

AN ABSTRACT OF THE THESIS OF

Barbara K. Burkholder for the degree of Masters of Science in Water Resources Science presented on November 26, 2007.

Title: Influence of Hyporheic Flow and Geomorphology on Temperature of a Large, Gravel-bed River, Clackamas River, Oregon, USA.

Abstract approved:

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The hyporheic zone influences the thermal regime of rivers, buffering temperature by storing and releasing heat over a range of timescales. We examined the relationship between hyporheic exchange and temperature along a 24-km reach of the lower Clackamas River, a large gravel-bed river in northwestern Oregon (median discharge = 75.7 m<sup>3</sup>/s; minimum mean monthly discharge = 22.7 m<sup>3</sup>/s in August 2006). With a simple mixing model, we estimated how much hyporheic exchange cools the river during hot summer months. Hyporheic exchange was primarily identified by temperature anomalies, which are patches of water that demonstrate at least a 1 °C temperature difference from the main channel. Forty hyporheic temperature anomalies were identified through field investigations and TIR (Thermal-Infrared-Radiometry) in summer 2006. The location of anomalies was associated with specific geomorphic features, primarily bar channels and bar heads that act as preferential pathways for hyporheic flow. Detailed field characterization and groundwater modeling on three Clackamas gravel bars indicate residence times of hyporheic water can vary from hours to weeks and months. This was largely determined by hydraulic conductivity, which is affected by how recently the gravel bar formed or was reworked. Upscaling of modeled discharges and hydrologic parameters from these bars to the other anomalies on the Clackamas network shows that hyporheic discharge from anomalies comprises a small fraction (<< 1 %) of mainstem

discharge, resulting in small river cooling effects (0.012 °C). However, the presence of cooler patches of water within rivers can act as thermal refugia for fish and other aquatic organisms, making the creation or enhancement of hyporheic exchange an attractive method in restoring the thermal regime of rivers.

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Influence of Hyporheic Flow and Geomorphology on Temperature of a Large, Gravel-  
bed River, Clackamas River, Oregon, USA

by

Barbara K. Burkholder

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Dean of the Graduate School

I understand that my thesis will become part of the permanent collection of Oregon State University libraries. My signature below authorizes release of my thesis to any reader upon request.

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Barbara K. Burkholder, Author

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## CONTRIBUTION OF AUTHORS

Gordon Grant, Peter Wampler, and Roy Haggerty created the initial study plan and project focus. Gordon Grant and Roy Haggerty provided continual guidance throughout the field campaign and subsequent data analysis. Tarang Khangaonkar provided knowledge of Clackamas River hydrodynamic model CE-QUAL-W2. All listed authors also contributed several helpful reviews and suggestions in preparation of and during the writing of the manuscript.

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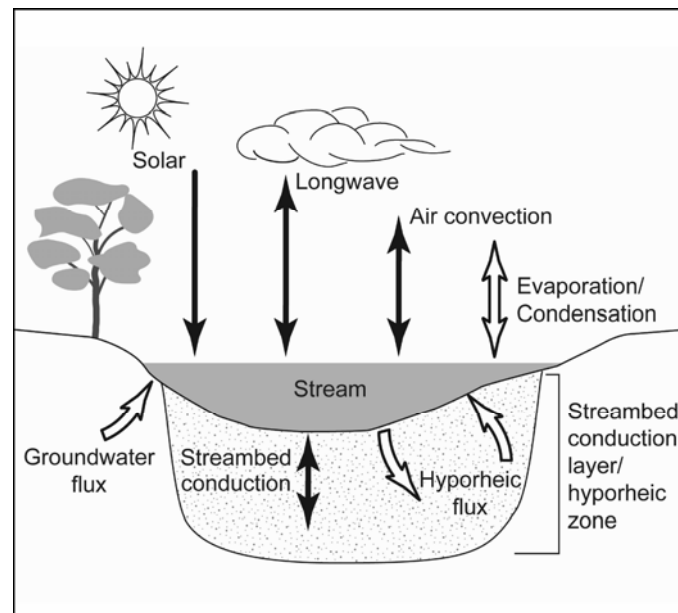
## 1 INTRODUCTION

A river's thermal regime is a key factor in determining the overall health of the river ecosystem. River temperature controls what species can exist within the river, as well as the distribution of those species (Vannote *et al.*, 1980; Ebersole *et al.*, 2001). It determines growth rates of aquatic organisms and timing of emergence and movement for fish such as salmon (Elliot and Hurley, 1997; Johnston, 1997). Water temperature also influences microbial processing rates, which govern nutrient cycling (Edwards, 1998).

River temperature varies diurnally and seasonally, cycles determined by numerous, interrelated variables and heat exchange processes (Fig. 1.1). Although these drivers may change naturally over time, several studies document how anthropogenic impacts, whether applied directly to a river (e.g. channel diversion, dams, or wastewater discharge) or to the land surrounding a river (e.g. deforestation, urbanization), can affect a river temperature (e.g. Brown, 1970; Webb and Walling, 1993b; Johnson and Jones, 2000; Lowney, 2000; Sinokrot and Gulliver, 2000). This is the case on the 6<sup>th</sup>-order, lower Clackamas River, where reservoir heating from a series of hydroelectric dams has resulted in a 1-3 °C increase in maximum daily temperature during summer low flows.

Regulatory temperature standards, such as those set by the Federal Clean Water Act, are created to maintain high quality aquatic habitat and motivate mitigation when river temperatures are out of compliance. However, mitigating temperature changes in rivers is no easy task. In trying to decrease river temperature, one mitigation approach is to increase shade, although this benefit decreases as rivers get wider and the fraction of effectively shaded river decreases. Floodplain restoration may lead to the development of alcoves or side channels that can provide thermal refugia for aquatic organisms (Bryenton, 2007). This project investigates another thermal mitigation strategy based on increasing hyporheic exchange through a planned program of gravel augmentation.

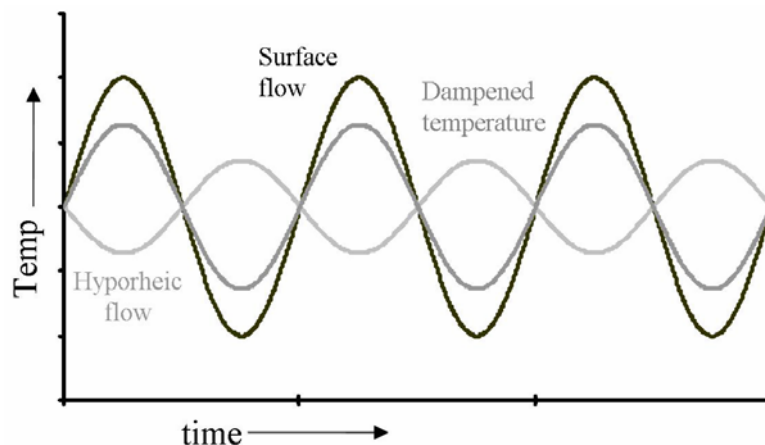
Hyporheic exchange, where river water downwells into the shallow subsurface and reemerges back into the main channel after a period of time, occurs where there



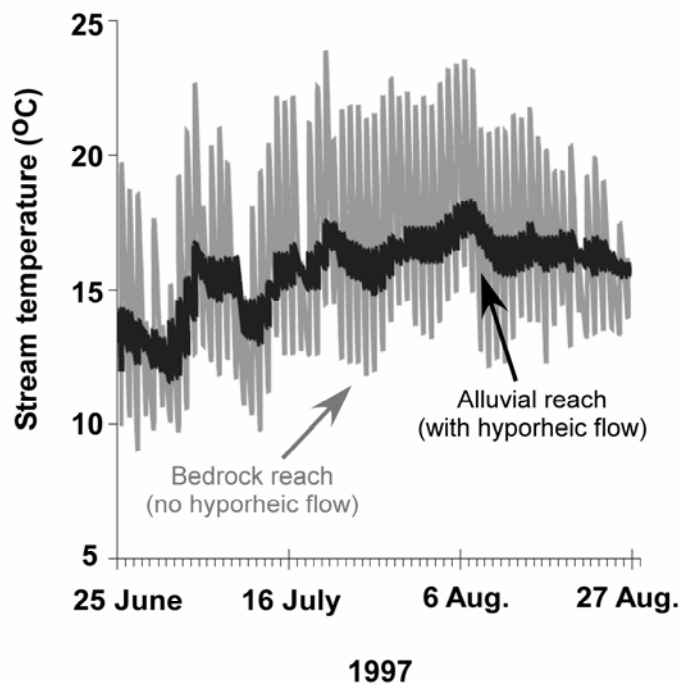
**Figure 1.1 Heat exchange mechanisms that comprise river temperature budgets.**

**From Loheide and Gorelick (2007).**

are changes hydraulic gradient within the river channel. This leads to river water downwelling into the channel bed, banks, or across bar morphology. The residence time of the water within the hyporheic zone can lead to out-of-phase mainstem and hyporheic temperatures, where reemerging hyporheic water is cooler than the mainstem in the middle of the afternoon and warmer than the mainstem at night. This buffers river temperature fluctuations, which could decrease maximum and minimum temperature peaks (Fig. 1.2). This effect is well documented over a range of river sizes and bar morphology. Most studies observe a localized effect associated with bar morphology, where emerging hyporheic water has a different temperature than the mainstem (White *et al.*, 1987; Evans and Petts, 1997; Brown *et al.*, 2005; Hancock and Boulton, 2005; Moore *et al.*, 2005; Sliva and Williams, 2005; Cozzetto *et al.*, 2006; Fernald *et al.*, 2006), but some studies do document a buffering of overall river temperature (Arscott *et al.*, 2001; Johnson, 2004). For example, Johnson (2004)

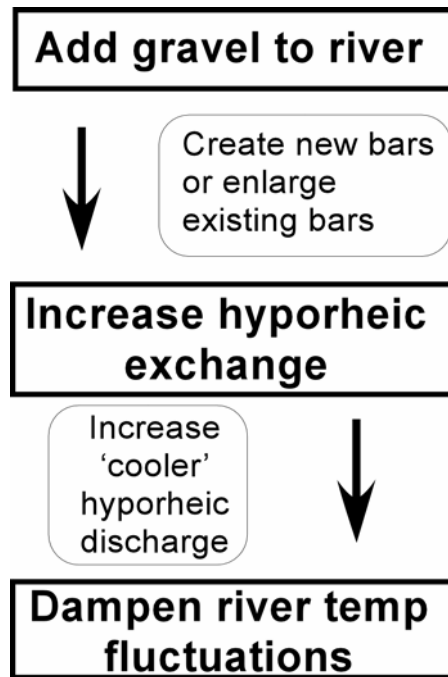


**Figure 1.2 Schematic of idealized out-of-phase mainstem and hyporheic temperature fluctuations and the resulting dampened temperature.**



**Figure 1.3 Stream temperature in two adjacent reaches of a stream in the HJ Andrews Experimental Forest, Oregon, USA. Note the large diurnal temperature fluctuations (gray) as water runs through the bedrock reach with no hyporheic zone versus the small temperature fluctuations (black) present in the alluvial reach with large hyporheic zone. Modified from Johnson, 2004.**





**Figure 1.4 Conceptual diagram describing how gravel augmentation can help thermally restore a river.**

reports that water temperatures are buffered up to 8.7 °C in a 2<sup>nd</sup>-order stream as it flows through an alluvial reach (Fig. 1.3).

Adding gravel to the river would not only create new bars and/or enhance existing bars, but would also increase the amount of water traveling through the hyporheic zone. Increased hyporheic discharge could lead to more temperature buffering which could affect the overall thermal regime of the river (Fig. 1.4). The owner of the hydroelectric projects on the Clackamas River, Portland General Electric (PGE), is interested in designing a gravel augmentation program below the dams in order to restore sediment transport and enhance fish habitat. Given the elevated temperatures on the lower river, they were also interested in learning about potential thermal benefits from adding gravel. This work addresses that question by qualifying and quantifying the amount of hyporheic exchange that currently affects

temperature on the lower Clackamas River, specifically hyporheic exchange that occurs through gravel bars.

The project approach includes three components: 1) a geomorphic and thermal characterization of the gravel bar population to identify where hyporheic exchange occurs and its connections to bar morphology, 2) a detailed characterization of three representative gravel bars in order to quantify the amount of emerging cooler hyporheic water; and 3) a 1<sup>st</sup>-order mixing model to assess how the quantified hyporheic exchange affects overall river temperature. Appendices A-J include much of the data used and obtained throughout the study, including methodology for collecting and using the data.

Understanding how much hyporheic exchange currently affects the lower Clackamas River will provide insight as to how a gravel augmentation scenario could potentially affect temperatures in a large river and improve aquatic habitat.

**2 INFLUENCE OF HYPORHEIC FLOW AND GEOMORPHOLOGY ON  
TEMPERATURE OF A LARGE, GRAVEL-BED RIVER, CLACKAMAS  
RIVER, OREGON, USA**

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## 2.1 Abstract

The hyporheic zone influences the thermal regime of rivers, buffering temperature by storing and releasing heat over a range of timescales. We examined the relationship between hyporheic exchange and temperature along a 24-km reach of the lower Clackamas River, a large gravel-bed river in northwestern Oregon (median discharge = 75.7 m<sup>3</sup>/s; minimum mean monthly discharge = 22.7 m<sup>3</sup>/s in August 2006). With a simple mixing model, we estimated how much hyporheic exchange cools the river during hot summer months. Hyporheic exchange was primarily identified by temperature anomalies, which are patches of water that demonstrate at least a 1 °C temperature difference from the main channel. Forty hyporheic temperature anomalies were identified through field investigations and TIR (Thermal-Infrared-Radiometry) in summer 2006. The location of anomalies was associated with specific geomorphic features, primarily bar channels and bar heads that act as preferential pathways for hyporheic flow. Detailed field characterization and groundwater modeling on three Clackamas gravel bars indicate residence times of hyporheic water can vary from hours to weeks and months. This was largely determined by hydraulic conductivity, which is affected by how recently the gravel bar formed or was reworked. Upscaling of modeled discharges and hydrologic parameters from these bars to the other anomalies on the Clackamas network shows that hyporheic discharge from anomalies comprises a small fraction ( $\ll 1\%$ ) of mainstem discharge, resulting in small river cooling effects (0.012 °C). However, the presence of cooler patches of water within rivers can act as thermal refugia for fish and other aquatic organisms, making the creation or enhancement of hyporheic exchange an attractive method in restoring the thermal regime of rivers.

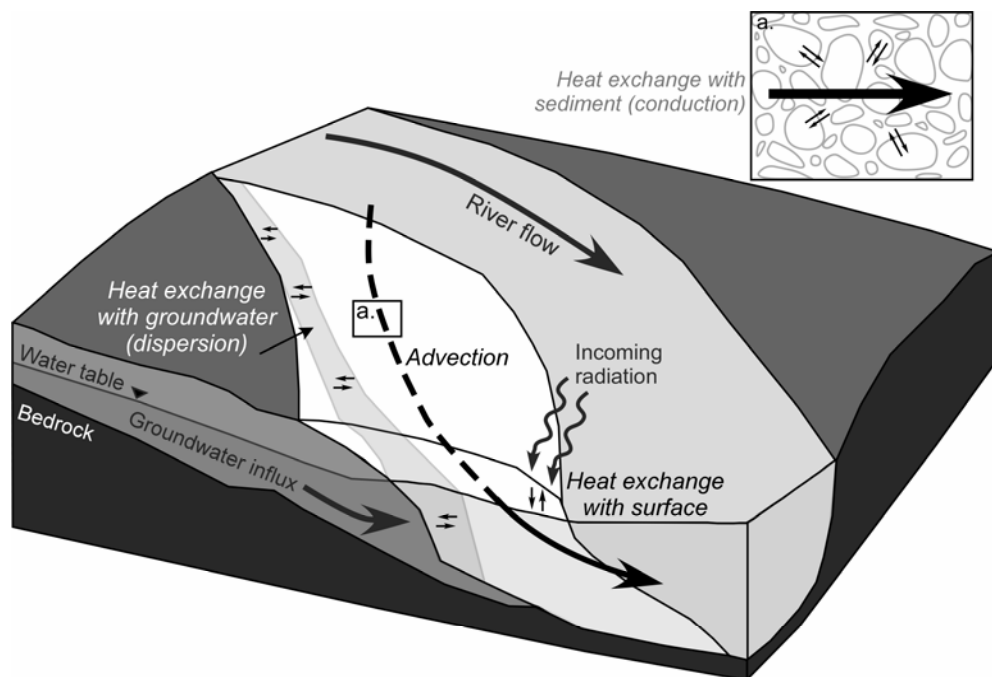
## 2.2 Introduction

Understanding heat fluxes within rivers is increasingly important as anthropogenic influences and changing climate alter river thermal regimes, which can lead to shifts in aquatic species composition and changing rates of biogeochemical processes (Evans *et al.*, 1998; Poole and Berman, 2001). Numerous and inter-related

physical mechanisms influence stream temperature, making it difficult to distinguish the magnitude or impact of individual drivers (Johnson, 2004).

Solar radiation (and shade), air temperature, groundwater inputs, and wind speed are the primary external drivers in most rivers that determine how much heat is added to or removed from the system (Sullivan and Adams, 1991). Internal drivers, which include bed conduction and hyporheic exchange, do not remove heat from the river channel but redistribute it temporally and spatially (Poole and Berman, 2001). Hyporheic exchange, where surface water enters the shallow subsurface (channel bed, banks or morphological features) and then reemerges back into the main channel, has previously been thought to have little impact on river temperature (Brown 1969), but a number of recent studies show that hyporheic exchange plays an important role in the thermal dynamics of some streams (Story *et al.*, 2003; Johnson, 2004; Loheide and Gorelick, 2006).

The hyporheic zone serves as transient storage within a river, where river water and heat can be retained for periods of time before being released back into the river (Bencala and Walters, 1983; Bencala, 2005). As surface water downwells into and is transported through the hyporheic zone, the heat within that water is transported and exchanged by several processes (Fig. 2.1). Advection via fluid flow dominates heat transfer (Stallman, 1965; Silliman *et al.*, 1993; Silliman *et al.*, 1995; Anderson, 2005; Keery *et al.*, 2006), although heat exchange may also influence hyporheic heat transfer. Along hyporheic flow paths, heat exchanges with sediment by conduction. This exchange is fast – dimensional analysis for cobbles of typical properties indicate thermal equilibrium is achieved within an hour or two. Heat also exchanges with groundwater by dispersion and conduction, and with the atmosphere by conduction and movement of latent and sensible heat. If the water table is high, solar heating of surface sediments may increase hyporheic water temperatures (Silliman *et al.*, 1995, Arrigoni *et al.*, *in press*). Collectively, these processes generally lead to a combination of “buffering, cooling and lagging” (Arrigoni *et al.*, *in press*) of temperatures within the hyporheic zone.



**Figure 2.1: Conceptual diagram showing the different processes that influence hyporheic water temperatures in a gravel bar (white). Advection (large dashed/solid black arrow) transports heat via fluid flow, conduction (small black arrows) transfers heat between sediment and hyporheic water, dispersion and conduction (shaded zone within gravel bar) occur as hyporheic water and groundwater interact, and incoming solar radiation indirectly warms hyporheic water via conduction and transfer of latent and sensible heat.**

Emergent hyporheic temperature may be different than the mainstem temperature. Transport through the hyporheic zone may result in a temporal phase shift between hyporheic and mainstem temperatures, where cooler hyporheic water reemerges back into a warmer mainstem and vice versa. However, the mixing of emerging hyporheic water and mainstem water does not ‘cool’ a river – mean temperature may stay constant – but it does dampen diurnal temperature fluctuations in the river by decreasing maximum temperatures and increasing minimum temperatures (Johnson, 2004; Arrigoni *et al.*, *in press*). This dampening results from

shielding of hyporheic water from changes in solar radiation and air temperature that influence mainstem surface water temperature.

Hyporheic exchange can occur across several spatial scales, from roughness elements on the stream bed to channel-scale riffles and bars to reach-scale meander necks and floodplains (Edwards, 1998; Harvey and Wagner, 2000). Most hyporheic temperature studies to date have focused on examining the relationship between hyporheic exchange and channel-scale morphology. In smaller catchments, several studies report finding cooler water emerging from the bottom of riffles or step-pool structures (Evans and Petts, 1997; Brown *et al.*, 2005; Hancock and Boulton, 2005; Moore *et al.*, 2005; Sliva and Williams, 2005; Hunt *et al.*, 2006). Peterson and Sickbert (2006) studied hyporheic exchange across a meander neck of a 3<sup>rd</sup>-order stream and found that hyporheic temperatures correlate with seasonal temperature variations, suggesting seasonal residence times. Fernald *et al.* (2000, 2006) reported on a larger river (8<sup>th</sup> order), that cooler water emerges from gravel bars into ‘alcoves,’ or off-channel lentic water connected at the downstream end to the mainstem. Additionally, hyporheic flows were more pronounced and had a greater impact on river temperature where gravel had been recently reworked by river flows. Arscott *et al.* (2001) found that hyporheic exchange generated significant temperature heterogeneity in higher-order reaches (2<sup>nd</sup> - 7<sup>th</sup>).

In reach-scale temperature studies, longitudinal trends in temperature demonstrate spatial and temporal thermal heterogeneity. Johnson (2004) compared bedrock and alluvial reaches along the same reach of 1<sup>st</sup>- and 2<sup>nd</sup>-order streams and found maximum daily temperatures were buffered by as much as 8.7°C. Torgersen *et al.* (1999) used thermal imagery along a river reach and found that the general increase in temperature downstream contained several peaks and troughs, reflecting bedrock and alluvial reaches respectively.

There are few hyporheic temperature studies for larger, lower-gradient rivers, and none have quantified the effect of hyporheic exchange on overall longitudinal river temperature. In this study we sought to: 1) identify areas of hyporheic exchange on a large, gravel-bed river and investigate their relationship with channel

morphological features, 2) quantify the amount of hyporheic exchange occurring, and 3) estimate how much hyporheic exchange affects overall river temperatures.

## 2.3 Methods

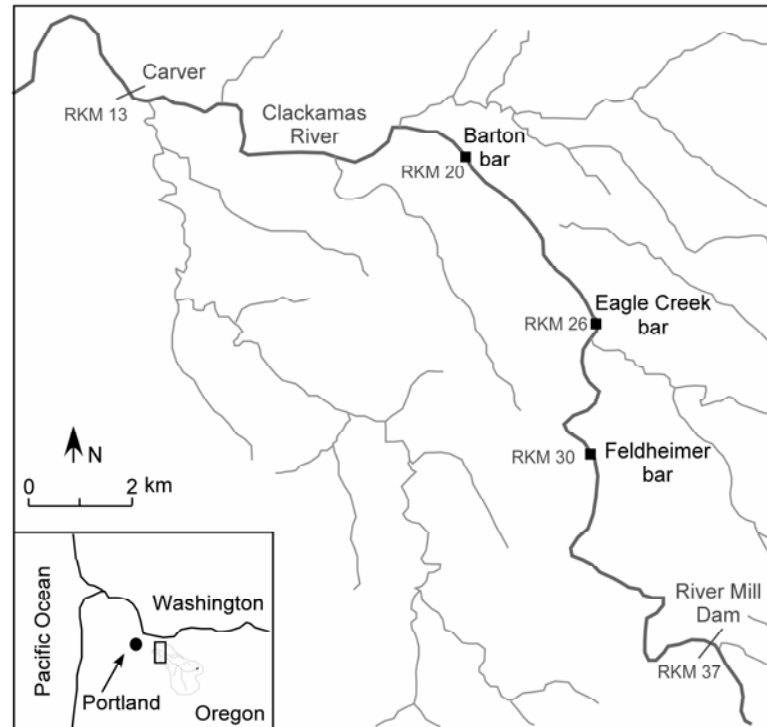
### 2.3.1 Study Area:

The Clackamas River is a 6th-order, gravel-bed river in northwestern Oregon, USA that drains approximately 2,430 km<sup>2</sup> from its headwaters in the Cascade Range to its confluence with the Willamette River in Oregon City. Our study focused on a 24-km reach on the lower Clackamas River, stretching from River Mill Dam (River km 37 (RKM 37)) to Carver, Oregon (RKM 13) (Fig. 2.2). The dam location marks a change of topography within the drainage basin, with the river moving from a confined canyon into a broad valley. Longitudinal gradients below the dam along the study reach average 0.0029 (Wampler, 2004). The median annual flow is 75.7 m<sup>3</sup>/s and the median summer flow is 25.9 m<sup>3</sup>/s.

Sediment supply to the lower river is generated primarily from periglacial sediment in the Cascade Range. Dam infrastructure on the Clackamas has cut off this supply for almost 100 years, and sediment inputs into the reach are limited to periodic erosion of alluvial Holocene terraces (Wampler, 2004). However, an extensive gravel bar population (> 50 bars) is distributed throughout the study reach, with median grain-size of 7.5 cm (Wampler, 2004). The population is composed primarily of mid-channel bars (55 % of bars by area), with lateral bars (34 %) and point bars (11 %) making up the rest of the network. The bar alluvium, which can range up to 6 m in thickness, rests on cemented, fine-grained Miocene volcanoclastics and mudstones. The Sandy River Mudstone, which underlies the lower 21 km of the study reach, is easily eroded, leading to rapid formation of flutes and potholes when bedrock surfaces are exposed (Wampler, 2004).

Gravel bar stability decreases downstream, with well-vegetated, coarse-grained, skeletal bars, bars without finer sediments (median grain size ( $D_{50}$ ) surface: 15 - 30 cm), in the upper 3 km of the reach grading into unvegetated bars with smaller grain sizes ( $D_{50}$  surface = 5 - 7 cm). Wampler (2004) points out that the presence of





**Figure 2.2 Site location and study reach, lower Clackamas River, Oregon, USA.**

the dam most likely causes this effect, as winter flows ( $850 - 1130 \text{ m}^3/\text{s}$ ) winnow out fines and smaller particles from the upper reaches and transport them downstream. Winter flows influence bar morphology throughout the reach, with most gravel reworking occurring between Feldheimer (RKM 30) and Carver (RKM 13).

The dam also affects the river temperature regime, especially during low flows in the summer months. The magnitude of this change has been modeled with CEQUAL-W2, a hydrodynamic 2D water quality model, which shows that the Clackamas River currently exceeds state temperature standards by  $1 - 3 \text{ }^\circ\text{C}$  from July to September (Portland General Electric, 2005). Current research in association with dam relicensing efforts are exploring natural mechanisms of thermal mitigation, including potential thermal benefits of adding gravel to the river to increase the amount of hyporheic exchange and hyporheic buffering.

### ***2.3.2 Field measurements and data collection:***

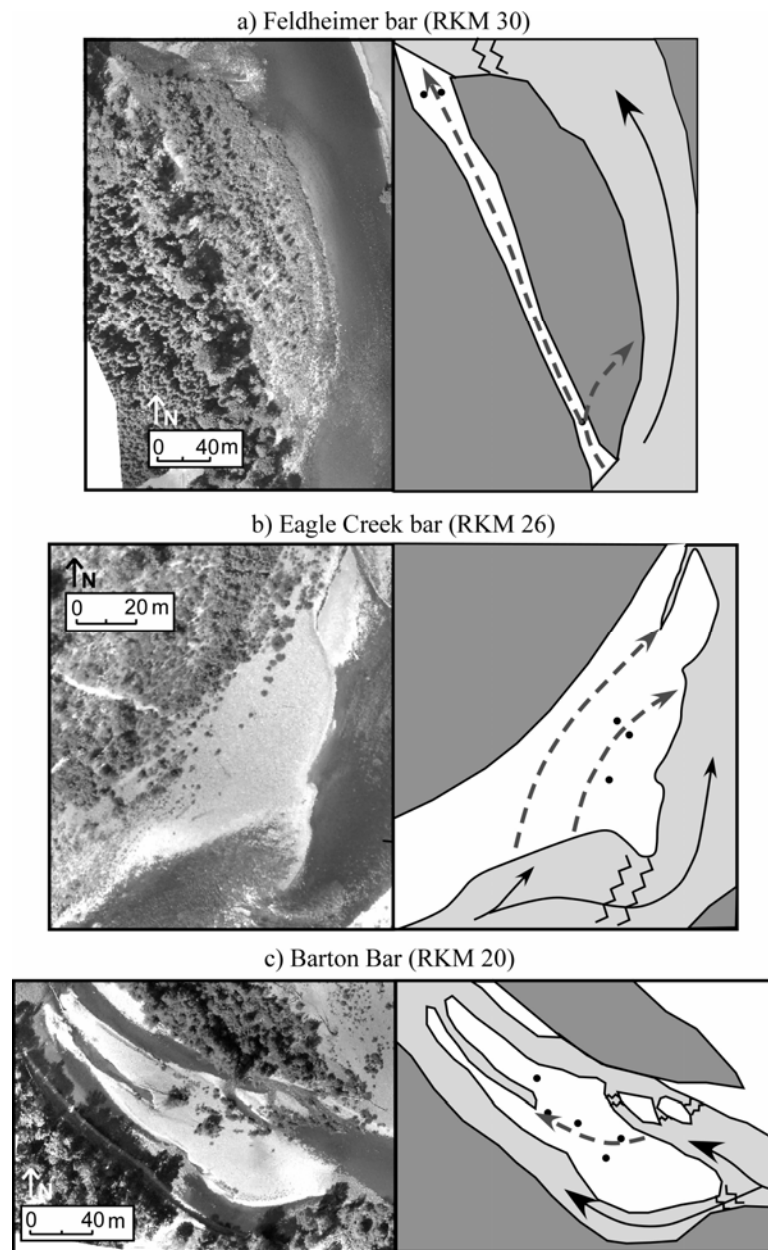
Our field campaign from July to September 2006 investigated the gravel bars within the study reach, the hypothesized primary location of hyporheic flow that could influence mainstem river temperature. Due to the length of the study reach, hyporheic exchange was identified using techniques that were easy to conduct and replicate over 24 km of river. During early reconnaissance we identified locations with visually observable flow from gravel bars and used a handheld YSI 63 electrical conductivity and temperature probe (Yellow Springs, Ohio, USA) to identify temperature anomalies, which we defined as patches of water that deviate from mainstem water temperatures by at least 1 °C. The handheld probe was used to conduct temperature surveys around bar perimeters and identify anomaly locations. Reference mainstem temperatures were taken during temperature surveys at each site to account for diurnal heating of the river. Once an anomaly was identified, we also recorded electrical conductivity and width and depth along gravel bar edges. Groundwater inputs were distinguished from hyporheic flow by: (1) water emerging from channel edges rather than gravel bars; (2) higher specific conductance ( $> 80 \mu\text{S}/\text{cm}$  compared to river  $55 - 65 \mu\text{S}/\text{cm}$ ); (3) iron-stained sediment resulting from groundwater oxidation; and/or (4) consistent temperatures representative of groundwater ( $10 - 12 \text{ }^\circ\text{C}$  (Well logs obtained from OWRD)). River discharge decreased throughout the summer (from  $28$  to  $21 \text{ m}^3/\text{s}$ ), and to capture how this impacted the hyporheic zone, most identified anomaly sites were revisited several times over the summer to take more temperature measurements and re-measure anomaly dimensions.

Two Thermal-Infrared Radiometry (TIR) surveys were flown over the study reach on August 13<sup>th</sup>, 2006, one at 6 am and the other at 3 pm (Watershed Sciences, Inc., Corvallis, Oregon, USA). This provided a complete 2D map of daily maximum and minimum river surface temperatures, as well as an additional visual method to observe and detect temperature anomalies. Longitudinal temperature profiles were constructed by taking the median temperature for each sampled image per river kilometer. In-stream temperature loggers deployed throughout the study reach before

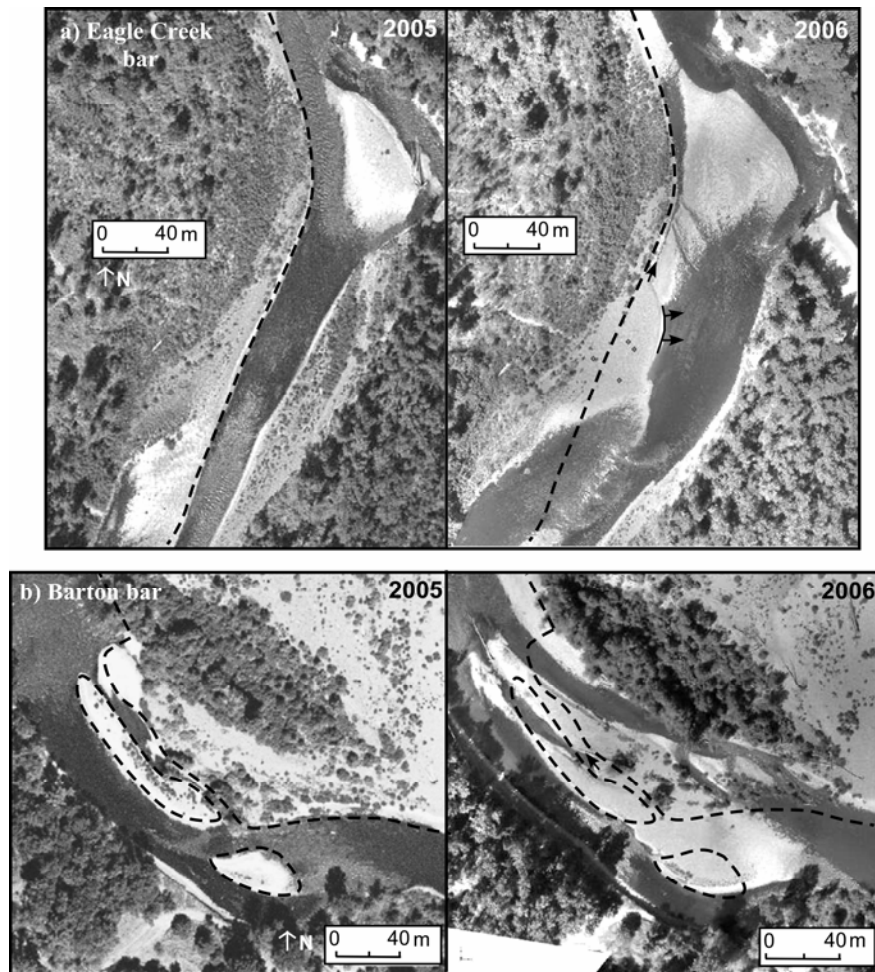
the flights were used to calibrate and verify the accuracy of TIR data. Pixel resolution of imagery is 0.9 m.

Three gravel bars with temperature anomalies were selected for detailed field characterization and modeling. These three representative bars exhibited geomorphic features and sedimentological textures characteristic of the majority of the gravel bar population on the lower Clackamas River. Field characterization included examination of bar type, location within the reach, sediment size, presence of vegetation, and bar history. Based on comparison of aerial photos from July 2005 (discharge,  $Q = 29.3 \text{ m}^3/\text{s}$ ) and August 2006 ( $Q = 23 \text{ m}^3/\text{s}$ ), gravel features that did not appear in 2005 photos but were mapped in 2006 are considered 'new' features. We refer to all other features as older, but recognize that these bars also have a distribution of ages. Figure 2.3 shows basic bar morphology and interpreted hyporheic flow paths for each bar. Feldheimer bar (RKM 30) is an older, large lateral bar that is well-vegetated except for a 350-m long unvegetated back-bar channel that becomes active during high flow. Eagle Creek bar (RKM 26) is a new gravel feature that formed along an older bar edge during 2005 winter flows (Fig. 2.4). Barton bar is a mid-channel bar (RKM 20) that has new infillings of gravel among older bar deposits (Fig. 2.4).

Each bar was instrumented with several 3.4-cm inner diameter (1.33-in) galvanized steel piezometers (Maas Midwest Manufacturing, Huntley, Illinois, USA) with 17.8-cm (7-in) screens immediately above a conical drive point (3 piezometers in Feldheimer bar, 3 in Eagle Creek bar, 5 in Barton bar). Given the large diameter of the sediment composing the gravel bars, it was not feasible to install the piezometers by hand-driven methods. A gas-powered jackhammer was used to drive the piezometers into the gravel bars, usually through at least 1 m of sediment to a depth of approximately 0.5 m beneath the water table. We assumed that flow across the gravel bars in the hyporheic zone is predominantly horizontal, which is hydrogeologically reasonable. Consequently, hydraulic head would have negligible changes with depth. Therefore, we put highest priority on horizontal separation of piezometers and did not install any multilevel piezometers. Alexander and MacQuarrie (2005) showed that



**Figure 2.3 Summer 2006 aerial imagery and schematic diagram for a) Feldheimer, b) Eagle Creek, and c) Barton gravel bars (see Fig. 2.2 for locations). Piezometer locations (black dots) and interpreted subsurface flow paths (dashed gray lines) are overlain on open gravel (white) and vegetated areas (dark gray). Mainstem (light gray) flow direction given by solid black arrows. Riffles represented by zigzag pattern.**



**Figure 2.4 Aerial imagery showing gravel reworking between summers 2005 (left) and 2006 (right) for a) Eagle Creek and b) Barton bars. Dashed black lines follows outline of 2005 gravel bars and solid black arrows indicate flow direction of temperature anomalies.**

temperature measurements within steel piezometers have less than 0.1 °C error and are perfectly correlated to in-situ measurements.

Topographic surveys were conducted at each bar, using both a Leica TCRP 1201 total station (Heerbrugg, Switzerland) and a Trimble 4700 RTK GPS (Sunnyvale, California, USA). We mapped water edges, notable topographic features, and piezometer locations. Heads within piezometers were obtained through surveying

the elevation of the top of the piezometer and subtracting the distance to the water table (2 cm vertical accuracy). Tidbit Stowaway thermistors (0.2 °C accuracy, Onset, Bourne, Massachusetts, USA) were checked against a 0.1 °C resolution NIST-traceable thermometer (Cole-Parmer, Vernon Hills, Illinois, USA) and placed within the screened section of the piezometers where they recorded temperature every 15 min for 7 - 10 days. Tidbits were also placed at head of the bar to record mainstem temperatures of water entering the bar and also placed in areas of emerging hyporheic flow. Slug tests were conducted within each piezometer, and results were analyzed using methods outlined by Bouwer and Rice (1976) and Butler and Garnett (2000).

### ***2.3.3 Model simulations of hyporheic exchange within gravel bars:***

Topographic surveys, slug tests, and temperature mapping from the selected gravel bars were used to build and parameterize steady-state groundwater flow models using MODFLOW (McDonald and Harbaugh, 1988) implemented via the GMS interface (Environmental Monitoring Systems, Inc., South Jordan, Utah, USA). Model domains were one-layer thick finite difference grids with square cells, generally ranging between 0.2 m and 0.5 m (depending on the size of the bar being modeled). Models were calibrated to water table elevations in piezometers and anomaly outflow dimensions. On two bars, residence time distributions from detailed Tidbit temperature surveys, simulated with the particle tracking package MODPATH (Pollack, 1994), were also used to calibrate the models. A flow-budget module within MODFLOW was used to calculate the hyporheic discharge emerging from the anomalies, and MODPATH provided a distribution of water residence times.

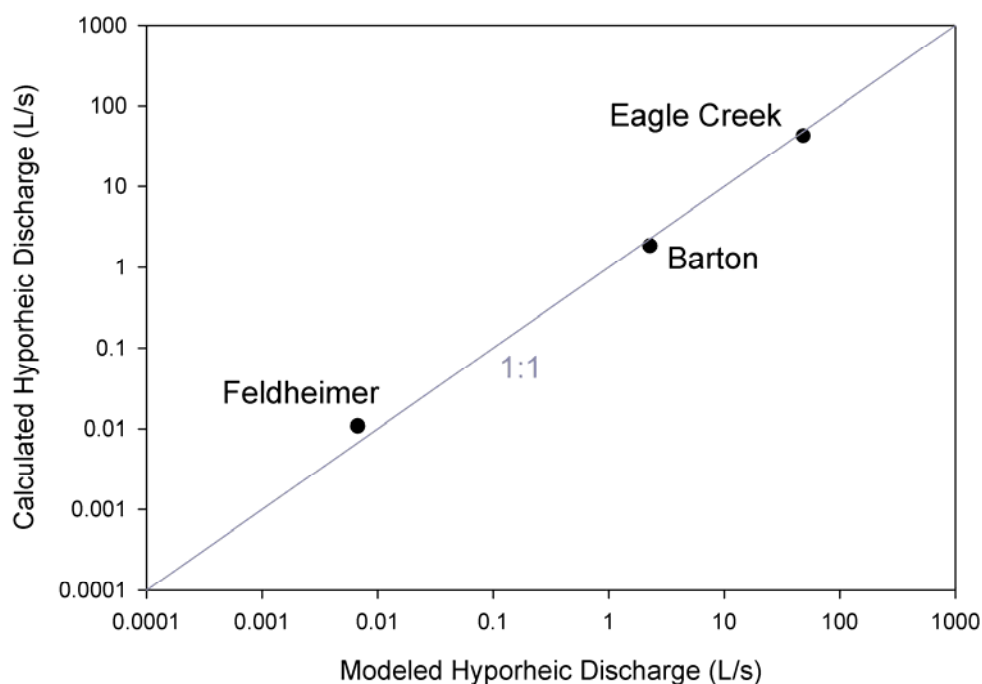
### ***2.3.4 Upscaling hyporheic exchange to the reach scale:***

To assess how hyporheic exchange from gravel bars affects overall river temperatures, we calculated discharges for all anomalies interpreted to be driven by primarily hyporheic flow. We intentionally excluded anomalies that were interpreted to be due to groundwater. We estimated flux through each representative anomaly using Darcy's law ( $Q_h = -K \nabla h A_h$ ). While technically valid at a point, we applied

Darcy's law across temperature anomalies by assuming uniform parameters; the accuracy of this is discussed below.  $Q_h$  is hyporheic discharge ( $L^3/T$ ) (as defined it is a vector, but we used only the magnitude),  $A_h$  is the cross-sectional area of the hyporheic discharge ( $L^2$ ),  $K$  is the hydraulic conductivity of the sediment ( $L/T$ ), and  $\nabla h$  is hydraulic gradient ( $L/L$ ).  $A_h$  was calculated by field measurement of the length across the edge of a gravel bar where we could detect a temperature difference and an estimate of the depth of gravel contributing to hyporheic flow. Hydraulic gradient across bars, in most cases, was measured in the field ( $N = 27$ ). On bars where hydraulic gradient was not directly measured ( $N = 13$ ), we used the average of the field measurements of cross-bar gradients.

Using aerial photographs from 2005 and 2006, we estimated  $K$  for each anomaly based on how recently a gravel bar has been created or significantly reworked. From our observations, we assumed that new gravel bars or portions of pre-existing bars that formed during the previous year's high flows were likely to have a higher  $K$  than older bars, inferring that these deposits will not have been substantially infiltrated by fines. Older gravel bars, on the other hand, were interpreted as more likely to have had finer sediments infiltrating the sediment matrix, leading to lower  $K$  values (Packman and Salehin, 2003). Some bars are a combination of both older and newer gravel deposits, which can lead to large differences in  $K$  over a limited area. Model data from our three representative bars helped us constrain hydraulic conductivities by giving us a  $K$  estimate for newer and older bars, as well as bars with both newer and older deposits. The limitations of this approach will be discussed in results.

We checked the accuracy of the Darcy's law discharge estimates against the discharge calculated by the groundwater flow models. We estimated parameters for Darcy's law using field estimates of average hydraulic gradient and hyporheic area. We also used a spatially-averaged  $K$  value from the groundwater models. Darcy's law and a full groundwater flow model yield nearly the same discharges: the relationship is approximately 1:1 and the mean difference between them is 25 % (Fig. 2.5). The discharges are nearly the same for the following reasons: changes in gradient (both



**Figure 2.5 Comparison of calculated (Darcy's law) and modeled (MODFLOW) hyporheic discharge for temperature anomalies on gravel bars. 1:1 line shown for reference.**

direction and magnitude) along the flow paths are small; we assumed  $K$  and cross-sectional area of hyporheic discharge are homogeneous along flow paths in both the Darcy's law and groundwater flow model calculations; and no sources or sinks of water exist along the flow paths. While there are significant heterogeneities in  $K$  within and between gravel bars, these within bar heterogeneities are at a large scale in comparison to the gravel bar, meaning that individual flow paths have relatively homogeneous  $K$ . Consequently, the Darcy's law approach provides a reasonable and feasible estimate of hyporheic discharge, and we confidently employ it for the other temperature anomalies on the Clackamas.

All field and model data can be obtained from appendices in Burkholder (2008).

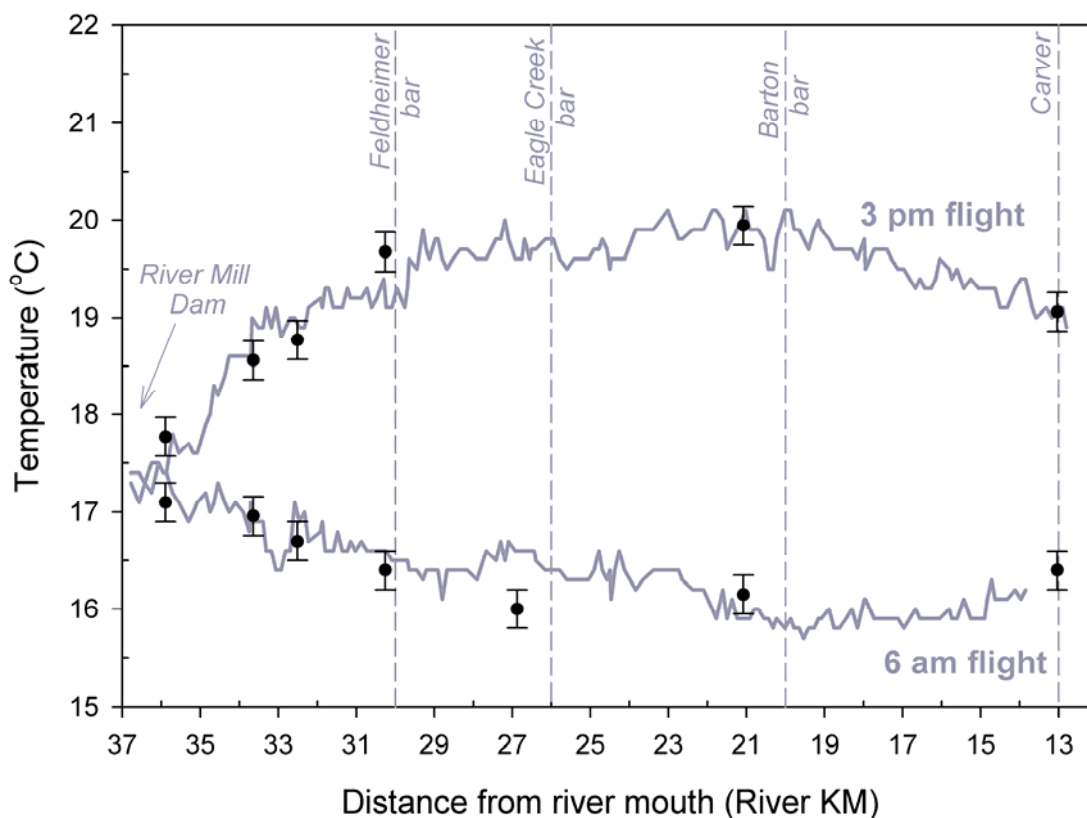


## 2.4 RESULTS

### 2.4.1 *Thermal Infrared Radiometry (TIR):*

TIR was used to construct a reach-scale longitudinal profile of stream temperatures as recorded at two points in time (Fig. 2.6). Comparison between thermal images and in-stream temperature loggers suggests that thermal images are within 0.5 °C of directly measured mainstem temperatures. Water released from the dam had a constant temperature of approximately 17.4 °C. Water warmed downstream during the day and cooled during the night, with rates of warming and cooling decreasing downstream, presumably either because stream temperatures are closer to thermal equilibrium with the atmosphere and/or because increased discharge downstream (from groundwater and tributary inputs) creates a larger volume of water to be heated/cooled. Consequently, the warmest point in the reach during the day was near Barton (RKM 21), which approximately corresponds to the distance water traveled in daylight hours from the dam (16 km) (see analysis in Khangaonkar and Yang, *in press*). Further downstream, water was cooler because this water traveled some distance downstream from the dam during the night. An inverse pattern was observable in the early morning, with minimum temperatures recorded at Barton (Fig. 6). This modulation of temperature amplitudes below a dam is well documented (Polehn and Kinsel, 1997; Lowney, 2000) and was recently re-visited for the Clackamas River by Khangaonkar and Yang (*in press*).

TIR demonstrates that significant spatial and temporal thermal heterogeneity exists within the study reach. TIR morning imagery detected 34 temperature anomalies using the 1 °C rule, 16 of which were not previously identified in the field. These warmer patches of water emerged from gravel bars into a cooler mainstem (Figs. 2.7, 2.8). Anomalies with temperatures cooler than the mainstem were also detected in morning imagery, suggestive of groundwater influx rather than hyporheic exchange. Afternoon flight imagery was not useful in identifying cooler hyporheic patches. TIR measures temperatures at the surface, which masked the denser, cooler water that emerged below the warmer surface water surface. The resolution of the



**Figure 2.6 Longitudinal temperature profiles of the lower Clackamas River from River Mill Dam (RKM 37) to Carver, Oregon (RKM 13) recorded by TIR on August 13th, 2006. In-stream data loggers (black circles) indicate river temperature with measurement error.**

imagery may also play a role in masking anomalies by averaging the much warmer gravel shoreline with cooler water temperatures in a single pixel.

#### **2.4.2 Bar geomorphology controls on hyporheic exchange:**

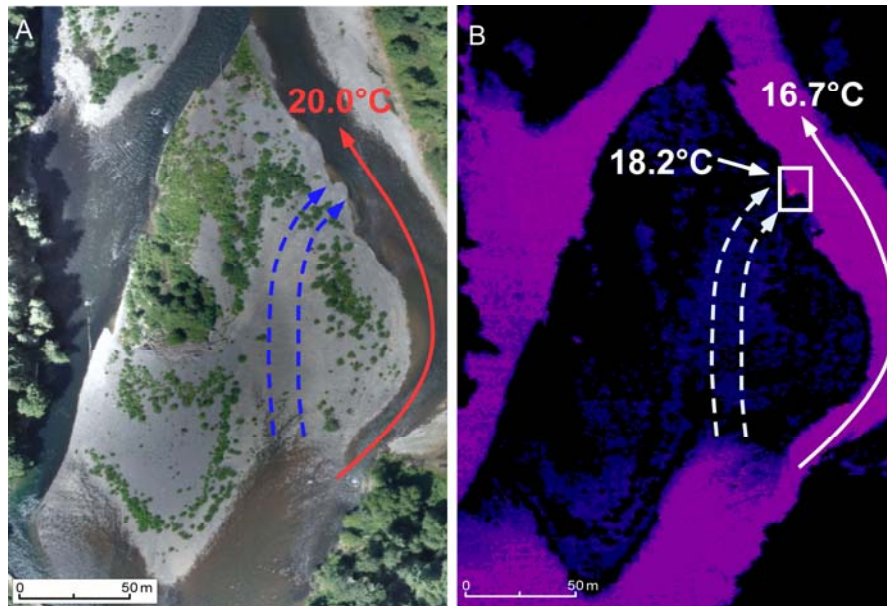
A total of 52 temperature anomalies were identified by a combination of field investigations and TIR imagery over summer 2006. Depending on time of day, these features discharged water that generally ranged from 1 to 4 °C different than the mainstem. The anomalies were distributed along the entire 24-km study reach, with the greatest anomaly density (3.0 anomalies/km) in the 6.4-km reach between the

Eagle Creek confluence to just below Barton (RKM 26.4 to RKM 20). The lowest density (1.4 anomalies/km) was in the 8-km reach immediately below River Mill Dam. This is consistent with previously interpreted levels of bar activity and presence of skeletal bars (bars without finer gravel) in the reaches immediately below the dam (Wampler, 2004).

Twelve anomalies were interpreted as primarily due to groundwater seepage rather than hyporheic exchange, based on the criteria outlined in methods. The remaining 40 anomalies are interpreted to be primarily driven by downwelling of river water, although we recognize they may also be influenced by some heat exchange with groundwater. This is supported by the fact that groundwater and hyporheic anomalies tended to occur adjacent to one another on individual gravel bars (6 of 12 identified groundwater seeps). One anomaly demonstrated warmer temperatures in the late afternoon, but the water table was near the uppermost gravel surface and was likely influenced by heat of the gravel.

All hyporheic temperature anomalies occur on the edges of gravel bars. However, in most cases, they do not extend across the entire downstream edge of a gravel bar. Instead, they occur in association with specific geomorphic features present on gravel bars, features whose hydraulic gradient and hydraulic conductivity promote hyporheic residence times that result in offset hyporheic and mainstem temperature signals.

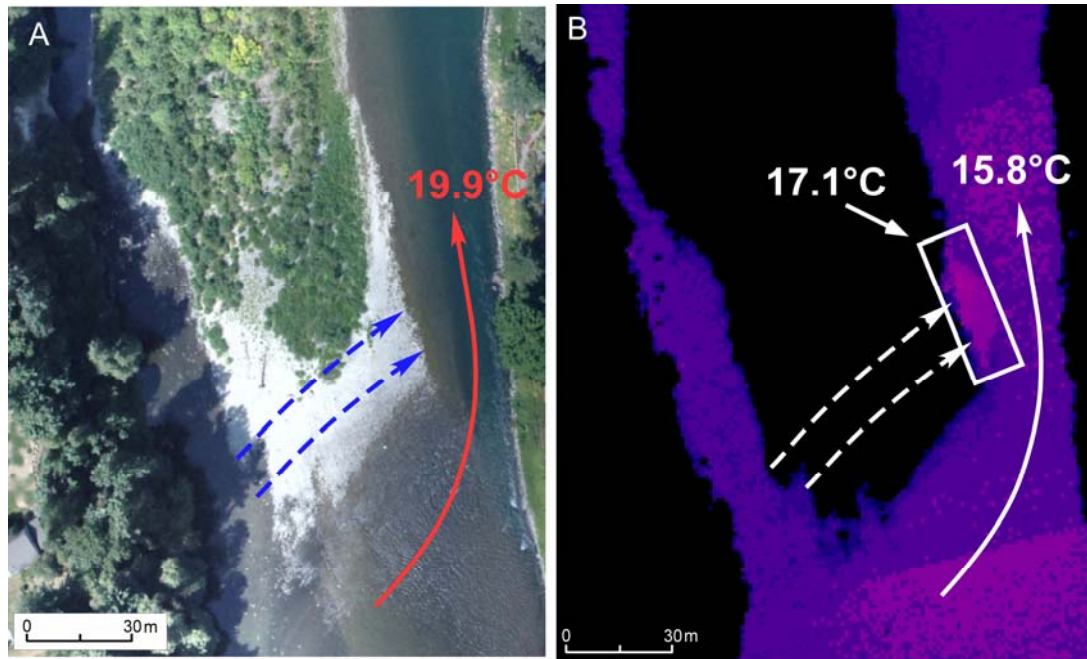
Twenty-four hyporheic anomalies (60 %) occur at the downstream end of bar channels, which are unvegetated pathways that are active during high flows (e.g., Feldheimer and Barton bars). These channels occurred along the back margin of bars (i.e., away from the mainstem), across bars, or as paleochannels that have been infilled by new gravel. Gradients along bar channels were higher than the longitudinal river gradient (mean cross-bar gradient: 0.007 compared to mean longitudinal gradient: 0.0029). Temperature anomalies associated with bar channels formed discrete, small patches (< 0.5 to 1 m in length as measured along the bar margin), due to the more defined structure of the feature (Fig. 2.7).



**Figure 2.7 Hyporheic exchange across a mid-channel bar (RKM 27). A) Dashed arrows on 2006 aerial photography indicate likely hyporheic flow paths through cross-bar channel feature. B) Small, discrete temperature anomaly identified on 6 am TIR photography.**

Sixteen hyporheic anomalies (40 %) were located downstream from bar heads, where hyporheic exchange follows a cross-bar gradient from hydraulically pooled water at the bar head to upwelling at the bar tail. (e.g. Eagle Creek bar) (Fig. 2.8). Unlike bar channels, we interpret hyporheic flow through this geomorphic feature as not being confined to discrete subsurface channels, but occurring across riffle structures, large sections of bars, or entire bars. Downstream temperature anomalies associated with this feature were laterally extensive (up to 25 m along gravel bar edges). Bar heads were primarily found on mid-channel bars, where branching of the mainstem creates higher hydraulic gradients (0.005 - 0.012) due to elevation differences between channels.

Decreases in river discharge throughout the summer, particularly from July to August, did influence the size of temperature anomalies. Generally, as discharge



**Figure 2.8 Hyporheic exchange across unvegetated section of mid-channel bar (RKM 15). A) Dashed arrows indicate likely hyporheic flow paths through bar head feature. B) Laterally extensive temperature anomaly identified on TIR 6 am photography.**

decreased, the width of several temperature anomalies along gravel bar edges also decreased (up to 1 – 2 m). However, all except 2 hyporheic anomalies persisted through late July and August when river temperatures were highest in the channel.

#### **2.4.3 Bar-scale data and model analysis:**

We summarize field and model data for each of the gravel bars selected for further characterization in Table 1. Changes in piezometer head elevations from upper to lower ends of the gravel bars varied, with about 0.1 - 0.2 m change across Eagle Creek and Barton bars and 0.682 m across the larger Feldheimer bar. Slug tests within piezometers demonstrated different behaviors between new and older gravel bars. In older bars (Feldheimer bar and sections of Barton bar),  $K$  ranges from  $1.1 \times 10^{-6}$  m/s to  $7.7 \times 10^{-5}$  m/s. In gravel that had been recently reworked (Eagle Creek bar and

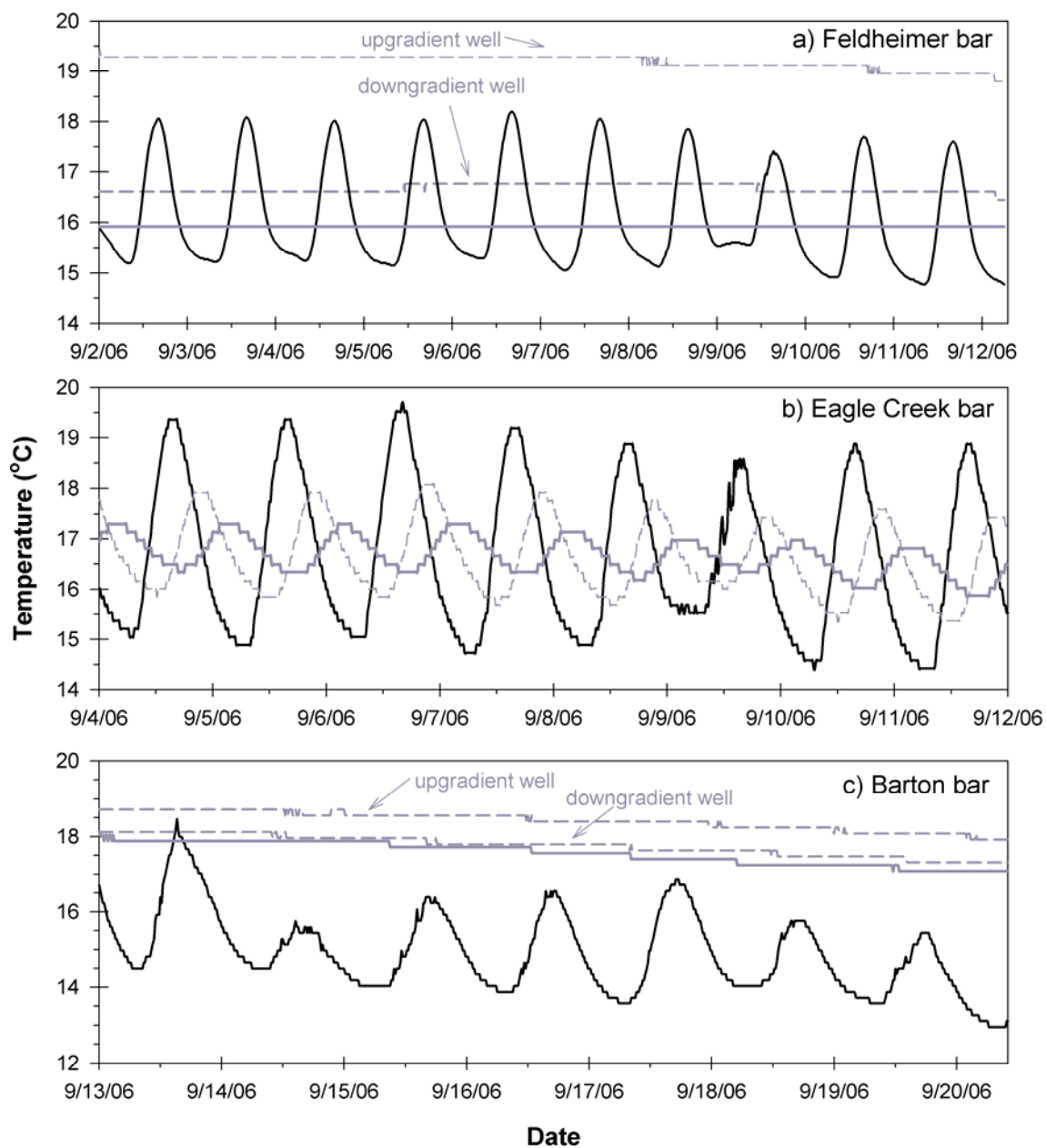
**Table 2.1: Field and model data for representative Clackamas gravel bars.**

Parameter	Feldheimer bar	Eagle Creek bar	Barton bar
	RKM 30	RKM 26	RKM 20
<b>Bar type</b>	Lateral	Point Bar	Mid-channel
<b>Geomorphic feature</b>	Back-bar channel	Bar head	Remnant channel
<b>Gradient (m/m)</b>	0.010	0.012	0.015
<b><math>D_{50}</math> surface (cm)</b>	6.4	5.8	6.9
<b><math>D_{50}</math> subsurface (cm)</b>	1.2	3.4	2.2
<b>Hyporheic area (m<sup>2</sup>)</b>	34	66	8
<b>Average <math>K</math> (m/s)</b>	$1.99 \times 10^{-5}$	$6.19 \times 10^{-2}$	$1.93 \times 10^{-3}$
<b>Residence time (d)</b>	~1040 d	0.49	~12
<b>Discharge (m<sup>3</sup>/s)</b>	$6.73 \times 10^{-6}$	$4.28 \times 10^{-2}$	$1.85 \times 10^{-4}$

sections of Barton bar), 5 - 10 second recovery to static water levels with atypical recovery curves made it difficult to assess hydraulic conductivity using established high- $K$  slug test analysis methods. Estimates of  $K$  were obtained by calibrating the appropriate MODFLOW models to travel time measured in offset temperature fluctuations. Hydraulic conductivity estimates average  $6.19 \times 10^{-2}$  m/s from the calibrated Eagle Creek bar model and  $1.93 \times 10^{-3}$  m/s from the calibrated Barton bar model.

Week-long temperature surveys also showed important differences between the older and newer gravel bars (Fig. 9). Temperatures in Eagle Creek bar showed a diurnal variation in temperature. As water from the mainstem moves through the bar, diurnal peaks in temperature were reduced to 20 % of their original peak height when they emerged back into the main channel, reflective of advective and conductive heat transfer. The phase lag in emerging hyporheic temperature indicates an 11.5 - 11.8 h water residence time, which approaches the maximum phase shift possible.

Temperature surveys from within Feldheimer and Barton bars did not fluctuate diurnally, but temperatures measured in downgradient piezometers were cooler than in upgradient piezometers (Fig. 2.9). The lack of diurnal temperature fluctuations is more indicative of groundwater rather than hyporheic exchange, but water temperatures



**Figure 2.9 Week-long temperature profiles for a) Feldheimer, b) Eagle Creek, and c) Barton bars. Surface mainstem temperatures (solid black lines) show dampening of diurnal fluctuations in emerging hyporheic flow (solid gray lines). Dashed gray lines represent within bar well temperatures.**

within the piezometers are well above ambient groundwater temperatures, suggesting that the water originated from the river channel. The loss of diurnal fluctuation is likely due to longer residence times (weeks to months), which is consistent with the much lower  $K$  values within the bars as estimated from slug tests and MODFLOW. Longer residence time can buffer and lag temperatures on a seasonal basis. For example, the temperature of emerging hyporheic water at Barton was consistently warmer than the mainstem channel in mid-September (Fig. 2.9) because cloudy, cooler weather reduced the amount of heat gained by the mainstem. Groundwater contributions may still be significant in emerging hyporheic temperatures, especially on Feldheimer bar which is connected to the channel edge.

Estimates of discharge emerging from each temperature anomaly are dependent on hydraulic gradient, hyporheic cross-sectional area, and  $K$  (Table 1). Of these variables,  $K$  has the most influence over hyporheic discharge. Eagle Creek bar, with the highest average  $K$  ( $6.19 \times 10^{-2}$  m/s) and largest hyporheic area ( $66 \text{ m}^2$ ), has the greatest calculated discharge of 42.5 L/s ( $0.0425 \text{ m}^3/\text{s}$ ), or 0.002 % of the mainstem discharge. Feldheimer bar, with the lowest average  $K$  ( $1.99 \times 10^{-5}$  m/s) and relatively large hyporheic area ( $34 \text{ m}^2$ ), has the lowest discharge of 0.00673 L/s ( $6.73 \times 10^{-6} \text{ m}^3/\text{s}$ ), almost four orders of magnitude lower than Eagle Creek. Barton bar, with an intermediate  $K$  ( $1.93 \times 10^{-3}$  m/s) but small hyporheic area ( $8 \text{ m}^2$ ) has an anomaly discharge of 1.85 L/s ( $1.85 \times 10^{-4} \text{ m}^3/\text{s}$ ), which is two orders of magnitude lower than Eagle Creek.

#### ***2.4.4 Hyporheic effect from anomalies on river temperature:***

Estimates of  $K$  for the three representative bars were used to estimate  $K$  values for the larger population of hyporheic temperature anomalies, using an inferred association between recent gravel reworking and  $K$ . Using aerial photo analysis to assess the degree of gravel reworking that occurred on bars during 2005-2006 winter flows, we assigned an Eagle Creek  $K$  value of  $6.19 \times 10^{-2}$  m/s to new bars or bars that were extensively reworked, a Barton  $K$  value of  $1.93 \times 10^{-3}$  m/s to bars that showed some degree of reworking, and a Feldheimer  $K$  value of  $1.99 \times 10^{-5}$  m/s to older bars



with little to no gravel reworking. We recognize that  $K$  is a highly variable and sensitive parameter, and our approach does not address downstream fining of sediments and changes in sediment packing. We view this approach as providing a rough estimate of the overall order-of-magnitude effect of anomaly-based hyporheic flow on stream temperatures that is consistent with the limited data available.

The change in river temperature due to hyporheic discharge can be approximated using a mixing equation

$$T_c = \frac{Q_m T_m + \sum (Q_h T_h)}{Q_c} \quad (2)$$

where  $Q_m$  is mainstem discharge ( $L^3/T$ ),  $T_m$  is mainstem temperature ( $^{\circ}C$ ),  $Q_h$  is hyporheic discharge ( $L^3/T$ ),  $T_h$  is hyporheic temperature ( $^{\circ}C$ ),  $Q_c$  is combined discharge ( $L^3/T$ ), and  $T_c$  is combined river temperature ( $^{\circ}C$ ). This equation neglects other sources and sinks of heat, offsets in time due to travel time from one anomaly to the next, and dispersion. These effects are discussed below. We emphasize that we investigated only hyporheic exchange, and not the effects of groundwater inputs on river temperature, so groundwater seeps were not included. Solving for  $T_c$  and subtracting it from mainstem temperature,  $T_m$ , gives the amount of river cooling expected from hyporheic exchange. To check the accuracy of the mixing equation approach, we compared it to results from a 2D hydrodynamic temperature model of the lower Clackamas River. We used CE-QUAL-W2 (Coles and Wells, 2004), a 2-D hydrodynamic model which incorporates the full spectrum of heat sources and sinks, to estimate river temperature sensitivity to hyporheic exchange. The CE-QUAL-W2 model was parameterized with a network of meteorological sensors that provided air temperature (2 points), short- and long-wave radiation (1 point), cloud cover (1 point), wind speed (4 points), and humidity (3 points). Other details on the model are provided by Battelle (2004) and Khangaonkar and Yang (*in press*). We used anomaly discharge, residence time, and temperature from the Eagle Creek bar and added 40 additional Eagle Creek-like anomalies throughout the river (in effect, doubling the number of current hyporheic anomalies), maintaining the same degree of anomaly density between different stretches of river. The model estimates river cooling of

0.16 °C. Using the mixing model, we estimated the cooling associated with the Eagle Creek anomaly (0.006 °C) and to simulate gravel augmentation, multiplied that effect by 40. This gives a river cooling estimate of 0.24 °C, an overestimate of 50%.

Using parameters shown in Table 2, the mixing equation estimates that existing hyporheic anomaly-based hyporheic discharge (0.07 % of total mainstem discharge) provides a local cooling of the summer time maximum daily temperature in lower Clackamas River by 0.012 °C.

Table 2.2: Values entered into mixing calculation.

Parameter	Value	Source
$Q_m$	22.547 m <sup>3</sup> /s	$Q_c - Q_h$
$T_m$	19.20 °C	Mean temperature for August 13th, 2006
$Q_h$	0.153 m <sup>3</sup> /s	Sum of all temperature anomaly discharges
$T_h$	depends	$T_m$ - magnitude of cooling for each anomaly
$\Sigma(Q_h T_h)$	2.660	
$Q_c$	22.7 m <sup>3</sup> /s	USGS River Gauge at Estacada, Oregon
$T_c$	19.187 °C	$Q_m T_m + \Sigma(Q_h T_h) / Q_c$
<b>Cooling</b>	0.012 °C	$T_m - T_c$

## 2.5 DISCUSSION

We estimate that existing hyporheic flow in the Clackamas has a minimal impact on daily maximum temperature. This estimate is subject to three significant sources of uncertainty detailed below: the estimate of  $K$ ; the calculation of discharge; and unaccounted for hyporheic exchange.

First, determining  $K$  for each of the gravel bars with temperature anomalies is difficult. We assigned  $K$  values using data from our 3 intensively studied bars to all anomalies in the study reach based on whether a bar was new, older, or a combination of new and older deposits. We do not know if this approach over- or under-predicts  $K$  values, but overall temperature effects in the mainstem are very sensitive to assignment of  $K$  values. By way of sensitivity analysis, if all gravel bars are assigned the maximum measured value of  $K$  (Eagle Creek), the mixing model estimates an overall reduction in maximum daily temperatures in the summer of 2006 as 0.021 °C.

If all gravel bars are assigned the minimum measured value of  $K$  (Feldheimer), the mixing model estimates a reduction in maximum daily temperatures of  $7.14 \times 10^{-6} \text{ }^\circ\text{C}$ .

Secondly, we used a simple mixing equation to estimate the effect of hyporheic discharge on mainstem temperature. The steady state simplification assumes that the cooling over multiple anomalies is cumulative and neglects decay and phase effects due to travel time (i.e., temperature is treated conservatively). This model may overestimate the temperature effect. Our comparison with CE-QUAL-W2, which accounts for longitudinal heat loss/gain, demonstrates that if we added 40 Eagle Creek bars on the lower Clackamas by gravel augmentation and make the same calculation with the mixing model as outlined above, the mixing model overestimates the cooling effect by 50 %.

Finally, our study has focused on quantifying hyporheic exchange over summer 2006 on gravel bars that consistently demonstrated different temperatures from the mainstem, due to buffering and lagging of heat resulting from advection and conduction. We did not quantify the thermal effects of diffuse hyporheic discharge through gravel bars where we did not detect a temperature difference, nor did we attempt to assign cooling associated with the simple downwelling of water into gravel bars (where water is not exposed to solar radiation or ambient air temperature). Also, we did not take other hyporheic spatial scales into account, including flow through submerged gravel bedforms (e.g., bed roughness elements), meander necks or floodplains. Exclusion of these effects underestimates the total amount of hyporheic cooling.

Reconciling these sources of error, which point in different directions, is difficult. Obtaining more refined estimates of  $K$  and hyporheic anomaly discharge would require building additional groundwater models for many more gravel bars on the lower Clackamas. Additional field studies and modeling exercises would examine other spatial scales of hyporheic flow and the thermal benefit afforded by water simply being shielded from solar radiation as it downwells into gravel.

Even within the constraints imposed by the uncertainties in our study, however, we believe our estimate of cooling is not likely to change drastically. Unlike

smaller streams that may see several degrees of cooling from hyporheic buffering (Johnson, 2004), our results suggest that hyporheic exchange will cool larger rivers only a fraction of a degree. This is likely due to diminishing opportunities for hyporheic exchange as channel size increases (D'Angelo et al., 1993; Boulton et al., 1998). We found that in the Clackamas River, hyporheic discharge comprised only a fraction of mainstem summer discharge ( $\ll 1\%$ ). It is therefore difficult for hyporheic exchange to exert significant effect on stream temperature, because any hyporheic buffering present is diluted by large mainstem discharges.

Although hyporheic discharge may not have a large effect on overall river temperature in a large river, we found that it can effectively create localized patches of water that have different temperatures from the mainstem. These patches increase thermal heterogeneity within the river channel and can provide thermal refugia (up to 4 °C cooler) for aquatic species that are stressed by conditions in the mainstem channel (Fernald *et al.*, 2006 and Arscott *et al.*, 2001).

Similar to previous studies (e.g., Kasahara and Wondzell, 2003; Poole *et al.*, 2006), we found that channel-scale morphology controls hyporheic exchange in the Clackamas River, which in turn influences thermal heterogeneity (Arscott *et al.*, 2001; Fernald *et al.*, 2006). All anomalies were associated with gravel bars, with the largest discharges emerging from anomalies located downstream from bar heads. The largest number of anomalies was associated with bar channels, but these produced only modest hyporheic discharges.

In most cases, the link between channel morphology and hyporheic flow reflects morphologic control on the distribution and hydraulic properties of preferential flow paths in bars. Temperature anomalies were consistently located downstream from observed or inferred flow paths, which are assumed to feed subsurface channels. Although these geomorphic features usually comprise only a fraction of a gravel bar's area, they generally have higher  $K$  values than other parts of the same bar (Wondzell and Swanson, 1999; Fernald *et al.*, 2006). The bar channels and heads that had associated anomalies with the greatest hyporheic discharges had been reworked recently during recent high winter flows and presumably had fewer

finer than older and less reworked parts of the bar. These older bar surfaces tended to be well-vegetated and have likely accumulated fines for longer periods of time. Our slug tests also suggested that  $K$  values can vary dramatically between newer and older bar features.

Bar channels and bar heads also have hydraulic gradients greater than the longitudinal river gradient due to downstream hydraulic controls and backwater effects. The slope transition at the head of the bar in effect acts as a broad-crested weir, slowing upstream flows. The water that does infiltrate the head of the bar will generally follow a shorter flow path directly through the bar; this will be the steepest gradient across the bar. Together, higher  $K$  and steeper hydraulic gradient create preferential flow paths, concentrating hyporheic flow. At Eagle Creek, we estimate that 76 % of the total hyporheic flow in the bar was focused along a preferential flow path, giving rise to the downstream temperature anomaly.

On some bars, we found recently reworked bar channels and bar heads that appeared ideal candidates for preferential hyporheic flow, but no temperature anomaly was found. We speculate that in these cases hyporheic flow was present but in phase with mainstem temperature. For a maximum temperature difference to occur, the travel time across the bar must be  $24(N-1/2)$  h where  $N$  is a positive integer. A minimum temperature difference occurs, regardless of hyporheic discharge, at  $24 N$  h. This means that certain bar sizes and  $K$  values can produce significant hyporheic flow but have no appreciable effect on the river temperature.

This study reveals the close coupling among channel morphology, hyporheic flow, and thermal heterogeneity. The relationship among these processes will be affected by channel dynamics in both natural rivers and those located downstream from dams or other anthropogenic influences. In the case of the Clackamas, long-term reduction in sediment supply and transport due to upstream dams has resulted in at least some reaches with limited gravel and skeletal coarse bars. The proposed artificial introduction of gravel to the river below the lowest dam has the potential to increase sediment transport, thereby affecting rates of bar construction, reworking, and channel migration. By the results presented here, there should be at least some local

effects on stream temperatures due to this increased channel activity. It remains to be seen what the magnitude and location of this effect is likely to be, but the opportunity to examine the relationships among channel morphology, stream temperature and hyporheic flow represents an ideal field experiment.

## 2.6 CONCLUSIONS

Our field investigation identified 40 temperature anomalies over a 24-km reach on the lower Clackamas River, a low gradient, gravel-bed river. Temperature anomalies are the result of hyporheic exchange deviating from mainstem temperatures throughout the day, largely due to buffering and lagging of advected heat. The occurrence of temperature anomalies depends strongly on the presence of bar morphology. More specifically, hyporheic exchange that directly influences river temperature is associated with geomorphic features on bars like bar channels and bar heads that exhibit higher gradients (versus river gradient) and higher hydraulic conductivities. The flow emerging from these anomalies is largely controlled by the hydraulic conductivity of the sediments, meaning that gravel bars that have recently formed or been reworked will have greater hyporheic discharges.

A simple mixing model demonstrates that the overall cooling effect associated with these temperature anomalies is small ( $0.012^{\circ}\text{C}$ ) due to the fact that hyporheic discharge emerging from these anomalies is only a small fraction ( $< 0.07\%$ ) of mainstem discharge in a large river. However, these patches of cooler water can benefit cold water species such as salmon, providing local habitat and refugia from warmer mainstem temperatures. With emerging interest in river restoration and incorporating natural river processes into restoration projects (Boulton, 2007), the creation or enhancement of cool patches resulting from hyporheic exchange is a viable method that could be used to offset the harmful effects of thermal degradation.

### 3 CONCLUSIONS

The motivation behind this project was to determine the sensitivity of a large, gravel-bed river to the temperature buffering effects of hyporheic exchange and postulate how gravel augmentation could cool a river by increasing hyporheic exchange.

Temperature surveys and TIR demonstrated that significant thermal heterogeneity exists on the lower Clackamas River, especially with regard to the gravel bar population. A large driver of this heterogeneity is due to patches of hyporheic water that demonstrate out-of-phase temperatures with the mainstem, referred to as temperature anomalies in this study. These anomalies are intimately connected with geomorphic features on gravel bars (bar channels and heads) that focus flow along preferential pathways. This anomaly network is reset each year with high flows, where flow path lengths, hydraulic conductivities, and hydraulic gradients of gravel bars may change as gravel is reworked.

The hyporheic discharges emerging from anomalies result from zones of high hydraulic conductivity, which occurs in gravel that has been recently reworked. However, the cumulative anomaly discharge on the lower Clackamas, in comparison with the large mainstem discharge, is small. Estimates of river cooling reflect this, composing only a fraction of a degree rather than several degrees observed in smaller rivers (Johnson, 2004). Our estimate does not include other potential thermal benefits governed by hyporheic exchange, including buffering effects from other hyporheic pathways (e.g. meander necks or submerged gravel), and thermal shielding resulting from water downwelling into the subsurface and not being exposed to solar radiation. Further studies would have to be developed to investigate these other effects. However, these other effects are not likely to drastically alter the amount of river cooling.

Adding gravel to a river will form new bars or enhance older bars, which will increase the amount of hyporheic exchange occurring throughout the river. This can lead to the development of new temperature anomalies that buffer river temperature. Still, this will not likely significantly affect overall river temperature (as modeled by

CE-QUAL-W2 and our mixing equation) but will provide localized fish habitat and refugia.



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**APPENDICES**

**APPENDIX A**

**AERIAL ANALYSIS OF LOWER CLACKAMAS RIVER BAR POPULATION**



### **A.1 Qualitative and semi-quantitative geomorphic description of lower Clackamas River gravel bar population**

We used aerial photos from summer 2005 and summer 2006 to help describe the lower Clackamas River gravel bar population. Lengths, widths and bar areas were calculated using measuring tools within ArcGIS. Field reconnaissance provided further insights on bar stability, including recency of gravel reworking and vegetation.

Table A.1 lists the parameters for the gravel bars.

Table A.1: Location and brief description of gravel bars on lower Clackamas River

RKM	Northing (ft) <sup>1</sup>	Easting (ft)	Bar Type <sup>2</sup>	Longitudinal Length (m)	Average Width (m)	Maximum Width (m)	Area (m <sup>2</sup> )	Vegetation	Reworked over 2005/2006?	Percent of Bar Network
36.4	601288	7724245	L	146	17	35	4168	mature	N	0.39
36.1	601254	7725196	L	162	19	29	3357	mature	N	0.31
35.8	600900	7723174	L	314	44	69	13320	zonation (immature to mature)	N	1.23
35.6	600808	7722913	L	323	71	87	19918	mature	N	1.84
35.2	599860	7721986	MC	186	26	31	3124	zonation	N	0.29
35.0	600588	7721070	MC	113	30	43	3028	zonation	N	0.28
34.7	601811	7721180	MC	456	94	136	41452	zonation	N	3.83
35.0	601017	7721399	L	207	41	63	8881	mature	N	0.82
34.3	602478	7721906	PB	271	33	56	9573	immature/none	N	0.89
33.8	604135	7722922	MC	211	44	60	9089	mature	N	0.84
33.5	604198	7722087	L	510	137	197	71396	mature	N	6.60
33.3	604388	7721397	MC	69	15	21	1045	zonation	N	0.10
33.3	604190	7721054	MC	32	14	22	485	immature/none	N	0.04
33.3	604932	7721631	MC	63	16	16	894	none	N	0.08
33.3	604808	7721361	MC	36	14	14	382	immature	N	0.04
33.1	604574	7721105	MC	547	105	146	45094	immature/mature	N	4.17
33.0	604744	7720297	MC	77	26	31	1715	zonation	N	0.16
32.8	605224	7720208	MC	166	55	56	8183	mature	N	0.76
32.6	605317	7719454	MC	784	77	125	60290	mature	N	5.58
32.5	605209	7719004	L	304	35	43	8759	mature	N	0.81
32.4	606034	7718909	L	198	37	37	7516	immature	N	0.70
32.1	605912	7717799	MC	315	65	81	16782	immature/mature	N	1.55
31.9	606346	7717301	PB	237	56	62	9259	immature	N	0.86
31.9	606080	7717152	L	151	19	24	3065	mature	N	0.28

Table A.1: Location and brief description of gravel bars on lower Clackamas River

RKM	Northing (ft) <sup>1</sup>	Easting (ft)	Bar Type <sup>2</sup>	Longitudinal Length (m)	Average Width (m)	Maximum Width (m)	Area (m <sup>2</sup> )	Vegetation	Reworked over 2005/2006?	Percent of Bar Network
31.6	607110	7716775	PB	287	76	76	11114	immature/mature	N	1.03
31.1	608169	7717663	L	265	27	52	9100	immature/mature	N	0.84
30.6	610108	7718182	L	294	27	53	9401	immature/mature	N	0.87
29.7	612816	7718130	L	326	69	85	21810	immature/mature	N	2.02
29.3	613634	7717603	MC	279	51	54	12589	immature/none	N	1.16
29.1	613973	7717170	L	245	62	139	18102	zonation	Y	1.67
28.9	614651	7716330	PB	77	49	49	8125	zonation	Y	0.75
28.7	615137	7716500	L	120	32	35	3967	immature	Y	0.37
28.4	616099	7716864	L	155	23	29	3167	zonation	N	0.29
28.0	616567	7717105	L	133	19	19	2298	mature	N	0.21
27.4	618107	7717641	MC	294	104	139	24217	zonation/none	N	2.24
27.2	618559	7717780	L	126	27	32	3122	none	Y	0.29
27.2	618674	7717484	MC	208	47	67	9247	immature/none	N	0.86
26.5	620328	7718141	L	213	62	82	11259	zonation	Y	1.04
26.4	620945	7718102	MC	534	183	234	61106	mature/none	Y	5.65
26.1	621420	7717932	PB	217	60	60	12448	zonation	Y	1.15
26.4	620667	7718281	MC	86	22	34	2282	immature/none	Y	0.21
26.0	621799	7718134	MC	70	40	63	3908	none	Y	0.36
25.7	623891	7716574	L	260	17	29	6800	immature	N	0.63
24.9	624536	7715811	L	435	32	41	11407	immature	N	1.05
24.5	625483	7714889	L	215	29	29	7110	none	Y	0.66
23.7	627385	7714015	L	481	169	206	65015	immature/mature	Y	6.01
24.2	626724	7714372	MC	283	64	78	12997	zonation	N	1.20
24.1	626774	7713852	L	76	11	14	1593	none	Y	0.15
24.1	626785	7713554	L	73	14	19	1304	none	Y	0.12

**Table A.1: Location and brief description of gravel bars on lower Clackamas River**

RKM	Northing (ft) <sup>1</sup>	Easting (ft)	Bar Type <sup>2</sup>	Longitudinal Length (m)	Average Width (m)	Maximum Width (m)	Area (m <sup>2</sup> )	Vegetation	Reworked over 2005/2006?	Percent of Bar Network
22.9	628167	7713893	L	70	29	29	1728	none	Y	0.16
22.3	629146	7713496	MC	253	70	102	17552	immature/none	N	1.62
21.9	629353	7712093	L	545	38	73	23148	immature/none	N	2.14
21.5	630326	7711139	L	554	33	49	1649	zonation	N	0.15
21.2	630807	7710608	L	216	36	37	5967	zonation	N	0.55
20.6	632425	7709709	MC	398	76	97	26906	zonation	N	2.49
20.6	632281	7709246	L	369	81	141	33873	zonation	N	3.13
20.5	632879	7709420	MC	59	34	36	1834	immature/none	Y	0.17
20.1	633208	7708721	MC	407	124	142	42214	zonation/none	Y	3.90
20.0	633747	7708382	MC	126	21	32	3204	immature/none	N	0.30
19.9	633782	7708037	PB	244	77	77	11625	zonation	N	1.08
20.2	632831	7708596	MC	196	46	48	7801	immature/none	Y	0.72
20.2	632935	7708710	MC	20	11	11	240	immature/none	Y	0.02
20.2	632931	7708781	MC	25	13	13	200	immature/none	Y	0.02
19.6	633839	7707092	L	169	14	16	2790	none	Y	0.26
19.1	633866	7705329	PB	318	137	156	35351	zonation	N	3.27
18.7	633285	7705151	L	178	26	58	6499	immature/mature	N	0.60
18.9	632935	7704733	L	28	14	16	621	none	Y	0.06
18.0	631409	7702850	MC	101	54	54	4655	zonation	Y	0.43
18.5	632454	7704302	L	193	23	24	3476	zonation	N	0.32
17.6	632019	7701353	L	127	54	93	23657	immature/mature	N	2.19
17.7	632024	7701964	L	140	10	12	2449	zonation	N	0.23
17.9	631657	7702595	PB	140	42	54	4163	zonation	N	0.39
16.7	632456	7698622	L	283	30	37	7609	immature	N	0.70
15.7	632818	7696007	PB	311	38	80	12767	none	N	1.18

**Table A.1: Location and brief description of gravel bars on lower Clackamas River**

RKM	Northing (ft) <sup>1</sup>	Eastings (ft)	Bar Type <sup>2</sup>	Longitudinal Length (m)	Average Width (m)	Maximum Width (m)	Area (m <sup>2</sup> )	Vegetation	Reworked over 2005/2006?	Percent of Bar Network
15.8	632592	7695733	MC	44	18	25	742	immature	N	0.07
15.0	634555	7695692	MC	700	45	83	36737	mature	Y	3.40
14.8	635550	7695072	PB	247	17	25	4109	zonation	N	0.38
14.6	635910	7694702	MC	27	51	51	1907	immature/none	Y	0.18
14.0	635782	7692740	MC	326	178	274	52282	zonation	Y	4.84
13.8	635310	7692126	PB	58	67	98	5237	none	Y	0.48
13.4	635600	7690981	MC	228	54	73	11294	immature/mature	N	1.04
13.2	635943	7690270	L	38	93	74	2260	none	Y	0.21
13.5	635552	7690806	MC	9	6	6	76	immature	N	0.01
13.3	635887	7690611	MC	13	26	32	411	none	Y	0.04

<sup>1</sup> Northings and Eastings are in NAD83 Oregon North State Plane Projection.

<sup>2</sup> MC = mid-channel; L = lateral; PB = point bar

**APPENDIX B**  
**SURFACE AND SUBSURFACE PEBBLE COUNT DATA**

### **B.1 Pebble Count Procedure**

Pebble counts were conducted using a method similar to Wolman (1954). Transects were laid out across gravel bars (ranging from 30 to 100 m), and pebbles were randomly picked along regular intervals of that transect. Subsurface pebble counts were conducted by throwing a Frisbee 10 times randomly along the transect, removing the upper layer of pebbles, and counting the first 10 pebbles touched.

The fine fraction ( $< 1$  mm) was qualitatively described (coarse sand/fine sand/silt/clay), and when entered into results, assigned a grain size according to the Udden-Wentworth scale (Wentworth, 1922). There were no attempts to further quantify these smaller grains.

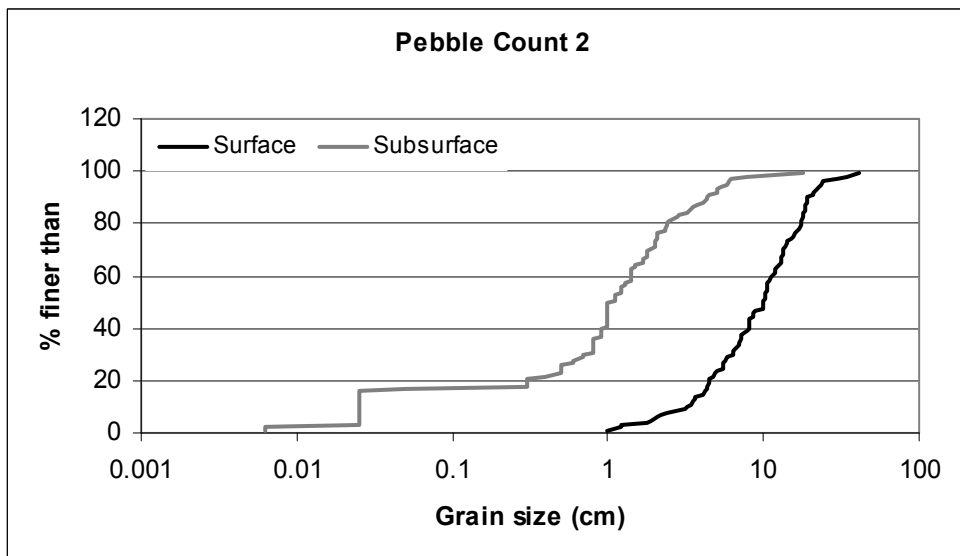
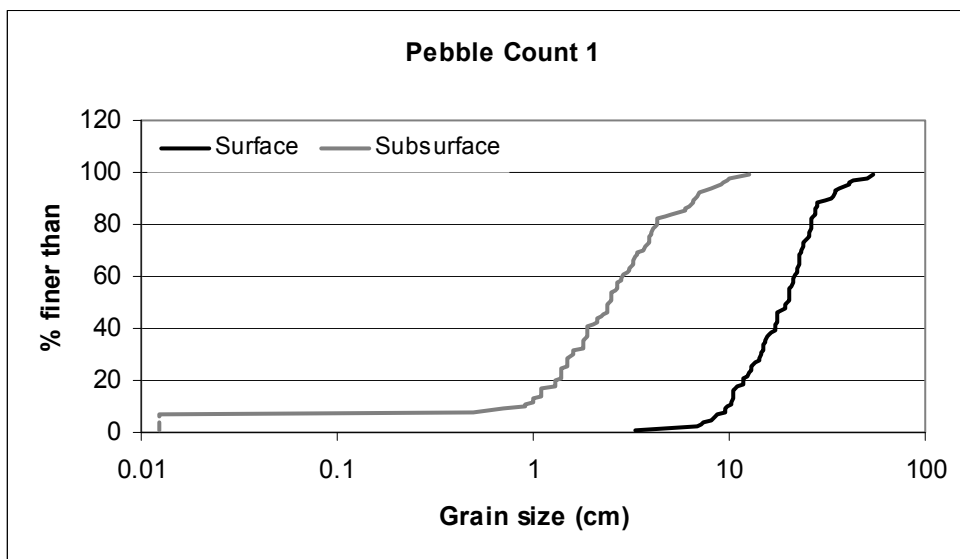
Table B.1 shows the locations where pebble counts were conducted.

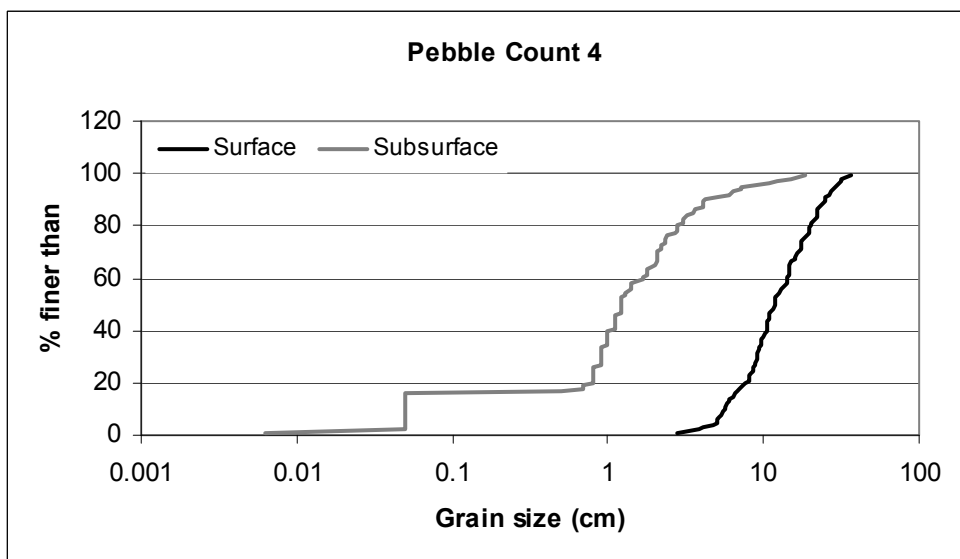
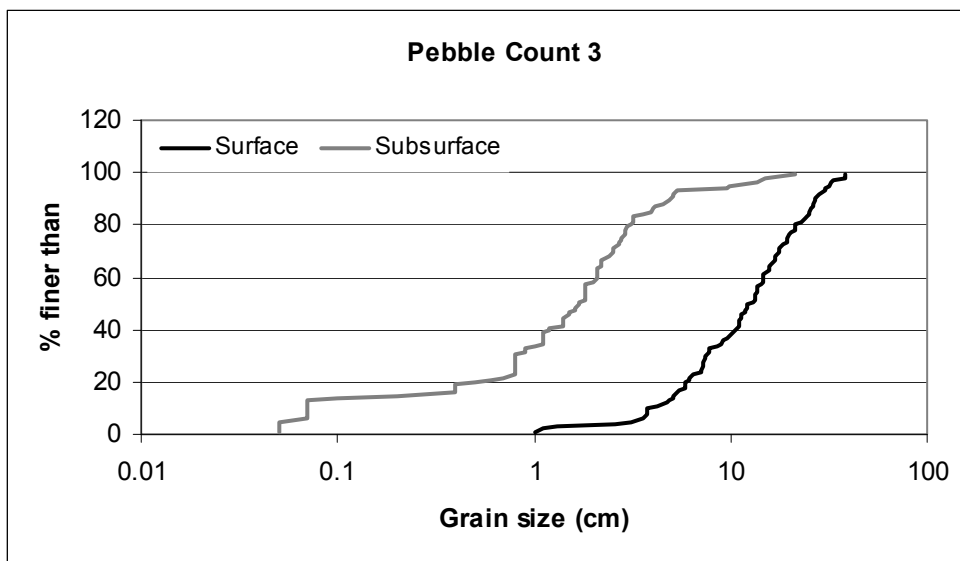
Table B.1 Pebble Count Data

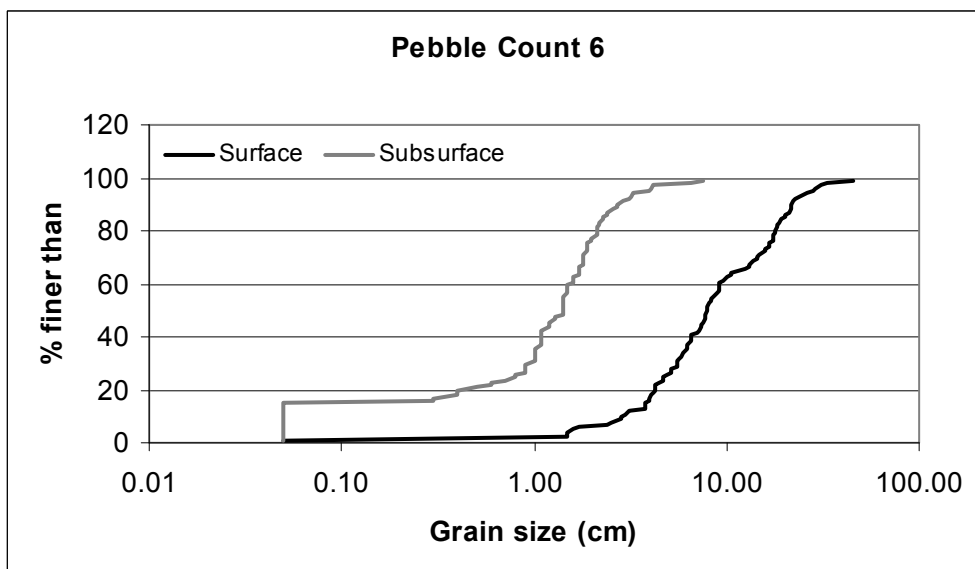
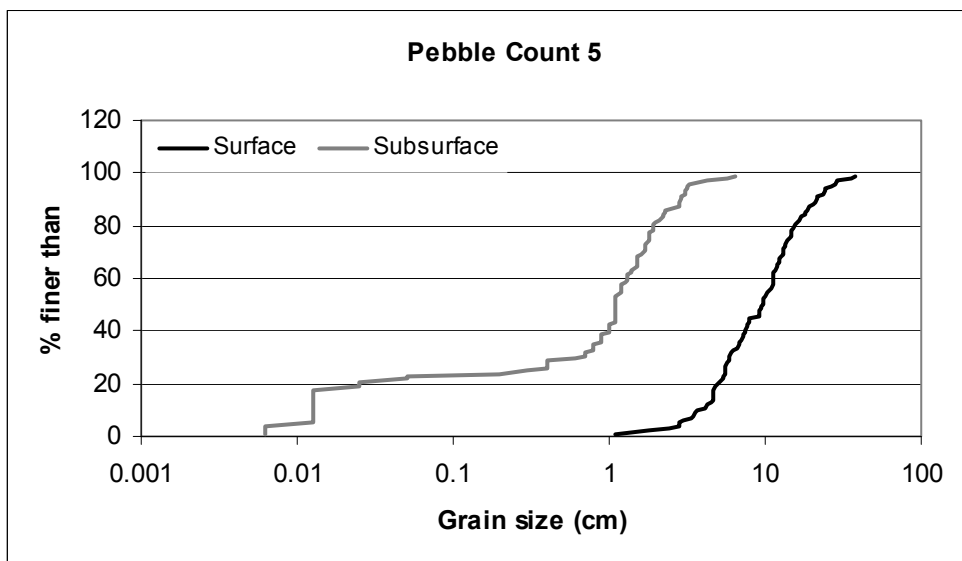
Pebble Count Number	Date	RKM	Northing (ft)	Easting (ft) <sup>1</sup>	Transect Length (m)	D50 (cm)	D50sub (cm)	Notes
1	7/21/2006	34.6	602063	7721618	66	10.0	1.0	Across bar tail
2	7/21/2006	34.6	601946	7721388	66	19.5	2.4	Down cross bar channel
3	7/21/2006	34.5	602339	7721831	66	12.2	1.7	Across bar head
4	7/21/2006	34.4	602496	7721907	66	11.8	1.2	Remnant channel
5	7/21/2006	32.1	605931	7717896	76	9.5	1.1	Unvegetated channel
6	7/18/2006	27.3	618028	7717713	87	4.8	0.8	Down cross bar channel
7	7/24/2006	27.5	617692	7717439	66	13.9	1.6	Across bar tail
8	7/18/2006	29.5	613191	7717806	35	7.9	1.4	Tail of back bar channel
9	7/18/2006	29.7	612465	7718101	33	10.4	1.1	Head of back bar channel
10	8/1/2006	29.7	612771	7717990	66	9.4	1.2	Middle of back bar channel
11	7/24/2006	27.1	618537	7717397	40	10.4	1.2	Across bar between hf and pool
12	7/24/2006	26.6	620392	7718132	73	5.9	0.9	Along new surface of gravel
13	7/24/2006	26.5	620632	7718374	66	7.9	1.4	Along bar edge
14	7/12/2006	26.1	621571	7717976	33	7.8	4.8	Small bar near HF channel
15	7/12/2006	26.2	621353	7717810	33	3.7	2.3	Head of bar
16	7/12/2006	26.1	621451	7717892	33	3.7	2.8	Mid-bar
17	7/12/2006	26.0	622021	7717955	33	3.5	2.8	Bar tail
18	7/26/2006	24.1	626700	7714233	2 16-m	5.9	1.5	Near HF
19	7/19/2006	20.8	631861	7710091	33	6.1	1.1	Across bar head
20	7/19/2006	20.5	632637	7709701	33	4.1	1.1	Near HF
21	7/17/2006	20.5	632795	7709414	66	6.9	1.6	Along unvegetated gravel at bar tail
22	7/19/2006	20.3	632990	7709133	100	7.2	0.7	Across bar head
23	7/19/2006	20.0	633371	7708339	66	7.6	1.3	Across new gravel exposure
24	7/19/2006	20.2	632836	7708680	47	6.8	2.2	Across bar head
25	7/17/2006	19.9	633478	7708129	33	7.0	1.0	Across point bar
26	7/25/2006	14.0	635900	7692993	100	4.3	1.1	Across interior
27	8/9/2006	13.8	635868	7692448	100	6.8	1.1	Along small finger of gravel

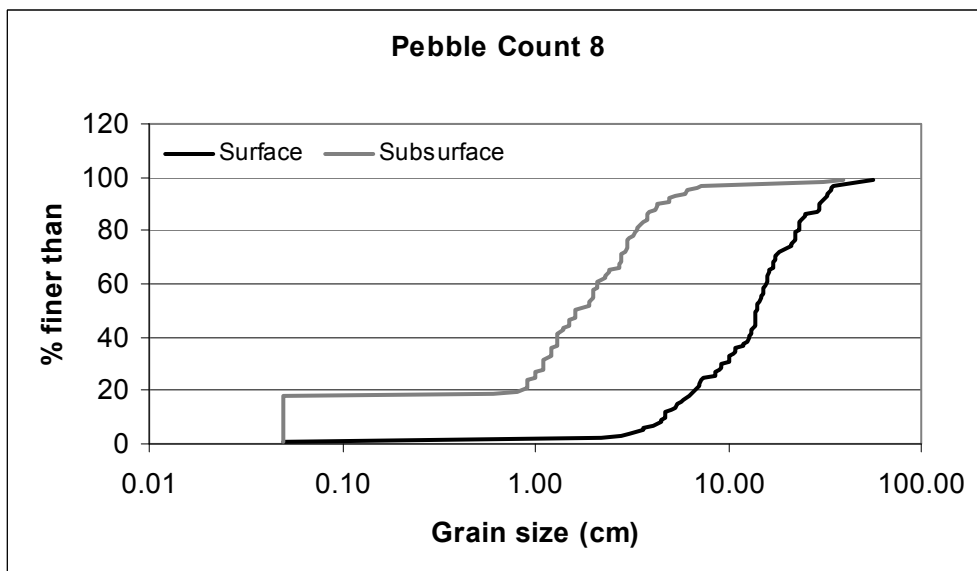
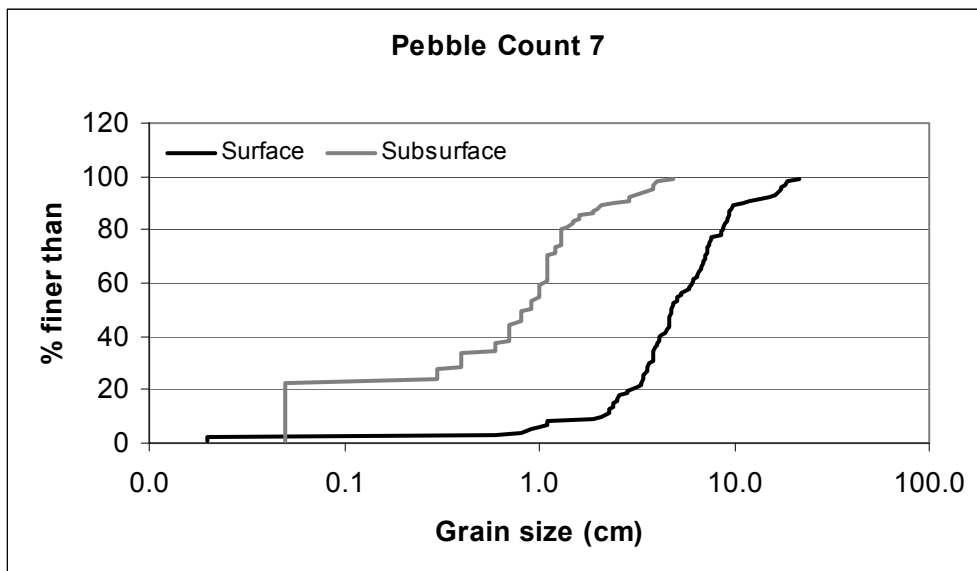
<sup>1</sup> Northings and Eastings are in NAD83 Oregon North State Plane Projection.

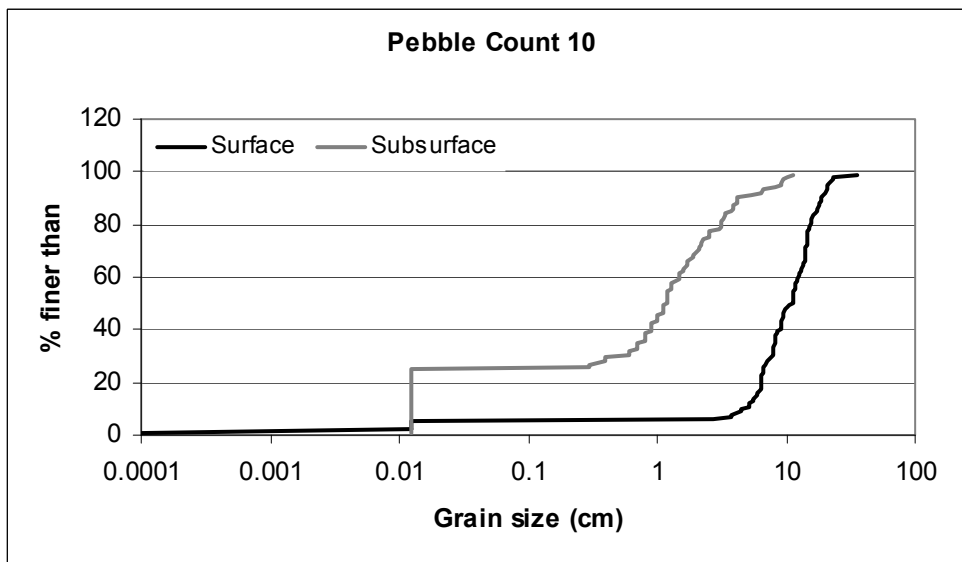
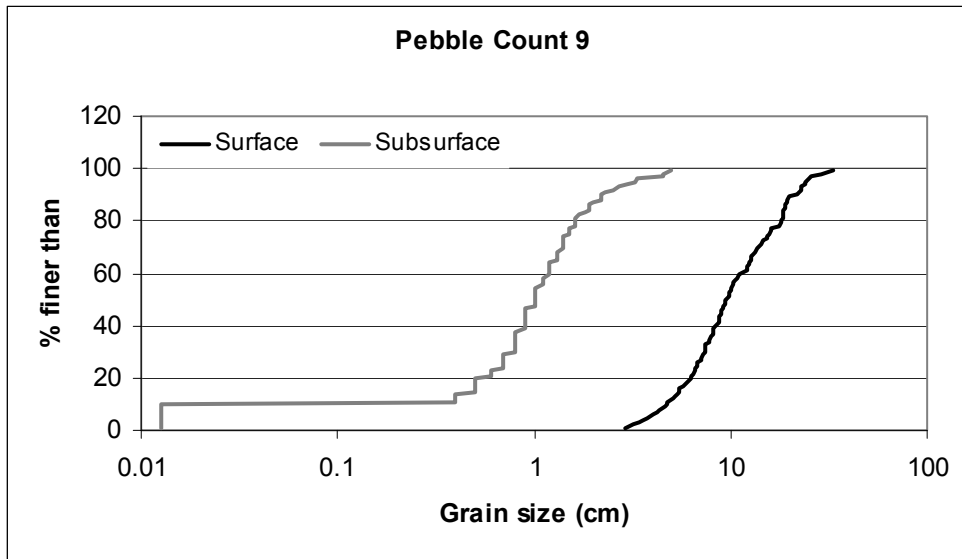


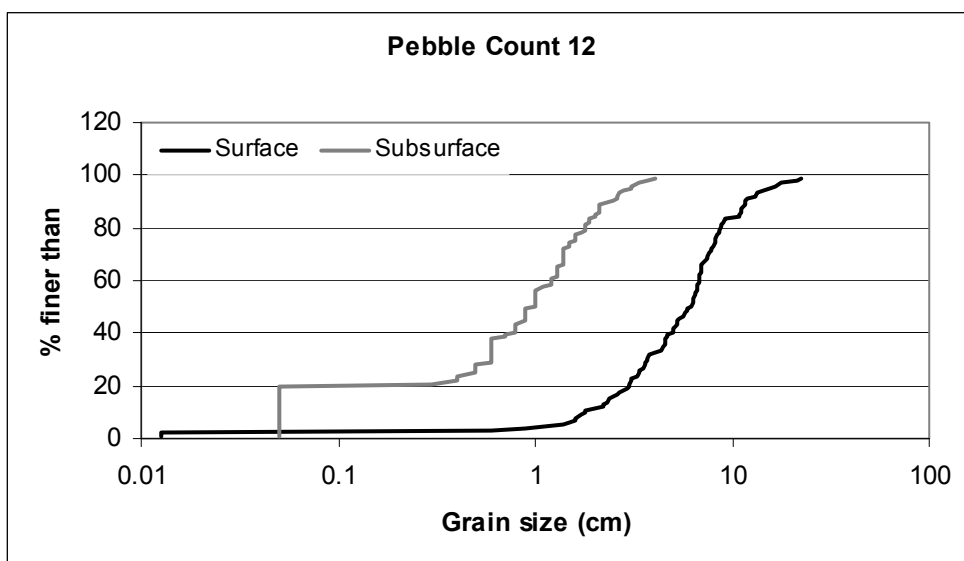
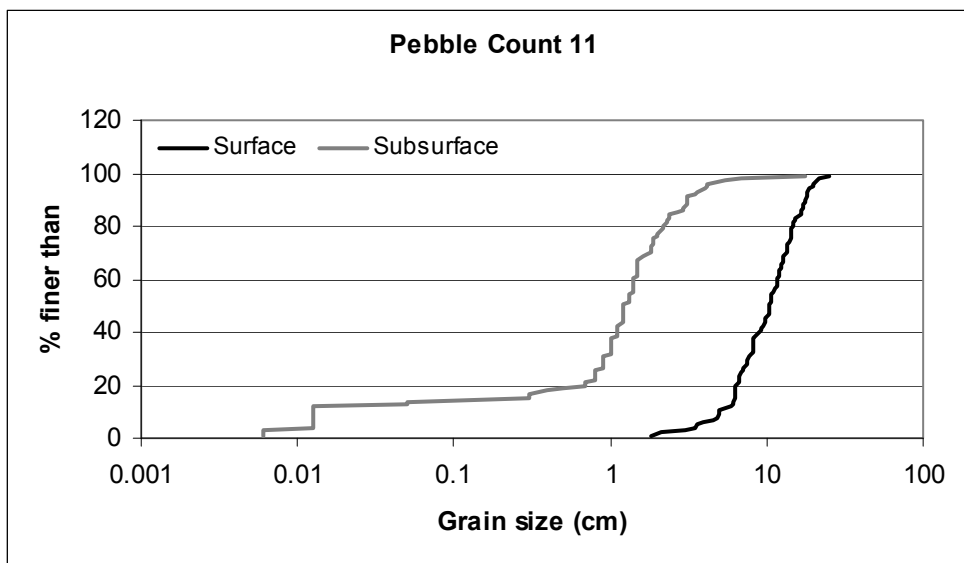


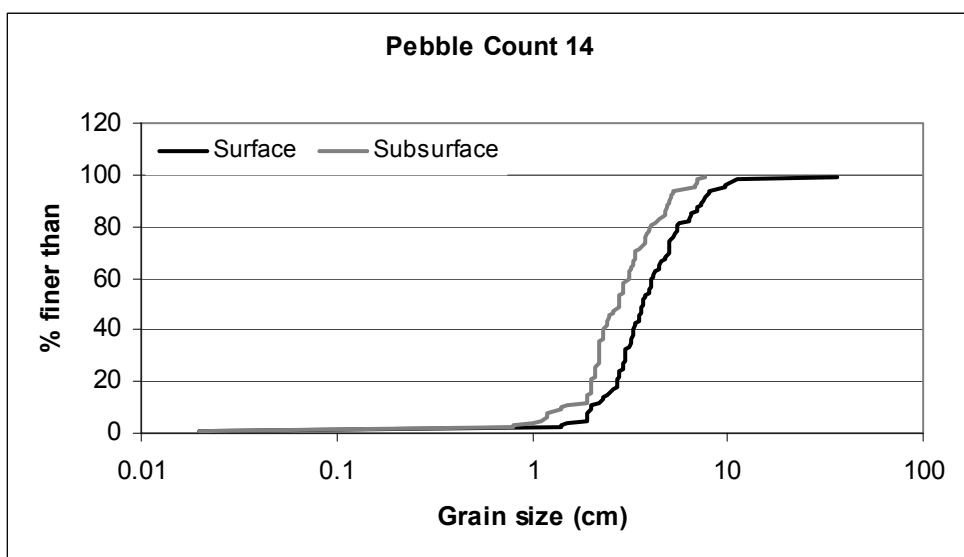
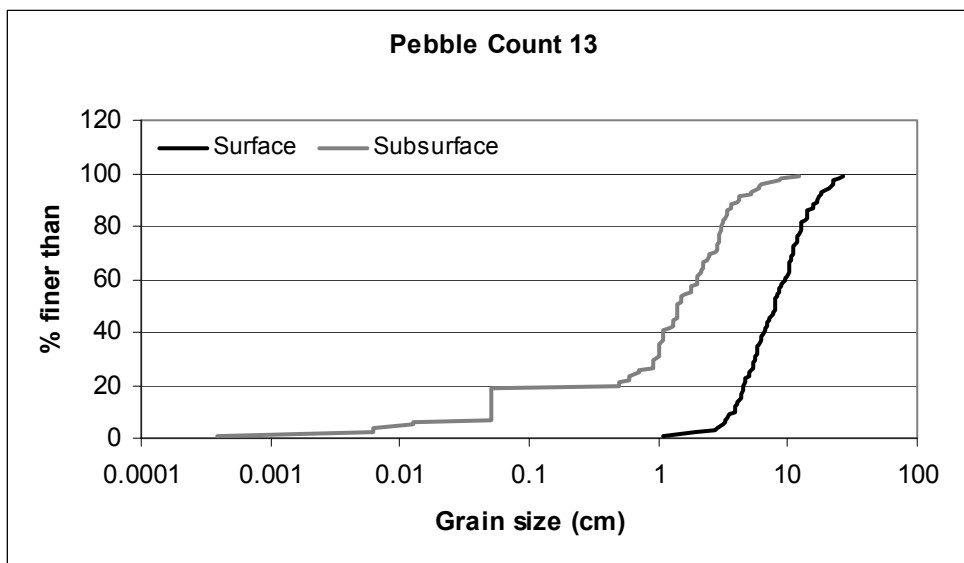


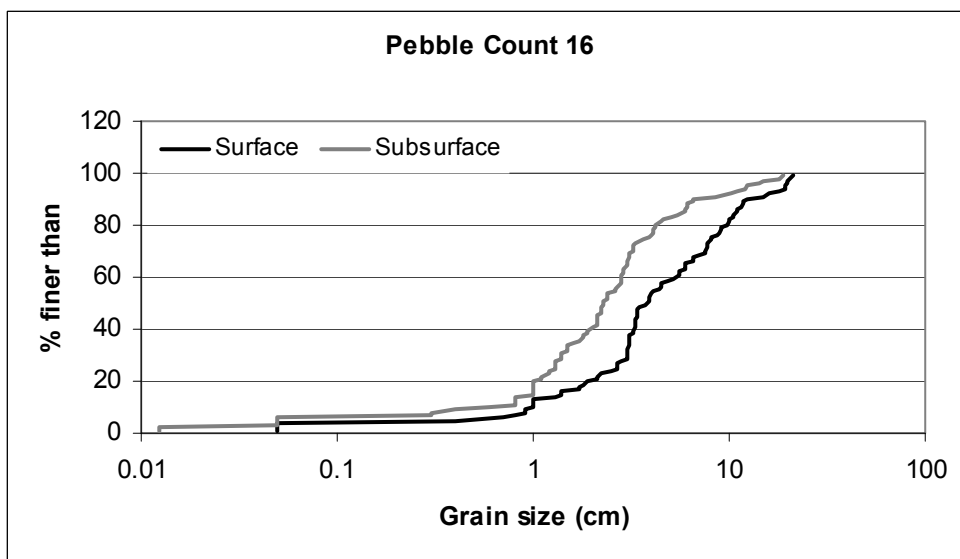
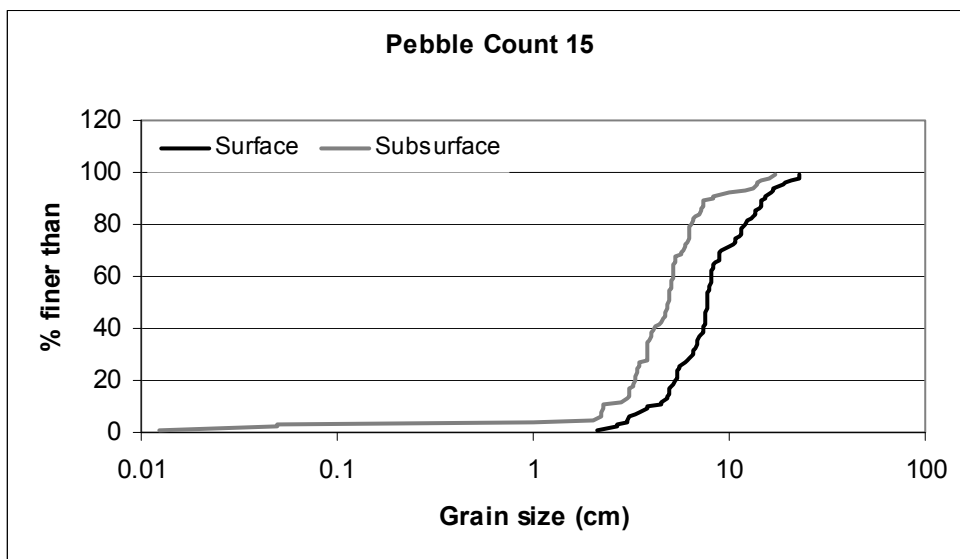




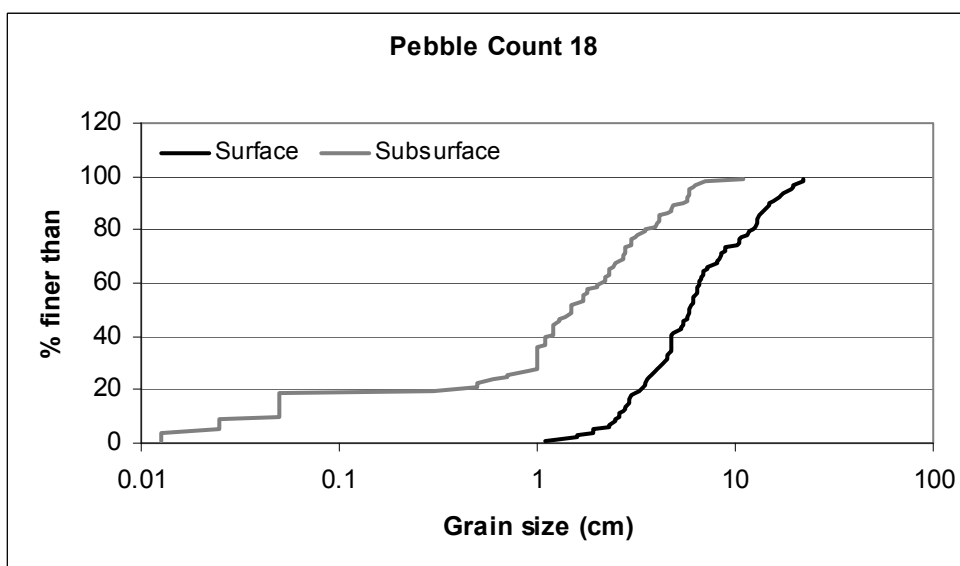
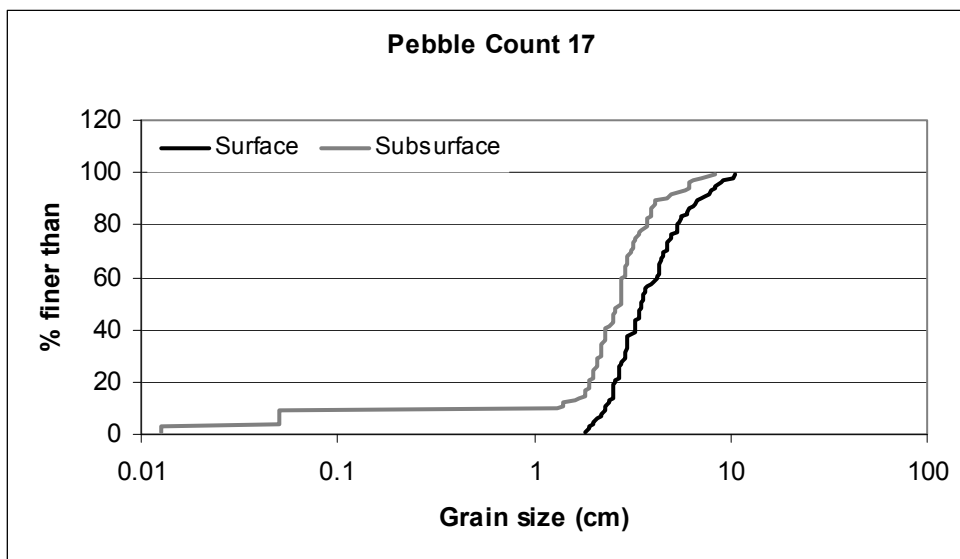


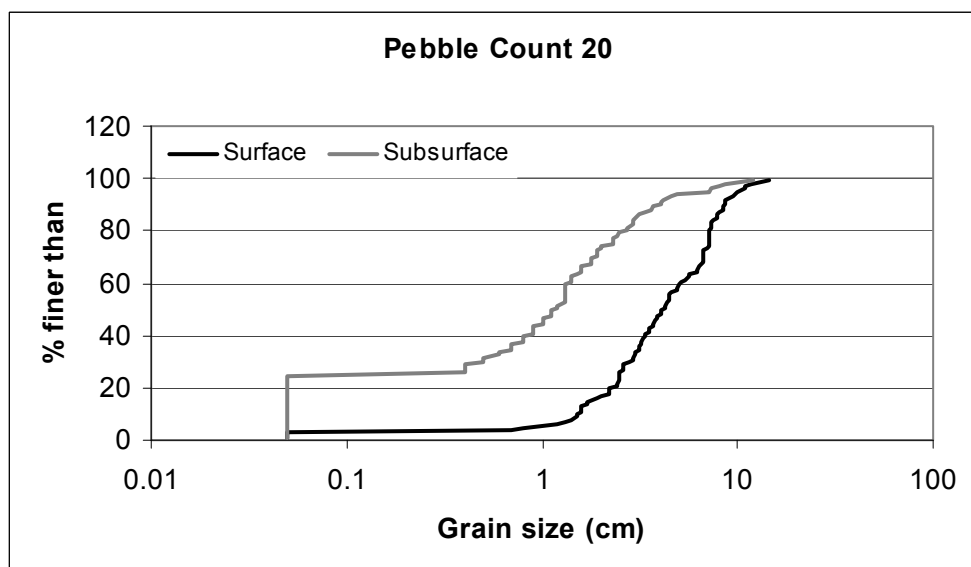
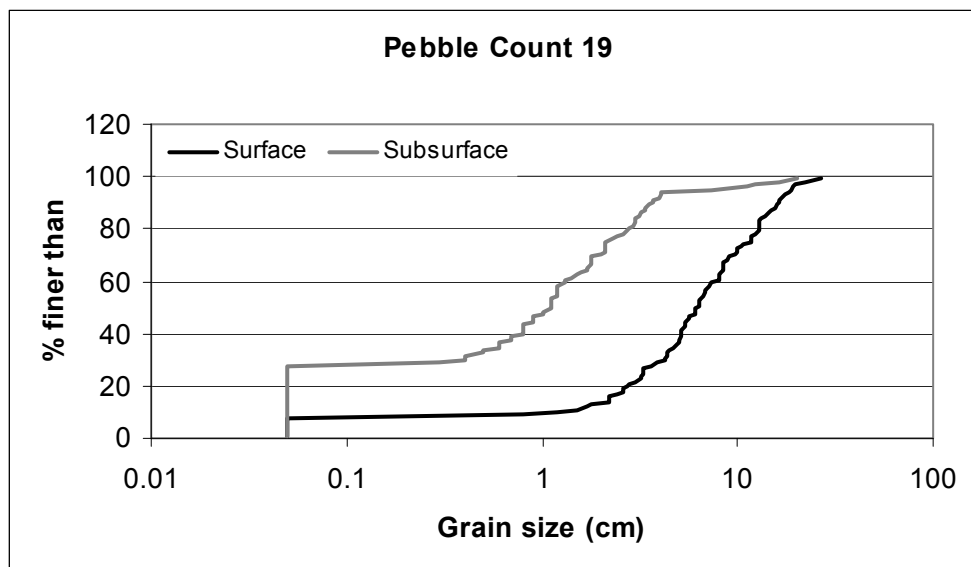


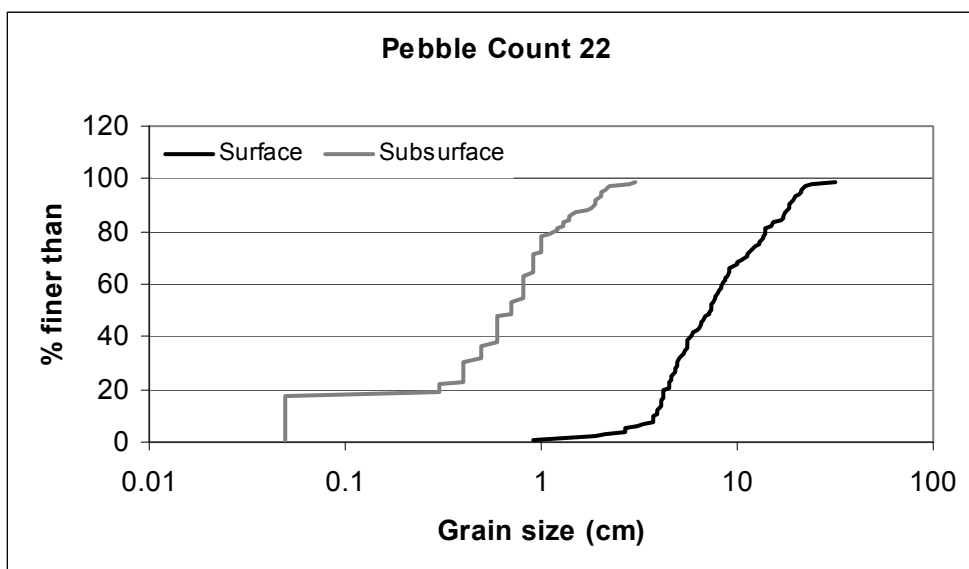
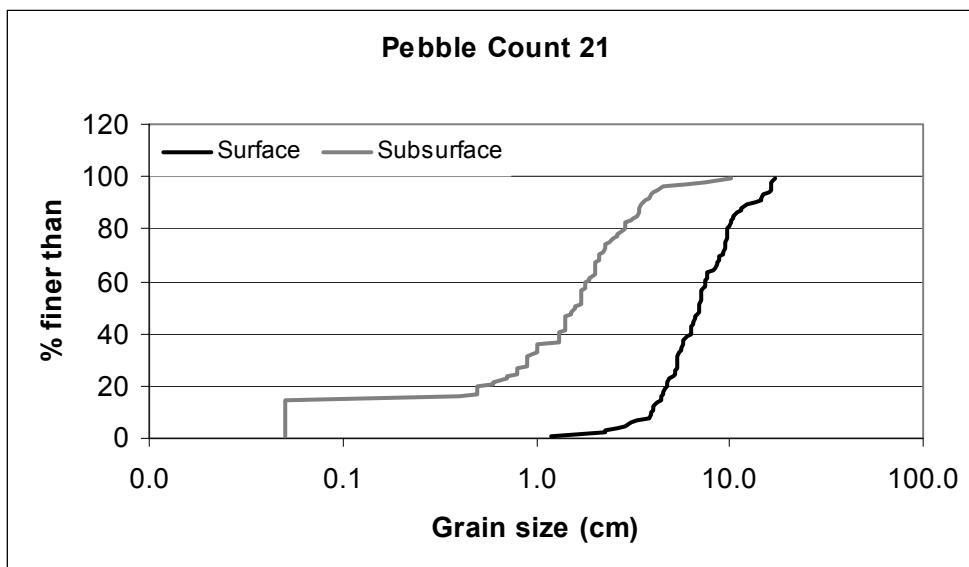


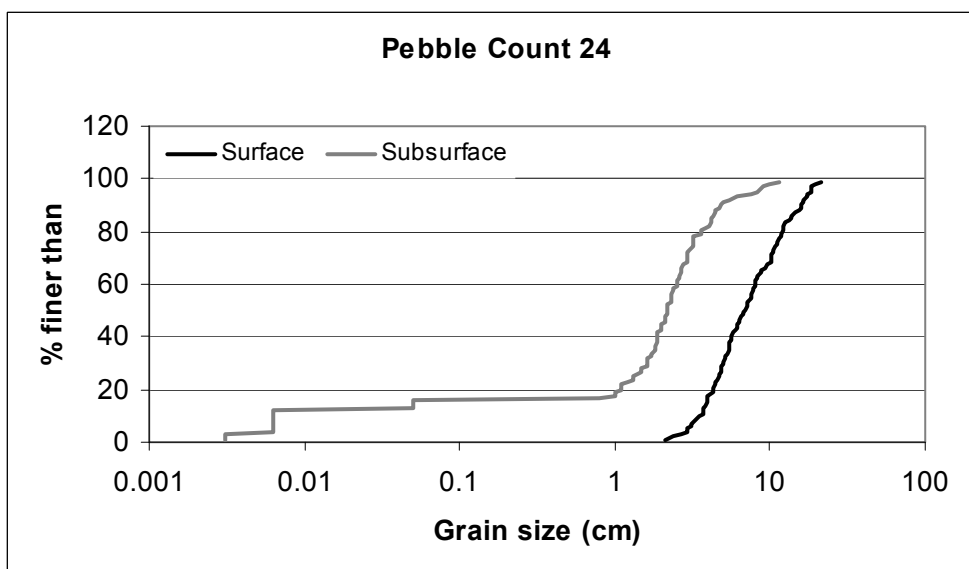
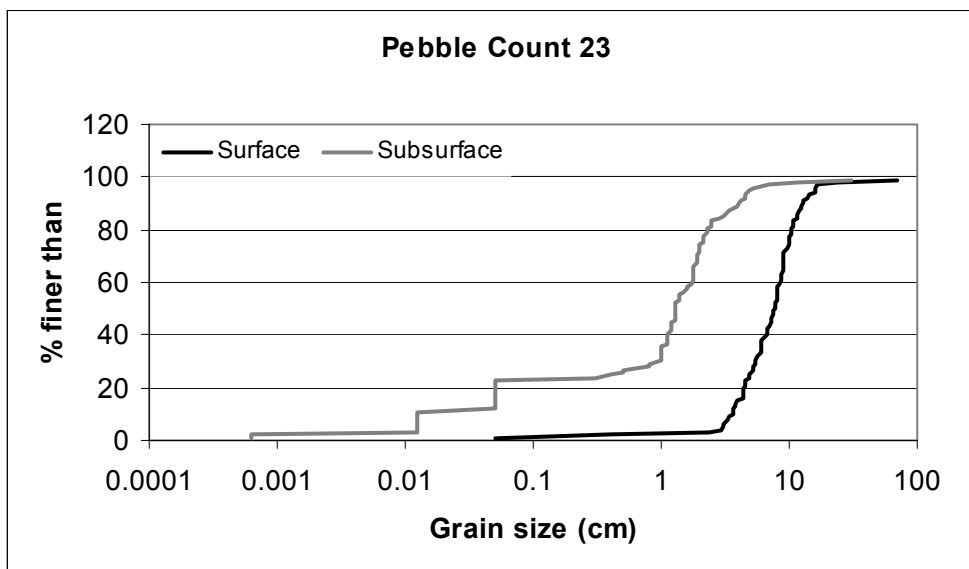


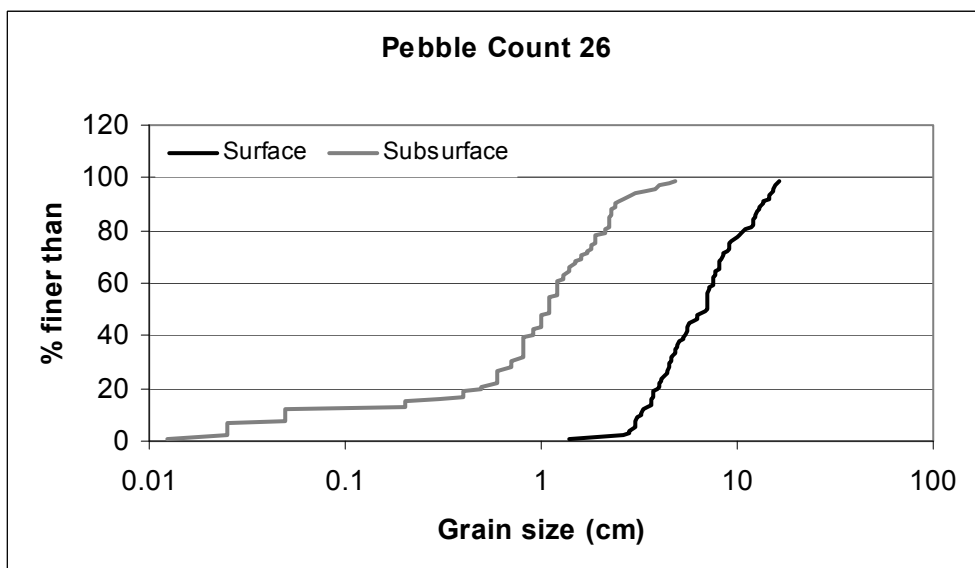
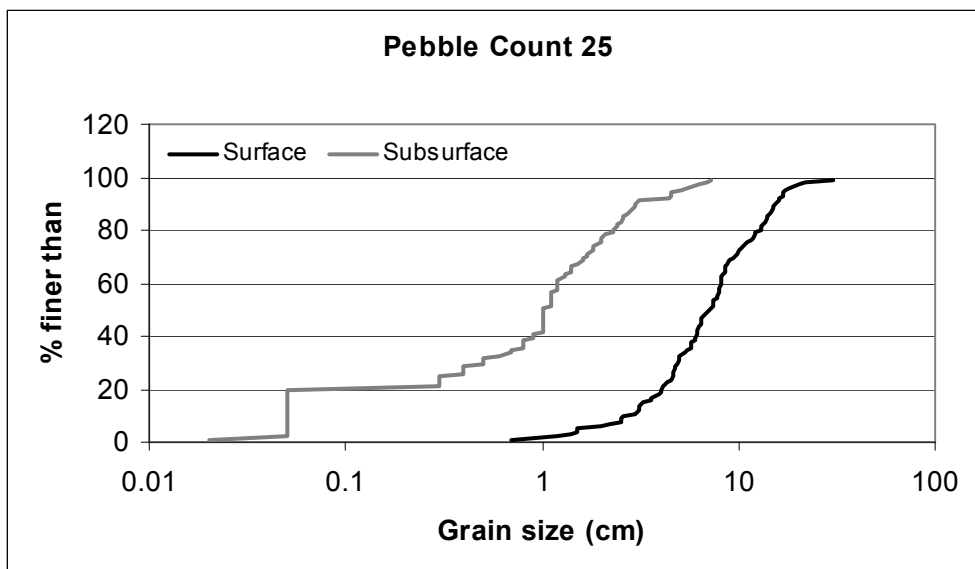


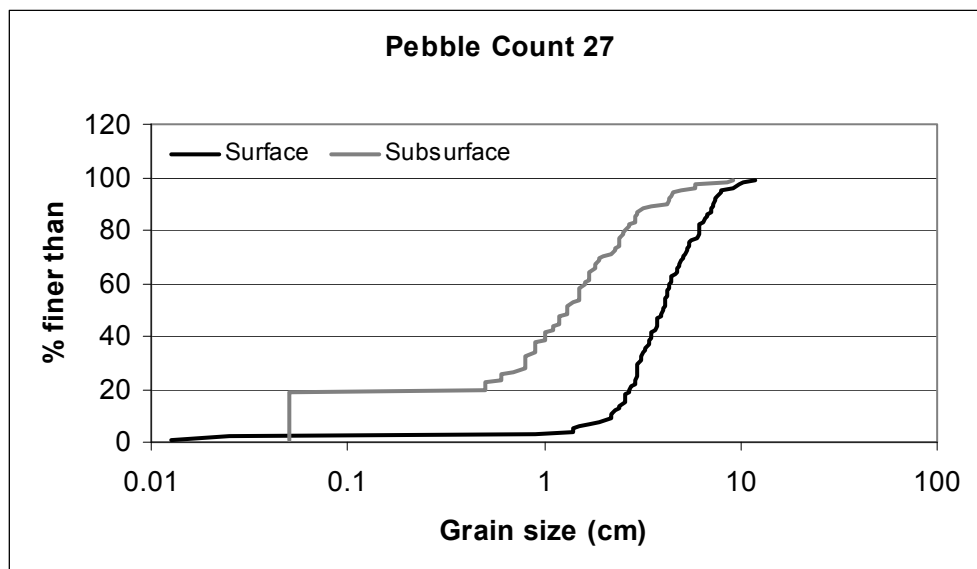












**APPENDIX C**

**LOCATION AND DESCRIPTION OF TEMPERATURE ANOMALIES**

**Table C.1: Location and brief description of temperature anomalies**

No.	RKM	Northing (ft) <sup>1</sup>	Easting (ft)	Type of Bar <sup>2</sup>	Field/TIR	Geomorphic feature	Bar recently reworked?	Conductivity (μS/cm)	Ave. ΔT (°C)	Ave. gradient	Ave. Width (m)	Ave. Depth (m)
1	34.6	602111.42	7721596.65	MC	Field	Bar Head (Ramp)	N	55-60	0.2	0.005	5	2.5
2	34.6	602170.76	7721363.09	MC	Field	BC: Cross Bar	N	55-60	1.4	0.015	3	2
3	34.6	602177.07	7721298.70	MC	Field	GW seep	N	55-60	4.8	0.015	1	1.5
4	34.3	602906.79	7722215.27	L	Field	GW seep	N	81.7	2.3	0.0057	1	0.05
5	33.5	603982.42	7722191.28	L	Both	BC: Back Bar/GW seep	N	-	0.7	0.005	15	1.5
6	33.1	604548.02	7720683.87	MC	Field	BC: Cross Bar	N	-	2.3	0.007	3	1
7	32.8	605196.93	7720590.45	MC	TIR	GW seep	N	-	3	--	Pool	2
8	32.5	605193.15	7718937.86	L	Field	BC: Back Bar/GW seep	N	80-120s	2.5	0.005	81	1
9	30.6	610165.10	7718132.26	L	Both	BC: Back Bar/GW seep	N	55 -	2.3	0.008	22	1
10	29.7	613291.98	7717772.59	L	Field	BC: Back Bar/GW seep	N	55-60	2.1	0.01	17	2
11	29.1	614059.56	7716988.58	L	Both	GW seep	N	-	5.4	0.003	chan edge	--
12	28.4	616197.42	7716887.59	L	Both	BC: Back Bar	N	127	4.8	0.005	1	1
13	27.4	618168.95	7717492.32	MC	Field	BC: Remnant	N	70-80	0.2	0.017	1	3
14	27.4	618325.50	7717761.22	MC	TIR	BC: Cross Bar	N	50-60s	1.5	0.0029	3.7	1.5
15	27.2	618540.12	7717328.19	MC	Field	Bar Head (Ramp)	N	50-60s	1.8	0.059	0.5	0.6
16	26.5	620414.91	7718201.83	L	Both	BC: Remnant	Y	50-120	1.1	0.007	6.7	0.2
17	26.5	620470.45	7718278.84	L	Both	BC: Back Bar	N	50-60s	1.3	0.008	15	0.2
18	26.5	620629.53	7718336.92	L	Field	GW seep	N	80s	5.1	0.007	25	0.5
19	26.4	620683.69	7717650.13	MC	Both	BC: Remnant	Y	80s	1	0.004	3.5	0.5
20	26.1	621509.86	7717982.16	PB	Both	Bar Head (Ramp)	Y	50-60	2.25	0.012	22	3
21	26.1	622222.28	7717839.50	PB	Field	GW seep	N	50-60	5	0.007	4	2-3
22	23.7	627363.74	7713715.75	L	Both	BC: Cross Bar	N	50-60	1.5	0.02	2	3
23	23.7	627780.23	7713957.36	L	Both	GW seep	N	70s	1	0.005	Pool	1
24	24.2	626533.66	7714443.42	MC	Both	BC: Cross-bar	N	50-60	1.1	0.007	2	1
25	24.2	626782.37	7714245.21	MC	Both	Bar Head (Ramp)	Y	50-60	2.8	0.007	2.6	1
26	24.2	626777.32	7714419.43	MC	Field	BC: Back Bar	N	50-60	0.4	0.007	27	1
27	24.2	627079.05	7714343.68	MC	Field	BC: Back Bar	Y	50-60	1.6	0.007	1	1
28	22.4	628860.03	7713530.39	MC	TIR	Bar Head (Ramp)	N	-	1.2	0.007	66	1.5
29	21.2	630789.11	7710552.19	L	Field	GW seep	N	80s	2.8	--	chan edge	--
30	20.6	632644.96	7708759.47	L	Both	GW seep	N	80s	1	0.005	2	0.1



**Table C.1: Location and brief description of temperature anomalies**

No.	RKM	Northing (ft) <sup>1</sup>	Easting (ft)	Type of Bar <sup>2</sup>	Field/TIR	Geomorphic feature	Bar recently reworked?	Conductivity (µS/cm)	Ave. ΔT (°C)	Ave. gradient	Ave. Width (m)	Ave. Depth (m)
31	20.4	632812.87	7709376.82	MC	Field	Bar Head (Ramp)	Y	50-60s	1.2	0.019	1	2
32	20.1	632929.02	7708505.71	MC	Both	BC: Remnant	Y	50-60	1.9	0.015	4	2
33	20.1	633394.87	7708307.50	MC	Both	BC: Remnant	Y	50-60	1.6	0.01	3.5	0.5
34	20.0	633799.75	7708410.26	MC	Both	Bar Head (Ramp)	Y	50-60	0.6	0.01	3	1.5
35	19.6	633860.35	7706996.28	L	TIR	BC: Back Bar	Y	-	1.5	0.007	3	0.5
36	19.0	633254.36	7705173.26	L	TIR	BC: Back Bar	Y	-	1.1	0.006	1	1
37	18.8	632740.78	7704584.94	L	Both	BC: Back-bar	Y	-	0.6	0.007	2.4	1
38	17.5	631695.45	7702119.31	L	Both	GW seep	N	100-120	1.2	--	chan edge	0.5
39	17.5	632220.64	7700837.89	L	Field	GW seep	N	226	6.3	0.005	0.05	0.01
40	16.7	632505.83	7698528.81	L	Field	Bar Head (Ramp)	N	-	1.9	0.013	35	0.5
41	15.0	634024.60	7698883.91	MC	TIR	Bar Head (Ramp)	Y	-	1	0.012	29	2.5
42	14.6	635867.83	7694699.70	MC	TIR	Bar Head (Ramp)	Y	-	1.6	0.01	4	1.5
43	13.8	635261.83	7692058.58	PB	TIR	BC: Remnant	Y	-	0.9	0.01	2.5	2.5
44	13.5	635525.69	7690794.84	MC	Field	BC: Cross Bar?	N	-	1	0.007	4	1
45	13.2	635846.36	7690601.68	MC	TIR	Bar Head (Ramp)	Y	-	1.1	0.007	20	1
46	27.2	619013.55	7717458.23	MC	TIR	Bar Head (Ramp)	Y	50-60s	1.1	0.004	7	0.5
47	27.2	618704.24	7717763.75	L	TIR	GW seep	Y	-	1.8	0.007	3	0.5
48	26.4	620820.82	7718413.50	MC	TIR	Bar Head (Ramp)	Y	-	1.1	0.01	3	0.75
49	14.8	635734.06	7695136.91	MC	TIR	Bar Head (Ramp)	Y	50-60s	1.4	0.01	2	2.5
50	24.1	626799.66	7713497.57	L	TIR	BC: BBC?/Bar Head	Y	-	1.8	0.007	8	0.5
51	24.1	626818.60	7713455.90	L	TIR	Bar Head (Ramp)	Y	-	0.7	0.007	3.6	0.5
52	24.1	626764.31	7713815.21	L	TIR	Bar Head (Ramp)	Y	-	0.8	0.007	1	0.5

<sup>1</sup> Northings and Eastings are in NAD83 Oregon North State Plane Projection.

<sup>2</sup> MC = mid-channel; L = lateral; PB = point bar

**APPENDIX D**  
**TIR METHODOLOGY AND REPORT**

# Airborne Thermal Infrared Remote Sensing Clackamas River, OR

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Survey Date: August 12, 2006  
Report Date: October 15, 2006

# REPORT FOR THERMAL INFRARED REMOTE SENSING CLACKAMAS RIVER, OR

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## Background

In 2006, researchers at the Water Resources Graduate Program at Oregon State University contracted with Watershed Sciences, Inc. to acquire thermal infrared (TIR) and true color imagery of the Clackamas River, OR from the River Mill Dam near the town of Estacada, OR to Carver, OR (~15 river miles). The objective of the survey was to map surface temperature patterns during both the minimum and maximum of the diurnal temperatures cycles in the river. Consequently, two flights were conducted. The first was conducted just prior to dawn on August 12<sup>th</sup> in order to capture daily minimum water temperatures. A second flight was also conducted on August 12<sup>th</sup> during the mid-afternoon in order to capture heat-of-the-day conditions.

Airborne thermal infrared (TIR) remote sensing has proven an effective method for mapping spatial temperature patterns in rivers and streams. These data are used to establish baseline conditions and direct future ground level monitoring. The TIR imagery illustrates the location and thermal influence of point sources, tributaries, and surface springs. This report details the work performed, including methodology and quantitative assessments of data quality. The images contained in this report are not meant to be comprehensive, but provide examples of image scenes and interpretations.

## Survey Extent

The TIR data were acquired on August 12, 2006 and consisted of an early morning flight (5:56–6:38) and a mid-afternoon flight (14:26–15:08). Both flights were conducted over the same river extent starting at the River Mill Dam (mile 23.0) and proceeding downstream to the Carver Bridge (mile 8.0). If the river split into multiple channels and the channels were outside of the sensor field of view, then a survey was conducted along each channel resulting in multiple flight lines over some sections of the river (see Figure 1). The map in Figure 1 also shows the location of temperature data loggers deployed by Watershed Sciences prior to the flight and used to calibrate the TIR images.

## Methods

### ***Data Collection***

Instrumentation: Images were collected with a Space Instruments FireMapper 2.0 sensor (8-12 $\mu$ m) mounted on the underside of a Bell Jet Ranger Helicopter (Figure 2). The TIR sensor was co-mounted with a high-resolution true color digital camera (*Nikon D2X w/ 24mm lens, 6.9 mega-pixels*). Both cameras were positioned to look vertically down from the aircraft (nadir).

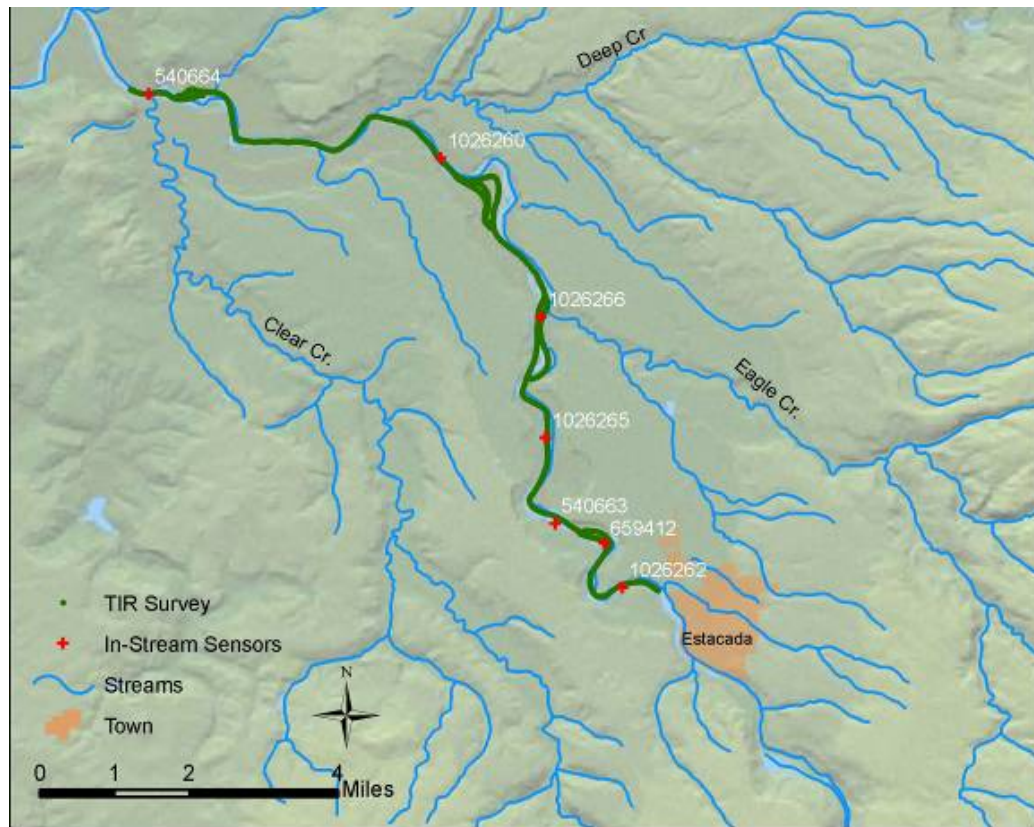


Figure 1 – The extent of the TIR survey conducted on the Clackamas River, OR on August 12, 2006. In-stream sensors used to calibrate the TIR images are shown on the map and labeled by serial number.

The TIR sensor has a horizontal field of view (H-FOV) of  $44^\circ$  and a pixel array of 320 x 240 pixels. The Firemapper 2.0 is a calibrated radiometer with internal non-uniformity correction and drift compensation. Thermal infrared images were recorded directly from the sensor to an on-board computer as raw counts, which were then



converted to radiant temperatures. The individual images were referenced with time, position, and heading information provided by a global positioning system (GPS). General specifications of the sensor are listed in Table 1.

Figure 2 – Bell Jet Ranger equipped with a thermal infrared radiometer and high resolution digital camera. The sensors are contained in a composite fiber enclosure attached to the

underside of the helicopter and flown longitudinally along the stream channel.

Image Characteristics: The aircraft was flown longitudinally along the stream corridor in order with the river in the center of the display. The objective was for the stream to occupy 30-60% of the image. The TIR sensor is set to acquire images at its maximum rate ( $\sim 1$  image/2 seconds) resulting in considerable vertical overlap between images. The airplane maintained an average flight altitude of 1,200ft (366 m) above ground level (AGL) resulting in a planned image ground footprint width of 977 ft (298 m) and a native pixel resolution of 3.1 ft (0.9 meters).

*Table 1. Summary of Thermal Image Acquisition Parameters.*

---

	Date:	August 12, 2006
	Acquisition Time:	5:56 – 6:38 (AM Flight) 14:26 – 15:08 (PM Flight)
	Flight Above Ground Level (AGL):	366 m (1200 ft)
	Sensor:	Space Instruments Firemapper 2.0
	Wavelength:	8-12 $\mu$ m
	Temperature Resolution:	0.01 $^{\circ}$ C
Noise Equivalent Temperature Differences (NETD)		0.07 $^{\circ}$ C
	Encoding Level:	16 bit
	Horizontal Field-of-View:	44.3 $^{\circ}$
	Image Footprint Width:	298 m (977 ft)
	Pixel Resolution:	0.9 m (3.1 ft)

---

Ground Control: Watershed Sciences deployed in-stream data loggers prior to the flight in order to calibrate and verify the accuracy of the TIR data. The data loggers were distributed at public access points along the survey extent. The sensors were placed on the bottom of the river in locations with good vertical mixing.

## **Data Processing**

Calibration: Calibration of the sensor is performed in the lab using an extended area black body to relate the response characteristics of the sensor to emitted radiance. The raw TIR images collected during the survey contain digital numbers that were converted to radiance ( $W/m^2 * sr * micron$ ) values based on the pre-season calibration.

The radiance values were adjusted based on a comparison of the measured radiance to the calculated radiance at each ground truth location. This adjustment was performed to correct for path length attenuation and the emissivity of natural water. The in-stream data were assessed at the time the image was acquired, with radiant values representing the median of ten points sampled from the image at the data logger location. The radiance values were then converted to surface temperatures using Planck's Black Body equation.

Interpretation and Sampling: Once calibrated, the images were integrated into a GIS in which an analyst interpreted and sampled stream temperatures. Sampling consisted of querying radiant temperatures (pixel values) from the center of the stream channel and saving the median value of a ten-point sample to a GIS database file. The temperatures of detectable surface inflows (i.e. surface springs, tributaries) were also sampled at their mouths. During sampling, the analyst provided interpretations of the spatial variations in surface temperatures observed in the images.

Geo-referencing: The images are tagged with a GPS position and heading at the time they are acquired. Since the TIR camera is maintained at vertical down-look angles, the geographic coordinates provide an accurate index to the location of the image scene. Due to the relatively small footprint of the imagery and independently stabilized mount, image pixels are not individually registered to real world coordinates. The image index is saved as an ESRI point shapefile containing the image name registered to an X and Y position (Oregon Lambert Projection) of sensor location at time of capture. In order to provide further spatial reference, the TIR images were assigned a river mile based on a routed stream layer (Figure 3).

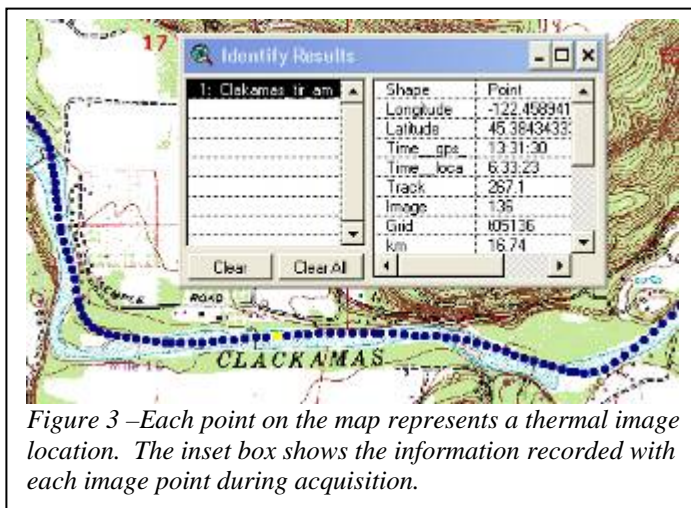


Figure 3 – Each point on the map represents a thermal image location. The inset box shows the information recorded with each image point during acquisition.

Temperature Profiles: The median temperatures for each sampled image were plotted versus the corresponding river mile to develop a longitudinal temperature profile. The profile illustrates how stream temperatures vary spatially along the stream gradient. The location and median temperature of all sampled surface water inflows (e.g. tributaries, surface springs, etc.) are included on the plot to illustrate how these inflows influence the main stem temperature patterns. Radiant temperatures were only sampled along what appeared to be the main flow channel in the river.

Geo-Rectification: The true color images were geo-rectified to real world coordinates using panchromatic ortho-photos (2000 available on the internet) as the reference layer. The true color digital images were initially oriented using the position and directional information collected on the aircraft. Individual frames were then geo-rectified by finding a minimum of six common ground control points (GCP's) between the true color images and existing ortho-photos. The images were then warped using a 1<sup>st</sup> order polynomial transformation. TIR images were geo-rectified



using the same general methodology with the true color images used as the control layer at an average of twelve ground control points. Due to the low relief along the river bottom, the photos were not corrected for terrain displacement.

### ***Thermal Image Characteristics***

Surface Temperatures: Thermal infrared sensors measure TIR energy emitted at the water's surface. Since water is essentially opaque to TIR wavelengths, the sensor is only measuring water surface temperature. Thermal infrared data accurately represents bulk water temperatures where the water column is thoroughly mixed; however, thermal stratification can form in reaches that have little or no mixing. Thermal stratification in a free flowing river is inherently unstable due to variations in channel shape, bed composition, and in-stream objects (i.e. rocks, trees, debris, etc.) that cause turbulent flow and can usually be detected in the imagery.

Expected Accuracy: Thermal infrared radiation received at the sensor is a combination of energy emitted from the water's surface, reflected from the water's surface, and absorbed and re-radiated by the intervening atmosphere. Water is a good emitter of TIR radiation and has relatively low reflectivity (~ 4 to 6%). However, variable water surface conditions (i.e. riffle versus pool), slight changes in viewing aspect, and variable background temperatures (i.e. sky versus trees) can result in differences in the calculated radiant temperatures within the same image or between consecutive images. The apparent temperature variability is generally less than 0.5°C (Torgersen et al. 2001<sup>1</sup>). However, the occurrence of reflections as an artifact (or noise) in the TIR images is a consideration during image interpretation and analysis. In general, apparent stream temperature changes of < 0.5°C are not considered significant unless associated with a surface inflow (e.g. tributary).

Differential Heating: In stream segments with flat surface conditions (i.e. pools) and relatively low mixing rates, observed variations in spatial temperature patterns can be the result of differences in the instantaneous heating rate at the water's surface. In the TIR images, indicators of differential surface heating include seemingly cooler radiant temperatures in shaded areas compared to surfaces exposed to direct sunlight.

Feature Size and Resolution: A small stream width logically translates to fewer pixels "in" the stream and greater integration with non-water features such as rocks and vegetation. Consequently, a narrow channel (relative to the pixel size) can result in higher inaccuracies in the measured radiant temperatures. This is a consideration when sampling the radiant temperatures at tributary mouths and surface springs.

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<sup>1</sup> Torgersen, C.E., R. Faux, B.A. McIntosh, N. Poage, and D.J. Norton. 2001. Airborne thermal remote sensing for water temperature assessment in rivers and streams. *Remote Sensing of Environment* 76(3): 386-398.

Temperatures and Color Maps: The TIR images collected during this survey consist of a single band. As a result, visual representation of the imagery (*in a report or GIS environment*) requires the application of a color map or legend to the pixel values. The selection of a color map should highlight features most relevant to the analysis (i.e. *spatial variability of stream temperatures*). For example, a continuous, gradient style color map that incorporates all temperatures in the image frame will provide a smoother transition in colors throughout the entire image, but will not highlight temperature differences in the stream. Conversely, a color map that focuses too narrowly cannot be applied to the entire river and will “washout” terrestrial and vegetation features.

Image Uniformity: The TIR sensor used for this study uses a focal plane array of detectors to sample incoming radiation. A challenge when using this technology is to achieve uniformity across the detector array. This sensor has an automatic correction scheme which nearly eliminates non-uniformity across the image frame.

## Results

### Weather Conditions

Weather conditions were considered good for the survey. Table 2 summarizes the weather conditions recorded at the Troutdale, OR Airport during the time frame of the survey.

Time PDT	Temp °F	Temp °C	Humidity %	Wind Direction	Wind Speed MPH	Sky Conditions
4:37 AM	51.8	11.0	82	Calm	Calm	Mostly Cloudy
4:53 AM	51.1	10.6	86	Calm	Calm	Scat. Clouds
5:53 AM	50.0	10.0	89	Calm	Calm	Mostly Cloudy
6:53 AM	51.1	10.6	86	Calm	Calm	Mostly Cloudy
7:04 AM	51.8	11.0	82	Calm	Calm	Overcast
7:53 AM	54.0	12.2	83	Calm	Calm	Overcast
8:53 AM	55.0	12.8	80	Calm	Calm	Overcast
9:53 AM	57.9	14.4	72	Variable	3.5	Overcast
10:53 AM	60.1	15.6	64	Variable	3.5	Overcast
11:53 AM	63.0	17.2	60	Variable	3.5	Scat. Clouds
12:53 PM	66.0	18.9	56	Variable	3.5	Clear
1:53 PM	71.1	21.7	47	NW	4.6	Clear
2:53 PM	73.9	23.3	43	Variable	4.6	Clear
3:53 PM	77.0	25.0	42	Variable	5.8	Clear
4:53 PM	79.0	26.1	39	West	8.1	Clear
5:53 PM	80.1	26.7	38	Variable	5.8	Clear
6:53 PM	79.0	26.1	38	Variable	6.9	Clear

Table 2. Weather conditions observed at the Troutdale Airport on August 12, 2006.

## ***Thermal Accuracy***

Table 3 provides a comparison between the kinetic temperatures recorded by the in-stream data loggers and the radiant temperatures derived from the TIR images for both the morning (AM) and afternoon (PM) flights on the Clackamas River. Since the in-stream data were used to compute an adjustment to the radiant temperatures, the table illustrates the range of differences after the images were calibrated. The correction was computed as an average offset from the raw radiant values for all sensor locations. Since the in-stream data are used in the radiant temperature calibration, they should not be considered an independent check of radiant temperatures.

The range of differences between the radiant temperatures and kinetic temperatures were generally within target values ( $\pm 0.5^{\circ}\text{C}$ ).

Table 3 – Comparison of radiant temperatures derived from the TIR images and kinetic temperatures from the in-stream monitors.

<b>Serial</b>	<b>Image</b>	<b>Local</b>	<b>Kinetic T<sub>⊙</sub></b>	<b>Radiant T<sub>⊙</sub></b>	<b>Difference T<sub>⊙</sub></b>
<b>Morning Flight</b>					
1026262	t01046	5:57	17.1	17.3	-0.2
659412	t02022	6:02	17.0	16.9	0.1
540663	t03018	6:08	16.7	17.1	-0.4
1026265	t03067	6:12	16.4	16.5	-0.1
1026266	t04043	6:19	16.0	16.1	-0.1
1026260	t05006	6:29	16.2	16.5	-0.4
540664	t05271	6:38	16.4	16.2	0.2
<b>Afternoon Flight</b>					
1026262	t06161	14:29	17.8	17.5	0.3
659412	t06008	14:34	18.6	18.8	-0.2
540663	t07045	14:35	18.8	19.3	-0.5
1026265	t08023	14:40	19.7	20.0	-0.3
1026266	t08218	14:46	21.2	21.0	0.1
1026260	t09008	14:59	19.9	20.4	-0.5
540664	t09297	15:08	19.1	19.0	0.1

## ***Longitudinal Profiles***

Median sampled temperatures were plotted versus river mile for the Clackamas River from River Mill Dam to the Carver Bridge for both the AM and PM flights (Figures 4 and 5). Tributaries and other sampled surface inflows (i.e. springs/seeps, side channels, off channel) are plotted on the profiles. The profiles were plotted over the same temperature ranges to more easily allow cross comparison.

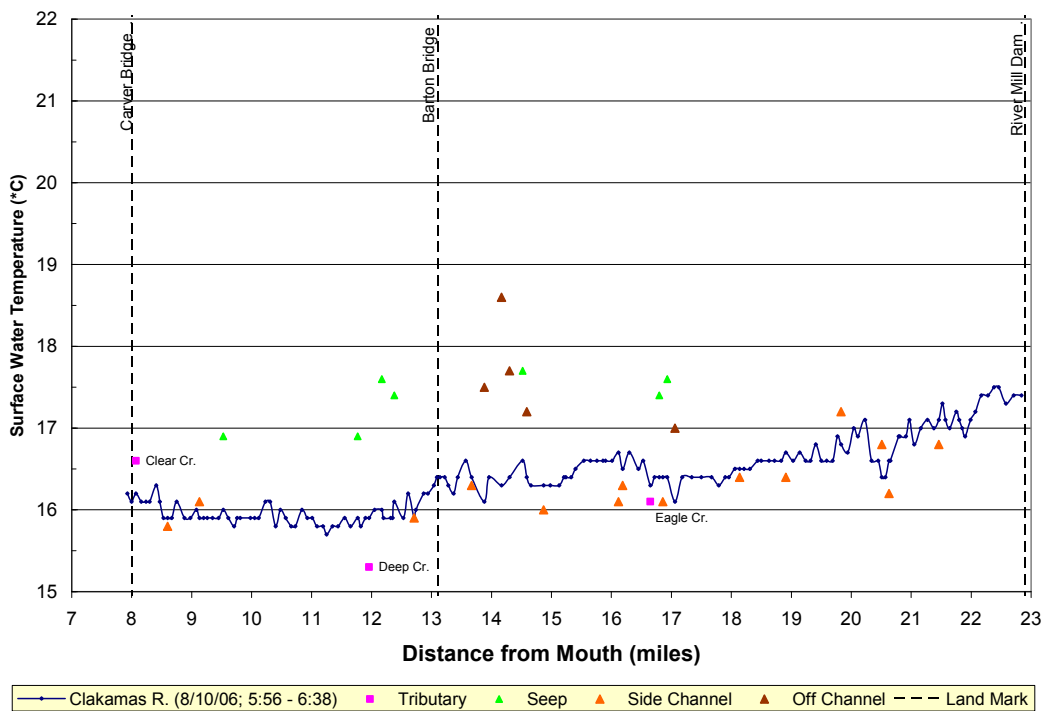


Figure 4 - Median sampled temperatures plotted versus river mile for the Clackamas River during the early morning of August 12, 2006.

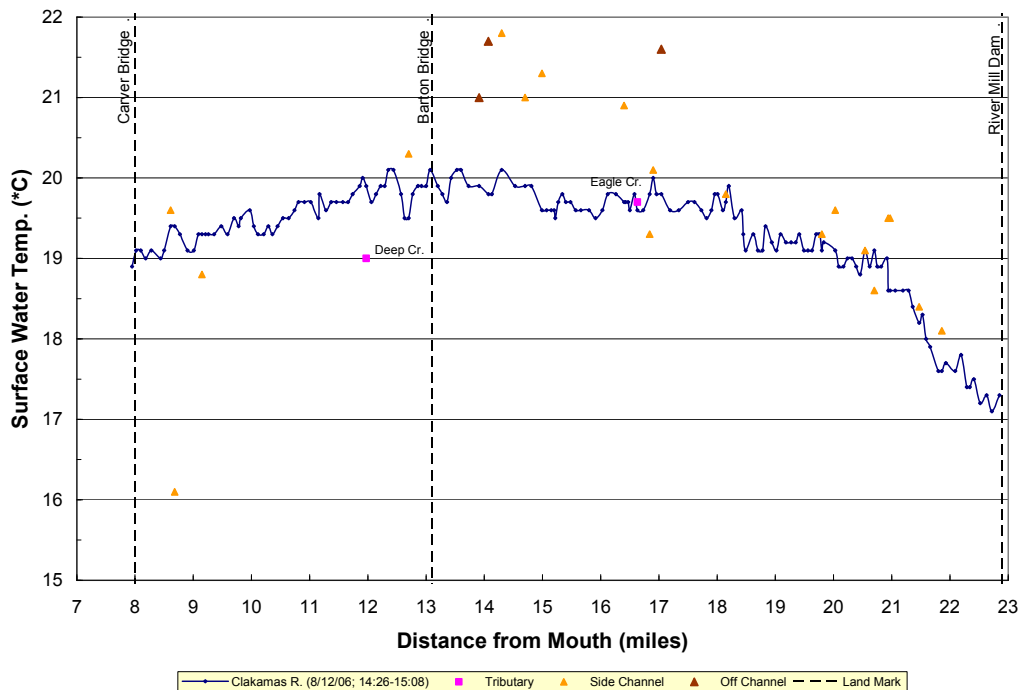


Figure 5 - Median sampled temperatures plotted versus river mile for the Clackamas River during the mid-afternoon on August 12, 2006.

## Observation and Analysis

### Morning Flight

Radiant water temperatures below River Mill Dam were  $\sim 17.4^{\circ}\text{C}$  at the time of the TIR survey with water temperatures in the main channel getting progressively cooler moving downstream. Over the full 15-mile survey water temperatures ranged from  $\sim 17.5^{\circ}\text{C}$  to a local minimum of  $15.7^{\circ}\text{C}$  (mile 11.3). While the range of sampled temperatures ( $1.8^{\circ}\text{C}$ ) was relatively small, inspection of the profile shows some apparent spatial trends along the river gradient.

Between river miles 21.0 and 20.6, stream temperatures exhibited a decrease of  $\sim 0.7^{\circ}\text{C}$  before increasing again in the downstream direction. While the magnitude of this decrease is close to the expected frame-to-frame variability (i.e.  $0.5^{\circ}\text{C}$ ), this was a notably larger change than observed at other locations along the profile and may warrant further investigation. Radiant water temperatures appeared relatively constant ( $\sim 16.4^{\circ}\text{C} \pm 0.3^{\circ}\text{C}$ ) between river mile 19.7 and 13.0 (*near Barton Bridge*). Downstream of Barton Bridge, bulk water temperatures again decreased before leveling off at  $\sim 15.8^{\circ}\text{C}$ .

As mentioned previously, radiant water temperatures were sampled along the main channel as determined based on size (*i.e. channel width*) and apparent flow. Secondary channels were classified as side channels and fourteen were sampled during the early morning flight. The side channels were sampled at the point where they rejoined the main channel. Most of the side channels had water temperatures consistent with water temperatures in the main stem.

Off-Channel features were identified as standing water or ponds that had surface connectivity to the main channel. During the morning flight, five off-channel features were identified and each had warmer radiant temperatures than the main channel. A number of “seeps” were also detected during the morning flight. These features were detected as areas of surface water that had significantly (i.e.  $\geq 0.5^{\circ}\text{C}$ ) different radiant temperatures than the main stem and appeared (*through interpretation of the imagery*) as an area of potential upwelling. The measured radiant temperatures were between  $16.9^{\circ}\text{C}$  and  $17.7^{\circ}\text{C}$ . Examples of both off-channel features and seeps are contained in the Sample Images section of this report.

### Afternoon Flight

During the afternoon flights, radiant water temperatures were  $\sim 17.4^{\circ}\text{C}$  and increased steadily downstream of the River Mill Dam (mile 23.0) reaching  $\sim 19.6^{\circ}\text{C}$  at river mile 18.2. Surface water temperatures appeared to increase slightly ( $19.6^{\circ}\text{C}$  to  $20.1^{\circ}\text{C}$ ) before exhibiting a steady decrease of  $\sim 1.0^{\circ}\text{C}$  between the Barton Bridge (mile 13.0) and the Carver Bridge (mile 8.0).

As with the morning flight, all detected surface water inflows were sampled where they entered the main channel. A total of nineteen side channels were sampled during

analysis of the afternoon imagery. Of these, seven side channels had radiant temperatures that were significantly different than the main channel. Three off-channel features were sampled and each had warmer surface temperatures than the main channel.

There were no “seeps” detected during the afternoon flight. Inspection of the TIR imagery showed that there was often little thermal contrast between terrain features and the surface water temperatures. This decreased contrast often made it difficult to detect small features with similar apparent temperatures (i.e. the stream bank and a small seep). Consequently, the seeps were detectable in the morning flight because of the cold background temperatures during the morning hours. The lack of detected seeps during the afternoon flight was probably due to the decreased contrast between the land and the water and not due to the absence of the seep.

### Comparison AM versus PM

A comparison of longitudinal temperature profiles from the afternoon and morning flight provides additional information on the processes driving spatial temperature patterns in the Clackamas River (Figure 6).

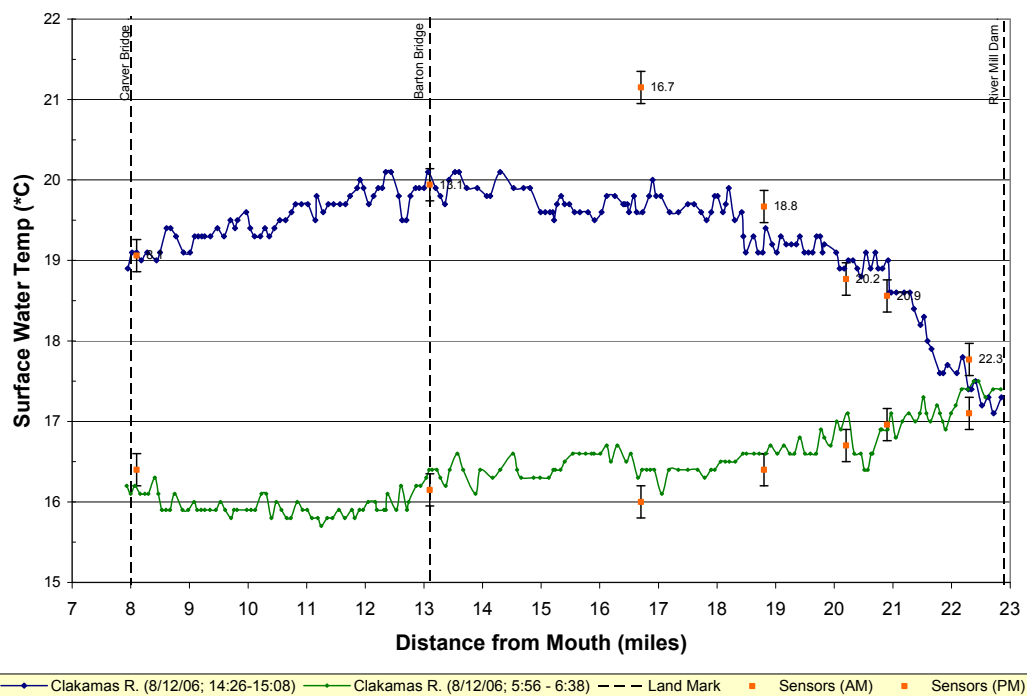


Figure 6 – Comparison of the longitudinal temperature profiles for the morning and afternoon flights on the Clackamas River. The plot also shows the location and recorded temperatures from the in-stream data loggers. The in-streams sensor temperatures at the time of the overflight are shown on the profiles. Note that the sensor at river mile 16.7 was not located within the main flow and therefore not representative of the bulk water temperatures during the afternoon flight.

While temperatures at the outlet of the dam were very similar between the morning and afternoon flights, the downstream spatial temperature patterns were almost mirror images. Both profiles show consistent temperature patterns over similar reaches. For example, both patterns showed a decrease in longitudinal heating (PM) or cooling (AM) between river miles 18 and 19. The warming (PM) (or cooling (AM)) continued at a lower rate in both profiles until approximately Barton Bridge (mile 13). In both profiles, the reach between Barton and Carver Bridges showed a distinct change in the downstream temperature pattern.

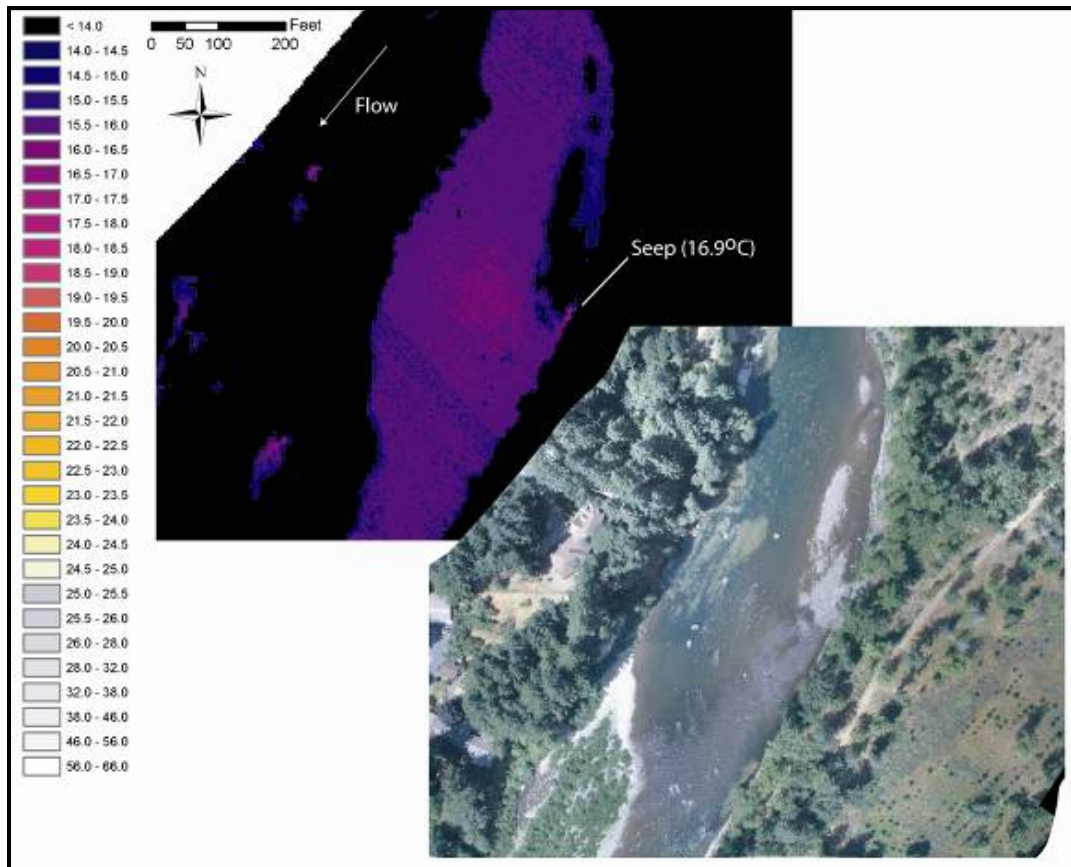
Over the surveyed reach, the Clackamas River was characterized by multiple channels, large gravel bars, and a number of off-channel ponds. This channel complexity combined with the observed spatial temperature patterns and evidence of “seeps” in the TIR imagery, suggests that hyporheic flow paths may have a regulating influence on in-stream temperature patterns. This is particularly true in the reach between Barton and Carver Bridges, which showed downstream cooling during heat-of-the day conditions and almost constant temperatures in the early morning profile.

## **Follow-On**

This report provides some hypotheses on the processes influencing spatial temperature patterns at this scale based on analysis of the TIR imagery. These hypotheses and observations are considered to be a starting point for more rigorous spatial analysis and fieldwork. Follow-on analysis may include:

- Since the seeps detected in the imagery are small, they should be considered detection of a process within a given reach and provide information on the type of channel and geomorphic conditions under which that process occurs in the Clackamas River. Follow on analysis may look at the significance of these seeps to temperatures at different spatial scale and localize thermal habitat for cold water fish.
- The TIR imagery and derived data sets provide a spatial context for analysis of seasonal temperature data from in-stream data loggers and for future deployment and distribution of in-stream monitoring stations.
- The rectified true color images provide a good data source evaluation of other physical habitat characteristics within the stream. These images may provide information at a spatial resolution and temporal significance that are not available from other sources.

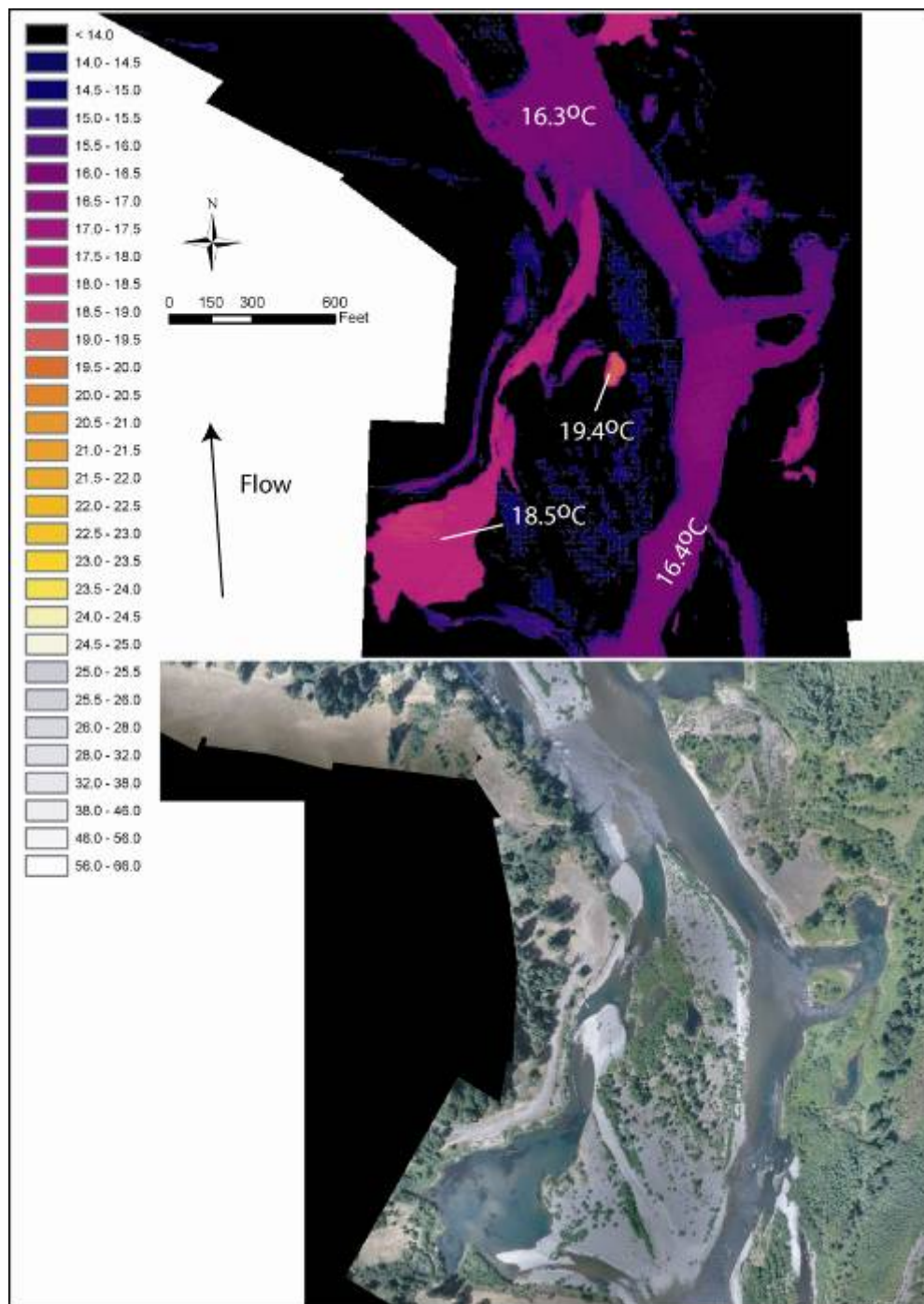
## Sample Images



*Example:* TIR (top) and true color image (bottom) showing the Clackamas River ( $15.9^{\circ}\text{C}$ ) at mile 11.8. The image pair shows an example the detection of apparent seep at the downstream end of the gravel bar along the left bank. The seeps were detectable in the early morning flight due to the large thermal contrast between the cold bank and terrain features and the water surface. The illustrated TIR image is from the geo-rectified mosaic and illustrates some of the slight uniformity and frame-to-frame differences in the thermal imagery.

The color map used to display the images exaggerates these differences. These artifacts can be reduced in the mosaic by using smoothing or averaging options available in most mosaicing programs. However, averaging can also result in the loss of small features such as the seeps due to small differences in pixel registration between frames.





*Example:* The TIR image (top) and true color image (bottom) shows the Clackamas River between miles 14.0 and 15.0. While bulk temperatures in the main channel are relatively constant, the side-channels and off-channel ponds show considerable variability in the surface temperatures. A number of seeps are also visible along the islands and gravel bars.

## Deliverables

The TIR imagery is provided in two forms: 1) individual un-rectified frames and 2) a continuous geo-rectified mosaic. The mosaic allows for easy viewing of the continuum of temperatures along the stream gradient, but also shows edge match differences and geometric transformation effects. The un-rectified frames are useful for viewing images at their native resolutions. The native resolution is often better for detecting smaller thermal features. A GIS point layer is included which provides an index of image locations, the results of temperature sampling, and interpretations made during the analysis.

Deliverables are provided on DVD:

Geo-Corrected Imagery is stored as: **Oregon Lambert, NAD83, Units = Int. Feet.**

- Unrectified – contains un-rectified single frame images.
  - Clackamas AM – calibrated, but un-rectified TIR image frames from the morning flight in ESRI GRID Format. These images retain the native resolution of the sensor. GRID cell value = radiant temp. (°C) \* 10.
  - Clackamas PM – calibrated, but un-rectified TIR image frames from the morning flight in ESRI GRID Format. These images retain the native resolution of the sensor. GRID cell value = radiant temp. (°C) \* 10.
  - TrueColor – un-rectified true color images (jpg).
  - Indices – ESRI shapefile (points) showing image locations for both TIR and true color image files.
- Rectified – contains geo-rectified images.
  - Clackamas AM – calibrated, but un-rectified TIR image frames from the morning flight in ESRI GRID Format. These images retain the native resolution of the sensor. GRID cell value = radiant temp. (°C) \* 10.
  - Clackamas PM – calibrated and rectified TIR image frames from the morning flight in ESRI GRID Format. These images retain the native resolution of the sensor. GRID cell value = radiant temp. (°C) \* 10.
  - Mosaics – Geo-rectified images mosaics for both the true color and thermal IR images in geo-tiff format.
- Report – Copy of this report.
- Longitudinal Profile – Excel File containing the longitudinal temperature profiles.
- Project – ArcGIS project illustrating the mosaic and the photo\_index for the rectified images.

## Contact Information

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**APPENDIX E**

**TOTAL STATION SURVEY DATA FOR FELDHEIMER, EAGLE CREEK  
AND BARTON BARS**

**Table E.1: 2006 Total station survey data for Feldheimer bar (RKM 30)**

Point #	Date	Northing (ft)	Easting (ft)	Elevation (ft)	Description
7000	07/30/2006	612319.688	7718189.536	228.134	WATER EDGE
7001	07/30/2006	612343.963	7718192.33	228.089	WATER EDGE
7002	07/30/2006	612368.502	7718201.301	228.024	WATER EDGE
7003	07/30/2006	612396.02	7718212.234	227.979	WATER EDGE
7004	07/30/2006	612422.982	7718219.838	227.885	WATER EDGE
7005	07/30/2006	612442.807	7718232.944	227.728	WATER EDGE
7006	07/30/2006	612473.584	7718246.25	227.581	WATER EDGE
7007	07/30/2006	612505.584	7718255.408	227.522	WATER EDGE
7008	07/30/2006	612529.436	7718272.684	227.123	WATER EDGE
7009	07/30/2006	612567.724	7718276.008	226.824	WATER EDGE
7010	07/30/2006	612608.622	7718270.963	226.79	WATER EDGE
7011	07/30/2006	612642.935	7718268.498	226.796	WATER EDGE
7012	07/30/2006	612676.212	7718262.128	226.736	WATER EDGE
7013	07/30/2006	612711.903	7718259.837	226.703	WATER EDGE
7014	07/30/2006	612747.745	7718254.769	226.8	WATER EDGE
7015	07/30/2006	612780.982	7718249.011	226.736	WATER EDGE
7016	07/30/2006	612832.505	7718243.281	226.749	WATER EDGE
7017	07/30/2006	612876.603	7718229.77	226.809	WATER EDGE
7018	07/30/2006	612924.865	7718213.648	226.753	WATER EDGE
7019	07/30/2006	612966.817	7718201.27	226.713	WATER EDGE
7020	07/30/2006	613006.845	7718181.591	226.75	WATER EDGE
7021	07/30/2006	613037.406	7718162.535	226.751	WATER EDGE
7022	07/30/2006	613080.578	7718141.542	226.744	WATER EDGE
7023	07/30/2006	613102.404	7718130.631	226.665	WATER EDGE
7024	07/30/2006	613105.608	7718116.916	226.697	WATER EDGE
7025	07/30/2006	613091.242	7718115.062	226.654	WATER EDGE
7500	07/30/2006	612299.443	7718129.723	228.795	TOPO_PT
7501	07/30/2006	612305.727	7718142.345	227.955	TOPO_PT
7502	07/30/2006	612313.462	7718153.869	228.446	TOPO_PT
7503	07/30/2006	612334.105	7718148.962	228.25	TOPO_PT
7504	07/30/2006	612334.205	7718136.255	228.095	TOPO_PT
7505	07/30/2006	612334.386	7718121.403	228.257	TOPO_PT
7506	07/30/2006	612349.578	7718114.418	228.418	TOPO_PT
7507	07/30/2006	612349.471	7718124.92	227.766	TOPO_PT
7508	07/30/2006	612349.116	7718136.176	228.697	TOPO_PT
7509	07/30/2006	612361.61	7718157.719	228.786	TOPO_PT
7510	07/30/2006	612384.396	7718096.783	230.735	TOPO_PT
7511	07/30/2006	612393.169	7718121.981	227.58	TOPO_PT
7512	07/30/2006	612403.217	7718148.36	228.439	TOPO_PT
7513	07/30/2006	612412.542	7718166.654	230.423	TOPO_PT
7514	07/30/2006	612442.015	7718115.331	227.262	TOPO_PT
7515	07/30/2006	612430.593	7718093.631	231.02	TOPO_PT
7516	07/30/2006	612434.57	7718103.423	227.426	TOE
7517	07/30/2006	612439.386	7718137.672	228.677	TOPO_PT
7518	07/30/2006	612447.42	7718163.341	229.876	TOPO_PT
7519	07/30/2006	612471.356	7718105.097	227.365	PETER_TR_ROCK
7520	07/30/2006	612473.872	7718115.967	227.858	TOE
7521	07/30/2006	612489.666	7718072.738	231.069	TOPO_PT
7522	07/30/2006	612507.952	7718101.951	227.727	TOPO_PT
7523	07/30/2006	612509.03	7718124.497	228.845	TOPO_PT
7524	07/30/2006	612542.392	7718081.851	226.445	TOE
7525	07/30/2006	612541.8	7718061.65	226.925	TOPO_PT
7526	07/30/2006	612539.198	7718089.719	228.334	TOPO_PT
7527	07/30/2006	612538.977	7718046.934	231.894	TOPO_PT

**Table E.1: 2006 Total station survey data for Feldheimer bar (RKM 30)**

Point #	Date	Northing (ft)	Easting (ft)	Elevation (ft)	Description
7528	07/30/2006	612551.657	7718070.806	225.803	TOPO_PT
7529	07/30/2006	612556.243	7718077.339	226.181	TOE
7530	07/30/2006	612558.678	7718085.754	229.574	TOPO_PT
7531	07/30/2006	612553.622	7718070.989	225.545	POOL
7532	07/30/2006	612553.306	7718069.697	225.579	POOL
7533	07/30/2006	612552.72	7718070.384	225.533	POOL
7534	07/30/2006	612572.439	7718062.414	225.475	POOL
7535	07/30/2006	612572.135	7718062.01	225.549	POOL
7536	07/30/2006	612572.083	7718062.025	225.551	POOL
7537	07/30/2006	612572.036	7718062.444	225.5	POOL
7538	07/30/2006	612598.99	7718060.497	225.461	POOL
7539	07/30/2006	612599.665	7718061.293	225.351	POOL
7540	07/30/2006	612598.914	7718061.152	225.401	POOL
7541	07/30/2006	612612	7718051.04	225.212	POOL
7542	07/30/2006	612611.206	7718049.862	225.305	POOL
7543	07/30/2006	612610.867	7718050.877	225.179	POOL
7544	07/30/2006	612623.372	7718056.97	225.612	TOE
7545	07/30/2006	612619.701	7718050.88	225.227	TOPO_PT
7546	07/30/2006	612620.887	7718052.364	225.242	POOL
7547	07/30/2006	612625.201	7718053.619	225.218	POOL
7548	07/30/2006	612629.157	7718052.134	225.241	POOL
7549	07/30/2006	612629.008	7718048.932	225.243	POOL
7550	07/30/2006	612626.78	7718048.695	225.235	POOL
7551	07/30/2006	612624.233	7718048.007	225.255	POOL
7552	07/30/2006	612623.345	7718045.157	225.243	POOL
7553	07/30/2006	612619.04	7718047.253	225.209	POOL
7554	07/30/2006	612630.227	7718041.102	225.141	POOL
7555	07/30/2006	612638.827	7718036.882	225.18	POOL
7556	07/30/2006	612643.343	7718035.384	225.184	POOL
7557	07/30/2006	612649.755	7718036.195	225.165	POOL
7558	07/30/2006	612653.408	7718040.218	225.155	POOL
7559	07/30/2006	612651.304	7718041.304	225.12	POOL
7560	07/30/2006	612640.19	7718044.625	225.137	POOL
7561	07/30/2006	612615.509	7718039.791	225.981	TOPO_PT
7562	07/30/2006	612660.1	7718036.548	225.104	POOL
7563	07/30/2006	612662.336	7718031.769	225.108	POOL
7564	07/30/2006	612625.987	7718060.823	227.114	TOPO_PT
7565	07/30/2006	612631.454	7718065.433	230.091	TOPO_PT
7566	07/30/2006	612670.626	7718032.25	224.995	POOL
7567	07/30/2006	612673.515	7718027.815	225.081	POOL
7568	07/30/2006	612678.131	7718020.554	225.041	POOL
7569	07/30/2006	612678.167	7718020.386	225.031	POOL
7570	07/30/2006	612683.077	7718018.922	225.063	POOL
7571	07/30/2006	612690.234	7718023.908	225.035	POOL
7572	07/30/2006	612686.817	7718012.111	225.007	POOL
7573	07/30/2006	612701.016	7718022.747	225.039	POOL
7574	07/30/2006	612702.839	7718006.506	225.078	POOL
7575	07/30/2006	612709.793	7718003.337	225.087	POOL
7576	07/30/2006	612720.976	7717999.608	225.046	POOL
7577	07/30/2006	612726.315	7718009.184	225.008	POOL
7578	07/30/2006	612719.647	7718014.044	225.087	POOL
7579	07/30/2006	612708.68	7718015.841	225.104	POOL
7580	07/30/2006	612704.19	7718021.001	225.146	POOL
7581	07/30/2006	612710.935	7718020.592	225.304	TOE
7582	07/30/2006	612712.951	7718028.409	229.281	TOPO_PT

**Table E.1: 2006 Total station survey data for Feldheimer bar (RKM 30)**

Point #	Date	Northing (ft)	Easting (ft)	Elevation (ft)	Description
7583	07/30/2006	612686.093	7717995.331	231.017	TOPO_PT
7584	07/30/2006	612703.384	7718013.253	224.69	TOPO_PT
7585	07/30/2006	612716.046	7718008.216	224.701	TOPO_PT
7586	07/30/2006	612730.09	7717988.615	225.997	TOE
7587	07/30/2006	612725.598	7717980.855	231.315	TOPO_PT
7588	07/30/2006	612731.101	7717993.828	225.01	POOL
7589	07/30/2006	612733.64	7717998.189	224.789	POOL
7590	07/30/2006	612734.115	7718000.305	224.903	POOL
7591	07/30/2006	612743.828	7717998.081	225.011	POOL
7592	07/30/2006	612750.13	7717997.431	224.91	POOL
7593	07/30/2006	612761.556	7717994.133	224.931	POOL
7594	07/30/2006	612766.227	7717985.757	224.982	POOL
7595	07/30/2006	612756.631	7717985.66	224.954	POOL
7596	07/30/2006	612748.265	7717988.773	224.933	POOL
7597	07/30/2006	612742.591	7717991.274	224.928	POOL
7598	07/30/2006	612751.958	7717992.751	224.552	TOPO_PT
7599	07/30/2006	612747.069	7717992.98	224.791	TOPO_PT
7600	07/30/2006	612749.445	7718000.939	225.02	TOPO_PT
7601	07/30/2006	612760.434	7717999.308	225.241	TOPO_PT
7602	07/30/2006	612741.896	7718011.996	226.176	TOPO_PT
7603	07/30/2006	612743.805	7718019.121	229.128	TOPO_PT
7604	07/30/2006	612771.334	7717994.486	225.123	TOPO_PT
7605	07/30/2006	612768.587	7717988.52	224.94	POOL
7606	07/30/2006	612765.77	7717980.023	225.039	TOPO_PT
7607	07/30/2006	612772.388	7718007.641	229.35	TOP
7608	07/30/2006	612771.392	7718003.668	226.643	TOE
7609	07/30/2006	612827.053	7717973.39	225.311	TOPO_PT
7610	07/30/2006	612761.999	7717977.318	225.56	TOE
7611	07/30/2006	612823.768	7717966.475	224.752	TOPO_PT
7612	07/30/2006	612760.148	7717967.404	230.053	TOPO_PT
7613	07/30/2006	612820.793	7717958.444	224.923	TOPO_PT
7614	07/30/2006	612820.876	7717958.22	224.889	TOPO_PT
7615	07/30/2006	612814.802	7717951.874	228.342	TOPO_PT
7616	07/30/2006	612829.489	7717978.935	225.266	TOE
7617	07/30/2006	612878.24	7717942.868	224.159	POOL
7618	07/30/2006	612880.811	7717936.153	224.124	POOL
7619	07/30/2006	612833.689	7717984.487	228.119	TOP
7620	07/30/2006	612882.871	7717945.217	224.055	POOL
7621	07/30/2006	612891.187	7717943.108	224.123	POOL
7622	07/30/2006	612897.866	7717932.319	224.105	POOL
7623	07/30/2006	612894.758	7717924.495	224.778	TOE
7624	07/30/2006	612897.615	7717930.342	224.415	TOPO_PT
7625	07/30/2006	612885.802	7717910.908	230.264	TOPO_PT
7626	07/30/2006	612908.918	7717947.311	224.559	TOE
7627	07/30/2006	612919.141	7717927.066	223.973	POOL
7628	07/30/2006	612927.44	7717924.612	224.067	POOL
7629	07/30/2006	612931.42	7717921.671	224.009	POOL
7630	07/30/2006	612925.691	7717919.417	224.02	POOL
7631	07/30/2006	612919.042	7717921.731	223.952	POOL
7632	07/30/2006	612938.795	7717883.335	231.46	TOP
7633	07/30/2006	612944.852	7717897.689	224.542	TOE
7634	07/30/2006	612950.189	7717907.445	223.956	POOL
7635	07/30/2006	612955.718	7717908.485	223.928	POOL
7636	07/30/2006	612959.417	7717915.267	223.924	POOL
7637	07/30/2006	612953.696	7717911.598	223.972	POOL

**Table E.1: 2006 Total station survey data for Feldheimer bar (RKM 30)**

Point #	Date	Northing (ft)	Easting (ft)	Elevation (ft)	Description
7638	07/30/2006	612950.055	7717914.086	223.943	POOL
7639	07/30/2006	612956.925	7717921.924	224.11	TOPO_PT
7640	07/30/2006	612960.757	7717930.606	224.56	TOPO_PT
7641	07/30/2006	612969.086	7717914.134	223.838	POOL 1
7642	07/30/2006	612962.198	7717944.155	227.939	TOPO_PT
7643	07/30/2006	612961.448	7717898.287	223.852	POOL 1
7644	07/30/2006	612976.347	7717885.927	223.839	POOL 1
7645	07/30/2006	612988.813	7717881.542	223.834	POOL 1
7646	07/30/2006	613002.926	7717873.673	223.8	POOL 1
7647	07/30/2006	613017.088	7717866.883	223.844	POOL 1
7648	07/30/2006	613036.34	7717861.964	223.921	POOL 1
7649	07/30/2006	613051.131	7717856.715	223.906	POOL 1
7650	07/30/2006	613064.224	7717853.77	223.926	POOL 1
7651	07/30/2006	613070.679	7717867.707	223.822	POOL 1
7652	07/30/2006	613050.993	7717879.864	223.895	POOL 1
7653	07/30/2006	613035.656	7717894.211	223.831	POOL 1
7654	07/30/2006	613011.21	7717911.632	223.845	POOL 1
7655	07/30/2006	612987.936	7717921.759	223.936	POOL 1
7656	07/30/2006	612973.345	7717918.262	223.952	POOL 1
7657	07/30/2006	612967.472	7717912.15	223.908	POOL 1
7658	07/30/2006	613020.37	7717922.225	226.608	TOP
7659	07/30/2006	613038.519	7717897.84	224.609	TOPO_PT
7660	07/30/2006	613045.38	7717905.056	225.041	TOPO_PT
7661	07/30/2006	613061.992	7717895.352	224.106	TOPO_PT
7662	07/30/2006	613059.862	7717881.688	224.707	TOPO_PT
7663	07/30/2006	613072.168	7717872.042	224.153	TOPO_PT
7664	07/30/2006	613077.847	7717877.331	224.943	TOPO_PT
7665	07/30/2006	613085.158	7717882.447	223.941	TOPO_PT
7666	07/30/2006	613013.494	7717859.013	227.246	TOP
7667	07/30/2006	613083.444	7717820.316	229.416	TOP
7668	07/30/2006	613086.705	7717833.222	227.183	TOP
7669	07/30/2006	613092.961	7717843.318	224.133	TOE
7670	07/30/2006	613095.217	7717850.208	224.02	TOPO_PT
7671	07/30/2006	613097.727	7717857.387	223.374	POOL
7672	07/30/2006	613101.882	7717862.261	223.336	POOL
7673	07/30/2006	613093.965	7717866.999	223.414	POOL
7674	07/30/2006	613075.378	7717897.691	223.223	POOL 2
7675	07/30/2006	613080.548	7717893.617	223.258	POOL 2
7676	07/30/2006	613086.751	7717893.209	223.134	POOL 2
7677	07/30/2006	613096.848	7717879.013	223.276	POOL 2
7678	07/30/2006	613107.413	7717864.762	223.238	POOL 2
7679	07/30/2006	613116.186	7717844.289	223.25	POOL 2
7680	07/30/2006	613124.352	7717832.813	223.205	POOL 2
7681	07/30/2006	613143.547	7717818.125	223.143	POOL 2
7682	07/30/2006	613157.933	7717820.193	223.306	POOL 2
7683	07/30/2006	613163.555	7717822.515	223.265	POOL 2
7684	07/30/2006	613150.032	7717834.856	223.244	POOL 2
7685	07/30/2006	613153.067	7717842.492	223.261	POOL 2
7686	07/30/2006	613172.804	7717834.425	223.271	POOL 2
7687	07/30/2006	613185.93	7717825.005	223.239	POOL 2
7688	07/30/2006	613171.298	7717844.546	223.31	POOL 2
7689	07/30/2006	613152.259	7717855.068	223.284	POOL 2
7690	07/30/2006	613136.568	7717866.328	223.228	POOL 2
7691	07/30/2006	613118.559	7717875.636	223.179	POOL 2
7692	07/30/2006	613110.806	7717881.459	223.283	POOL 2

**Table E.1: 2006 Total station survey data for Feldheimer bar (RKM 30)**

Point #	Date	Northing (ft)	Easting (ft)	Elevation (ft)	Description
7693	07/30/2006	613125.009	7717890.475	228.724	TOP
7694	07/30/2006	613153.888	7717837.03	223.449	TOPO_PT
7695	07/30/2006	613167.015	7717858.936	226.211	TOP
7696	07/30/2006	613186.402	7717820.665	223.302	TOPO_PT
7697	07/30/2006	613180.886	7717806.541	223.497	TOPO_PT
7698	07/30/2006	613142.766	7717807.118	227.027	TOP
7699	07/30/2006	613232.79	7717802.708	223.927	TOPO_PT
7700	07/30/2006	613219.867	7717787.723	223.561	TOPO_PT
7701	07/30/2006	613207.872	7717775.9	224.487	TOPO_PT
7702	07/30/2006	613241.865	7717816.796	225.793	TOP
7703	07/30/2006	613241.51	7717814.889	224.087	TOE
7704	07/30/2006	613250.419	7717795.705	223.147	TOPO_PT
7705	07/30/2006	613239.242	7717778.619	223.949	TOPO_PT
7706	07/30/2006	613224.156	7717768.464	224.696	TOPO_PT
7707	07/30/2006	613205.158	7717755.034	228.494	TOP
7708	07/30/2006	613270.197	7717784.641	221.321	POOL
7709	07/30/2006	613274.791	7717781.35	220.895	POOL
7710	07/30/2006	613283.225	7717778.615	220.566	POOL
7711	07/30/2006	613274.421	7717778.206	220.865	POOL
7712	07/30/2006	613272.122	7717776.352	221.155	POOL
7713	07/30/2006	613270.722	7717773.87	221.899	TOPO_PT
7714	07/30/2006	613261.763	7717767.287	223.251	TOPO_PT
7715	07/30/2006	613276.259	7717768.468	222.219	TOPO_PT
7716	07/30/2006	613285.578	7717766.55	221.112	TOPO_PT
7717	07/30/2006	613285.467	7717779.506	220.611	WATER_E
7719	07/30/2006	613263.136	7717798.582	224.196	TOP
7720	07/30/2006	613258.297	7717755.356	224.583	TOP

Note: Northings and Eastings are in NAD83 Oregon North State Plane Projection. Elevations are relative to the NAVD88 vertical datum.



**Table E.2: 2006 Total station survey data for Eagle Creek bar (RKM 26)**

<b>Point #</b>	<b>Date</b>	<b>Northing (ft)</b>	<b>Easting (ft)</b>	<b>Elevation (ft)</b>	<b>Description</b>
0002	07/31/2006	623193.315	7717187.880	178.42	GW WELL 1
0003	07/31/2006	623813.82	7716717.63	174.76	DS WATER EDGE
0001	07/31/2006	620628.2	7717437.82	198.48	US WATER EDGE
5000	07/31/2006	621178.519	7717648.343	194.726	WATER EDGE
5001	07/31/2006	621193.779	7717670.989	194.544	WATER EDGE
5002	07/31/2006	621193.196	7717678.676	194.469	WATER EDGE
5003	07/31/2006	621208.644	7717690.839	194.457	WATER EDGE
5004	07/31/2006	621221.798	7717706.858	194.347	WATER EDGE
5005	07/31/2006	621231.431	7717721.561	194.409	WATER EDGE
5006	07/31/2006	621248.567	7717747.643	194.216	WATER EDGE
5007	07/31/2006	621265.997	7717763.446	194.121	WATER EDGE
5008	07/31/2006	621286.024	7717784.053	193.984	WATER EDGE
5009	07/31/2006	621289.654	7717807.089	194.087	WATER EDGE
5010	07/31/2006	621296.672	7717826.703	193.932	WATER EDGE
5011	07/31/2006	621306.798	7717856.662	193.591	WATER EDGE
5012	07/31/2006	621325.483	7717890.75	193.14	WATER EDGE
5013	07/31/2006	621329.081	7717914.672	192.904	WATER EDGE
5014	07/31/2006	621349.032	7717924.485	192.551	WATER EDGE
5015	07/31/2006	621348.476	7717943.296	192.353	WATER EDGE
5016	07/31/2006	621341.677	7717959.842	191.833	WATER EDGE
5017	07/31/2006	621338.68	7717974.533	190.599	WATER EDGE
5018	07/31/2006	621355.387	7717973.432	190.555	WATER EDGE
5019	07/31/2006	621383.509	7717980.099	190.647	WATER EDGE
5020	07/31/2006	621393.014	7717979.396	190.62	WATER EDGE
5021	07/31/2006	621396.997	7717974.698	190.712	WATER EDGE
5022	07/31/2006	621420.73	7717981.596	190.699	WATER EDGE
5023	07/31/2006	621450.922	7717996.105	190.696	WATER EDGE
5024	07/31/2006	621472.372	7717997.643	190.739	WATER EDGE
5025	07/31/2006	621506.086	7718000.985	190.652	WATER EDGE
5026	07/31/2006	621530.185	7717997.939	190.679	WATER EDGE
5027	07/31/2006	621538.744	7718012.691	190.616	WATER EDGE
5028	07/31/2006	621574.194	7718019.232	190.448	WATER EDGE
5029	07/31/2006	621602.536	7718021.328	190.378	WATER EDGE
5030	07/31/2006	621628.723	7718014.982	190.121	WATER EDGE
5031	07/31/2006	621642.024	7718009.617	189.301	WATER EDGE
5032	07/31/2006	621654.329	7718002.221	188.744	WATER EDGE
5033	07/31/2006	621682.423	7718011.039	188.341	WATER EDGE
5034	07/31/2006	621711.064	7718021.153	187.478	WATER EDGE
5035	07/31/2006	621735.793	7718023.426	186.67	WATER EDGE
5036	07/31/2006	621761.851	7718019.897	186.532	WATER EDGE
5037	07/31/2006	621790.818	7718017.391	186.37	WATER EDGE
5038	07/31/2006	621821.925	7718012.681	186.268	WATER EDGE
5039	07/31/2006	621853.866	7718005.361	186.22	WATER EDGE
5040	07/31/2006	621886.89	7717996.561	186.265	WATER EDGE
5041	07/31/2006	621913.798	7717989.792	186.227	WATER EDGE
5042	07/31/2006	621946.649	7717983.607	186.159	WATER EDGE
5043	07/31/2006	621972.775	7717991.414	185.797	WATER EDGE
5044	07/31/2006	621988.485	7717997.05	185.441	WATER EDGE
5045	07/31/2006	621997.656	7718007.023	184.886	WATER EDGE
5046	07/31/2006	622016.495	7717995.309	184.866	WATER EDGE
5047	07/31/2006	622043.621	7717982.09	184.932	WATER EDGE
5048	07/31/2006	622069.515	7717962.748	184.923	WATER EDGE
5049	07/31/2006	622090.563	7717943.018	184.763	WATER EDGE
5050	07/31/2006	622113.902	7717922.797	184.822	WATER EDGE

































































































































































































