AN ABSTRACT OF THE THESIS OF

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A new method was developed to produce an anti-fungal drug, itraconazole, $(C_{35}H_{38}C_{12}N_8O_4)$, using supercritical carbon dioxide. Different operating conditions (five levels of temperature, four levels of pressure, four different treatment times, flow, cooling and mixing) were tested in order to produce a desired itraconazole product which does not degrade during the product formation and has the highest dissolution rate in gastric fluid. An intrinsic mathematical model was also developed to predict some of the products.

The optimum treatment condition was found to be at 135 °C, 300 atm and 30 minutes of SC CO₂ flow through itraconazole solution. The dissolution profiles of itraconazole in gastric fluid at different treatment conditions predicted by the mathematical model agreed with experimental data.

Itraconazole Formation Using Supercritical Carbon Dioxide

by

Yi-Min Tang

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NOMENCLATURE

A	Interfacial area of drug, cm ²
С	Concentration in gastric fluid at any time, mg/L
k	Convective- mass transfer coefficient, cm/min
М	Mass of drug substance remaining to be dissolved, mg
Р	Treatment pressure, atm
R^2	R-square value
SEE	Sum of the squares of the errors
SST	Sum of the squares of the deviations
Т	Treatment temperature, °C
t	Time

Greek letter

α	Constant in E	qn. (6.4),	kA/V, min '	

Subscripts

i	Experiment identifier
С	Critical property
S	Property at saturation condition

Superscripts

Exp	Experimental determined parameter
Cal	Calculated parameter

Symbol

-

Average

ITRACONAZOLE FORMATION USING SUPERCRITICAL CARBON DIOXIDE

CHAPTER 1 INTRODUCTION

Supercritical Fluid science and technology have given new directions in research and applications in the last few years. Supercritical Fluid technology is growing rapidly because of the unique physical properties of such fluids. They can simply change from gas-like to liquid-like by adjusting the pressure and temperature. Because of these special characteristics, supercritical fluids are used in extractions, separations, chemical reactions, impregnation, polymer processing, food processing, environmental remediation and pharmaceutical production (Kiran and Brennecke, 1993).

Supercritical carbon dioxide has been chosen in the new technology because of its several advantages: cheapness, non-toxicity and nonflammable properties, and its availability. It is also easy to operate because of the convenient critical temperature and pressure of carbon dioxide ($T_c = 31.3$ °C, P_c = 72.9 atm).

One important application of SCFs is in drug formation. The Food and Drug Administration (FDA) examines new product ingredients, manufacturing processes, toxicological studies on animals, therapeutic claim, and clinical trials on human beings very strictly (Ansel. Popvich and Allen, jr. 1995). The FDA has strict requirements for the use of organic solvents and surfactants in drugs because many organic solvents and surfactants are not safe for humans or the environment. Organic solvents and detergents are used in some conventional drug formulations to produce a homogeneous solution. Therefore the FDA requires that most solvents and detergents need to be removed from the solution before the drug can be used for human use. Removal of such chemicals usually involves a high temperature process (spray drying and melt pressing), which may cause drug degradation. A comparison between conventional drug formation methods and supercritical carbon dioxide method is shown in Table 1.1.

Itraconazole is an anti-fungal agent, which has therapeutic effects for patients who have fungal diseases, for example, AIDS (Acquired Immune Deficiency Syndrome) patients. It is poorly soluble in aqueous solutions and since it is to be dissolved in gastric or intestine fluids, it is desirable to increase its solubility in aqueous solutions.

In order to reduce drug blood level fluctuations, dosage frequency and health care cost, controlled-release drugs have been developed rapidly. Some drugs, such as itraconazole, need to have rapid oral absorption. Drug particles from conventional formulation methods are larger and less porous resulting in smaller surface area, so the drug takes longer to dissolve in the fluids of human bodies. Sometimes the efficacy of the drug can be severely limited by its poor aqueous solubility, and some side effects of certain drugs are due to poor solubility. Therefore, increasing drug dissolution rate would be highly valuable.

Table 1.1Comparison of conventional method and supercritical carbon
dioxide method.

Conventional Method	Supercritical Carbon Dioxide Method
Several steps, such as dissolving drug in solvent, removal of solvent, coating and milling or grinding.	Fewer steps. No need for solvent removal, and drying.
Organic solvent and surfactant are needed	SC carbon dioxide instead of organic solvent. CO_2 is safe (nonflammable and nontoxic).
High temperature operation. Degradation or denaturation caused by heat or oxygen in the process.	Mild temperature condition.
High cost of solvent disposal.	Lower cost of solvent disposal (CO ₂ is safe).
Size reduction techniques (i.e. milling and grinding) are needed and such techniques usually affect the crystallinity and chemical stability of pharmaceuticals.	Fine particles can be produced.

Supercritical fluid technology has the potential to solve some of the problems associated with conventional drug formulations. The focus of this research is forming itraconazole into a successful drug product formulation using supercritical fluids. Itraconazole and all other ingredients are mixed with supercritical carbon dioxide instead of an organic solvent. Higher porous itraconazole particles can be produced in supercritical carbon dioxide. The larger surface area of itraconazole particles should result in faster dissolution rate of the drug in gastric fluid. Since no or little organic solvent needs to be used in the process, the solvent-handling fee is expected to be lower.

To find the optimum treatment temperature and pressure of supercritical carbon dioxide and the treatment time to produce itraconazole, different experiments at different conditions were performed in this study. The dissolution profiles of itraconazole products produced in this study were measured for each sample in order to determine the dissolution rate of itraconazole in gastric fluid. Dissolution studies were carried out in simulated gastric fluids at 37.5 °C and the results compared with the commercial itraconazole product, Sporanox, as a reference.

Chapter 2 presents an introduction to itraconazole, conventional methods to produce the itraconazole, formulation Sporanox[®], and the problems, an introduction to supercritical fluids and a literature review of drug delivery systems, and the controlled release of drugs. The objectives of this work are given in Chapter 3. Chapter 4 discusses experimental materials and methods. The results are presented in Chapter 5. Finally conclusions, and future work are included in Chapter 6.

CHAPTER 2

BACKGROUND AND LITERATURE REVIEW

Itraconazole formulation development includes several steps: solubility study in SC CO₂, formulation study, drug formation methods, drug delivery system and dissolution study. Then there will be some clinical investigations and drug regulatory evaluation before going to market. Those steps are shown in the flow chart (Fig 2.1). Formulation study has been done in the Pharmacy Department. This study focused on supercritical fluids technology and dissolution study. Drug delivery systems development will be studied in the future. SCF technology is introduced in **Chapter 2.1**. **Chapter 2.2** discusses drug delivery systems. **Chapter 2.3** is the introduction of itraconazole. **Chapter 2.4** includes conventional methods to produce itraconazole and its problems.



Figure 2.1 Flow chart of itraconazole development.

2.1 Supercritical Fluids

A pure supercritical fluid is a substance, which is heated and compressed above its critical point (including its critical temperature T_c and critical pressure P_c). Above its critical point, it is neither a liquid nor a gas, but a fluid changing continuously from liquid-like to gas-like as its pressure decreases. The phase diagram of a single substance is shown in Figure 2.2. In the diagram, C represents the critical point, and T represents the triple point. Curve TC means the gas-liquid coexistence curve when liquid and gas are in equilibrium. As both the temperature and pressure are increased, curve TC tends towards C. The liquid becomes less dense because of the effect of thermal expansion and the gas becomes denser due to the increasing pressure. SCFs can have better mass transfer through a porous matrix due to the higher diffusivities than normal liquids (Saad and Gulari, 1984). Because the densities of SCFs are higher than normal gases, SCFs can facilitate higher solubility than The densities of liquid and gas phases become equal (called critical gases. density, ρ_{c}) at the critical point and the substance becomes a supercritical fluid. The values of densities, solubility and other physical properties in the supercritical region are between those of typical liquids and gases. A comparison of SCF and typical gas and liquid is presented in Table 2.1.

Supercritical Fluids Technology offers a convenient way to change solvating properties from gas-like to liquid-like without changing chemical structure (McNally and Bright, 1992). Therefore, Supercritical Fluids Technology has grown rapidly. Table 2.2 presents the critical parameters (critical temperatures, criticalpressure and critical densities) of some compounds as supercritical fluids. The most popular compound today is carbon dioxide because of its low critical temperature, non-toxicity, non-flammable property and cheapness. The carbon dioxide molecule is non-polar so it is a non-polar solvent. However, it has some affinity with polar solutes due to its large molecular quadrupole (Westwood, 1993). Therefore, pure carbon dioxide can be used to dissolve many large organic solutes. The most popular application currently is the extraction and recovery of polar organic compounds from aqueous media. In industries, supercritical carbon dioxide technology is used for separation of natural components, such as caffeine from coffee beans and rose oil from roses. Table 2.3 shows some applications. Drug product formulation has caught much attention in application of SCFs Technologies in past years.



Figure 2.2 Phase diagram of a single substance.

Table 2.1	A comparison of physical properties of SCFs, a typical gas and
	liquid (Westwood, 1993).

Phase	Gas	SCF	Liquid
Diffusion Coefficient (cm ² /s)	10-1	10-3	10-5
Density (g/cm ³)	10-3	0.2-0.9	1.0
Viscosity (mPa s)	10-2	10 ⁻² -10 ⁻¹	1.0

Substance	$T_{c}(^{o}C)$	P _c (MPa)	$\rho_{\rm c}$ (10 ³ Kg/m ³)
CO ₂	31.30	7.39	0.47
N ₂ O	36.50	7.35	0.45
SF ₆	45.50	3.76	0.74
NH ₃	132.50	11.40	0.24
H ₂ O	374.00	23.00	0.34
n-C4H10	152.00	3.80	0.23
n-C ₅ H ₁₂	197.00	3.78	0.23
Xe	16.60	5.92	1.10
CC ₁₂ F ₂	112.00	4.13	0.56
CHF ₃	25.90	4.75	0.52

Table 2.2Critical parameters of some useful compounds as SCFs
(Anderson, 1993).

Process	Plant Location
Coffee Decaffeination	Bremen, Germany (two plants), Italy, Poszzillo, Houston and Texas
Tea Decaffeination	Germany and Munchmuenster
Fatty Acids from Spent Barley	Dusseldorf and Germany
Nicotine Extraction	Hopewell and Virginia
Rose-Residual Oil SCE	Oklahoma City
CO ₂ Refining of Extracted Pyrethrum	United Kingdom
Hops Extraction and Spices	Australia, Germany (two plants), Melbourne, Munchmuenster, Reigat, United Kingtom, Wolnzach, Nebraska, Washington (two plants) and Yakima
Flavors Extraction	France and Grasse
Flavors/Aromas	Germany and Rehlingen
Corn Oil	Japan
Color Extraction-Red Pepper	Japan (six plants)

Table 2.3Commercial-scale supercritical CO2 extraction processes
(Anonymous, 1995).

2.2 Drug Delivery Systems

After producing effective drugs, the next step will be to develop the best drug delivery system for the specific drug and control drug release at the desired rate, which can enhance the efficacy of therapeutic agents through controlled release. Drug delivery systems refer to the technology utilized to deliver drugs to the desired site inside the body for drug release and absorption. The difference between the approach of the classical or traditional drug discovery process and new ones is that screening systems now are much more selective, involving the use of in vitro receptor binding techniques and enzyme inhibition assays. In order to develop the successful dosage forms, it is convenient to use delivery route as a meaning of classifying drug delivery issues. There are sitespecific, implantable, ocular, transdermal, intranasal, sublingual, buccal, intravenous, intramuscular, subcutaneous, inhalation, and oral delivery systems, etc. The site-specific delivery systems deliver drugs directly to affected tissues. Implantable drug delivery systems are placed completely under the skin-usually in a convenient but inconspicuous location. They are small solid dosage forms containing concentrated drug and they continuously release their medication over prolonged periods without repeated insertion of needles. Ocular drug delivery includes drug-impregnated membranes. Transdermal supports the passage of drug substances from the surface of the skin through its various layers and into the systemic circulation. Drug materials applied topically to the nasal conjunctiva will enter the nose through the nasolacrimal duct just beneath the anterior end of the inferior turbinate. Sublingual drug delivery systems are to put drugs under tongue. Buccal drug delivery is to place drug tablets at the

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sides inside mouth. Intravenous drug delivery is to inject drugs directly into blood. Intramascular delivery systems are to inject drugs directly into muscles. Subcutaneous drug delivery systems deliver drug into skin by injection. Inhalation drug delivery is to spray drugs through mouth. Oral is, and will be the most convenient and commonly employed route of drug delivery systems. There are many technologies available for oral drug delivery systems from liquids, capsules and tablets through various sustained-release systems to highly sophisticated osmotic devices (Gardner, Sharp, Laboratories and Point, 1987). The oral drug delivery system is also the system chosen in this study.

2.3 Itraconazole

Itraconazole ($C_{35}H_{38}C_{12}N_8O_4$, molecular weight = 705.64) is a synthetic triazole anti-fungal drug (Figure 2.3). Itraconazole is a white to slightly yellowish powder. It consists of a 1:1:1:1 racemic mixture of four diastereomers, each of which has three chiral centers. Itraconazole is highly lipophilic so it is barely soluble in aqueous solutions (less than 100 mcg /100 mg in aqueous media within PH = 1-12.7). It is most soluble in dichloromethane (25 mg /100 mg). The solubility of itraconazole is a weak base (pKa = 3.7) and has a log C (n-octanol/water) partition coefficient of 5.66 when PH = 8.11 (Kapsi, 1998). It can distribute extensively in tissues and especially is found in higher-level tissues, such as in brain. The half-life of itraconazole, the time required for the drug's blood or plasma concentration to decrease by one half is very long (about 20 hours). Itraconazole can inhibit cytochrome

P-450-dependent metabolism of ergosterol, which is a vital component of fungal cell membranes, and then interfere in sterol biosynthesis causing the death of cells inside the membranes of cells (Kapsi, 1998). Clinical use of itraconazole is treatment of fungal infections in immunocompromised and non-immunocompromised patients. Patients who have blastomycosis, pulmonary, extrapulmonary, histoplasmosis and aspergillosis diseases can take itraconazole. Itraconazole is also used for patients with onychomycosis of the toenail with or without fingernail involvement due to dermatophytes (marketed itraconazole, Sporanox).



Figure 2.3 Chemical structure of itraconazole.

Solvent	Solubility in g/100ml Solution
Water (PH = 7.0)	<0.0001
Hexane	<0.001
Diethyl ether	0.002
2-propanol	0.008
Polyethylene glycol 400	0.013
Tetrachloroethane	0.013
Ethanol	0.026
4-methyl 2-pentanone	0.058
Methanol	0.061
Acetonitrile	0.11
Toluene	0.12
Ethyl acetate	0.16
Polyethylene glycol 400	0.19
2-propanone	0.20
2-butanone	0.23
Dimethyl sulfoxide	1.1
Tetrahydrofuran	2.2
N,N-dimethyl formamide	3.5
Dichloromethane	25

Table 2.4Itraconazole solubility in different solvents and aqueous media
(Kapsi, 1998).

2.4 Conventional Method and Problems of Producing Itraconazole and Formulations

From Table 2.4, it is seen that itraconazole is most soluble in dichloromethane (methylene chloride); however, it is poorly soluble in water, and other aqueous or organic solvents. In today's pharmaceutical industry, the existing formulation of itraconazole is Sporanox produced by Janssen Pharmaceutica. A solution was prepared by adding itraconazole powder and hydroxypropyl methylcellulose (1:1.5) into dichloromethane and denatured ethanol (60:40) while stirring. Another seal-coating spraying solution with dichloromethane and polyethylene glycol 20000 (5.4:1) were prepared while stirring, denatured ethanol was added, and the solution was stirred until homogeneous. The itraconazole solution was sprayed to the spheres of sugar beads and then those sugar beads were dried to remove dichloromethane at a temperature of about 80 °C and at a pressure of about 200-300 mbar (20-30 kPa). The prepared seal-coating solution was then sprayed to the itraconazole containing beads from the former step, and dried again at 50-55°C. Because itraconazole has very low solubility in other aqueous or organic solvents, sticks together easily after the process, and precipitates in gastric fluids, HPMC was added as a hydrophilic agent as well as to avoid precipitating, and polyethylene glycol 20000 (PEG) was added to prevent the drug loaded beads from sticking together. The biggest problem here is the use of dichloromethane because the FDA has very strict requirements for minimum presence of dichloromethane (less than 0.005 %). Therefore a drug delivery system without the use of highly regulated organic solvents needs to be developed. Another problem is too many steps in this process. In addition, it is known that itraconazole needs a

faster release in gastric fluids because it is only 56 % bioavailiable. Using SCF technology has solved those problems.

CHAPTER 3

OBJECTIVES OF THIS RESEARCH

The goal of this study is to develop an immediate release delivery system for itraconazole. There are three main objectives summarized below:

Objective 1

Avoid the use of organic solvents to develop a product of the water-insoluble anti-fungal agent, itraconazole while is bioequivalent to Sporanox. Carbon dioxide will be used instead of methylene chloride.

Objective 2

Find the optimum operating conditions in this itraconazole formulation production process, including temperature, pressure, treatment time, mixing and flow.

Objective 3

Meet the itraconazole dissolution requirement: higher than 80 % drug dissolution at 45 minutes in simulated gastric fluid at 37.5 °C, 100 rpm.

CHAPTER 4

EXPERIMENTAL MATERIALS AND METHODS

4.1 Introduction

This research was designed to produce on itraconazole formulation, which has high dissolution in simulated gastric fluid (higher than 85 % at 45 minutes). The optimum extraction pressure and temperature were found during SCF extraction of itraconazole. In this chapter, the experimental apparatus, methods and materials used in this study to form what itraconazole are discussed. Section 4.2 discusses the itraconazole formulation used in this study. Section 4.3 describes the equipment used for the treatment of itraconazole formulation with SC CO₂. Experimental method is discussed in section 4.4 and the last section of this chapter explains the chemicals used in this study.

4.2 Formulation of Itraconazole Formation

Ingredients used in the itraconazole formulation have been studied by Shivakumar Kapsi in 1998 in the college of Pharmacy at Oregon State University. The formulation includes five ingredients: itraconazole, polyethylene glycol 20000 (PEG), a hydrophilic polymer, a super disintegrated sodium starch, and a wetting agent. PEG 20000 was selected between PEG 3350, 8000 and 20000 because itraconazole dissolution in gastric fluid improved considerably (10 %) as the molecular weight of PEG increased. The hydrophilic polymer was found to prevent precipitation of the drug during dissolution. The sodium starch was added to speed up drug release in gastric fluid. A wetting agent has been chosen to enhance the solubility of the drug (Kapsi, 1998). The problem of this method was the difficulty of controlling treatment temperature and high temperature may cause degradation of drug. In this study, treatment temperature was well controlled by the SCF Extraction system. SC CO_2 is added to the above formulation in order to increase drug dissolution and enhance drug release in gastric fluid.

4.3 Supercritical Fluid Extraction System

The schematic diagram of experimental apparatus is shown in Figure 4.1. This equipment consists of a SCF Extractor (SFXTM 2-10) and a syringe pump and controller system (ISCO 260D). Supercritical Fluid Extractor is made for high-temperature and high-pressure usage. It consists of an oven for heating, a temperature controller and two 10-ml stainless steel cells. The syringe pump from ISCO was used to feed carbon dioxide to the extractor. The pump system consisted of a control panel to set the pressure or flowrate. The pressure range was 10 to 7,500 psi and the pressure accuracy was $\pm 2\%$ of full scale (ISCO manual). A vial was connected to the extractor to collect samples.



Figure 4.1 Schematic diagram of experimental equipment.

4.4 Experimental Method

A simple one-step extraction method was used in this study. There was no secondary solvent removal step required using this method. Therefore, all waste disposal fees were eliminated. First a desired amount of sample including all ingredients (itraconazole, PEG 20000, the hydrophilic polymer, the sodium starch and glycerol) was loaded into the cell and mixed before introducing the treatment system. The syringe pump was then filled with carbon dioxide from a supply cylinder. Parameters, such as cell temperature and pump pressure, were set to the desired values. Carbon dioxide at supercritical conditions was added to the cell. After treatment equilibrium was reached (about 15 minutes), supercritical solution was allowed to flow into the vial. To generate mixing in the cell, flow rates of 0.5 to 2.0 ml/min were used in all experiments. After a desired period of time, the pressure in the cell was suddenly dropped to atmospheric pressure.

The solution in the cell was cooled by a cooling system Dionex SFE 703 or in dry ice. The product was ground in a blender (Waring commercial laboratory blender) and particle ranging in size between 0.2-1 mm were sieved through two different meshes. Dissolution profiles of itraconazole release were obtained using the United States Pharmacopoeia (USP) XXII apparatus II (VK 7000®, Vankel Industries, Inc., Edison, NJ). The dissolution measurement was a paddle stirring method as shown in Figure 4. The equipment of VK 7000 is shown in Figure 4.2. Dissolution media consisted of 900 ml of enzyme-free simulated gastric fluid (PH = 1.4 ± 0.1) maintained at 37 °C. The solution was mixed at 100 rpm for 60 minutes. 3 ml dissolution samples were collected at 5.

diluted to 10ml with simulated gastric fluid. Finally, the10 ml diluted solution was taken for UV analysis at a fixed wavelength of 226 nm using a Beckman DU-600 spectrometer.


Figure 4.2 Schematic diagram of dissolution apparatus.

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4.5 Source of Materials

Grade 2.8-carbon dioxide was purchased from Industrial Welding Supply (Albany, Oregon). Itraconazole powder was provided by College of Pharmacy, Oregon State University. Polyethylene glycol 20000 was purchased from Sigma Chemical Co, St. Louis. Sodium starch was purchased from Edward Mendell Co. The hydrophilic polymer was from Dow Chemical Co, Midland, and the wetting agent was provided by Sigma Chemical Co, St. Louis.

CHAPTER 5

RESULTS AND DISCUSSION

The dissolution profile of innovator itraconazole formulation (Sporanox[®]) is shown in Figure 5.1. 90 % itraconazole was dissolved in gastric fluid after 60 minutes. Better products, which have higher dissolution and faster drug release than Sporanox[®] were produced. This chapter presents in this study important results obtained from scanning electron microscopic pictures and dissolution measurements is divided into five sections. The first section presents two different ways to show the effect of carbon dioxide on the product formed and its dissolution profiles; the particle morphology and solvent power. The second section shows the effect of treatment temperature. The effect of treatment time is explained in the third section. The next section discusses how mixing during the treatment process affects the dissolution profiles of itraconazole. The last section shows the effect of two cooling methods on the dissolution results after the drug was formed. The solubility of itraconazole in SC CO₂ is low because no drug was found in the collecting vial. However, SC CO₂ is soluble in drug solution because it was visually seen CO₂ coming out of the drug solution when dropping the pressure after treatment. The solubility of SC CO2 in drug solution is a function of treatment temperatures, treatment pressures, treatment time and mixing. The products from SC CO₂ method are white and porous solid. 96 % of the chemicals were recovered. Yellowish solid would be formed due to high treatment temperature (>140 °C) or long treatment time (> 30 minutes).



Figure 5.1 Dissolution profile of itraconazole from innovator product, Sporanox.

5.1 Effect of Carbon Dioxide

Supercritical carbon dioxide has significant effect on the itraconazole and its dissolution profile. This fact can be proved from two ways: the particle morphology, and solvent power.

5.1.1 Particle Morphology of Itraconazole Products

Scanning electron microscopic (SEM) photomicrographs of two different samples are shown in Figures 5.2 and 5.3. The sample in Fig. 5.2 was without supercritical carbon dioxide and that in Fig. 5.3 was treated with carbon dioxide at 300 atm. The one without SC CO₂ results in a solid network consisting of intertwining aggregated cubes. The morphology in Fig. 5.3 consists of many thin layers with small pores inside. The different morphology in Fig. 5.3 was due to the effect of CO₂ during the treatment and depressurization. The expansion of the drug solution by depressurizing SC CO₂ produced more porous products. BET surface area measurement is needed to quantify the actual surface area of these samples.



Figure 5.2 SEM photomicrograph of itraconazole formed at the treatment condition: without SC CO₂, T = 135 °C and t = 10 minutes.



Figure 5.3 SEM photomicrograph of itraconazole formed at the treatment condition : with SC CO₂ (P = 300 atm), T = 135 °C and t = 10 minutes.

To see the effect of CO_2 on dissolution profile, experiments were performed with and without CO_2 at different conditions and the results are presented in Figures 5.4, 5.5 and 5.6. These figures show that the amount of dissolved drug in gastric fluid increases significantly (23-40 %) in one-hour dissolution experiment with CO_2 at 300 atm compared to runs without CO_2 . Results from dissolution measurement and SEM photomicrographs of the product prove that CO_2 has significant effects on the morphology of the drug and its dissolution profile. Figures 5.4, 5.5 and 5.6 are all the same P, T, treatment time but they differ in whether explotab was added at the end (Fig. 5.4) and if there was mixing during heating process (Fig. 5.6). Figure 5.6 is without mixing during heating process and explotab was added at the beginning with other ingredients. Fig. 5.4 shows that the drug precipitated after 20 minutes. Product, that precipitate in gastric fluid are not desirable and thus explotab was added to the ingredients at the beginning of the process in all other experiments. From Figures 5.5 and 5.6, it can be concluded that mixing during heating process did not have significant effect on the products, and thus the other experiments are wither with mixing or without mixing during the heating process.

In Figures 5.4, 5.5 and 5.6, the itraconazole dissolution in gastric fluid were much higher when CO₂ was used during the treatment conditions compared to runs without CO₂. This shows that the use of CO₂ enhances the dissolution rate of the product in gastric fluid. Another way of showing the importance of CO₂ is to look at the temperature needed to obtain the same dissolution rates with and without CO₂ (Fig. 5.7). As shown in the figure, almost the same dissolution profiles are obtained for drugs produced with and without CO₂. However, the drug produced with CO₂ requires 15 °C lower temperature than that produced without CO₂. As higher temperatures (> 140 °C) may result in drug decomposition, the product produced with CO₂ is more favorable. The time delay in Fig. 5.7 is due to the fact that the capsule dissolved about 1–4 minutes slower than the other samples after it was placed in gastric fluid.



Figure 5.4 Dissolved amount of itraconazole as a function of time. Treatment conditions: with CO_2 (P = 300 atm) or without CO_2 , T = 130 °C, t = 10 minutes and add explotab at the end.



Figure 5.5 Dissolved amount of itraconazole as a function of time. Treatment conditions: with CO_2 (P = 300 atm) or without CO_2 , T = 130 °C and t = 10 minutes and without mixing during heating process.







Figure 5.7 Dissolved amount of itraconazole as a function of time. Treatment conditions: with CO_2 (P = 300 atm, T = 135 °C) or without CO_2 (T = 150 °C), t =10 minutes and with mixing during heating process.

5.1.2 Solvent Power

Solvent power is the strength of solvent for dissolving solutes. A SEM photomicrograph of the product formed at a subcritical pressure (P = 30 atm) is presented in Figure 5.8. The picture shows two kinds of morphologies. On the right side is a network of aggregated cubes similar to Figure 5.2. The left side consists of some large pieces with a few pores inside. Fig. 5.8 seems to be a combination of Fig. 5.2 and Fig. 5.3. The significantly different morphologies observed in Figures 5.8 and 5.3 may due to the different solvent powers at the to pressures.

Figures 5.9, 5.10 and 5.11 present the dissolved drug as a function of time at different treatment pressures. Higher operating pressures give higher dissolution rates because the solvent strength increases and more SC CO₂ gets into the drug solution as pressure increases. Results from these figures show that CO_2 and its solvent power are important in producing a product with a high dissolution rate in gastric fluid. From Figures 5.9 and 5.10, the drugs that were conditioned to a pressure of 400 atm precipitated in gastric fluid. Therefore, pressures above 300 atm were not used in proceeding experiments.

Fig. 5.9 shows a much lower (about 30-60 %) dissolution than Figures 5.10 and 5.11 due to the lower temperature used in Figure 5.8 (120 °C compared to 130 and 135 °C). Temperature was an important parameter on dissolution of the product in gastric fluid because solubility of itraconazole in the solution is a strong function of temperature. Effect of temperature on dissolution profile is discussed in section 5.2.



Figure 5.8 SEM photomicrograph of itraconazole formed at the treatment condition: with CO_2 (P = 30 atm), T = 135 °C, t = 30 minutes.



Figure 5.9 Dissolved amount of itraconazole as a function of time. Treatment conditions: P = 200, 300 and 400 atm, T = 120°C, t = 10 minutes, without mixing during heating process and with flow.



Figure 5.10 Dissolved amount of itraconazole as a function of time. Treatment conditions: P = 200, 300 and 400 atm, T = 130 °C, t = 10 minutes, without mixing during heating process and with flow.



Figure 5.11 Dissolved amount of itraconazole as a function of time. Treatment conditions: P = 30, 200 and 300 atm, T = 135 °C, t = 30 minutes, with mixing during heating process and with flow.

5.2 Effect of Temperature

Two SEM photomicrographs of samples formed at two different treatment temperatures are shown in Figure 5.12 and 5.3. The product formed at the lower temperature (120 °C) (Figure 5.12) consists of intertwining solid pieces, which may have lower porosity and surface area. Dissolved itraconazole as a function of time at various treatment temperatures are shown in Figures 5.14, 5.15 and 5.16. From Figure 5.14, the dissolution profile of the product at 140 °C resulted in precipitation of itraconazole in gastric fluid; therefore, this temperature has been eliminated in later experiments. Higher treatment temperatures showed higher dissolution of drug in gastric fluid due to the fact that more itraconazole would dissolve in PEG solution at high temperatures. Of course temperatures of 140 °C and higher may result in decomposition or degradation of drug. The optimum temperature was found to be 135 °C.



Figure 5.12 SEM photomicrograph of itraconazole formed at treatment condition: P = 300 atm, T = 120 °C and t = 10 minutes.



Figure 5.13 SEM photomicrograph of itraconazole formed at treatment condition: P = 300 atm, T = 135 °C and t = 30 minutes.



Figure 5.14 Dissolved amount of itraconazole as a function of time. Treatment conditions: T = 110, 120, 130 and 140 °C, P = 200 atm, t = 10 minutes, without mixing during heating heating process and with flow.



Figure 5.15 Dissolved amount of itraconazole as a function of time. Treatment conditions: T = 110, 120 and 130 °C, P = 300 atm, t = 10 minutes, without mixing during heating process and with flow.



Figure 5.16 Dissolved amount of itraconazole as a function of time. Treatment conditions: T = 120, 130 and 135 °C, P = 300 atm, t = 10 minutes, with mixing during heating process and with flow.

5.3 Effect of Treatment Time

Figures 5.3 and 5.13 present the different morphology of the products produced at different treatment times. No notified difference in morphologies was observed. Effect of treatment time on dissolution profile of itraconazole in

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gastric fluid is shown in Figures 5.17 and 5.18. The amount of dissolved itraconazole in gastric fluid increased with the increase of treatment time, except for one-hour treatment time. One-hour treatment time may cause decomposition of drug due to a long exposure of drug to a high temperature and formed yellowish product. Therefore, the optimum treatment time was found to be 30 minutes.



Figure 5.17 Dissolved amount of itraconazole as a function of time. Treatment conditions: t = 10 or 30 minutes, T = 130 °C, P = 300 atm, without mixing during heating process and with flow.



Figure 5.18 Dissolved amount of itraconazole as a function of time. Treatment conditions: t = 10, 20, 30 and 60 minutes, T = 135 °C, P = 300 atm, with mixing during heating process and with flow.

5.4 Effect of Mixing during Treatment

Dissolution profile of itraconazole formed with CO₂ flow (0.5-2 ml/min) or without CO₂ flow during the treatment process is shown in Figure 5.19. Having a small CO₂ flow rate (≤ 2 ml/min) resulted in higher dissolution rates. Flow of SC CO₂ through the treatment cell may generate a better mixing of the ingredients leading to a product, which contains more itraconazole and has a higher dissolution rate in gastric fluid.



Figure 5.19 Dissolved amount of itraconazole as a function of time. Treatment conditions: with flow (0.5-2 ml/min) or without flow, T = 135 °C, P = 300 atm, t = 30 minutes and with mixing during heating process.

5.5 Effect of Cooling

When the treatment process is completed, the solution must be rapidly cooled to entrap the drug in solution in the interstitial spaces of PEG 20000. To see the effect of cooling rate on dissolution profile of itraconazole in gastric fluid, two different cooling methods were used. Cooling in Dionex (-6 °C) or dry ice (-57 °C) did not have a considerable effect (about 3 %) on the dissolution of drug in gastric fluid (Fig. 5.20). Cooling in Dionex system was selected for all other experiments.





CHAPTER 6

MODEL DEVELOPMENT FOR ITRACONAZOLE RELEASE

6.1 Introduction

It is well known that drug availability in the market is usually determined by the dissolution rate of the drug from the dosage form. The release of drug from a drug product may be influenced by the physical and chemical properties of the drug dosage form. Also, the release of a drug from its physical structure is determined by the rate at which it dissolves in the surrounding medium (Banakar, 1992). The rate of dissolution of a drug is defined as the amount of the drug substance going into the solution from a solid state per unit time in standard conditions. In this study, a simple but clear intrinsic dissolution model was developed to define itraconazole dissolution in the gastric fluids.

6.2 Mathematical Model Used for Dissolution Profile

The intrinsic dissolution model was chosen in this study. Dissolution rate involves some physical parameters, such as interfacial area, shape and the substance and the solubility of the substance in the solution. Dissolution can be described as a heterogeneous system resulting in a net effect of mass transfer from the escape from the surface of small drug particles to solution. It can be expressed mathematically as

$$\frac{dM}{dt} = kA(C_s - C) \tag{6.1}$$

$$V\frac{dC}{dt} = kA(C_s - C) \tag{6.2}$$

where *V* is the volume of the solution; *M* is the mass of drug substance in the solution; *A* is the interfacial surface area of drug; C_s is the saturation concentration usually referred to as solubility in the medium; *C* is the concentration dissolved into the solution at any time *t*; and *k* is the convective-mass transfer coefficient.

In this model, the capacity coefficient, *kA* was assumed to be constant during the dissolution process because the solution was a very dilute system as the amount of dissolved drug into the solution medium was small compared to the 900-ml gastric fluid. Therefore, the volume of the solution was also assumed to be constant.

The initial and final conditions in this study were C = 0 at t = 0 and $C = C_s$ at $t = \infty$.

Rearranging equation (6.2) gives

$$\frac{dC}{dt} = \alpha(C_s - C) \tag{6.3}$$

where $\alpha = k(A/V)$

give

Integrating equation (6.3) and applying the initial and final conditions

$$C = C_{3}(1 - e^{-\alpha_{1}})$$
(6.4)

or

 C_x was experimentally determined by keeping the itraconazole formulation for about two days in gastric fluid. Two products were used to determine C_x . One product was obtained at the best treatment condition (T = 130 °C. P = 300 atm, t = 30 minutes, with mixing during heating process and with flow during treatment), and the other product was obtained without CO₂ (T = 150 °C) to obtain the same dissolution profile. The average of C_x of two products was 140.3744 mg/L.

The R-square fitting method was used to find the parameters, α . The equation is expressed mathematically as

$$R^2 = 1 - \frac{SSE}{SST} \tag{6.5}$$

where SSE is the sum of the squares of the errors, and SST is the sum of the squares of deviations.

The mathematical definition for SSE and SST are as follows

$$SSE = \sum_{i} (Ci^{Exp} - Ci^{Cal})^{2}$$
 (6.6)

$$SST = \sum_{i} (Ci^{Exp} - \overline{C}^{Exp})^{2}$$
(6.7)

where Ci^{Exp} is the experimental concentration at time *t* and Ci^{Cal} is the calculated concentration at the same time. \overline{C}^{Exp} is the average experimental concentration.

6.3 Results and Discussion

The time delay happened sometimes in dissolution test due to the fact that capsules dissolved in gastric fluid slower (1-4 minutes). Those dissolution profiles have been shifted to correct the time delay before model fitting.

Parameters α and R^2 for different treatment conditions are tabulated in Table 6.1. Experimental and predicted values of dissolved itraconazole in gastric fluid for different treatment times are shown in Figure 6.1. The model for 30-minute treatment condition fitted the data very well (the R-square = 0.9597). The model can fit better for longer treatment time. Experimental and calculated dissolution profile for different treatment temperatures are shown in Figure 6.2. The model for the highest treatment temperature (T = 135 °C) fitted the model best (R-square = 0.9458). The model can predict better fit for higher treatment temperature condition. A similar comparison plot was generated for the treatment pressures (Fig. 6.3). The model for the highest treatment pressure fitted the model very well (R-square = 0.9597).

Conditions during the treatment					Parameters of the model	
P (atm)	Т	Treatment	Mixing	Flow	α	R^2
	(°C)	Time (min)				
300	135	30	Yes	Yes	0.046115	0.9597
300	135	20	Yes	Yes	0.041999	0.9378
300	135	10	Yes	Yes	0.022093	0.9458
300	130	10	Yes	Yes	0.023569	0.8409
300	120	10	Yes	Yes	0.008953	0.2697
200	135	30	Yes	Yes	0.013422	0.5045
30	135	30	Yes	Yes	0.008908	0.1945

 Table 6.1
 Calculated parameters of the intrinsic model



Figure 6.1 Experimental and calculated dissolved amount of itraconazole as a function of time. Treatment conditions: t = 30, 20 and 10 minutes, T = 135 °C, P = 300 atm, with mixing during heating process and with flow.



Figure 6.2 Experimental and calculated dissolved amount of itraconazole as a function of time. Treatment conditions: T = 135, 130 and 120 °C, P = 300 atm, t = 10 minutes, with mixing during heating process and with flow.



Figure 6.3 Experimental and calculated dissolved amount of itraconazole as a function of time. Treatment conditions: P = 300, 200 and 30 atm, T = 135 °C, t = 10 minutes, with mixing during heating process and with flow.

CHAPTER 7

CONCLUSIONS AND RECOMMENDATIONS

7.1 Conclusions

A new method was developed to form a soluble anti-fungal agent, itraconazole, using pure supercritical carbon dioxide, instead of highly regulated organic solvents. This method was easy to operate because the treatment temperature and pressure were well controlled by ISCO SFE Extractor system.

All the samples were formed using the same formulation in this study, but the amounts of itreonazole dissolved in the drug solution at different treatment conditions were different and this explains why some products have lower dissolution rate than the others.

100 % itraconazole dissolution in one-hour was achieved at the treatment condition: T= 135 °C, P = 300 atm, t = 30 minutes, with mixing during heating process, with flow and cooling in Dionex system. SC CO₂ treatment improved dissolution of itraconazole in gastric fluid by 23-40 %. This increase in dissolution rate was due to the solvent power of CO₂ and possibly the higher porosity of the products. Higher pressure gives higher solvent power, but treatment pressures in excess of 300 atm caused precipitation of drug in gastric fluid. In order to get the same dissolution, the product without SC CO₂ treatment had to be produced under higher treatment temperature (15 °C higher). Treatment temperature also has a significant effect on dissolution results. Temperatures higher than 140 °C may degrade the drug or cause precipitation in gastric fluid. Low temperatures (<120 °C) resulted in low dissolution rates of
itraconazole in gastric fluid. Therefore, the optimum treatment temperature was found to be 135 °C. Treatment time when used with a high temperature was proved to be an important factor on dissolution results. The product at 135 °C treated for 30 minutes obtained 25 % higher dissolution than one, which was treated for 10 minutes. Mixing during the treatment was also found to be an important effect to improve the dissolution. Due to the equipment limitations, mixing was generated by flow rate of the SC solution. The dissolution increased 20-25 % when mixing was generated. Rapid cooling can trap itraconazole in the solution in the interstitial spaces of PEG 20000. However, the dissolution was not significantly affected by the cooling rate.

An intrinsic dissolution model was developed with different parameters (α) at higher treatment temperature, pressure and longer treatment time and was tested to be able to predict the dissolution profiles of itraconazole in gastric fluid. The R-square values ranged from 0.1945 to 0.9597.

7.2 Recommendations

BET surface area measurements would be useful in correlating products' surface area to dissolution profile.

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Appendix A: Standard Curve of Itraconazole

Preparation

20 mg raw itraconazole dissolved in 200 ml acetonitrile completely gave 100 % dissolution for 100 mg itraconazole in 1 L simulated gastric fluid. The solution was diluted in to 10, 20, 40, 60, and 80 %. Those solutions were tested for UV absorbance at fixed wavelength, 226 nm, using a Beckman DU-600 spectrophotometer.

Standard Curve Data

Standard Concentration (1ml drug /1L gastric fluid)	Abs1	Abs2	Absorbance at 226nm.	Estimated Value	% Theory
10	0.04245	0.04424	0.04335	9.94333	99.43333
20	0.08931	0.08998	0.08965	20.23222	101.16111
40	0.18251	0.18195	0.18223	40.80667	102.01667
60	0.26561	0.26624	0.26593	59.40556	99.00926
80	0.36569	0.36255	0.36412	81.22667	101.53333
100	0.45139	0.45088	0.45114	100.56333	100.56333
				Average	100.61951
				Standard Deviation	1.19025
				%C.V.	1.18293

Standard Curve of Itraconazole



Appendix B: Calculation for Dissolved Percent of Itraconazole in Gastric Fluid

Those dissolution experiments of 100 mg itraconazole were carried out in 900 ml gastric fluid so the standard data were converted into the same ratio. The absorbance correction of 100 % dissolution is below:

The 100 % standard absorbance in 900 ml gastric fluid = 0.45114 (the absorbance for 20 mg itraconazole in 200 ml acetonitrile) × 1000 ml/ 900 ml = 0.5012667

Those absorbance data were converted into percent of 100 mg itraconazole dissolved in gastric fluid by following formula:

Percent = (absorbance at any time / 0.5012667) × 100%

Appendix C: Data of Dissolution Study

Formulation: Itraconazole + PEG 20000 branched chain + Glycerol + HPMC (K15M) + Explotab

Device: ISCO cell

.

	Со	nditions c	luring tl	ne Tre	eatment		L	Dissol	ution S	Study E	Data	
D (star)	T (%C)	Treatment	Mixing	ng the Treatment II ing Flow Cooling Time E*1 (min) [20 20 30 45 10 20 30 45 60 45	Absor	bance	Per	cent				
P (atm)	I(C)	(min)	whxing	FIOW	Coom	added	(min)	#1	#2	#1	#2	
						nent Dissolution Study ooling Time E*1 Time (min) Absorbance F added (min) $#1$ $#2$ $#1$ onex*2 Beginning 5 0.079 0.075 15.7 10 0.152 0.138 30.3 onex*2 Beginning 5 0.079 0.075 15.7 10 0.152 0.138 30.3 30.3 onex*2 Beginning 20 0.164 0.162 32.6 30 0.171 0.174 34.1 45 0.172 0.181 34.2 oling Time E Time E Time Image Absorbance 10 11	15.72	15.06				
							10	0.152	0.138	30.34	27.48	
20	125	20	Var	Var	Dionar	² Paginning	20	0.164	0.162	32.62	32.38	
50	155	50	105	105	Dionex	Deginning	30	0.171	0.174	34.13	34.73	
							45	0.172	0.181	34.23	36.18	
							60	0.174	0.182	34.75	36.33	
	Со	nditions d	luring tl	ne Tre	eatment		Dissolution St			Study D	udy Data	
D (star)	T (9C)	Treatment	Mining	Flow	Casting	Time E	Time	Abse	orbance	Pe	rcent	
P (atm)	T(C)	(min)	wixing	Flow Coo	Cooling	added	(min)	#1			#1	
							5	0	.079	1:	5.67	
							10	0	.131	2	6.13	
200	110	10	No	Ves	Dionex	Beginning	20	0	146	29	9.07	
200	110	10	110	105	Dionex	Deginning	30	0	.156	3	1.05	
							45	0	.162	32	2.25	
							60	0.165		32	32.82	
	Со	nditions d	luring tl	ne Tre	eatment		L L	Dissol	ution S	Study D	Pata	
D (star)	T (9C)	Treatment	Mining	Flow	Caslina	Time E	Time	Abso	orbance	Pe	rcent	
P (atm)		(min)	Mixing	FIOW	Cooling	added	(min)		#1		#1	
							5	0	.084	10	6.74	
				10	0	.109	2	1.69				
200	120	10 No Yes	Dioney	Reginning	20	0	.140	2	7.87			
200	120		INU	105	Diolicx	Destimiting	30	0	.170	34	4.01	
			10 No Y				45	0	182	30	5.40	
							60	0	.176	3.	5.08	

	Conditions during the Treatment atm) T (°C) Treatment Time (min) Mixing Flow Cooling Tim add							Dissol	ution St	udy Da	ta	
D (atm)	T (%C)	Treatment	Mining	Flow	Casting	Time E	Time	Absor	bance	Per	cent	
P (atm)	- I ('C)	(min)	wirxing	FIOW	Cooling	added	(min)	#1	#2	#1	#2	
							5	0.111	0.086	22.14	17.25	
				·			10	0.172	0.142	34.22	28.33	
200	135	30	Ves	Yes	Dionex	Reginning	20	0.226	0.196	45.03	39.09	
200	155	50	103	103	Diolicx	Deginning	30	0.256	0.214	50.98	42.66	
							45	0.255	0.226	50.82	45.09	
							60	0.265	0.233	52.93	46.42	
	Con	ditions du	uring th	e Trea	atment			Dissol	ution St	tudy Data		
P (atp)	T (%C)	Treatment	Mixing	Flow	Cooling	Time E	Time	Absoi	bance	Percent		
r (aun)	1(C)	(min)	wiixing	riow	Coomg	added	(min)	#	1	#1		
							5	0.0)53	10	.56	
							10	0.1	29	25	.69	
200	130	10	Yes	Yes	Dionex	Beginning	20	0.2	19	43	.78	
200	100			105	Dionex	Dionex	beginnig	30	0.2	.87	57	.24
							45	0.3	15	62	.90	
							60	0.3	23	64	.52	
	Con	ditions du	uring th	e Trea	atment			Dissolı	ution St	udy Dat	a	
P (atm)	T (°C)	Treatment Time	Mixing	Flow	Cooling	Time E	Time	Absor	bance	Per	cent	
r (atm)	1(0)	(min)	Mixing	110,4	cooning	added	(min)	#1	#2	#1	#2	
							5	0.031	0.018	6.21	3.68	
							10	0.224	0.168	44.75	33.52	
200	200 135 30	30	Yes	Yes	Dionex	Beginning	20	0.394	0.435	78.65	86.87	
				Yes			30	0.427	0.452	85.24	90.16	
							45	0.454	0.478	90.64	95.33	
							60	0.487	0.458	97.06	91.32	

	Conditions during the Treatm (atm) T (°C) Treatment Time (min) Mixing Flow Co 200 140 10 No Yes Di 200 140 10 No Yes Di Conditions during the Treatm							Dissolution St	udy Data	
D	T (0C)	Treatment	N 4 · ·	E)		Time E	Time	Absorbance	Percent	
P (atm)	[] (°€) 	(min)	Mixing	Flow	Cooling	added	(min)	#1	#1	
							5	0.326	64.96	
							10	0.440	87.80	
200	140	10	No	Voc	Dionar	Paginning	20	0.384	76.57	
200	140		INU	165	Dionex	Degimning	30	0.347	69.14	
							45	0.333	66.50	
							60	0.351	69.96	
	Con	ditions du	iring th	e Trea	atment			Dissolution St	udy Data	
D (atm)	T (%C)	Treatment	Mixing	g Flow Cooling Time E added		Time	Absorbance	Percent		
r (aun)	I (C)	(min)	witxing	FIOW	Cooning	added	(min)	#1	#1	
							5	0.065	12.92	
								10	0.114	22.83
200	110	10	No	Vac	Dianar	Decimains	20	0.140	27.84	
500	110	10	INO	ies	Dionex	Dionex	Desinuns	30	0.155	30.92
							45	0.155	31.01	
							60	0.158	31.61	
	Con	ditions du	iring th	e Trea	atment]	Dissolution St	udy Data	
P (otm)	T(PC)	Treatment	Mixing	Flow	Cooling	Time E	Time	Absorbance	Percent	
r (atili)	1(0)	(min)	wirxing	FIUW	Coomig	added	(min)	#1	#1	
							5	0.149	29.72	
						10	0.176	35.02		
300	120	10	No	Ves	Dioney	Reginning	20	0.181	36.05	
500	120	10	180	105	Diolicx	Degiminig	30	0.184	36.67	
							45	0.189	37.61	
					60	0.195	38.83			

	Con	ditions du	uring th	e Trea	atment			Dissolı	ition St	udy Da	ta	
P (atm)	T (°C)	Treatment	Mixing	Flow	Cooling	Time E	Time	Absor	bance	Perc	cent	
r (atm)	1(0)	(min)	MIXING	TIOW	Coomg	added	(min)	#	1	#	1	
							5	0.0	75	15.	00	
			• • •				10	0.1	38	27.	52	
300	120	10	Vac	Vec	Dioney	Beginning	20	0.1	64	32.	64	
500	120		105	105	DIOREX	Deginning	30	0.1	73	34.	56	
							45	0.1	78	35.	58	
							60	0.1	80	35.	35.92	
	Con	ditions du	uring th	e Trea	atment			Dissolu	tion St	udy Da	ta	
P (atm)	T(PC)	Treatment	Miving	Flow	Cooling	Time E	Time	Absor	bance	Per	cent	
1 (attii)	1(C)	(min)	wirking	$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	#1	#2						
				No No Dionex Beginning			5	0.065	0.059	12.92	11.76	
							10	0.219	0.206	43.64	41.00	
300	130	10	No		20	0.300	0.293	59.90	58.436			
500	150	10	110	110	Dionex	Desminis	5 0.065 0.059 12.92 10 0.219 0.206 43.64 4 20 0.300 0.293 59.90 5 30 0.319 0.310 63.582 6	61.82				
							45	0.328	0.318	65.34	63.43	
							60	0.331	0.326	66.11	64.99	
	Con	ditions du	iring th	e Trea	atment			Dissolu	tion St	udy Dat	ta	
P (atm)	T (%C)	Treatment	Mixing	Flow	Cooling	Time E	Time	Absor	bance	Pero	cent	
r (am)	1(0)	(min)	wiixing	Flow	Cooning	added	(min)	#	1	#	l	
							5	0.0	49	9.	80	
							10	0.1	40	27.	.96	
300	130	60	Ves	No	Dionex	End	20	0.4	56	90.	88	
200			140		Dienex	Linu	30	0.4	90	97.	67	
							45	0.5	06	100	.94	
							60	0.4	98	99.	31	

	Conditions during the Treatmenttm) $\frac{T}{(^{\circ}C)}$ $\frac{Treatment}{Time}$ (nin)Mixing MixingFlowCooling $\frac{Tin}{advertailed}$ 1013010NoYesDionexBeginstructure1013010NoYesDionexBeginstructureConditions during the TreatmentTreatment Time (min)10Treatment (min)MixingFlowCoolingTin advertailed15010YesNoDionexBeginstructure						Dis	soluti	ion St	udy E	Data		
D (stars)	Т	Treatment	Mining	Elaur	Coolina	Time E	Time	At	osorbar	nce		Percen	t
P (atm)	(°C)	(min)	Mixing	riow	Cooling	added	(min)	#1	#2	#3	#1	#2	#3
							5	0.134	0.098	0.065	26.75	19.46	13.05
							10	0.251	0.245	0.257	49.99	48.87	51.30
300	130	10	No	Yes	Dionex	Reginning	20	0.346	0.306	0.301	68.94	60.99	59.97
500	150	10		103	Dionex	Degiming	30	0.359	0.334	0.325	71.64	66.65	64.93
							45	0.376	0.351	0.348	74.96	70.08	69.42
							60	0.388	0.352	0.355	77.46	70.24	70.92
	Со	nditions	during t	he Tro	eatment			Dis	soluti	ion St	udy D	ata	
	Т	Treatment			Guiltin	Time E	Time	At	osorbar	nce		Percen	t
P (atm)	(°C)	(min)	Mixing	Flow	Cooling	added	(min)	#1	#2	#3	#1	#2	#3
							5	0.044	0.046	0.041	8.82	9.13	8.25
							10	0.172	0.194	0.168	Percent3#1#2#336526.7519.4613.25749.9948.8751.301 68.94 60.99 59.32571.64 66.65 $64.$ 34874.9670.08 $69.$ 35577.4670.2470.Study DataPercent3#1#2#216815.9038.6833.35544.2976.3970.45069.3698.9589.47995.7198.6295.51299.57102.0102Study DataPercent#1#2211.446.43829.6425.60959.3863.55871.5673.47675.7677.00176.3578.08	33.58	
1	150	10	Ves	No	Dionex	Reginning	20	0.326	0.383	0.355	44.29	76.39	70.83
I	150	10	105	110	Dionex	Degining	30	0.381	0.496	0.450	69.36	98.95	89.85
							45	0.419	0.494	0.479	95.71	98.62	95.64
							60	0.425	0.511	0.512	99.57	102.0	102.1
	Co	nditions	during t	he Tro	eatment			Dis	soluti	ion St	udy D	ata	
D (atm)	T (%C)	Treatmen	Mivino	Flow	Cooling	Time E	Time	Ab	sorban	ce	ł	Percent	
r (atm)	I (C)	(min)	witxing	FIOW	Coomig	added	(min)	#1		#2	#1		#2
							5	0.05	7 0.	.032	11.44	t (5.43
							01	0.14	9 0	128	29.64	4 2	5.60
300	130	30	No	Ves	Dionex	Reginning	20	0.29	8 0.	.319	59.38	3 6	3.55
500	150	50	140	103	Dionex	Deginning	30	0.359	9 0.	.368	71.50	5 7	3.47
							45	0.38	0 0.	386	75.70	5 7	7.00
							60	0.38	3 0.	391	76.35	5 7	8.08

	Conditions during the Treatment tm) T (°C) Treatment Time (min) Mixing Mixing Flow Cooling 00 130 10 Yes Yes Dionex 00 130 10 Yes Yes Dionex Conditions during the Treatment Mixing Flow Cooling Mixing Flow Cooling On different during the Treatment (min) T (°C) Treatment (min) Mixing Flow Cooling 00 130 10 Yes Yes Dionex Conditions during the Treatment					Dissolu	tion Stu	udy Da	ta		
P (atm)	T (⁰ C)	Treatment	Mixing	Flow	Cooling	Time E	Time	Absor	bance	Per	cent
r (atin)	I (C)	(min)	MIXINg	110w	Coome	added	(min)	#1	#2	#1	#2
							5	0.052	0.089	10.37	17.68
			:				10	0.185	0.189	36.85	37.69
300	130	10	Ves	Ves	Dionex	Reginning	20	0.300	0.273	59.91	54.38
500	150	10	163	105	Dionex	Deginning	30	0.358	0.298	71.45	59.50
							45	0.402	0.310	80.17	61.92
							60	0.398	0.337	79.39	67.24
	Con	ditions du	iring th	e Trea	atment			Dissolution St		udy Da	ta
D (atm)	T (9C)	Treatment	Mixing	Flow	Cooling	Time E	Time	Absor	bance	Perc	cent
P (atm)	I ('C)	(min)	wiixing	FIOW	Coomg	added	(min)	#	1	#	1
			Ves	Yes			5	0.0	44	8.8	35
) 10					10	0.2	53	50.	39
200	120				Dionex	End	20	0.3	94	78.	63
300	150	10	105	105	Dionex	LIIU	30	0.3	81	75.	96
							45	0.391		77.95	
							60	0.3	98	79.	44
	Con	ditions du	uring th	e Trea	atment			Dissolu	tion Stu	udy Da	ta
D(stm)	T (%C)	Treatment	Mining	Flow	Cooling	Time E	Time	Absor	bance	Perc	cent
r (atm)	$\Gamma(\mathbf{C})$	(min)	winxing	TIOW	Coome	added	(min)	#1	#2	#1	#2
							5	0.054	0.130	10.69	26.01
							10	0.197	0.213	39.22	42.43
300	130	10	No	Yes	Drvice	Reginning	20	0.281	0.270	56.15	53.76
500	150		110		Lory icc	Beginnig	30	0.320	0.299	63.79	59.64
-							45	0.341	0.319	67.93	63.66
							60	0.340	0.325	67.77	64.90

	Conditions during the Treatment Time Mixing Flow Co (min)atm)T (°C)Treatment (min)Mixing YesFlow CoCo0013510YesYesDi0013510YesYesDiConditions during the Treatment Time (min)atm)T (°C)Treatment Time (min)Mixing YesFlow Co0013520YesYesDi							Dis	soluti	ion St	udy I	Data	
D (atm		Treatment	Mining	Flow	Cooling	Time E	Time	e (Absort	ance		Percer	nt
P (atm) I (°C)	(min)	wixing	FIOW	Cooling	added	(min)	#1	#2	#	I	#2
							5	0.	059	0.065	11.	78	13.05
							10	0.	133	0.173	26.	45 3	34.41
300	135	10	Ves	Ves	Dionex	Reginning	20	0.	222	0.260	44.	36 5	51.90
500	155	10	105	105	DIOIICX	Degnining	30	0.	319	0.310	63.	63 (51.78
							45	0.	369	0.357	73.	52	71.13
							60	0.	392	0.372	78.	10 7	74.20
	Сс	nditions c	luring t	he Tre	eatment			Dis	soluti	ion St	udy I	Data	
D (atm		Treatment	Mixing	Flow	Cooling	Time E	Time	e '	Absorb	ance		Percent	
r (aun		(min)	wiixing	riow	Cooling	added	(min)	¥1	#2	#	1	#2
					5	0.	058	0.037	11.	49	7.395		
				10	0.	215	0.180	42.	88 3	35.82			
300	135	20	Ves	Vec	Dionex	Reginning	20	0.	346	0.372	69.	07 7	74.19
500	135	20	103	103	Dionex	Degining	30	0.	416	0.441	82.	90 8	37.90
							45	0.	447	0.447	89.	21 8	39.11
			 				60	0.	455	0.459	90.	70 9	91.58
	Сс	onditions c	luring t	he Tre	eatment			Dis	soluti	on St	udy I	Data	
Р	TCC	Treatment	Mixing	Flow	Cooling	Time E	Time	Ał	osorbai	nce		Percen	t
(atm)	1(0)	(min)	mang	1100	Cooning	added	(min)	#1	#2	#3	#1	#2	#3
							5	0.020	0.026	0.015	4.08	5.18	2.95
				10	0.162	0.132	0.166	31.14	26.39	33.02			
300	135	30	Yes	Yes Yes [Dionex	Beginning	20	0.300	0.335	0.356	65.72	66.88	70.94
							30	0.355	0.435	0.423	84.81	86.71	84.42
							$\begin{array}{c c c c c c c c c c c c c c c c c c c $	0.442	100.8	98.56	88.15		
							60	0.377	0.510	0.479	101.5	101.8	95.49

	Conditions during the Treatment Time (min) Mixing Flow Conditions 1135 30 Yes No Dia 1135 60 Yes Yes Dia]	Dissolu	tion Stu	idy Dat	ta
P (atm)	T (°C)	Treatment Time	Mixing	Flow	Cooling	Time E	Time	Absor	bance	Per	cent
i (utili)	1 (C)	(min)	i.i., iiig	110.0	Cooms	added	(min)	#1	#2	#1	#2
							5	0.044	0.051	8.74	10.24
							10	0.162	0.189	32.24	37.72
200	125	20	Vas	No	Dianar	Paginning	20	0.300	0.324	59.04	64.62
500	155	50	168	INU	Dionex	Deginning	30	0.355	0.356	70.74	71.01
							45	0.368	0.375	73.47	74.79
							60	0.377	0.390	75.11	77.85
	Со	nditions d	uring th	ne Tre	atment]	Dissolu	tion Stu	idy Dat	ta
P (atm)	T (የ ር)	Treatment	Mixina	z Flow Coolii		Time E	Time	Absor	bance	Per	cent
r (aun)	1(0)	(min)	winxing	TIOW	Coomg	added	(min)	#]	#2	#1	#2
					5	0.038	0.015	7.50	2.95		
					10	0.151	0.121	30.03	24.13		
200	125	60	Yes Yes	Vaa	Dianar	Paginning	20	0.254	0.223	50.76	44.48
500	155	00	105	105	Dioliex	Deginning	30	0.310	0.295	61.81	58.88
							45	0.321	0.314	64.12	62.64
							60	0.352	0.333	70.23	66.48
	Co	nditions d	uring th	ne Tre	atment]	Dissolu	tion Stu	idy Dat	ta
P (atm)	T (°C)	Treatment Time	Mixing	Flow	Cooling	Time E	Time	Abso	rbance	Per	cent
	- (- /	(min)				added	(min)	#	<i>‡</i> 1	#	1
							5	0.	146	29	.11
							10	0.	188	37	.44
300	200 140 10 No Ver	Dioney	Beginning	20	0.	198	39	.44			
500	140	10	NU		DIOIICA	Deginning	30	0.	298	59	.36
							45	0.	322	64	.16
							60	0.	340	67.91	

	Con	ditions du	iring th	e Trea	atment		E	Dissolu	tion St	udy Da	nta	
	-	Treatment				Time E	Time	Absor	bance	Per	cent	
P (atm)	Γ (°C)	Time (min)	Mixing	Flow	Cooling	added	(min)	#	1	#	1	
							5	0.1	10	21	.86	
							10	0.1	24	24	.72	
400	110	10	NI-	Vaa	Dianay	Designing	20	0.0	96	19	.10	
400	110	10	NO	ies	Dionex	Deginning	30	0.1	39	27	.77	
							45	0.1	47	29	.28	
							60	0.1	45	28	.83	
	Con	ditions du	iring th	e Trea	atment		I	Dissolu	tion St	udy Da	ita	
D	T (0C)	Treatment	Mining	EI	Castina	Time E	Time	Absor	bance	Per	cent	
P (atm)	1 (°C)	(min)	wiixing	FIOW	Cooling	added	(min)	#	1	#	1	
							5	0.1	04	20.65		
							10	0.1	61	32	. 11	
400	120	10	No	Vec	Dioney	Reginning	20	0.2	.02	40	.32	
400	120	10	NO	103	Diolicx	Degnining	30	0.1	70	33	.99	
							45	0.174		bancePercen $#1$ 1021.862424.722619.103927.774729.284528.83ion Study DatabancePercen $#1$ 0420.655132.110240.327033.997434.713136.14bancePercen $#2$ $#1$ 0.07324.0910.24044.6140.30056.7950.29566.0850.30568.1260.29170.045	34.71	
							60	0.1	81	36	.14	
	Con	ditions du	iring th	e Trea	atment		I	Dissolu	tion St	udy Da	nta	
D (atm)	T (°C)	Treatment	Mixing	Flow	Cooling	Time E	Time	Absor	bance	Per	cent	
r (aun)	r(C)	(min)	MIXIUS	FIOW	Cooning	added	(min)	#1	#2	#1	#2	
							5	0.121	0.073	24.09	14.65	
							10	0.224	0.240	44.61	47.89	
400	130	10	No	Ves	Dioney	Beginning	20	0.285	285 0.300 56.79 59	59.86		
400	150		110	Yes		ex Beginning	30	0.331	0.295	66.08	58.77	
							45	0.341	0.305	68.12	60.76	
							60	0.351	0.291	70.04	58.04	

	Con	ditions du	ring th	e Trea	itment			Dissolı	ition St	udy Da	ta
	T (9C)	Treatment		F 1	Certine	Time E	Time	Absor	bance	Pere	cent
P (atm)	1 (°C)	(min)	wirxing	FIOW	Coonng	added	(min)	#	1	#	1
							5	0.0	82	14	.65
							10	0.1	73	47.	.89
400	130	10	Ves	Ves	Dioney	Beginning	20	0.2	27	59.	.86
400	150	10	103	105	Dionex	Deginning	30	0.2	255	58	.77
							45	0.3	03	60.	.76
							60	0.2	.89	58.04	
	Con	ditions du	iring th	e Trea	atment			Dissolı	ition St	udy Da	ta
D (utma)	T (⁰ C)	Treatment	Minina	Elow	Caoling	Time E	Time	Absor	bance	Pero	cent
r (atm)	I (C)	(min)	wirxing	LIOM	Cooning	added	(min)	#1	#2	#1	#2
							5	0.029	0.047	5.72	9.41
					Dionex Beginning		10	0.148	0.176	29.62	35.15
400	135	30	Yes	Yes		20	0.179	0.215	35.64	42.95	
400	155	50	103	105	Dionex	Beginning Time E added Beginning Time E added Beginning Beginning	30	0.230	0.315	45.98	62.86
							45	0.316	0.356	63.01	71.02
							60	0.352	0.382	70.32	76.26
	Con	ditions du	iring th	e Trea	atment			Dissolu	tion St	udy Da	ta
P (atm)	T (የር)	Treatment	Mixing	Flow	Cooling	Time E	Time	Absor	bance	Pero	cent
r (attii)	Γ(C)	(min)	wirking	TIOW	Cooning	added	(min)	#	1	#	1
							5	0.0)44	8.	74
	100 140 10 No Yes Dic				10	0.1	45	29	.00		
400		Diopex	Reginning	20	0.2	:50	49.	.89			
	1 +0			105	Pronex	205111115	30	0.3	01	60.	.03
							45	0.3	28	65.	41
							60	0.3	58	71.	47

	Con	ditions du	uring th	e Trea	atment			Dissolu	ition St	udy Da	ta			
P (atm)	T (°C)	Treatment	Mixing	Elow	Cooling	Time E	Time	Absoi	bance	Per	cent			
r (attit)	I(C)	(min)	mang	FIUW	Coomig	added	(min)	#	1	#	1			
							5	0.0)65	12	.91			
							10	0.1	37	27	.30			
	130	10	No	No	Dionex	Reginning	20	0.1	83	36	.47			
	150		1.0		biolicx	Deginning	30	0.2	200	39	.82			
							45	0.2	208	41	.57			
							60	0.2	209	41.	.76			
	Con	ditions du	iring th	e Trea	itment			Dissolı	ition St	udy Data				
P (atm)	T (°C)	Treatment	Mixina	Flow	Cooling	Time E	Time	Absoi	bance	Pero	cent			
T (attri)	r(c)	(min)	uring the Treatment Mixing Flow Cooling Time E added Tim (mir (mir added) Yes No Dionex Beginning 20 30 45	(min)	#1	#2	#1	#2						
							5	0.067	0.110	13.39	21.85			
					Dionex		10	0.141	0.170	28.03	34.00			
1	130	10	Yes	No		Reginning	20	0.170	0.130	33.83	25.83			
	100		105			Dionex			Degining	30	0.192	0.159	38.32	31.75
											45	0.198	0.171	39.57
							60	0.206	0.195	41.04	38.95			
	Con	ditions du	iring th	e Trea	atment			Dissolu	ition St	udy Da	ta			
P (atm)	T (የር)	Treatment	Mixina	Flow	Cooling	Time E	Time	Absor	bance	Perc	ent			
1 (atti)	1(0)	(min)	wirking	110w	Coomg	added	(min)	#	1	#	1			
							5	0.1	12	22.	31			
							10	0.2	45	48.	80			
ł	130 10 Ves No Dic	Dionex	End	20	0.3	32	66.	24						
	150	10	103	1.0	Dionex	Lind	30	0.3	02	60.	17			
							45	0.2	35	46.	85			
							60	0.2	81	56.	02			

Conditions during the Treatment							Dissolution Study Data					
P (atm)	T (°C)	Treatment Time (min)	Mixing	Flow	Cooling	Time E added	Time (min)	Absorbance		Percent		
								#1	#2	#1	#2	
1	135	10	Yes	No	Dionex	Beginning	5	0.086	0.081	17.20	16.14	
							10	0.154	0.158	30.66	31.60	
							20	0.211	0.190	41.99	37.94	
							30	0.220	0.203	43.93	40.47	
							45	0.226	0.207	45.10	41.23	
							60	0.225	0.204	44.96	40.65	
Conditions during the Treatment							Dissolution Study Data					
P (atm)	T (°C)	Treatment Time (min)	Mixing	Flow	Cooling	Time E added	Time (min)	Absorbance		Percent		
								#1	#2	#1	#2	
I	145	10	Yes	No	Dionex	Beginning	5	0.075	0.015	15.00	2.97	
							10	0.243	0.130	48.56	25.91	
							20	0.292	0.245	58.29	48.81	
							30	0.304	0.296	60.55	59.04	
							45	0.304	0.318	60.58	63.37	
							60	0.327	0.327	65.22	65.25	
Conditions during the Treatment								Dissolution Study Data				
P (atm)	T (°C)	Treatment Time (min)	Mixing	Flow	Cooling	Time E added	Time (min)	Absorbance		Percent		
								#1		#1		
Ι	150	10	No	No	Dionex	Beginning	5	0.024		4.70		
							10	0.172		34.35		
							20	0.326		65.00		
							30	0.281		75.97		
							45	0.419		83.50		
							60	0.425		84.71		

*¹ E is explotab.

Beginning means adding explotab at the beginning with other ingredients. End means adding explotab after mixing other ingredients well until 120 °C.

*² Dionex is the cooling system inside the SFE-703 Extraction System from Dionex.