	5 511321
1630.57	195.19	2033.62	125.32	5 511321
1693.09	192.66	2034.67	127.10	5 511321
537.11	0.0	3162.50	0.0	5 511330
537.11	91.63	3162.47	335.23	5 511330
546.70	91.23	3333.65	253.47	5 511330
3951.55	0.0	0.0	0.0	5 511340
3951.55	275.32	0.00	0.00	5 511340
3942.21	276.39	0.00	0.00	5 511340
2953.76	0.0	2034.43	0.0	5 511341
2953.77	271.77	2034.43	151.15	5 511341
2949.64	275.19	2091.61	147.31	5 511341
0.0	0.0	143.75	0.0	5 521251
0.00	0.00	143.75	111.09	5 521251
0.00	0.00	124.97	54.92	5 521251
227.23	0.0	5.17	0.0	5 521270
227.23	36.64	5.17	2.30	5 521270
220.61	41.33	5.64	1.81	5 521270
533.94	0.0	72.90	0.0	5 521290
533.94	83.76	72.90	28.08	5 521290
549.79	103.59	80.53	25.56	5 521290
214.02	0.0	23.90	0.0	5 521291
214.02	49.63	23.95	15.53	5 521291
214.77	56.35	30.33	12.51	5 521291
671.72	0.0	422.30	0.0	5 521310
671.72	92.57	422.35	91.10	5 521310
654.46	105.22	443.22	78.59	5 521310
182.18	0.0	1491.12	0.0	5 521311
182.18	48.49	1491.13	162.27	5 521311
179.24	37.41	1542.99	135.14	5 521311
60.05		263.60		5 521320
60.05	3.77	263.60	12.38	5 521320
60.25	3.32	263.43	13.00	5 521320

E BETA	UNC BETA	E GAMMA	UNC GAMMA	NUCLIDE
819.97		883.2+		5 521330
319.98	120.39	883.2+	143.38	5 521330
826.62	130.68	1024.17	113.55	5 521330
552.07	.0.0	1266.14	0.0	5 521331
552.07	84.33	1366.15	176.34	5 521331
852.50	92.76	1335.35	150.07	5 521331
152.09		824.97		5 521340
152.09	20.65	824.97	24.94	5 521340
151.50	23.11	824.41	24.07	5 521340
135.50	0.0	333.23	0.0	5 531310
135.50	29.27	333.23	47.34	5 531310
139.09	33.63	331.50	45.57	5 531310
524.69	0.0	2237.7	0.0	5 531320
524.69	95.10	2237.71	174.37	5 531320
524.69	87.55	2305.13	149.39	5 531320
417.19	0.0	593.90	0.0	5 531330
417.19	66.50	593.95	76.36	5 531330
426.79	73.38	607.15	59.82	5 531330
530.93	0.0	2592.60	0.0	5 531340
690.93	105.37	2592.65	211.67	5 531340
704.09	103.26	2658.23	176.04	5 531340
0.0	0.0	315.70	0.0	5 531341
0.00	0.00	315.70	27.56	5 531341
0.00	0.00	315.56	27.76	5 531341
393.65	0.0	1456.00	0.0	5 531350
393.65	66.37	1456.04	236.03	5 531350
+00.35	66.38	1510.03	217.28	5 531350
1811.03	0.0	2213.49	0.0	5 531360
1811.03	227.13	2213.49	290.56	5 531360
1822.91	224.41	2202.55	258.19	5 531360
1939.61	0.0	1925.44	0.0	5 531361
1939.61	220.06	1925.44	139.12	5 531361
1945.69	210.21	1929.45	138.59	5 531361
0.0	0.0	167.54	0.0	5 541311
0.00	0.00	167.54	8.35	5 541311
0.00	0.00	153.00	8.23	5 541311
101.88	0.0	31.44	0.0	5 541330
101.88	.39	31.44	.38	5 541330
101.31	1.73	31.43	.55	5 541330
0.0	0.0	232.69	0.0	5 541331
0.00	0.00	232.69	6.78	5 541331
0.00	0.00	232.85	6.31	5 541331
303.89	0.0	261.43	0.0	5 541350
309.39	3.10	261.43	1.09	5 541350
310.59	3.58	259.56	.41	5 541351
0.0	0.0	526.82	0.0	5 541351
0.00	0.00	526.82	3.24	5 541351
0.00	0.00	526.73	3.62	5 541351
1940.72	0.0	195.26	0.0	5 541370
1840.72	78.11	195.26	32.42	5 541370
1942.50	79.08	189.07	36.42	5 541370

E_BETA	UNC_BETA	E_GAMMA	UNC_GAMMA	NUCLIDE
657.77	0.0	1195.05	0.1	5 541380
657.78	90.53	1195.06	24.27	5 541380
658.96	90.10	1194.44	26.35	5 541380
1786.77	0.0	327.43	0.0	5 541390
1786.78	159.26	327.52	10.19	5 541390
1786.79	141.01	328.72	3.46	5 541390
161.63	0.0	1579.72	0.0	5 551340
161.73	26.52	1579.72	123.23	5 551340
162.34	29.74	1585.77	111.16	5 551340
0.0	0.0	137.60	0.0	5 551341
0.00	0.00	137.60	13.00	5 551341
0.00	0.00	138.21	13.04	5 551341
119.23	0.0	2157.74	0.0	5 551360
119.23	20.29	2157.35	147.39	5 551360
120.26	42.58	2171.87	143.32	5 551360
174.44	0.0	0.0	0.0	5 551370
174.44	1.39	0.00	0.00	5 551370
171.13	1.65	0.00	0.00	5 551370
1262.40	0.0	2329.12	0.0	5 551380
1262.43	149.34	2329.13	68.79	5 551380
1290.96	145.57	2329.01	70.35	5 551380
1146.90	0.0	2049.66	0.0	5 551381
1146.96	173.63	2033.66	153.34	5 551381
1152.19	194.78	2110.54	153.62	5 551381
1753.69	0.0	310.76	0.0	5 551390
1763.69	117.71	310.76	5.26	5 551390
1763.98	122.09	302.43	22.30	5 551390
1831.24	0.0	2131.03	0.0	5 551400
1831.24	271.74	2131.03	297.54	5 551400
1903.73	234.50	2413.15	163.32	5 551400
0.0	0.0	662.17	0.0	5 561371
0.00	0.00	662.13	2.34	5 561371
0.00	0.00	662.11	3.54	5 561371
337.27		52.23		5 561390
937.22	129.53	52.23	21.21	5 561390
378.35	145.10	37.06	15.36	5 561390
230.27		215.37		5 561400
230.27	28.47	215.37	8.78	5 561400
279.33	34.51	215.73	7.33	5 561400
915.52	0.0	387.30	0.0	5 561410
915.53	129.91	387.32	11.37	5 561410
955.75	113.09	835.72	13.26	5 561410
423.22	0.0	1012.63	0.0	5 561420
429.28	70.32	1012.63	37.57	5 561420
446.28	61.80	1014.39	37.44	5 561420
517.01	0.0	2204.30	0.0	5 571400
517.02	73.01	2204.31	217.76	5 571400
520.46	83.36	2223.33	169.39	5 571400
439.38	0.0	32.31	0.0	5 571410
433.39	82.67	32.31	1.47	5 571410
988.00	63.37	27.23	0.00	5 571410

C BETA	JNC BETA	E GAMMA	JNC GAMMA	NUCLIDE
947.02	0.0	2564.67	0.0	5 571420
947.02	194.99	2564.67	69.24	5 571420
973.45	132.35	2553.26	69.47	5 571420
159.49	0.0	71.70	0.0	5 581410
159.49	21.37	71.70	14.56	5 581410
157.42	26.02	75.11	16.49	5 581410
414.13		235.33		5 581430
419.13	27.57	230.34	32.11	5 581430
418.07	65.37	234.17	37.00	5 581430
32.96		23.87		5 581440
32.96	.34	23.87	1.14	5 581440
32.91	1.76	23.73	1.32	5 581440
529.94	0.0	743.90	0.0	5 581450
629.94	96.37	743.93	92.42	5 581450
531.09	103.46	752.83	86.30	5 581450
242.69	0.0	314.30	0.0	5 581460
242.69	39.21	314.30	43.31	5 581460
244.44	45.92	313.34	40.49	5 581460
323.92	0.0	0.0	0.0	5 591430
323.92	52.33	0.00	0.00	5 591430
309.68	61.20	0.00	0.00	5 591430
1262.77		31.01		5 591440
1262.77	1.64	31.01	0.30	5 591440
1275.47	4.70	33.53	0.00	5 591440
0.39	0.0	59.73	0.0	5 591441
0.39	.10	59.73	0.03	5 591441
0.00	0.00	55.92	9.02	5 591441
704.65	0.0	13.73	0.0	5 591450
704.65	113.26	13.73	4.35	5 591450
683.05	131.57	17.66	3.37	5 591450
427.90	0.0	1634.90	0.3	5 591460
427.90	146.96	1634.94	221.03	5 591460
935.10	145.43	1632.66	187.13	5 591460
747.93	0.0	320.00	0.0	5 591470
747.93	111.72	321.00	140.79	5 591470
746.51	120.56	319.23	120.76	5 591470
2043.53	0.0	300.00	0.0	5 591480
2043.53	217.18	300.00	30.15	5 591480
2047.79	225.35	238.36	33.11	5 591480
1157.82	0.0	251.26	0.0	5 591490
1157.82	191.66	251.27	54.53	5 591490
1123.43	175.51	255.35	56.63	5 591490
241.69	0.0	113.70	0.0	5 601470
241.69	37.49	113.70	50.77	5 601470
239.37	50.00	109.97	37.15	5 601470
474.39	0.0	330.75	0.0	5 601490
474.39	67.70	336.76	9.66	5 601490
480.16	69.14	337.11	10.39	5 601490
644.13	0.0	839.26	0.0	5 601510
644.13	96.51	839.27	195.31	5 601510
632.03	80.26	322.73	78.59	5 601510

E BETA	UNC BETA	E GAMMA	UNC GAMMA	NUCLEUS
63.00	0.0	0.10	0.0	5 611470
63.00	10.18	.10	.17	5 611470
61.70	10.51	0.00	0.00	5 611470
7+4.30	0.0	630.37	0.0	5 611480
744.30	107.33	630.33	179.59	5 611480
726.01	133.64	657.05	217.81	5 611480
147.38	0.0	2009.37	0.0	5 611481
147.38	24.20	2009.33	115.48	5 611481
149.21	25.28	2013.08	115.79	5 611481
370.58	0.0	14.23	0.0	5 611490
375.62	60.64	14.23	7.93	5 611490
380.67	73.25	12.25	4.28	5 611490
311.35	0.0	704.60	0.0	5 611510
311.35	49.41	304.60	61.77	5 611510
305.72	47.58	332.84	46.17	5 611510
1438.77	0.0	238.14	0.0	5 611520
1+38.78	178.13	288.14	24.39	5 611520
1444.26	187.08	297.30	24.70	5 611520
419.48	0.0	1237.25	0.0	5 611521
419.48	91.60	1237.25	126.71	5 611521
428.34	77.36	1311.97	134.74	5 611521
672.63	0.0	77.43	0.0	5 611530
672.63	72.31	77.43	17.17	5 611530
676.66	60.44	32.24	21.03	5 611530
230.70	0.0	104.52	0.0	5 621530
230.70	29.02	104.52	1.38	5 621530
231.69	24.73	104.75	4.50	5 621530
430.20	0.0	1317.70	0.0	5 631560
430.20	82.57	1317.70	246.50	5 631560
432.10	90.24	1347.97	168.21	5 631560
1.65		0.0		5 751870
.05	.05	0.00	0.00	5 751870
.05	.05	0.00	0.00	5 751870

## Appendix III

A TABULATION OF FISSION PRODUCT  
DECAY ENERGIES AND UNCERTAINTIES

This is a file of decay energies and energy uncertainties for those nuclides which might contribute significantly to reactor decay heat. The decay energies listed here were obtained from ENDF/B-IV; the uncertainties were estimated using the techniques of this thesis.

The column headed "NUCLIDE" identifies the nuclides for which data is displayed. Each nuclide identified is a six digit integer; the first three digits give the atomic mass number, the next two digits give the atomic charge number, and the last digit indicates the metastable state. The columns headed "E BETA" and "E GAMMA" give the beta and gamma energy of decay for the nuclide as obtained from ENDF/B-IV. The columns headed "UNC BETA," "UNC GAMMA" and "CORR TOTAL" give the uncorrelated and correlated energy uncertainties. The column headed "E TOTAL" lists the sum of the beta and gamma decay energies, and the column headed "UNC TOTAL" is the quadratic sum of the uncorrelated beta and gamma energy uncertainties. An asterisk following a nuclide identifier indicates that the energy data for that nuclide was obtained experimentally.

NUCLIDES	$\alpha$ BETA	UNO BETA	$\delta$ GAMMA	UNO GAMMA	$\delta$ TOTAL	UNO TOTAL	CORE TOTAL	UNO TOTAL
72220	5.73090	2.19823	2.84810	2.63466	8.57860	4.22433	1.51909	
72230	2.00440	1.06200	1.20280	1.02037	3.20720	2.08237	0.97800	
72290	3.34220	1.22022	1.34390	.95291	4.69110	2.17313	.44933	
72300	.23600	.21347	.14400	.27715	.23000	.48062	.15691	
72310	.53100	.16032	2.72000	1.76860	3.22100	1.32342	.03419	
72320	0.00000	1.00000	0.10000	0.00000	0.00000	0.00010	0.00000	
73260	0.00000	0.00000	1.00000	0.00000	0.00000	0.00000	0.00000	
73270	4.77530	1.93244	2.84830	2.05464	7.62420	3.39743	1.55016	
73280	3.13630	1.41379	1.33850	1.38726	6.37540	2.30707	.91409	
73290	2.27230	.92450	1.13620	.87450	3.45350	1.79910	.45509	
73300	1.71020	.61475	.74507	.51337	2.45527	1.13312	.15953	
73310	.14460	.14204	.31300	.20735	.76300	.34943	.02141	
73321	0.00000	0.00000	.06700	.04355	.06700	.04355	.04300	
73330	0.00000	0.00010	0.00000	0.00000	0.00000	0.00000	0.00000	
74260	1.00000	0.06000	0.01000	0.00000	0.10000	0.05000	0.00000	
74270	0.20270	2.81829	3.33466	2.83866	9.53730	4.65637	1.54000	
74280	2.57700	1.18957	1.67700	1.29153	4.25000	2.48150	.92543	
74290	3.81170	1.35438	1.79450	1.23463	7.50620	2.55343	.48200	
74300	.76351	.36349	.43026	.33994	1.19077	.69333	.15300	
74310	1.07000	.34240	3.04000	1.97600	4.11000	2.31340	.03152	
74320	0.07000	1.00000	0.01000	0.00000	0.00000	0.00000	0.00000	
75270	5.21170	2.22949	3.35850	2.43392	8.56320	4.71741	2.34754	
75280	.035220	1.75041	2.36920	1.73290	6.41210	3.53321	1.53521	
75290	2.30500	1.26217	1.64070	1.25231	4.50570	2.51444	.91223	
75300	2.17440	.39923	1.10410	.82450	3.27350	1.72373	.45177	
75310	1.36200	.51316	.02090	.03634	1.33090	.54360	.13040	
75321	0.00000	1.00000	.13900	.09035	.13000	.14035	.04300	
75330	.43020	.17760	.03590	.02334	.46590	.16034	.01646	
75270	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	
75280	3.03660	1.31559	2.17560	1.58932	5.27220	2.90431	.94634	

MOLIDE	E BETA	UNC BETA	E GAMMA	UNC GAMMA	E TOTAL	UNC TOTAL	CORR TOTAL
76290	+3.33070	1.52131	2.24360	1.52194	6.52930	3.04376	.47059
76300	1.35760	.51318	.84130	.54755	2.19890	1.19063	.16934
76310	1.63300	.53750	2.31600	1.62650	4.49030	2.36410	.32911
76320	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
76330	1.13670	.76374	.76294	.82841	1.43964	.59315	.1-652
76340	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
77260	+.51030	2.05176	2.87940	2.81062	7.33370	4.27235	2.33194
77280	3.40330	1.59435	2.11850	1.65535	5.52150	3.24371	1.53734
77300	2.72250	1.22816	1.50470	1.17080	4.22720	2.33395	.90451
77310	1.63130	.77514	.37746	.89343	2.55376	1.7357	.44463
77321	.35000	.40037	.06390	.09489	1.03390	.43576	.12373
77320	.54800	.31359	1.16000	.82053	1.80800	1.13327	.14233
77330	.74103	.077713	.10236	.06692	.34399	.14435	.01735
77341	0.00000	0.00000	.25000	.16250	.25000	.16250	.04310
77340	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
78260	3.53570	1.35611	2.70660	2.16196	6.30330	4.31207	2.37254
78280	4.84460	1.95234	2.74270	1.49947	7.59130	3.34541	1.53659
78300	1.34950	1.02650	1.24420	1.06179	7.09370	2.04633	.96971
78310	3.12860	1.15906	1.45530	1.02636	4.53410	2.13542	.48653
78320	.23800	.23521	.27700	.30099	.61500	.53530	.15579
78330	1.40000	.44800	1.03300	.86350	2.43000	1.11750	.0242
78340	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
79290	3.31170	1.32336	2.62660	2.07519	6.33380	4.30305	2.33715
79300	3.27080	1.06459	1.99010	1.57994	5.26030	3.14453	1.32923
79310	2.22540	1.11132	1.27540	1.05147	3.50170	2.16329	.49740
79320*	1.39265	.21732	.25137	.07457	2.14462	.24262	1.00010
79330	.36100	.37646	.01800	.03849	.37900	.41535	.12336
79341	.00010	.00003	.09500	.06175	.03510	.06173	.04239
79340	.04200	.01344	.00010	.00007	.04210	.01351	.01170
79351	0.00000	0.00000	.21000	.13650	.21000	.13650	.04306
79350	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
80280	0.00070	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
80290	5.31220	2.26700	3.72550	2.60170	9.23770	4.30372	1.57623
80300	2.35700	1.13708	1.70330	1.32581	4.06530	2.46234	.93709
80310	3.70050	1.32135	1.92230	1.31933	5.62280	2.54123	.46737

NUCLIDE	E BETA	UNC BETA	E GAMMA	UNC GAMMA	E TOTAL	UNC TOTAL	CORR TOTAL
31320	.52705	.32126	.40153	.32935	1.02363	.65061	.10234
31330*	2.52264	.26420	.50653	.10602	3.12322	.37022	3.00000
31340	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
31351	0.00000	0.00000	0.03500	.05590	.09600	.09590	.00100
31350	.71829	.22935	.25290	.16429	.97119	.38424	.14643
31360	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
31290	5.23940	2.24625	3.31320	2.77593	9.11160	5.02214	2.34829
31300	+.30660	1.85765	2.36580	2.15956	7.26640	3.36724	1.57967
31310	2.75930	1.27501	1.72030	1.30993	4.43010	2.54500	.38261
31320	2.05960	.86971	1.13700	.83311	3.24660	1.75132	.45694
31330*	1.65943	.22139	0.00000	0.00000	1.66943	.22139	0.00000
31341	0.00000	0.00000	.10300	.05695	.10300	.05695	.04300
31340	.60500	.19350	.00760	.00494	.61260	.19354	.01695
31350	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
31361	0.00000	0.00000	.10000	.12350	.13000	.12330	.00100
32290	0.11000	0.05000	.1+000	.09100	.14000	.09100	.01100
32300	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
32300	3.73910	1.49226	2.94020	2.05902	6.72930	3.55123	.37204
32310	4.75967	1.63335	2.33070	1.89568	7.59030	3.52963	.49267
32320	1.21790	.47336	.24633	.59424	2.06423	1.06812	.16703
32331*	1.31323	.21448	2.93465	.29222	4.31384	.49553	0.00000
32330*	3.21093	.27774	.23309	.07193	7.49902	.34367	0.00000
32340	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
32351	.02742	.00878	.06583	.03632	.08330	.04510	.15718
32350	.1+010	.04430	2.65000	1.72250	2.79000	1.76730	.27036
32360	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
33300	+.63430	2.09774	3.33140	2.62331	3.22570	4.72105	2.34839
33310	+.23630	1.80000	2.37260	2.10060	7.13350	3.30350	1.57304
33320	3.03660	1.30134	2.08420	1.46076	5.04050	2.73270	.93614
33330	1.67930	.77316	.38446	.76903	2.66076	1.54213	.45303
33341*	1.30171	.11332	.00933	.05775	2.21104	.17157	0.00000
33340*	.4+135	.06615	2.55927	.04272	3.03113	.10837	0.00000
33350	.32430	.10358	.09730	.00475	.33130	.10843	.01518
33361	0.00000	0.00000	.04180	.02717	.04180	.02717	.04300
33360	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000

NUCLICE	E BETA	UNC BETA	E GAMMA	UNC GAMMA	E TOTAL	UNC TOTAL	COFF TOTAL
8+300	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
8+310	5.16500	2.03230	3.35000	2.39624	3.54500	+0.42364	1.57709
8+320	2.42120	1.14355	1.31350	1.45503	4.38476	2.50468	1.93235
8+330	3.76120	1.33907	2.10360	1.43607	5.36460	2.77514	1.47339
8+3+0*	.53084	.03919	.40770	.04006	.33354	.07325	0.00000
8+351*	.39554	.07165	2.76840	.17819	3.56394	.24434	0.00000
8+360*	1.25574	.15645	1.75274	.16490	3.00548	.26135	0.00000
8+360	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
85310	+0.63130	2.09339	3.38730	2.33014	3.37866	4.52213	2.38212
85320	+0.51860	1.61660	2.55050	1.92252	6.36410	3.54512	1.57412
85330	2.35840	1.25733	2.15900	1.50562	5.03746	2.35235	1.36435
853+1	2.1+670	.89023	1.74730	.94435	3.+.9+12	1.37433	.46677
85340	2.05000	.86304	1.29370	.95259	3.35370	1.32053	.45543
85350*	.39421	.19855	.06463	.02701	1.05959	.22566	0.00000
85361*	.22603	.06533	.19322	.03687	.40930	.01140	0.00000
85360*	.25053	.06073	.00223	.00156	.25242	.00229	0.00000
85370	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
85380	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
85310	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
85320	3.03620	1.36974	2.47130	1.73129	5.55750	3.09103	.96804
85330	+0.15770	1.45423	2.64790	1.73376	6.30560	3.23733	.45512
85340	1.+1960	.53006	1.01980	.70213	2.43940	1.23212	.17040
85351	3.03550	.96735	1.65610	1.03297	4.75160	2.17133	.32454
85360*	1.77520	.25330	3.31735	.14346	5.09305	.39375	0.00000
85360	0.10000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
85371	0.00000	0.00000	.56000	.36400	.56000	.36400	.30100
85370	.67000	.21440	.09430	.06130	.70430	.27570	.12703
85380	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
87320	4.07490	1.74330	3.05010	2.22419	7.12500	3.37239	1.69758
87330	5.11130	1.31275	2.73570	1.98346	5.39700	3.23621	.95773
87340	2.43980	.98237	1.73350	1.22600	4.23830	2.20337	.47957
87350*	2.13559	.23045	1.72630	.30124	3.66189	.53153	0.00000
87360*	1.37450	.05075	.79260	.52599	2.12710	.07574	0.00000
87370	.09219	.02950	.04957	.03157	.14976	.06107	.01659
87381	.00011	.00013	.38638	.25147	.38699	.25150	.30030

NUCLIDE	E BETA	UNC BETA	E GAMMA	UNC GAMMA	E TOTAL	UNC TOTAL	COPR TOTAL
873 <sup>80</sup>	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
883 <sup>80</sup>	3.50369	1.82434	2.99030	2.35373	6.49499	4.17809	2.42155
893 <sup>80</sup>	4.80350	1.93720	3.13290	2.22376	7.30640	4.16663	1.36932
893 <sup>80</sup>	2.10050	1.67770	1.52640	1.29115	3.72690	2.36335	1.36032
893 <sup>80</sup>	3.05720	1.13975	1.38110	1.30419	4.34830	2.44834	1.47531
893 <sup>80*</sup>	.24853	.03648	2.21183	.05398	2.46041	.09033	0.00000
893 <sup>72*</sup>	2.03260	.15539	.67393	.06191	2.75563	.15740	0.00000
893 <sup>80</sup>	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
893 <sup>80</sup>	4.21630	1.98759	3.11740	2.38346	7.33370	4.37105	2.38181
893 <sup>80</sup>	2.33810	1.48430	2.15710	1.71304	5.09520	3.19737	1.56824
893 <sup>80</sup>	2.81500	1.24460	1.38210	1.47706	4.79710	2.72303	1.42235
893 <sup>80*</sup>	1.24121	.14954	2.06306	.02536	3.30427	.17433	0.00000
893 <sup>70*</sup>	.92934	.12614	2.28893	.05719	3.21832	.18333	0.00000
893 <sup>80*</sup>	.53200	.03437	0.00000	0.00000	.53200	.03437	0.00000
893 <sup>91</sup>	0.00000	0.00000	.91000	.59150	.91000	.59150	.04300
893 <sup>90</sup>	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
903 <sup>80</sup>	5.36230	2.46742	3.56450	2.79567	9.02730	5.26404	3.31024
903 <sup>40</sup>	2.51210	1.62306	2.07760	1.86585	4.53970	3.49321	2.36736
903 <sup>50</sup>	3.35830	1.56034	2.31570	1.73676	5.67400	3.36760	1.56231
903 <sup>80*</sup>	1.13703	.11790	1.74913	.06804	2.83616	.18603	0.00000
903 <sup>71*</sup>	1.10670	.16356	3.61591	.30683	4.72221	.47164	0.00000
903 <sup>70*</sup>	1.65863	.23530	2.66042	.34595	4.31905	.58405	0.00000
903 <sup>80*</sup>	.13800	.03118	0.01000	0.00000	.19300	.03116	0.00000
903 <sup>91*</sup>	.07038	.00024	.68247	.05459	.68330	.05433	0.00010
903 <sup>90*</sup>	.33100	.05618	.00028	.00020	.33128	.05535	0.00000
904 <sup>01*</sup>	0.01000	0.00000	2.31481	.23624	2.31481	.23624	0.00000
904 <sup>00</sup>	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00010
913 <sup>40</sup>	3.71870	1.87579	2.92660	2.23020	6.54530	4.10539	2.38646
913 <sup>50</sup>	3.06510	1.51119	2.32630	1.81397	5.39190	3.32506	1.59077
913 <sup>60*</sup>	2.57730	.26351	.72356	.14180	3.30136	.46937	1.36830
913 <sup>70*</sup>	1.33415	.18454	2.73316	.38132	4.06732	.56536	0.00000
913 <sup>80*</sup>	.55229	.08331	.69540	.12471	1.34769	.20362	0.00000
913 <sup>91*</sup>	0.00000	0.00000	.55515	.05348	.55515	.05343	0.00000
913 <sup>90*</sup>	.50600	.10641	.30256	.00156	.50366	.10327	0.00010
914 <sup>00</sup>	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000

NUCLEIDE	E BETA	UNC BETA	E GAMMA	UNC GAMMA	E TOTAL	UNC TOTAL	CORR TOTAL
92340	2.36240	1.71071	2.60680	2.15756	5.56960	3.36827	2.41532
92350	3.70440	1.65611	2.93550	2.20085	5.63390	3.35636	1.81141
92360*	2.40721	.24520	.75134	.02495	3.15505	.27435	2.00000
92370*	3.45927	.27127	.26136	.01032	3.720e3	.28153	0.00000
92380*	.14229	.03561	1.33884	.04257	1.33113	.03413	0.00000
92390*	1.46424	.18931	.24821	.11432	1.71249	.30363	0.00000
92400	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
93340	4.03560	1.95372	3.41880	2.53664	7.51440	.45405	2.42364
93350	3.58720	1.65330	2.87720	2.13171	6.56440	3.78501	1.60218
93360	2.75730	1.23100	2.03960	1.51734	4.73740	2.74334	.34917
93370	2.02740	.85857	1.41450	1.03293	3.44200	1.39110	.47327
93380*	1.15105	.16903	1.33500	.12919	2.55655	.23722	0.00000
93391	0.00000	0.00000	.25000	.15250	.25000	.16250	.04310
93390*	1.13449	.03132	.03357	.00199	1.27406	.03331	0.00000
93400	.01254	.00401	.00742	.00482	.01396	.00833	.01530
93411	0.01000	0.00000	0.3040	.01975	.03040	.01975	.30100
93410	0.01000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
94340	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
94350	4.36440	1.94638	3.60120	2.54370	8.45560	.44965	1.60590
94360	2.07030	1.36775	1.79300	1.49529	3.35830	2.47303	.36910
94370	3.60080	1.12238	1.96100	1.37022	4.93040	2.49320	.46928
94380*	.36964	.04529	1.24246	.14033	2.11210	.22562	0.00000
94390*	1.71740	.19238	.93613	.11175	2.70353	.33473	0.00010
94400	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
94411	.00135	.00043	.04123	.02593	.04263	.02725	.22542
94410	.19100	.06112	1.56000	1.01400	1.75100	1.07312	.26460
94420	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
95340	0.00000	0.00000	0.00000	0.00000	0.00000	0.10010	0.00000
95350	4.03400	2.17734	3.40210	2.72093	7.49510	.43932	3.84657
95360	3.25460	1.77457	2.63440	2.14591	5.83800	3.82003	2.34157
95370	2.50000	1.39355	1.97210	1.62575	4.52210	3.02530	1.56906
95380	1.33930	1.04432	1.36140	1.13102	3.30370	2.17534	.31957
95390*	1.74573	.20162	.43832	.10090	2.23405	.30242	0.00000
95400*	.11529	.01734	.73609	.00655	.35238	.02333	0.00000
95411*	0.00000	0.00000	.23546	.03710	.23546	.03710	0.00000

NUCLIDE	E BETA	UNC BETA	E GAMMA	UNC GAMMA	E TOTAL	UNC TOTAL	COPR TOTAL
95410*	.04355	.00739	.76584	.07556	.30940	.08346	.00000
95420	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
95540	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
96350	5.29120	2.0e030	4.07760	2.84400	9.36380	4.9e430	1.62676
96360	2.54220	1.17351	2.31110	1.78504	4.35330	2.37367	.3e007
96370	3.51100	1.26375	2.66040	1.88111	6.17140	3.36456	.49546
96380	1.33240	.51056	1.11960	.76331	2.47200	1.27331	.17423
96390	2.40370	.77056	1.46850	.94333	3.35380	1.71330	.02452
96400	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
96410	.24900	.07958	2.46000	1.59900	2.70900	1.67353	.25434
96420	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
97360	3.37440	1.3e836	3.18130	2.46013	6.39570	4.34304	.42352
97370	2.72690	1.42334	2.50400	1.95572	5.23090	3.34456	1.62436
97380	2.34370	1.13347	1.33780	1.41056	4.13750	2.54433	.94046
97390*	2.15210	.23054	.93500	.08181	3.09710	.31245	0.00000
97400*	.70712	.12249	.13175	.03783	.33837	.16037	0.00000
97411*	0.00000	0.00000	.74270	.07401	.74270	.07311	0.00000
97410*	.45794	.08872	.67703	.06755	1.14497	.15627	0.00000
97420	0.00000	0.00000	0.00000	0.00000	0.00000	1.00003	0.00000
98360	2.90840	1.69380	2.79860	2.2828	5.70700	3.46208	2.45303
98370	3.5e210	1.63e24	3.16710	2.31901	6.30520	3.35700	1.67130
98380	1.63010	.98631	1.49603	1.24408	3.18610	2.23034	.94951
98390	2.34490	1.37670	1.3e260	1.34910	4.73750	2.42530	.4e170
98400	.30200	.38696	.00100	.00361	.30300	.39557	.12273
98411*	.34e12	.17703	2.51493	.17771	3.36309	.31474	0.00000
98410*	1.85523	.20937	.1e023	.03231	2.00951	.24163	0.00010
98420	0.01000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
99360	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
99370	2.35150	1.67161	3.17950	2.53493	6.62200	4.20594	2.51729
99380	2.37200	1.46541	2.33420	1.83372	5.20420	3.28913	1.65433
99390	2.08150	1.07530	1.6e650	1.30497	3.73310	2.33027	.94343
99400*	1.62052	.18171	.79370	.03493	2.41422	.27659	0.00000
99411*	.95365	.14651	1.39426	.21281	2.3e791	.35942	0.00000
99410*	1.52253	.21312	.13974	.03497	1.72227	.24303	0.00000
99420*	.33474	.00718	.19606	.00626	.57046	.01343	0.00000

MOLICE	E_BETA	UNC_BETA	E_GAMMA	UNC_GAMMA	E_TOTAL	UNC_TOTAL	COPR	TOTAL
99431*	0.01000	0.00000	.14274	.01544	.14274	.01544	0.00000	
99430	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
100360	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
100370	+0.73050	1.91258	3.72960	2.63670	8.45950	4.54326	1.62077	
100380	2.04300	1.05912	1.92030	1.48715	3.96320	2.54627	.97325	
100390	3.39700	1.23137	2.42790	1.65233	5.82560	2.88460	.43934	
100400	.73600	.34715	.56233	.47391	1.36920	.32100	.16525	
100411	2.01350	.67735	1.36563	.68764	3.44420	1.56559	.02456	
100410*	2.05950	.23614	1.92053	.08036	3.93012	.31570	0.00000	
100420	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
100430	1.44000	.44600	.07300	.05070	1.47300	.49370	.13772	
100440	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
101370	3.37530	2.12614	3.42950	2.80478	7.37460	4.93032	3.42854	
101380	3.25700	1.77327	2.32660	2.26927	6.02450	4.04254	2.42002	
101390	2.52000	1.79056	2.09180	1.70682	4.61270	3.09733	1.58857	
101400	2.04000	1.15728	.35290	.40350	2.73290	1.56075	.77746	
101410*	1.31055	.23136	.32999	.04801	2.23054	.27337	0.00000	
101420*	.59479	.62720	1.39620	.02340	1.93119	.05050	0.00000	
101430*	.47936	.33456	.33625	.01419	.81621	.04875	0.00000	
101440	0.00000	1.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
102320	2.44670	1.66347	2.43340	2.16946	6.37970	3.71237	2.44555	
102330	3.31530	1.68475	2.31860	2.16174	6.73390	3.33642	1.59915	
102400	1.13240	.87511	1.03750	1.01790	2.15390	1.39311	.92461	
102410	2.43700	.97921	1.53850	1.19396	4.17550	2.17317	.47747	
102420*	.31112	.05734	0.70000	0.00000	.31112	.05734	0.00000	
102431*	.71348	.10223	.54664	.22869	3.26612	.38092	0.00000	
102430*	1.50333	.18537	.45334	.08952	1.97217	.27653	0.00000	
102440	0.00000	0.00010	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
103370	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
103380	3.64770	2.07562	3.37470	2.74753	7.02240	4.82640	3.43476	
103390	2.34180	1.70533	2.59750	2.15382	5.53930	3.36015	2.41649	
103400	2.24880	1.33433	1.33840	1.60250	4.13720	2.93733	1.58105	
103410	1.73640	.99395	1.33230	1.16443	3.11370	2.16338	.93230	
103420	1.31650	.68412	.93750	.79601	2.23400	1.48013	.46346	
103430	.71337	.34331	.50325	.39377	1.22712	.73703	.15846	

NUCLIDE	E BETA	UNC BETA	E GAMMA	UNC GAMMA	E TOTAL	UNC TOTAL	COPR TOTAL
103440*	.06753	.01137	.43002	.03345	.55755	.06432	.000000
103451*	0.00000	0.00000	.03373	.00400	.03373	.00400	0.00000
103450	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
104390	2.91550	1.68854	3.05610	2.45104	5.87160	+1.1254	2.49239
104390	+1.3350	1.77217	3.44300	2.47341	7.62660	+1.24544	1.62529
104400	1.50350	.94638	1.46330	1.24730	2.37690	2.19363	.95531
104410	2.9+300	1.10313	2.15250	1.46287	5.09580	2.38500	+1.5821
104420	.5+722	.30213	.43751	.32283	1.03023	.69430	.16172
104430*	1.18296	.16956	1.44814	.22362	2.64110	.39333	0.00000
104440	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
104451*	.00053	.00015	.13213	.01340	.13277	.01365	0.00000
104450*	1.02237	.19119	.01149	.01050	1.01446	.20153	0.00000
104460	0.01000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
105390	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
105390	3.43460	2.03651	3.21190	2.66605	6.64660	+1.72256	2.43249
105400	2.65380	1.64543	2.37670	2.06664	5.01050	3.59207	2.41143
105410	2.13680	1.31211	1.81950	1.57054	3.35630	2.38255	1.57932
105420	1.71900	.99479	1.39650	1.17563	3.11550	2.17042	.93069
105430	1.05360	.62848	.80733	.70067	1.36393	1.32915	.45529
105440*	.41264	.01025	.73763	.01627	1.23032	.02712	0.00000
105451*	0.00000	0.00000	.12970	.04779	.12970	.04779	0.00000
105450*	.15223	.02851	.07377	.00335	.23105	.03216	0.00000
105460	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
105390	+5+970	2.27031	3.31060	3.01140	8.46630	5.28271	3.41487
105400	1.35141	1.51230	2.00350	1.91241	3.36990	3.42480	2.42865
105410	3.35170	1.57423	2.65290	2.06612	6.00460	2.58035	1.59916
105420	.92050	.86368	.37447	.94215	1.78497	1.78231	.31320
105430	2.23540	.92528	1.60230	1.14454	3.33770	2.06932	.47762
105440*	.00937	.00156	0.00000	0.00000	.00397	.00156	0.00000
106451*	.3+966	.05364	2.6+524	.17924	2.39390	.27253	0.00000
106450*	1.4+567	.18523	.13944	.06020	1.64511	.245+3	0.00000
106460	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
107390	3.75370	2.09533	3.71260	2.95390	7.47630	>1.04373	3.47824
107400	3.03150	1.73134	2.90750	2.33910	5.33910	4.37103	2.45815
107410	2.60630	1.40429	2.36150	1.87410	4.36330	3.27833	1.61702

NUCLIDE	E BETA	UNC BETA	E GAMMA	UNC GAMMA	E TOTAL	UNC TOTAL	COPR TOTAL
107420	1.93650	1.04436	1.72620	1.36734	3.59280	2.41220	.35541
107430	1.53540	.73557	1.26560	.96112	2.30100	1.59653	.47756
107440*	1.23743	.18534	.25137	.07156	1.43885	.26050	0.00000
107450*	.42119	.06836	.31225	.03523	.73344	.10373	0.00000
107461	0.00000	0.00000	.21000	.13650	.21000	.13650	.04730
107460	.01030	.00330	.00010	.00007	.01040	.00337	.01107
107470	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
108400	2.33010	1.97531	2.52620	2.18722	4.35630	3.76253	.47531
108410	3.83250	1.58564	3.13040	2.32013	7.01300	4.10532	1.62138
108420	1.33980	.91132	1.35140	1.19373	2.63120	2.16555	.98650
108430	2.62030	1.01374	2.00110	1.39975	4.62140	2.41649	.48870
108440*	.47006	.08153	.04620	.01651	.51526	.09834	0.00000
108451*	.80406	.13940	2.43950	.16835	3.24396	.36776	0.00000
108450*	1.82866	.22139	.70853	.11912	2.53659	.34051	0.00000
108460	1.00000	0.00010	0.00000	0.00000	0.00000	0.00000	0.00000
108471	1.00000	0.00000	.90000	.58560	.90000	.58560	.30100
108470	.50127	.16041	.23406	.13464	.73533	.34565	.14523
108480	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
108490	3.41920	2.62675	3.44150	2.81566	6.36070	.434341	.47777
108410	7.00910	1.71391	2.36650	2.33422	5.33560	.04513	.45575
108420	2.39420	1.35940	2.13750	1.73343	4.53170	3.14323	1.61309
108430	1.37920	1.04746	1.74400	1.37781	3.72320	.24232	.35951
108440	1.23670	.67802	1.09490	.96800	2.38160	1.54602	.47336
108451	0.00000	0.00000	.25000	.05700	.25000	.05700	.30100
108450	.71285	.34155	.66227	.42959	1.27512	.77114	.16181
108461*	0.00000	0.00000	.18900	.01336	.13300	.01336	0.00000
108460*	.36411	.06843	.00021	.00006	.36432	.06843	0.00000
108471*	0.00000	0.00000	.06770	.00884	.06770	.00884	0.00000
108470	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
108460	.02465	.00739	.01599	.01039	.04064	.01623	.11195
110400	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
110410	.413770	1.75710	3.59460	2.63790	7.33230	4.39500	1.64775
110420	1.63810	.98117	1.81040	1.44787	3.50350	2.42304	.38469
110430	3.12530	1.15300	2.51260	1.71231	5.63790	2.36531	.43776
110440	.77479	.35573	.76407	.55752	1.63386	.31325	.17110

NUCLES	E BETA A	UNC BETA A	E GAMMA A	UNC GAMMA A	E TOTAL	UNC TOTAL	CORR TOTAL
110451*	2.43122	.24646	.05607	.03738	2.53729	.23334	.00000
110450*	1.34568	.19925	2.26753	.15486	3.31336	.35411	.00000
110468	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
110471	.05800	.02176	2.79000	1.81350	2.85800	1.83326	.25335
110470	1.13000	.37763	.0+160	.02704	1.22160	.40464	.12952
111450	0.01000	0.00000	0.01000	0.00000	0.00000	0.00000	0.00000
111418	3.35700	2.01631	3.40610	2.80300	6.77310	4.81631	.47364
111420	2.75770	1.68268	2.72070	2.25534	5.47840	3.91302	2.45763
111430	2.35810	1.39142	2.20950	1.90009	4.56700	3.15151	1.61740
111440	1.71200	.99868	1.52030	1.26373	3.24240	2.25443	.95217
111450	1.23030	.66554	1.0+400	.83949	2.27480	1.50513	.47120
111461*	.16711	.02974	.42139	.01450	.53350	.04424	.00000
111460*	.3+413	.05778	.05234	.00634	.39706	.06412	.00000
111471*	0.00000	0.00000	.06500	.00540	.06500	.00540	0.00000
111470*	.35+76	.07131	.07627	.01080	.39173	.08311	.00000
111481	0.00000	0.00000	.39600	.25740	.39600	.25740	.04703
111480	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
112410	+.44570	2.2+137	+.15930	3.18063	8.59480	5.42207	3.48805
112420	2.14200	1.52108	2.23200	2.68259	4.33400	3.60357	2.47615
112430	3.50350	1.85533	3.0+630	2.25137	6.54980	3.85670	1.62853
112440	1.07790	.86358	1.12300	1.09900	2.20590	1.35153	.94577
112450	2.30030	.92796	1.77300	1.25468	4.07330	2.13254	.43565
112460	.07900	.20071	.07605	.20139	.15514	.48210	.13271
112470*	1.42830	.18095	.66377	.10734	2.03266	.23329	.00000
112480	0.01000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
113470	3.16540	1.73775	3.25620	2.55798	6.41200	4.29573	.49433
113480	2.72420	1.42+54	2.70220	2.68399	5.42700	3.50333	1.64502
113490	2.05310	1.06149	1.03502	1.02312	4.04410	2.58351	.97851
113470	1.55060	.74+62	1.+3240	1.06687	3.01350	1.31143	.48777
113460	1.06410	.43118	.32212	.64799	1.33622	1.07317	.17149
113471	.64953	.20735	.53127	.34533	1.18080	.55313	.02334
113470	.57947	.18543	.47307	.30808	1.05344	.49351	.02274
113481	.15843	.05370	.12539	.03160	.28382	.13220	.01923
113480	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
113491	0.00000	0.00000	.39300	.25545	.39300	.25545	.30100

NUCLICE	E BETA	UNC BETA	E GAMMA	UNC GAMMA	E TOTAL	UNC TOTAL	CORR TOTAL
113490	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
11420	2.38630	1.57310	2.81030	2.36284	5.19660	3.34094	2.52183
114430	3.90240	1.69453	3.67310	2.57001	7.48150	4.26954	1.66588
114440	1.39900	.91934	1.54670	1.31324	2.34570	2.23303	.37772
114450	2.64220	1.81832	2.21600	1.53131	4.85820	2.54363	.46707
114460	.57923	.80373	.53359	.45975	1.17292	.76361	.16721
114470	2.11300	.67618	.08700	.05655	2.20200	.73271	.01976
114480	0.00000	0.00000	0.00000	0.00000	0.00000	0.10010	0.00000
114491	.01672	.00535	.19613	.12743	.21285	.13233	.24637
114490	1.00000	.72000	.33743	.25186	1.33743	.57166	.14476
115400	0.00000	0.00000	0.00000	0.00000	0.00000	0.00003	0.00000
115420	3.43220	2.03430	3.72550	2.99145	7.21770	5.02625	3.51111
115430	3.69160	1.72374	3.23190	2.84974	6.32390	.27243	2.49808
115440	2.42990	1.36169	2.46000	1.95496	4.33390	3.31565	1.64418
115450	1.32750	1.03325	1.85760	1.45607	3.72510	2.48932	.37407
115460	1.32360	.63568	1.25030	.96615	2.57940	1.65138	.45414
115471	1.01530	.41812	.83261	.63050	1.30791	1.34652	.17171
115470	.35176	.40143	.33673	.59659	1.73849	.29812	.17051
115481	.45372	.14869	.33830	.25240	.86262	.40073	.02275
115480	.31721	.10151	.26562	.17265	.58283	.27416	.02123
115491	.30337	.00268	.32931	.21405	.33763	.21673	.04009
115490	.13430	.04238	.10753	.06993	.24183	.11231	.01930
115500	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
116420	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
116430	.23760	1.77318	4.02430	2.84670	5.23240	.462675	1.56729
116440	1.72370	.98256	2.00530	1.57104	3.72300	2.55360	1.06247
116450	3.04270	1.12361	2.69410	1.43150	5.73686	2.95451	.50555
116460	.75165	.34938	.91708	.59318	1.56373	.34264	.17421
116471	1.95170	.62774	1.59470	1.03656	3.55643	1.66433	.02554
116470	2.18500	.69920	.70960	.46124	2.39466	1.1e3+4	.92240
116480	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
116492	0.00000	0.00000	.25000	.16250	.25000	.16250	.30100
116491	1.01050	.32339	.72760	.47293	1.73319	.79532	.16356
116490	.93265	.31755	.71468	.46454	1.70734	.78213	.16476
116500	0.00000	0.00000	0.00000	1.00000	0.00000	0.00000	0.00000

NICLICE	E_BETA	UNC_BETA	E_GAMMA	UNC_GAMMA	E_TOTAL	UNC_TOTAL	CORR_TOTAL
117430	3.34720	2.00339	3.67560	2.97626	7.02280	4.38025	3.53060
117440	2.84020	1.97375	2.93000	2.41342	5.82020	4.08717	2.44951
117450	2.27170	1.32939	2.31660	1.87902	4.55830	3.20341	1.64007
117460	1.53200	.94230	1.67720	1.36211	3.36920	2.34431	.97053
117471	1.34080	.67867	1.25910	.97059	2.59990	1.66305	.45426
117470	1.27850	.67450	1.20060	.97553	2.47910	1.51204	.45232
117481	.71565	.34154	.65529	.49018	1.37094	.33182	.16639
117480	.63402	.72206	.53055	.44686	1.21457	.76332	.16476
117491	.26206	.08386	.37454	.24345	.53666	.32731	.02373
117490	.40742	.13037	.36235	.22935	.76827	.36372	.02207
117501	0.30000	0.00000	.31700	.29605	.31700	.20505	.04306
117500	0.30000	0.00000	0.00000	0.00000	0.30000	0.06000	0.30000
118430	4.0320	2.22373	4.52350	3.41344	8.32670	5.62117	3.52510
118440	1.33520	1.56526	2.43410	2.18469	4.42930	3.53337	2.51325
118450	3.47830	1.59558	3.20970	2.35832	6.68800	3.85433	1.84964
118460	1.05040	.65135	1.20560	1.14781	2.25600	1.38276	.96232
118471	1.23570	.67316	1.22350	.95431	2.62420	1.63247	.49380
118470	2.31940	.93152	1.93330	1.39667	4.31270	2.32734	.49548
118480	.21260	.23010	.22678	.27163	.43935	.50079	.15040
118492	0.00000	0.00000	.25000	.16250	.25000	.16250	.04300
118491*	1.77532	.20639	.21812	.09927	1.99794	.30626	0.70000
118490*	.62946	.09180	2.57557	.18660	3.20533	.27343	0.00000
118500	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
118440	6.07520	1.71339	3.43960	2.71613	6.56490	4.2352	2.53545
118450	2.56240	1.38534	2.75370	2.13158	5.31510	3.51532	1.66756
118460	2.11050	1.07326	2.17300	1.64486	4.23250	2.71512	.96227
118470	1.59130	.74537	1.53830	1.16675	2.13610	1.31212	.49676
118481	1.04950	.42635	1.01520	.70483	2.16370	1.13513	.17564
118490	.24005	.39732	.31013	.64469	1.35023	1.04251	.17341
118491	.73212	.23428	.69309	.45051	1.42521	.63474	.02409
118490	.69935	.22379	.65012	.42258	1.34947	.54637	.02347
118501	0.00000	0.00000	.03900	.05785	.08900	.05735	.04300
118500	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
120440	2.33820	1.56148	2.93240	2.48070	5.32060	4.04213	2.66423
121450	3.03650	1.64136	3.69700	2.66097	7.33350	4.30233	1.67459

NUCLIDE	E BETA4	UNC BETA4	E GAMMA	UNC GAMMA	E TOTAL	UNC TOTAL	CORR TOTAL
120460	1.33700	.90339	1.61400	1.36599	2.95100	2.26344	.94141
120470	2.72510	1.03938	2.44920	1.68011	5.17430	2.71957	.60416
120480	.44491	.27622	.50303	.41413	.34794	.69235	.16608
120491*	2.47143	.23012	.17574	.11715	2.64722	.34724	0.00000
120490*	1.03965	.19314	3.05971	.22644	4.39336	.37352	0.36000
120500	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
121450	2.32840	1.68472	3.30421	2.61275	6.23320	.23742	.52752
121460	2.34030	1.33727	2.61910	2.05685	4.99440	3.47412	1.67220
121470	1.37900	1.61937	1.98290	1.84151	3.36190	2.56054	.98954
121480	1.34120	.59344	1.40420	1.06086	2.79540	1.75930	.49274
121491	1.03030	.43750	1.03130	.75063	2.17260	1.19313	.17715
121490	1.02000	.41352	1.01110	.70746	2.03160	1.12312	.17616
121501	.17333	.05556	.16402	.10661	.33795	.16227	.02036
121500	.10491	.03357	.09893	.06431	.20384	.03733	.01933
122450	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	1.00000
122440	1.00000	0.80000	0.00000	0.00000	0.00000	0.00000	0.00000
122450	3.33830	1.69033	4.07220	2.89223	7.97120	.59256	1.69071
122460	1.66270	.96539	2.10330	1.84080	3.76650	2.65669	1.01739
122470	2.96580	1.10497	2.91130	1.97406	5.37770	3.07902	.51456
122480	.66074	.32669	.73835	.53016	1.44369	.90535	.17553
122491	2.17130	.69432	1.92840	1.25246	4.03970	1.34826	.02613
122490	2.09380	.67032	1.35950	1.26868	3.95330	1.37379	.02617
122500	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
122511	0.00000	0.00000	.16200	.10530	.16200	.10530	.36100
122510	.55774	.19158	.45631	.30310	1.03466	.43473	.18932
122520	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00010
123450	3.17160	1.72914	3.74630	2.57169	6.91340	.60033	2.55862
123460	2.63060	1.39435	3.05940	2.32198	5.69000	3.71633	1.54953
123470	2.22520	1.69270	2.47360	1.83083	4.63380	2.92232	1.01008
123480	1.60210	.74551	1.75580	1.23073	3.36790	2.02624	.60697
123491	1.32460	.56118	1.39430	.94692	2.71390	1.44810	.18235
123490	1.25300	.48120	1.31830	.89974	2.57190	1.33102	.18161
123501	.47183	.15039	.45548	.30256	.37731	.45355	.02313
123500	.40120	.12338	.33579	.25726	.74699	.38564	.02270
123510	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000

NUCLEUS	E_BETA	NUC_BETA	E_GAMMA	NUC_GAMMA	E_TOTAL	NUC_TOTAL	E_TOTAL	NUC_TOTAL
1230108	0.00000	0.00000	0.24750	0.16083	0.24750	0.16083	0.24750	0.16083
123021	0.00000	0.00000	0.02603	0.01460	0.02603	0.01460	0.02603	0.01460
1230320	0.00000	0.00000	0.00003	0.00000	0.00003	0.00000	0.00003	0.00000
1230406	0.00000	0.00000	0.00003	0.00000	0.00003	0.00000	0.00003	0.00000
1230460	1.34550	1.07220	2.57240	1.99146	4.51720	3.03720	4.51720	3.03720
1230470	3.27470	1.13140	3.35530	2.25690	6.63270	2.43300	6.63270	2.43300
1230470	1.31470	0.41021	1.27270	0.77650	2.22740	0.99170	2.22740	0.99170
1230480	2.25520	0.77140	2.14930	1.42947	4.45560	1.46150	4.45560	1.46150
1230500	0.00000	0.00000	0.00001	0.00000	0.00000	0.00000	0.00000	0.00000
1230512	0.00000	0.00000	0.25420	0.16250	0.25420	0.16250	0.25420	0.16250
1230511	0.00000	0.00000	0.01070	0.00680	0.01070	0.00680	0.01070	0.00680
1230510	-0.3173	-0.2707	-0.74623	-0.44483	1.62767	-0.70353	1.62767	-0.70353
1230500	0.00000	0.00000	0.10800	0.06060	0.10800	0.06060	0.10800	0.06060
1230462	2.36140	1.05611	3.51730	2.76782	6.35971	2.41774	6.35971	2.41774
1230470	2.32560	1.07230	2.35560	2.26125	5.47410	3.05841	5.47410	3.05841
1230470	1.33050	1.01936	2.15970	1.45512	4.37330	2.05100	4.37330	2.05100
1230491	1.738640	0.74178	1.75120	1.42462	3.55700	1.32213	3.55700	1.32213
1230490	1.52990	0.72020	1.70115	1.24387	3.27140	1.37132	3.27140	1.37132
1230501*	-0.73301	-0.14629	-0.34545	-0.33460	1.14347	-0.14347	1.14347	-0.14347
1230500*	-0.36150	-0.16372	-0.31227	-0.24450	1.14448	-0.21632	1.14448	-0.21632
1230510*	-0.33636	-0.21641	-0.42267	-0.34561	0.63493	-0.16134	0.63493	-0.16134
1230511*	0.00000	0.00000	0.14373	0.05482	0.14373	0.05482	0.14373	0.05482
1230520	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
1230480	2.24270	1.05037	3.03945	2.66644	6.57710	2.16241	6.57710	2.16241
1230470	3.47310	1.56540	4.73370	2.73475	8.20850	2.42164	8.20850	2.42164
1230470	1.27420	0.69930	1.63670	1.12130	2.87460	0.36560	2.87460	0.36560
1230460	2.36180	1.36720	2.54720	1.77380	5.12810	2.76421	5.12810	2.76421
1230500	-0.37200	-0.19634	-0.34980	-0.16761	0.14986	-0.34986	0.14986	-0.34986
1230511	1.00760	0.32111	1.12523	0.54597	1.33985	0.38305	1.33985	0.38305
1230510	-0.37800	-0.11450	2.67100	1.77560	3.12240	1.43010	3.12240	1.43010
1230520	0.01000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
1230470	2.36140	1.05253	3.45710	2.72120	6.18350	2.37314	6.18350	2.37314
1230480	2.39670	1.26304	2.56190	2.09776	4.65350	3.34032	4.65350	3.34032
1230491	1.05730	0.83140	2.23080	1.73293	4.24410	2.76440	4.24410	2.76440
1230490	1.37230	1.01454	2.13310	1.67753	4.05600	2.51140	4.05600	2.51140
1230511*	1.13421	0.21649	0.49400	0.64712	1.62641	0.25751	1.62641	0.25751

JUL/ICE	E_BETA	U40_BETA	E_GAMMA	UVC_GAAMA	E_TOTAL	UMD_TOTAL	WGT_L1	L1_P2	TOTAL
127500*	-0.57455	-1.12549	-1.1+3431	-0.57147	2.11344	-1.1753	-0.30670		
127510*	-0.31835	-0.74857	-0.6+432	-0.14787	-0.3133	-0.16727	-0.30616		
127521	-0.01493	-0.00136	-0.0+137	-0.05971	-0.04493	-0.06143	-0.07773		
127520*	-0.22723	-0.54133	-0.00517	-0.03181	-0.21341	-0.0431	-0.0431		
127530	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000		
128480	-0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000		
128470	-0.62060	-1.01177	-0.03673	-0.01062	-0.63070	-0.04457	-0.07174		
128490	1.05750	-0.94023	2.13763	1.07413	2.05452	2.05141	1.03197		
128480	2.03423	1.00573	3.00430	2.07642	3.05692	3.01842	1.05234		
128500*	-0.21720	-0.03550	-0.53651	-0.03210	-0.3133	-0.0731	-0.06103		
128511*	-0.4726	-0.15931	1.03603	-0.37163	2.13334	-0.27421	-0.05601		
128510*	-0.41843	-0.07320	3.03960	-0.0174	2.51-0.7	-1.1346	-0.01070		
128520	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000		
128530	-0.74203	-0.23336	-0.15500	-0.10375	-0.30330	-0.84012	-0.17721		
128540	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000		
128470	-0.10000	-0.00000	0.00000	0.00000	0.00000	0.00000	0.00000		
128480	2.3+513	1.32356	3.00833	2.36468	3.02691	3.05937	1.01151		
128490	2.05730	1.05271	2.055130	1.08187	4.01320	2.0446	1.03264		
128501	1.21640	-0.60439	1.47040	1.11782	2.04725	1.07724	1.06172		
128500	1.1+520	-0.83477	1.038470	1.058373	2.052390	1.071360	0.61703		
128510*	-0.36911	-0.19423	1.30175	-0.16143	1.66316	-0.21560	-0.05101		
128521*	-0.21402	-0.05039	-0.22830	-0.11261	-0.24352	-0.0533	-0.06000		
128520*	-0.03334	-0.17359	-0.07293	-0.02856	-0.03574	-0.02411	-0.00613		
128530	-0.56243	-0.01937	-0.04213	-0.02663	-0.1021	-0.04533	-0.01177		
128541	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000		
128540	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000		
130460	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000		
130460	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000		
130470	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000		
130480	-0.63453	1.006518	2.059490	1.09724	-0.67250	0.07127	1.06014		
130490	2.053031	1.07936	3.0+3240	2.031262	0.62360	0.34243	0.03274		
130500	-0.50250	-0.25326	-0.63651	-0.52763	-0.14924	-0.16657	-0.17603		
130511*	1.029322	-0.15270	2.043946	-0.14702	3.05326	-0.2993	-0.00000		
130510*	1.25067	-0.18210	2.014048	-0.14526	2.0+116	-0.62730	-0.00000		
130520	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000		
130531	-1.4567	-0.04373	-0.4705	-0.22553	-0.23372	-0.04331	-0.15741		

DECIMAL	DECIMAL	DECIMAL	DECIMAL	DECIMAL	DECIMAL	DECIMAL	DECIMAL	DECIMAL	DECIMAL	DECIMAL	DECIMAL	DECIMAL	DECIMAL	DECIMAL	DECIMAL	DECIMAL	DECIMAL	DECIMAL	DECIMAL
1.31530	.22532	.29446	2.12010	1.37807	2.41863	1.47247	1.24744												
1.31540	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	
1.31541*	3.1+5.9	1.71058	4.25820	3.20115	7.+0+10	+.31127	2.0+0+14												
1.31542*	2.3+3.2	1.82744	3.07030	2.85567	6.+1409	7.34432	1.12729												
1.31543*	1.30541	.99336	1.73680	1.43082	3.04236	2.35247	1.03044												
1.31544*	.71353	.99447	1.75271	.17397	2.41620	.27247	.0+0+13												
1.31545*	.12213	.03741	1.43113	.13814	1.57331	.17224	.0+0+12												
1.31546*	.57172	.16522	.42335	.07454	1.03457	.17741	.0+0+11												
1.31547*	.13553	.76058	.54928	.44567	.57477	.07743	.0+0+10												
1.31548*	1.01003	0.00001	.16754	.00382	.14754	.06387	.0+0+09												
1.31549*	0.01002	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	
1.32420	2.64123	1.61973	3.43768	3.16212	6.04841	.0+0+12	.0+0+11												
1.32440	3.82470	1.66256	4.60050	3.57482	6.0+037	.0+0+10	.0+0+09												
1.32506*	.66033	.10314	1.32273	.03143	1.33354	.11167	.0+0+08												
1.32511*	1.52553	.49256	2.05862	.12710	2.73+16	.51373	.0+0+07												
1.32510*	1.71212	.21721	2.10680	.17783	2.72611	.34114	.0+0+06												
1.32521*	.36265	.00338	.26860	.01366	.32865	.31632	.0+0+05												
1.32530*	.52453	.04758	2.23771	.14284	2.76238	.23744	.0+0+04												
1.32540	0.03000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	
1.33490	2.33723	1.78337	.44654	3.31564	7.30272	.0+0+11	.0+0+10												
1.33500	2.03249	1.27264	2.31430	2.21987	3.89730	.4+0741	.0+0+09												
1.33510*	.53711	.09128	.16247	.05347	.53495	.4+0315	.0+0+08												
1.33521*	.57207	.09276	1.35615	.15067	.4+1122	.2+2+5	.0+0+07												
1.33530*	.31333	.18338	.93324	.11737	1.30382	.2+2+7	.0+0+06												
1.33531	0.07000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	
1.33532*	.41713	.67638	.63835	.16482	1.01813	.13334	.0+0+05												
1.33541*	0.00000	0.00000	.23268	.00841	.23265	.0+0+04	.0+0+03												
1.33542*	.10183	.01173	.08144	.00965	.15302	.0+0221	.0+0+02												
1.33543*	0.01000	0.00000	.00100	.00000	.00000	0.0+000	0.0+000												
1.33544*	.51115	1.70512	.11770	.05723	.1+055	.0+775	.0+0+01												
1.33545*	1.65423	.96634	.47110	.07973	4.13032	.28327	.0+0+00												
1.33546*	2.93377	.47519	.03843	.14741	5.04820	.42313	.0+0+00												
1.33547*	2.43105	.27634	.06000	.00000	.00000	.05103	.27533	.0+0+00											
1.33548*	.16203	.02311	.02427	.02467	.37762	.0+773	.0+0+00												
1.33549*	0.07000	0.00000	.01570	.02776	.31570	.02776	.0+0+00												



NUC-L109	F-BETA4	UNC-F:TA	C-GAMMA44	UNC-GAMMA	F-TOTAL	UNC-F TOTAL	UNC-G TOTAL	F TOTAL
133510	7.22030	1.51436	4.22840	3.68395	7.44320	4.54342	1.78059	
133520	1.41020	.98412	2.17900	1.71313	2.43320	2.37211	1.74712	
133530	2.12120	.97072	2.79112	1.63634	2.42230	2.37113	1.61159	
133540*	.55770	.09410	1.13526	.52625	1.35270	.17443	.30003	
133551*	1.14690	.19475	2.03968	.15362	2.24658	.54341	.30730	
133550*	1.23240	.14657	2.32913	.07295	2.52153	.21762	.30610	
133560	3.10002	3.22076	2.30653	3.02068	3.02000	3.01031	3.02001	
133570	1.00000	3.00000	.84001	.54600	.84000	.54600	.30100	
133580	1.30000	1.61000	1.00000	3.00003	3.00000	3.00000	3.00000	
133590	2.65370	1.41557	3.34260	2.94790	4.48682	4.34577	2.61748	
133600	2.14540	1.27455	3.11460	2.59920	2.26000	2.08735	1.67441	
133610	1.76120	.97735	2.47273	1.86618	1.22350	1.14611	1.01463	
133620	1.73673	.14151	.82762	.00346	2.71433	.14537	.30000	
133630*	1.70363	.12239	.31076	.02294	2.07445	.14304	.30000	
133640*	.39722	.14316	.05223	.01596	.34951	.14112	.30000	
133650	3.01002	3.00000	0.00000	0.00000	3.00000	3.00000	3.00000	
140520	1.68370	1.41237	2.61230	2.87079	4.24256	3.72975	2.68131	
140530	2.03760	1.27011	2.93243	2.23614	5.01973	3.56515	1.70423	
140540	.84274	.20617	1.35240	1.29298	2.24314	2.03703	1.61564	
140550*	1.83124	.23450	2.13113	.29754	4.06232	.53264	.30000	
140560*	.29027	.03431	.21687	.00733	.4714	.04192	.30000	
140570*	.51732	.64736	2.20411	.14439	2.72144	.27425	.30000	
140580	3.00002	1.05000	0.00000	0.00000	3.00000	3.00000	3.00000	
141510	3.00000	3.00000	0.00000	0.00000	3.00000	3.00000	3.00000	
141520	2.47980	1.79643	3.60040	3.04756	5.01322	.36343	1.74424	
141530	1.34790	1.47612	2.85670	2.44546	4.33463	.36312	2.66413	
141540	1.37140	1.17219	2.27010	1.54553	3.34159	.12174	1.71414	
141550	1.37700	.95635	1.32430	1.43654	3.20181	.12342	1.61349	
141560*	.21563	.14359	.83732	.01325	1.8345	.12634	.30000	
141570*	.33933	.05327	.03231	.00147	1.02263	.03624	.30000	
141580*	.15943	.02652	.07170	.01049	.23113	.03711	.30000	
141590	3.00000	3.00000	0.00000	0.00000	3.00000	3.00000	3.00000	
142520	1.74040	1.42657	2.30630	2.52277	4.53276	.36342	2.65412	
142530	2.31410	1.44157	3.33120	2.85933	6.33593	.40031	1.71312	
142540	1.04730	.64239	1.75540	1.53381	2.36276	.34575	1.37742	

NUCLIDES	E BETA	UNC BETA	E GAMMA	UNC GAMMA	E TOTAL	UNC TOTAL	CORR TOTAL
142550	2.04430	.45171	2.54450	1.76221	4.58930	2.51392	.52757
142560*	.42825	.16130	1.01269	.63744	1.44097	.03924	0.00000
142570*	.34702	.13235	2.56469	.86997	3.51171	.26232	0.00000
142580	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00010
142591	0.00000	0.00000	.25000	.16250	.25000	.16250	.30100
142592	.81701	.25624	.05820	.03783	.86520	.23627	.12546
142600	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
143520	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
143530	2.21000	1.76362	3.31060	2.92401	5.51060	4.58470	3.67555
143540	1.73530	1.44930	2.53390	2.33774	4.44870	3.83764	2.60063
143550	1.55540	1.17446	2.15880	1.88471	3.73320	3.05917	1.71166
143560	1.03380	.94802	1.57060	1.37982	2.55380	2.32764	1.81809
143570	.33124	.57114	1.14330	.94890	1.97204	1.62304	.56256
143580*	.41913	.06537	.29534	.03760	.71497	.10237	0.00000
143590*	.32392	.06120	0.00000	0.00000	.32392	.06120	0.00000
143600	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
144520	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
144530	3.01130	1.91137	4.20310	3.35635	7.21660	5.26322	3.67649
144540	1.23660	1.35748	2.00390	2.10614	3.20450	3.444365	2.54988
144550	2.34970	1.72856	3.04130	2.37582	5.39160	3.66537	1.73016
144560	.64757	.76027	1.04620	1.15245	1.63407	1.31142	.99279
144570	1.61050	.71977	1.93650	1.33605	3.44700	2.11530	.62137
144580*	.03296	.66176	.92867	.00132	.11183	.00303	0.00000
144591*	.00130	.00010	.05973	.00202	.05005	.00212	0.00000
144592*	1.26277	.00470	.03101	.00080	1.29373	.00553	0.00000
144600	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
145530	2.43250	1.79348	3.79490	3.15702	6.22740	4.36047	3.72039
145540	1.33570	1.47311	3.05040	2.59212	5.03610	4.16323	2.82939
145550	1.64070	1.18417	2.33110	2.00759	4.02180	3.19176	1.72362
145560	1.24660	.38269	1.92180	1.57196	3.20840	2.45456	1.03340
145570	1.05520	.61635	1.51950	1.15431	2.57790	1.76015	.51807
145580*	.62924	.10346	.74893	.03680	1.37387	.19026	0.00000
145590*	.72465	.13157	.01373	.00435	.71343	.13592	0.00000
145600	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
146540	1.44920	1.37365	2.50410	2.35333	3.95330	3.72693	2.64257

NUCLIDE	$\beta^-$	$\beta^+$	$\gamma$ GAMMA	$\alpha$	$\gamma$ GAMMA	$\tau$ TOTAL	$\nu$ TOTAL	$\bar{\nu}$ TOTAL	$\beta^-$ TOTAL
146550	2.47340	1.35131	3.32320	2.00463	5.30160	3.37537	1.75477		
146560	.72447	.77239	1.21593	1.23386	1.34977	2.02265	1.01134		
146570	1.75773	.75015	2.35768	1.45322	4.12621	2.43537	1.75612		
146580*	.24893	.04932	1.31436	.04044	1.65610	1.37541	1.30616		
146590*	.32720	.14543	1.63434	.16713	2.56244	1.36265	1.75600		
146600	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000		
146610	2.18340	1.94327	3.53233	3.36535	5.71513	3.74722	1.24413		
146620	1.26266	1.72246	2.34763	2.74750	4.38521	1.41537	3.35613		
146630	1.44132	1.35717	2.21593	2.18294	3.65520	1.31711	2.35740		
146640	1.15173	1.69514	1.72443	1.71384	2.67546	2.74703	1.65413		
146650	.36132	.95276	1.27143	1.23477	2.12272	1.24437	1.33946		
146660*	.74733	.12030	.82009	.12074	1.50307	.24117	1.00410		
146670*	.24104	.05035	.11371	.03710	1.50304	.14727	1.21510		
146680*	.25330	.01451	.00010	.00157	.00810	.11361	1.30114		
146690	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000		
146700	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000		
146710	2.72370	1.84976	7.44276	2.11777	6.56547	4.21483	1.24134		
146720	.35933	.91213	1.56380	1.46774	2.61383	2.27987	1.30419		
146730	1.43410	.02649	2.56651	1.44502	4.60666	2.36751	1.03679		
146740	.36632	.25331	.61256	.30164	.33050	.76132	1.17551		
146750*	2.04555	.22546	.73093	.05311	2.34362	.24331	2.02657		
146760	0.00010	0.01026	0.00000	0.00000	0.00000	0.00000	0.00000		
146770*	.14763	.03072	2.00973	.11573	2.15071	.14410	1.30438		
146780*	.74430	.10334	.63033	.21781	1.37467	.35147	1.22010		
146790	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000		
146800	2.24830	1.76147	3.42251	3.52752	5.72131	4.74713	1.70246		
146810	1.64210	1.41341	3.65740	2.46774	4.30794	3.19112	1.36463		
146820	1.73430	1.18724	2.13220	1.52743	3.63206	3.36342	1.37512		
146830	.34953	.12617	1.62420	1.37934	2.24761	2.19641	1.31461		
146840*	1.16732	.11551	.25127	.05663	1.42204	.27214	1.17415		
146850*	.47432	.07914	.33575	.01794	.41110	.07112	1.14426		
146860*	.57653	.07825	.61423	.02424	.89041	.02757	1.30750		
146870	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000		
150550	2.11830	1.435676	4.34220	3.12375	7.26110	4.50731	1.71679		
150560	1.21330	.15733	2.19310	1.75530	3.41110	2.61237	1.17413		

NUCLEUS	z	3ETR	INC 3ETR	z	G444A	JJC G444A	z	TOTAL	INC TOTAL	JJC TOTAL	z
151570	2.14260	.47204	3.12750	2.17454	5.27310	3.10002	2.14545				
152590	.55133	.29708	.95795	.70422	1.51386	1.16123	1.46518				
153590	1.35450	.47444	1.35760	1.26744	5.21210	1.54047	1.60735				
151630	0.00010	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	
153510	.75920	.23620	1.51070	.94169	2.24300	1.21571	1.25617				
151620	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	
151560	1.37310	1.67752	1.22430	1.67152	5.27710	1.41414	1.47172				
151570	1.63070	1.42617	2.71950	2.43622	5.20351	1.35533	1.38173				
151580	1.17790	1.03247	1.99320	1.92147	5.17804	1.42265	1.472437				
151590	.32615	.21417	1.44863	1.38546	5.37600	2.14387	1.31714				
151610*	.54413	.18028	.63827	.10771	1.43843	.11357	1.16015				
151610*	.51135	.14739	.32030	.04617	5.21450	.14373	0.75012				
151620	.31950	.17634	.33040	.03283	5.19293	.10253	.31153				
151630	0.11030	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	
152560	1.46530	1.76628	2.72600	2.43283	5.14190	3.16110	3.46436				
152570	2.33800	1.32110	3.63343	2.74274	5.07190	1.36335	1.37143				
152580	.73372	.78026	1.44260	1.36697	5.27630	2.14725	1.16216				
152590	1.62261	.74207	2.35320	2.04450	5.35540	1.42697	1.37465				
152600	.23305	.22611	.55920	.07041	5.36223	.08532	.17102				
152610	.30266	.21914	1.15060	.74734	1.96226	1.08642	1.21621				
152611*	.41343	.67738	1.24720	.43474	1.70573	.21212	1.36516				
152610*	1.45675	.18768	.24314	.02470	1.72642	.21243	1.00010				
152620	1.30600	0.60630	0.60600	1.02960	5.20300	1.06060	0.60600				
152630	1.30600	0.60600	0.37300	.05357	5.27780	.08357	.280400				
152631	.43363	.13378	.57816	.27645	1.31275	.11421	.17224				
152670	.42547	.18618	.55327	.07435	5.3774	.07825	.17222				
152640	0.39000	0.50000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	
153570	1.43610	1.45495	3.26270	2.82761	5.22211	.14311	1.67307				
153580	1.40360	1.12650	2.41050	2.07146	5.11110	3.17711	1.71611				
153590	1.19350	.96047	1.34510	1.60574	5.14780	2.40100	1.34667				
153600	.73190	.65745	1.23660	1.07544	5.03900	1.51233	1.23841				
153610*	.57263	.41344	.37743	.07103	5.35114	.09347	.26610				
153620*	.23070	.02478	.10452	.06480	5.2622	.02323	.10010				
153630	1.30000	0.60600	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	
153640	1.30000	0.60600	.12000	.07400	5.27300	.07610	.17100				

WCLL175	L BETA	UNC BETA	L GAMMA	UNC GAMMA	L TOTAL	UNC TOTAL	CORR TOTAL
154570	2.62620	1.76664	2.20750	3.05620	6.33370	-1.2244	6.36304
154580	1.02430	.71576	1.92620	1.62341	2.95110	2.43311	1.62756
154600	1.30740	.79716	2.45670	1.97520	4.72310	1.77551	1.84712
154630	.33341	.25935	.69855	.55053	1.07366	.31249	.15415
154611	1.03370	.67678	1.52230	.96950	2.57650	1.32324	2.27719
154612	.75030	.24520	1.82470	1.22506	2.84470	1.46624	2.30936
154620	2.03070	0.03620	0.01920	0.00370	2.03000	0.31011	2.00000
154630	.24700	.07230	1.25000	.71250	1.49701	.49101	.21642
154640	0.03330	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
154670	2.23360	1.74331	3.34030	3.27725	6.12046	5.02146	6.71139
154690	1.54950	1.46012	2.93650	2.57641	4.57100	3.27451	3.67643
154690	1.47220	1.16537	2.45840	2.05725	3.36450	2.31450	2.76113
154690	.93330	.50344	1.61040	1.04446	2.55370	2.02454	2.04304
154610	.77243	.54818	1.21350	1.00928	1.35075	1.56344	1.01714
154620	.67145	.25921	.611187	.43582	.74372	.76551	.17867
154630	.75453	.31743	.34735	.25661	.14206	.55471	.68143
154640	1.00000	0.00000	1.00000	0.00000	1.00000	1.00000	1.00000
154650	1.30360	1.07358	2.62273	2.41046	3.37870	2.74461	2.67743
154690	2.11400	1.26237	3.32460	2.93726	5.30380	3.24243	4.71444
154690	.53486	.74127	1.13020	1.07112	1.72450	1.37235	1.32726
154610	1.26631	.76431	1.42010	1.42017	2.21546	2.07233	2.03349
154620	.14875	.03570	.27775	.12381	.42724	.55417	.15410
154630	.43520	.08124	1.31770	.41021	1.74790	.25345	.03676
154640	1.00000	0.00000	1.00000	0.00000	1.00000	1.00000	1.00000
154650	1.61110	1.14411	2.65210	2.45173	3.83780	2.24267	2.31014
154660	1.75530	1.16521	3.34240	2.41111	4.79770	3.35961	4.76473
154670	1.15420	.74631	2.04720	1.62760	3.84540	2.54741	3.08747
154610	.97722	.69318	1.42497	1.26579	2.62256	1.94436	1.67260
154620	.55363	.20772	.35777	.10796	1.62140	1.10147	.139416
154630	.25812	.06207	.47374	.32668	.73167	.39354	.02473
154640	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
154650	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
154660	2.31521	1.31637	3.32310	2.69463	6.31180	4.21123	4.12906
154660	.35535	.74547	1.63030	1.56294	2.53620	2.24347	1.30304
154610	1.69120	.73337	2.55410	1.73813	4.14530	2.51419	.64374

NUCLEUS	$\pi^-$ BETA	UNO BETA	$\pi^+$ BETA	$\pi^-$ GAMMA	UNO GAMMA	$\pi^+$ GAMMA	$\pi^-$ TOTAL	UNO TOTAL	$\pi^+$ TOTAL	CORR TOTAL
163620	-2.41+7	-2.32+7	-2.32+7	-4.65+0	-4.28+0	-4.28+0	-7.36+7	-6.61+7	-4.17+7	-4.17+7
163630	-3.2+7	-3.0+3	-3.0+3	-1.37+0	-1.37+0	-1.37+0	-2.42+7	-1.14+7	-0.62+7	-0.62+7
163640	-3.07+0	-3.07+0	-3.07+0	-3.10+0	-3.07+0	-3.07+0	-3.00+0	-3.00+0	-3.00+0	-3.00+0
163650	-2.144+6	-2.144+6	-2.144+6	-3.63+3	-2.97+3	-2.97+3	-3.72+3	-3.43+3	-2.71+3	-2.71+3
163660	-1.337+0	-1.114+3	-1.114+3	-2.36+3	-2.13+3	-2.13+3	-3.35+7	-3.2+5	-1.74+6	-1.74+6
163670	-1.256+3	-1.866+6	-1.866+6	-2.13+3	-1.75+6	-1.75+6	-3.45+7	-2.61+3	-1.36+7	-1.36+7
163680	-1.701+6	-1.639+4	-1.639+4	-1.275+3	-1.077+3	-1.077+3	-1.37+7	-1.14+3	-1.57+7	-1.57+7
163690	-1.776+3	-1.362+6	-1.362+6	-1.325+3	-1.72+6	-1.72+6	-1.64+6	-1.12+6	-1.12+6	-1.12+6
1636A0	-1.139+2	-1.603+4	-1.603+4	-1.351+2	-1.20+3	-1.20+3	-1.55+4	-1.24+2	-1.59+4	-1.59+4
1636B0	-0.210+0	-0.203+0	-0.203+0	-0.30+0	-0.30+0	-0.30+0	-0.30+0	-0.30+0	-0.30+0	-0.30+0
1636C0	-0.210+0	-0.203+0	-0.203+0	-0.20+0	-0.16+0	-0.16+0	-0.30+0	-0.16+0	-0.16+0	-0.16+0
1636D0	-1.117+9	-1.828+6	-1.828+6	-2.257+3	-1.513+3	-1.513+3	-2.371+6	-1.8+4	-1.7+4	-1.7+4
1636E0	-1.434+3	-1.794+3	-1.794+3	-3.039+0	-2.67+3	-2.67+3	-4.338+3	-2.48+1	-1.51+3	-1.51+3
1636F0	-1.538+3	-1.805+4	-1.805+4	-1.192+3	-1.24+6	-1.24+6	-1.74+6	-1.12+1	-1.19+1	-1.19+1
1636G0	-1.355+2	-1.273+4	-1.273+4	-1.413+3	-1.91+5	-1.91+5	-2.264+4	-1.192+5	-1.527+5	-1.527+5
1636H0	-1.202+3	-1.875+3	-1.875+3	-1.802+3	-1.802+3	-1.802+3	-2.163+5	-1.17+1	-1.22+6	-1.22+6
1636I0	-1.711+6	-1.128+7	-1.128+7	-1.6+2	-1.416+3	-1.416+3	-1.6+3	-1.24+3	-1.17+3	-1.17+3
1636J0	-0.303+0	-1.302+0	-1.302+0	-0.30+0	-0.30+0	-0.30+0	-0.319+0	-0.30+0	-0.30+0	-0.30+0
1636K0	-1.656+20	-1.389+6	-1.389+6	-5.212+3	-4.759+3	-4.759+3	-4.50+3	-1.1+7	-2.727+5	-2.727+5
1636L0	-1.537+3	-1.143+7	-1.143+7	-2.734+3	-2.2+18	-2.2+18	-4.322+1	-3.42+2	-1.79+11	-1.79+11
1636M0	-1.362+3	-1.61+3	-1.61+3	-1.73+3	-1.54+5	-1.54+5	-2.71+7	-2.7+17	-1.21+13	-1.21+13
1636N0	-1.739+6	-1.143+5	-1.143+5	-1.357+3	-1.09+5	-1.09+5	-2.076+5	-1.38+7	-1.524+6	-1.524+6
1636O0	-1.431+6	-1.271+6	-1.271+6	-1.272+3	-1.63+4	-1.63+4	-1.274+6	-1.37+7	-1.18+4	-1.18+4
1636P0	-1.121+4	-1.163+2	-1.163+2	-2.157+5	-1.4+24	-1.4+24	-1.372+1	-1.17+3	-1.02+4	-1.02+4
1636Q0	-0.110+0	-0.105+0	-0.105+0	-0.08+0	-0.07+0	-0.07+0	-0.362+1	-0.1+3	-0.105+0	-0.105+0
1636R0	-0.105+0	-0.105+0	-0.105+0	-0.08+0	-0.07+0	-0.07+0	-0.362+1	-0.1+3	-0.105+0	-0.105+0
1636S0	-1.124+3	-1.056+3	-1.056+3	-2.647+3	-2.775+3	-2.775+3	-3.412+7	-4.261+2	-1.412+4	-1.412+4
1636T0	-1.712+4	-1.756+4	-1.756+4	-1.458+5	-1.437+5	-1.437+5	-2.174+4	-2.16+3	-1.31+5	-1.31+5
1636U0	-1.246+10	-1.649+4	-1.649+4	-2.132+3	-1.829+3	-1.829+3	-3.34+7	-2.17+5	-1.34+3	-1.34+3
1636V0	-1.212+3	-1.28+36	-1.28+36	-1.416+3	-1.416+4	-1.416+4	-1.612+7	-1.612+3	-1.273+3	-1.273+3
1636W0	-1.386+3	-1.319+2	-1.319+2	-1.1+6	-1.74+3	-1.74+3	-1.372+6	-1.36+2	-1.327+1	-1.327+1
1636X0	-1.623+6	-1.211+6	-1.211+6	-1.052+3	-1.6+4	-1.6+4	-1.642+3	-1.386+3	-1.228+7	-1.228+7
1636Y0	-1.312+0	-1.308+10	-1.308+10	-2.00+0	-2.00+0	-2.00+0	-3.00+0	-1.00+0	-1.00+0	-1.00+0
1636Z0	-0.300+0	-0.300+0	-0.300+0	-0.30+0	-0.30+0	-0.30+0	-0.30+0	-0.30+0	-0.30+0	-0.30+0
1636AA	-1.227+3	-1.943+2	-1.943+2	-2.372+3	-1.47+3	-1.47+3	-3.676+3	-2.713+2	-1.33+16	-1.33+16

WICLIDF	E_BETA4	UND_BETA4	E_GAMMA4	UND_GAMMA4	E_TOTAL	UND_TOTAL	E_DIF	UND_DIF
1e-6e20	1.04630	.60263	1.96170	1.44737	2.30869	2.63797	-.32974	.32974
1e-3e40	.59303	.70232	1.03650	.77364	1.46669	1.46669	0.00000	0.00000
1e-3e50	.73333	.11450	.65933	.42460	1.31772	.77324	.54448	.54448
1e-3e60	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
1e-4e10	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
1e+0e20	.94081	.72417	1.04465	1.63229	2.33741	2.17504	.16237	.16237
1e+0e30	1.57820	.72325	2.37150	1.96674	2.37150	2.37150	0.00000	0.00000
1e+0e40	.34725	.25124	.72739	.57437	1.37464	.52621	.84843	.84843
1e+0e50	.37275	.27923	1.48980	.96344	2.36261	2.12773	.23488	.23488
1e+0e60	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
1e-5e20	1.45910	1.11504	2.33080	2.33014	4.33074	3.42027	.90947	.90947
1e-5e30	1.23840	.56456	2.43370	1.95073	2.74306	2.74306	0.00000	0.00000
1e-5e40	.77760	.54642	1.54840	1.81386	2.32706	1.70514	.62192	.62192