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## Abstract approved



The molecular structure and root-mean-square amplitudes of vibration of gaseous nitrogen dioxide have been investigated by electron diffraction at a nozzle temperature of $380^{\circ} \mathrm{K}$. The results are $r_{\mathrm{N}-\mathrm{O}}=1.202+0.0013 \AA, \mathrm{r}_{\mathrm{O}} \cdots \mathrm{O}=2213 \pm 0.0050 \AA, \angle \mathrm{O}-\mathrm{N}-\mathrm{O}=$ $134.02 \pm 0.65^{\circ}, l_{\mathrm{N}-\mathrm{O}}=0.0382 \pm 0.0025 \AA$ and $\mathrm{l}_{\mathrm{O}} \ldots \mathrm{O}=0.0470 \pm 0.0050 \AA$. The interatomic distances given are $r_{a}$ values from the third cycle of least-squares refinement of intensity curves and differ from the equilibrium values $r_{e}$ by small amounts; the $l_{a}$ values correspondingly differ from the $l_{e}$ values. The estimated standard errors include standard deviations derived from least-squares, deviations of the individual photographic plates at a given camera distance, estimates of correlation among the data, uncertainty in the constants of the experiment, and uncertainty in the factors employed in the data reduction. These errors are clearly conservative estimates.

By combining the mean-square-amplitudes (described above) with the normal vibrational frequencies, a reasonable set of values have been obtained for the potential constants of the general quadratic function

$$
\begin{aligned}
2 V=f_{r}\left[\left(\Delta r_{1}\right)^{2}+\left(\Delta r_{2}\right)^{2}\right] & +2 f_{r r}\left(\Delta r_{1}\right)\left(\Delta r_{2}\right)+f_{a}\left(r_{e} \Delta a\right)^{2} \\
& +2 f_{r a}\left(\Delta r_{1}+\Delta r_{2}\right)\left(r_{e} \Delta a\right)
\end{aligned}
$$

The values in millidynes $/ \AA$ (with estimated standard errors) for the observed fundamental and harmonic frequencies, respectively, are $\mathrm{f}_{\mathrm{r}}=10.77_{1} \pm 0.90_{3}$ and $11.15_{8} \pm 1.00_{1} ; \mathrm{f}_{\mathrm{rr}}=2.36_{8} \pm 0.90_{3}$ and $2.25_{1} \pm 1.00_{1} ; f_{a}=0.96_{9} \pm 0.59_{9}$ and $1.09_{4} \pm 0.67_{7} ; f_{r a}=0.52_{0} \pm 0.32_{8}$ and $0.53_{3} \pm 0.38_{5}$.

In addition to the potential constants described above, various combinations of frequencies and mean-square amplitudes were investigated using a least-squares procedure. These results are expressed in terms of symmetrized compliance constants based on valence force coordinates.

The agreement between the various sets of internal potential constants and compliance constants derived in this work with those of isotopic spectroscopy suggests very strongly that mean-square amplitudes from electron diffraction (at least for small molecules composed of similar atoms) are consistent with spectroscopy data (vibrational frequencies).

# A STRUCTURE INVESTIGATION OF NITROGEN DIOXIDE 

I. GEOMETRY AND AMPLITUDES OF VIBRATION II. QUADRATIC POTENTIAL CONSTANTS
by

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# A STRUCTURE INVESTIGATION OF NITROGEN DIOXIDE 

## INTRODUCTION

An understanding of the forces operating between atoms in a molecule is one of the principle objectives of vibrational spectroscopy. When applied to simple molecules this technique yields results (vibrational frequencies) which may be interpreted in terms of the values of potential constants defining a vibrational potential function; the values of the potential constants in principle permit one to make deductions concerning bond properties.

The main trouble encountered in the application of vibrational spectroscopy to the elucidation of vibrational potential functions lies not in the experiment itself, but in the physics of the problem. Even in the simpler harmonic cases the $3 n-6$ (or $3 n-5$ ) data (vibrational frequencies) for a single isotopic species generally number fewer than the parameters (potential constants) one would like to determine. The investigator must thus either content himself with an assumed abbreviated potential function, or he must study other isotopic species. The desirable latter alternative is not always possible for molecules due to experimental difficulties and interpretation problems.

Recent work (22, p. 594-598; 37, p. 643-652) indicates that another possible approach to this problem lies in combining the
vibrational amplitudes of electron diffraction with the frequencies of vibrational spectroscopy. The feasibility of this approach for simple molecules constitutes the purpose of this work; that is, this work is an attempt to ascertain the reliability and consistency of the observed vibrational amplitudes of electron diffraction, using the results (quadratic potential constants) of vibrational spectroscopy of isotopic species as the principal reliability criteria. The past thorough studies of nitrogen dioxide, together with the structural simplicity of the molecule from the electron diffraction point of view, make it especially useful as a test case. This structural simplicity involves the facts that (a) there are only two, wellresolved, interatomic distances in the molecule ( $\mathrm{N}-\mathrm{O}$ and $\mathrm{O} \cdots \mathrm{O}$ ), and (b) the atomic number difference of the atoms is very small whick minimizes the complicating phase shift effect (13, p. 667-671).

## PART I

GEOMETRY AND AMPLITUDES OF VIBRATION

## PREVIOUS STRUCTURAL INVESTIGATIONS OF NITROGEN DIOXIDE

Structural investigations of gaseous nitrogen dioxide by electron diffraction, ultraviolet, infrared and microwave spectroscopy have been carried out over a period in excess of thirty years (see bibliographies given in references cited belowl). Though some of the early investigations (15, p. 775-784; 31, p. 738-742) indicated a non-linear symmetric structure with a large bond angle, precise values of the equilibrium N - O distance, $\mathrm{O}-\mathrm{N}-\mathrm{O}$ angle, vibrational frequencies, and the quadratic potential constants have only recently been obtained (5 p. 1040-1043; 45, p. 1248-1251; 1, p. 413-427). These recent investigations make nitrogen dioxide an especially favorable example for establishing the reliability of electron diffraction measurements in the determination of potential constants. In order to better acquaint the reader with the structural history of nitrogen dioxide, some of the results referred to above are summarized in Table 1.

[^0]
## ELECTRON DIFFRACTION METHOD

## List of Symbols (In order of appearance in Part I of text)

n
$\lambda$
v

C

V
$\theta$
s

I(s) number of electrons scattered per unit solid angle per unit time.
number of electrons crossing unit area per unit time in the incident beam.
electronic mass.
electronic charge.
planck's constant.
atomic number
atomic scattering factor for $x$-rays.
$f_{i} \quad$ atomic scattering factor for electrons.

$$
\mathrm{f}_{\mathrm{i}}=(Z-F)_{\mathrm{i}} / \mathrm{s}^{2}
$$

$n_{i j}$
total number of atomic nuclei in the molecule. electron wavelength of the incident beam. velocity of the incident beam electrons. velocity of light in vacuum. electron accelerating voltage. one-half the scattering angle. electron diffraction variable. $s=4 \pi \lambda^{-1} \sin \theta$.
$\mathrm{m}_{\mathrm{e}}$
$\epsilon$
h

Z

F
the number of times the $i$, jth distance occurs in
the molecule.
$r_{i j}$
distance between ith and $j$ th atoms in the molecule as measured by electron diffraction. instantaneous distance between ith and jth atoms in the molecule.
equilibrium distance between ith and $j$ th atoms in the molecule.
root-mean-square vibrational amplitude corresponding to the $i$, jth distance. $l_{i j}=\left\langle\left(r_{i j}^{i}-r_{i j}^{e}\right)^{2}\right\rangle^{\frac{1}{2}}$.

S
incoherent scattering factor for $x$-rays tabulated by Bewilogua (4, p. 470-474) according to a theory of Heisenberg (18, p. 737-740).
$\eta_{i}$

```
            c'
```

c'
$r D(r)$
$r D^{\prime}(r)$
$\Delta s$
$r D^{\prime}(r) E_{x p}$
$r^{\prime}(r)$ Theor
$\mathrm{x}_{\mathrm{i}}$
$f\left(x_{1}, x_{2}, \ldots, x_{m}\right)$
N
m
$\mathrm{x}_{\mathrm{i}}^{0}$
$\mathrm{f}\left(\mathrm{x}_{1}^{\mathrm{o}}, \mathrm{x}_{2}^{\circ}, \ldots, \mathrm{x}_{\mathrm{m}}^{\mathrm{o}}\right)$
$\Delta \mathrm{x}_{\mathrm{i}}$
$\mathbb{F}_{\mathrm{N}} \quad$ matrix of function corresponding to adjusted values of parameters. $\mathbb{E}_{\mathrm{N}}=\mathbb{F}$.

| $\mathbf{F}_{\mathrm{N}}^{\circ}$ | matrix of function corresponding to trial values of parameters. $\quad \mathbf{F}_{\mathrm{N}}^{\circ}=\mathbf{F}^{\mathrm{o}}$. |
| :---: | :---: |
| ${ }^{A_{N m}}$ | matrix of derivatives. ${ }^{A_{N m}}=\mathbb{A}$. |
| $\overline{\mathrm{x}}_{\mathrm{m}}$ | matrix of corrections to trial values of para- |
|  | meters. $\overline{\mathrm{X}}_{\mathrm{m}}=\overline{\mathrm{X}}$. |
| $\mathbb{E}_{\mathrm{N}}^{\mathrm{Obs}}$ | matrix of observed values of function. $\mathbb{F}_{\mathrm{N}}^{\mathrm{Obs}}=\mathbb{F}^{\mathrm{Obs}}$. |
| $\mathbf{V}_{\mathrm{N}}$ | matrix of residuals. $\mathbf{N}_{N}=\mathbb{V}=\mathbb{F}_{N}-\mathbb{F}_{\mathrm{N}}^{\mathrm{Obs}}$. |
| $\mathbb{N}$ | $\mathbb{N}=\mathbb{F}^{\text {Obs }}-\mathbb{F}^{\circ}$. |
| $\mathbb{P}$ | diagonal weight matrix. |
| B | $\mathbb{B}=A^{\prime} \mathbb{P} \mathbb{A}$. |
| $\mathbb{Y}$ | $\boldsymbol{Y}=\mathbb{A} \cdot \mathbb{P} \mathbb{N}$. |
| ${ }^{\sigma}\left(\mathrm{x}_{\mathrm{i}}\right)$ | standard error in $\mathrm{x}_{\mathrm{i}}$. |
| $k^{\prime}$ | amplitude scale factor with respect to the |
|  | modified experimental intensity function. |
| b | arbitrary constant used in calculation of $\mathbb{P}$. |
| $\mathrm{x}_{\mathrm{T}}$ | linear distance on the microdensitometer trace, |
|  | measured from position of undiffracted beam. |
| $\mathrm{x}_{\mathrm{p}}$ | linear distance on photographic plate, measured |
|  | from position of undiffracted beam. |
| $I_{0}$ (dens) | intensity of incident microdensitometer light |
|  | beam. |
| I(dens) | intensity of transmitted microdensitometer light. |
| $\mu$ | light absorption coefficient. |


| D | photographic density. |
| :---: | :---: |
| $D^{\prime}$ | apparent photographic density determined from |
|  | amplified trace. |
| $\Delta \mathrm{D}_{1}$ | amplification correction to $\mathrm{D}^{\prime}$. |
| $\Delta \mathrm{D}_{2}$ | scale correction to $\mathrm{D}^{\prime}$. |
| $\mathrm{h}_{\mathrm{k}}$ | the kth camera distance (perpendicular distance |
|  | from photographic plate to scattering point); |
|  | $\mathrm{k}=\mathrm{a}, \mathrm{b}$, and c denotes 478.00, 192.07 and |
|  | $120.00 \mathrm{~mm} .$, respectively. |
| $\delta$ | blackness correction. |
| $\gamma$ | proportionality constant related to the blackness |
|  | correction. |
| $I_{p}(s)$ | electron intensity incident on a flat photographic |
|  | plate mounted perpendicular to the direction |
|  | of the undiffracted electron beam. |
| t | exposure time. |
| E | exposure. |
| $I_{p}^{\mathrm{k}(\mathrm{i})}$ | $I_{p}(s)$ function from the ith plate at the kth camera |
|  | distance. |
| $I_{p}^{k}(s)$ | composite $I_{p}(s)$ function from the kth camera |
|  | distance. |
| $\mathrm{r}_{5}$ | radius on the sector measured from the undif- |
|  | fracted beam position. |

$\rho \quad$ proportionality factor related to the sector calibration (nearly constant except at small scattering angles).
$a\left(r_{s}\right)$ angular opening of the sector. sector function.
total scattered intensity per unit solid angle corresponding to the kth camera distance. experimental background function corresponding to the kth camera distance. molecular intensity function corresponding to the kth camera distance.
composite molecular intensity function from the three camera distances.
$t(s)$
$\mathrm{t}(\mathrm{s})=\mathrm{I}_{\mathrm{p}}^{\mathrm{a}}(\mathrm{s}) /\left[\mathrm{I}_{\mathrm{p}}^{\mathrm{a}}(\mathrm{s})+\mathrm{I}_{\mathrm{p}}^{\mathrm{b}}(\mathrm{s})\right]$
$u(s)$
$u(s)=I_{p}^{b}(s) /\left[I_{p}^{a}(s)+I_{p}^{b}(s)\right]$
$\mathrm{v}(\mathrm{s})$
$\mathrm{v}(\mathrm{s})=\mathrm{I}_{\mathrm{p}}^{\mathrm{b}}(\mathrm{s}) /\left[\mathrm{I}_{\mathrm{p}}^{\mathrm{b}}(\mathrm{s})+\mathrm{I}_{\mathrm{p}}^{\mathrm{c}}(\mathrm{s})\right]$
w (s)
$I_{E}^{T}(s) E_{x p}$
$\mathrm{w}(\mathrm{s})=\mathrm{I}_{\mathrm{p}}^{\mathrm{c}}(\mathrm{s}) /\left[\mathrm{I}_{\mathrm{p}}^{\mathrm{b}}(\mathrm{s})+\mathrm{I}_{\mathrm{p}}^{\mathrm{c}}(\mathrm{s})\right]$
experimental modified molecular intensity function (composite) from the three camera distances.
$I_{E}^{T}(s)$ Theor $I_{E}^{k}\binom{i}{s}$
$I_{E}(s)$ function from the ith plate at the kth camera distance.

```
I
    composite I }\mp@subsup{I}{E}{(s) function from the kth camera distance. amplitude scale factor with respect to experimental radial distribution functions \(\left(r D^{\prime}(r)_{E x p}\right)\).
error matrix derived from least-squares refinement.
\(\bar{s}^{2}=\mathbb{V} \cdot \mathbb{P} \mathbf{V} /\left(\mathbb{N}-\mathrm{mi}^{2}\right)\).
X matrix of parameters actually adjusted by leastsquares (includes interactomic distances and vibrational amplitudes).
U matrix of parameters of interest (includes interatomic distances, bond angle and vibrational amplitudes).
D matrix of coefficients transforming \(X\) to \(U\). \(\mathbf{U}=\mathbb{D} \mathbf{X}\).
\(a^{\prime}\)
\(\mathrm{a}^{\prime}=\mathrm{a}(<\mathrm{O}-\mathrm{N}-\mathrm{O}) / \partial \mathrm{r}_{\mathrm{N}-\mathrm{O}}=-\mathrm{r}_{\mathrm{O}} \ldots \mathrm{O}^{/ \mathrm{r}_{\mathrm{N}-\mathrm{O}}^{2} \cos }\) ( \(<\mathrm{O}-\mathrm{N}-\mathrm{O} / 2\) ).
\(b^{\prime}\)
\[
\begin{aligned}
\mathrm{b}^{\prime}= & \partial(<\mathrm{O}-\mathrm{N}-\mathrm{O}) / \partial \mathrm{r}_{\mathrm{O}} \ldots \mathrm{O}=\left[\mathrm{r}_{\mathrm{N}}-\mathrm{O} \cos \right. \\
& (<\mathrm{O}-\mathrm{N}-\mathrm{O} / 2)]^{-1} .
\end{aligned}
\]
\(\sigma_{i} \operatorname{LS} \quad\) same as \(\sigma\left(x_{i}\right)\)
```

$\sigma_{2}\left(x_{j}\right) \quad$ standard error derived from variations in the most probable parameters as obtained from the individual photographic plates at a given camera distance. most probable parameters obtained from leastsquares analysis of the ith plate at 478.00 mm . most probable parameters obtained from leastsquares analysis of the ith plate at 192.07 mm . most probable parameters obtained from leastsquares analysis of the 478.00 mm composite. most probable parameters obtained from leastsquares analysis of the 192.07 mm composite. $\left.\sigma_{2}^{\mathrm{a}(\mathrm{i})} \mathrm{x}_{\mathrm{j}}\right)$ variation in the interatomic distances and vibrational amplitudes derived from the ith plate at the 478.00 mm camera distance. $\sigma_{2}^{b(i)}\left(x_{j}\right)$ variation in the interatomic distances and vibrational amplitudes derived from the ith plate at the 192.07 mm camera distance.
$\sigma_{2}(<\mathrm{O}-\mathrm{N}-\mathrm{O}) \quad$ same as $\sigma_{2}\left(\mathrm{x}_{\mathrm{j}}\right)$ where the parameter is the bond angle.
$\sigma_{\mathrm{T}}\left(\mathrm{x}_{\mathrm{j}}\right) \quad$ overall standard error in the parameter $\mathrm{x}_{\mathrm{j}}$.

## Scattering Theory

Since scattering theory applicable to gaseous electron diffraction has been presented by many authors (8, p. 231-239; 13, p. 667$671 ; 39$, p. 19-199), there seems to be no need for more than a brief summary here.

In investigations of the structure of free molecules by gaseous electron diffraction, high velocity electrons ${ }^{1}$ are used. The information obtained includes only the number (roughly) and magnitudes of interatomic distances, and their corresponding vibrational amplitudes.

Scattering theory for gaseous electron diffraction is developed by first considering the elastically scattered electrons, and then the aggregate effect of all the various kinds of inelastic scattering.

In the case of elastic scattering, a single atom is treated and then an array of atoms having fixed relative positions (a molecule). In this treatment, a single atom is represented by a small, spherically symmetrical region (a central force field) in which the potential energy of the scattered electrons is different from zero. The distribution of the scattered electrons is assumed to be observed at large
${ }^{1}$ Operating voltages fall in the range of $30-50$ kilovolts. For example, if $\lambda$ is equal to $0.06458 \mathrm{~A}^{\circ}$, one finds by calculation that $\mathrm{v} / \mathrm{c}$ and V are equal to 0.352 and 34.9 kilovolts, respectively.
distances from the atom, and an asymptotic solution is sought. An important approximation often utilized in this treatment is due to Born (39, p. 116-126), and amounts to an assumption that inside the atom the amplitude of the incident wave is much greater than that of the scattered wave. Further, it is assumed that no phase shift occurs in the scattering process. The solution for a molecule, obtained by summing the scattered waves due to the atoms, is averaged over all possible orientations in order to account for the random phase relations between the waves scattered by different molecules.

Unfortunately, in the case of inelastic scattering a reasonably rigorous theory is still lacking. Therefore, in lieu of treating the aggregate effect of the inelastic scattering by molecules, the atoms are treated separately and then summed over.

The result of these considerations for the intensity of scattering per unit solid angle is

$$
\begin{align*}
& I(s)=I_{0}\left(8 \pi^{2} m_{e} e^{2} / h^{2}\right)^{2}\left(\sum_{i, j}^{\prime} n_{i j} f_{i} f_{j}\left(s r_{i j}\right)^{-1} \sin \left(s r_{i j}\right) \exp \left(-l_{i j} s^{2} / 2\right)\right. \\
&\left.+\sum_{i} f_{i}^{2}+\sum_{i} S_{i} s^{-4}\right) \tag{I,l}
\end{align*}
$$

Equation (I, l) is valid in the approximation of harmonic molecular vibrations. The first term on the right-hand side is the molecular structure sensitive part of the total scattered intensity. It can be

[^1]more generally written as
\[

$$
\begin{equation*}
I_{o}\left(8 \pi^{2} m_{e} \epsilon^{2 /} h^{2}\right)^{2} \sum_{i, j}^{l} n_{i j} f_{i} f_{j} \cos \left|\eta_{i}-\eta_{j}\right| M(s)\left(s r_{i j}\right)^{-1} \sin \left(s r_{i j}\right) \tag{I,2}
\end{equation*}
$$

\]

where $\cos \left|\eta_{i}-\eta_{j}\right|$ denotes the phase shift (13, p. 667-671) which was assumed to be unity in the Born approximation, and $M(s)$ is some function expressing the effect of a more general type of molecular vibration.

Principles of Structural Determination

Several methods are currently in use for elucidation of structural information from gaseous diffraction data. All of these begin, essentially, with the diffraction data in a form assumed to be described by an analytical function such as equation (I, l) or (I, 2) or a convenient modification of them. The process by which the experimental data (the photographic blackening) is converted into the desired form is termed "data reduction" and will be described later in connection with the nitrogen dioxide work. The data in the chosen form may be called the "experimental intensity curve" or "function," or the "radial distribution curve" or "function," the latter being the Fourier sine transform of some experimental intensity curve. Each of these types of curves has advantages. Some investigators prefer to work almost entirely with radial distribution curves, fitting theoretical curves to the experimental one, often by least-squares
techniques (7, p. 705-708); others use radial distribution curves in the early stages of an investigation, and refine the parameters by least-squares fitting based on intensity curves (17, p. 529-533; 24, p. 533-537). The latter approach was used in this thesis work. The radial distribution method was employed for the purpose of obtaining approximate values of the structural parameters, and these approximate values were then used as starting values in a least-squares refinement based on intensity curves.

The concluding portion of this section will be devoted to a brief discussion of the radial distribution method (44, p. 671-690) and of least-squares applied to electron diffraction intensity curves (17, p. 529-533; 24, p. 533-537).

## Radial Distribution Method

It is convenient to use the following molecular intensity function

$$
\begin{equation*}
I_{E}(s)=\sum_{i, j}^{\prime} n_{i j} r_{i j}^{-1} A_{i j}(s) \exp \left(-1{ }_{i j}^{2} s^{2} / 2\right) \sin \left(s r_{i j}\right) \tag{I,3}
\end{equation*}
$$

Further, it is convenient for the initial discussion to treat the $A_{i j}$ 's as constants.

In order to gain some insight as to the appearance of the distance spectrum for a molecule, it suffices to treat the contribution of a single ${ }^{l} i, j$ pair to $I_{E}(s)$. Consider the integral

[^2]\[

$$
\begin{gather*}
\int_{0}^{\infty}\left[I_{E}(s)\right]_{i j} \sin (r s) d s=c^{\prime} \int_{0}^{\infty} \exp \left(-11_{i j}^{2} s^{2} / s\right) \sin \left(r_{i j} s\right) \\
x \sin (r s) d s \tag{I,4}
\end{gather*}
$$
\]

Using the trigonometric identity

$$
\begin{equation*}
\sin x \sin y=2^{-1}[\cos (x-y)-\cos (x+y)] \tag{I,5}
\end{equation*}
$$

the right-hand side of equation ( $I, 4$ ) can be written as

$$
\begin{align*}
& c^{\prime} / 2 \int_{0}^{\infty} \exp \left(-1 i j s^{2} / 2\right) \cos \left[\left(r-r_{i j}\right) s\right] d s \\
& \quad-c^{\prime} / 2 \int_{0}^{\infty} \exp \left(-1{ }_{i j} s^{2} / 2\right) \cos \left[\left(r+r_{i j}\right) s\right] d s . \tag{I,6}
\end{align*}
$$

Evaluating (I, 6) by standard methods, it is found that

$$
\begin{align*}
\int_{0}^{\infty}\left[I_{E}(s)\right]_{i j} \sin (r s) d s= & {\left[c^{\prime \prime} / l_{i j}(2 \pi)^{1 / 2}\right]\left[\exp \left(-\left(r-r_{i j}\right)^{2} / 21 i_{i j}^{2}\right)\right.} \\
& \left.-\exp \left(-\left(r+r_{i j}\right)^{2} / 21_{i j}^{2}\right)\right] \tag{I,7}
\end{align*}
$$

It is clear that the second exponential term can be neglected with respect to the first one, so that

$$
\begin{align*}
\int_{0}^{\infty}\left[I_{E}(s)\right]_{i j} \sin (r s) d s \simeq & {\left[c^{\prime \prime} / 1_{i j}(2 \pi)^{1 / 2}\right] } \\
& \times \exp \left[-\left(r-r_{i j}\right)^{2} / 21_{i j}^{2}\right] \tag{I,8}
\end{align*}
$$

The right-hand side of equation ( $I, 8$ ) is seen to be the normal
Gaussian distribution. Each i, j pair in the molecule will make such a contribution and hence the curve representing the entire distance spectrum will be composed either of distinct Gaussian peaks (one for each $i, j$ pair in the molecule), or when two or more $r_{i j}$ 's are approximately equal in magnitude, of composites of Gaussian peaks.

Letting $r \mathrm{D}(\mathrm{r})$ represent the theoretical radial distribution function [in the literature, $\sigma(r) / r$ is often used to denote $4 \pi r D(r)$ ], it is clear from the preceding that $I_{E}(s)$ can be written as ${ }^{1}$

$$
\begin{equation*}
I_{E}(s)=(2 / \pi)^{1 / 2} \int_{0}^{\infty} r D(r) \sin (s r) d r \tag{I,9}
\end{equation*}
$$

In the derivation of equation (I. 7), the $A_{i j}{ }^{\prime}$ s were assumed to be independent of $s$. Since this is not usually the case, all but one of the peaks ${ }^{2}$ in the theoretical radial distribution function will be slightly distorted from the ideal Gaussian form. Further distortion results from anharmonic instead of harmonic vibrations.

In practice, $\mathrm{I}_{\mathrm{E}}(\mathrm{s})$ as obtained experimentally is rarely available outside of the range $2 \leq s \leq 60$. The effect of not evaluating the integral in equation ( $I, 9$ ) over the whole range in which the integrand is different from zero is the introduction of ripples (diffraction rings) in the experimental $r D(r)$ curve, which, of course, cortributes to skewing of the true peaks. For this reason, the factor $\exp \left(-a s^{2}\right)$, often referred to as the artificial temperature factor, is usually introduced in the integrand to compensate for the finite upper limit, and the experimental radial distribution curve takes the form

[^3]\[

$$
\begin{equation*}
r D^{\prime}(r)=\sum_{s(\min )}^{s(\max )} I_{E}(s) \exp \left(-a s^{2}\right) \sin (r s) \Delta s \tag{I,10}
\end{equation*}
$$

\]

where the integral has been replaced by a summation. The finite lower limit is often handled by the introduction of a theoretical intensity curve in the interval from zero to $s(\min )$. Further, since $I_{E}(s)$ is usually obtained experimentally at a constant $\Delta s$ interval, $\Delta s$ can be factored out of the summation and the equation actually used for evaluating $r D^{\prime}(r)$ is

$$
r D^{\prime}(r) E_{\operatorname{Exp}}=\sum_{s=0}^{s(\max )} \mathrm{I}_{\mathrm{E}}(\mathrm{~s}) \exp \left(-a s^{2}\right) \sin (\mathrm{rs})
$$

The theoretical radial distribution curve corresponding to $r D^{\prime}(r) E_{x p}$ can be calculated from the expression

$$
\begin{align*}
& r D^{\prime}(r)_{\text {Theor }}=\sum_{i, j}^{\prime} n_{i j} Z_{i} Z_{j}\left(r_{i j}\right)^{-1}\left(11_{i j}^{2}+2 a\right)^{-1 / 2}  \tag{I,12}\\
& x \exp \left[-\left(r-r_{i j}\right)^{2} / 2\left(1_{i j}^{2}+2 a\right)\right]
\end{align*}
$$

Least-Squares Method

The problem of refinement by least-squares based on intensity curves is that of fitting a theoretical curve (which is a function of the molecular parameters) to an appropriate experimental curve. Since the adjustment is linear only for small ranges of parameter changes, it is necessary to have fairly good starting parameter values. As indicated earlier, such a starting model can be obtained from the
$r D^{\prime}(r) \operatorname{Exp}$ curve.
The principles of least-squares curve-fitting in matrix form will be summarized in the following. Suppose $f\left(x_{1}, x_{2}, \cdots, x_{m}\right)$ is a non-linear function representing a curve which consists of N experimental data. If approximate values for $x_{1}, x_{2}, \cdots, x_{m}$ are known, $f\left(x_{1}, x_{2}, \cdots, x_{m}\right)$ may be expanded as

$$
\begin{equation*}
f\left(x_{1}, x_{2}, \cdots, x_{m}\right)=f\left(x_{1}^{o}, x_{2}^{o}, \cdots, x_{m}^{o}\right)+\sum_{i=1}^{m}\left(\frac{\partial f}{\partial x_{i}}\right){ }_{o} x_{i} \tag{I,13}
\end{equation*}
$$

We have N such equations corresponding to the N observed points. If matrix notation is introduced,

$$
\begin{equation*}
\mathbb{F}_{\mathrm{N}}=\mathbb{E}_{\mathrm{N}}^{\circ}+\mathbb{A}_{\mathrm{N}_{\mathrm{m}}} \bar{X}_{\mathrm{m}} \tag{I,13'}
\end{equation*}
$$

equation ( $1,13^{\prime}$ ) is usually referred to as the conditional equations. Since $\mathbb{F}_{N}$ and $\mathbb{F}_{N}^{O b s}$ differ by $\mathbb{V}_{N}$, equation (I, 13') gives (dropping subscripts)

$$
\begin{align*}
\mathbb{E}^{\mathrm{Obs}}+\mathbb{V} & =\mathbb{E}^{0}+\mathbb{A} \overline{\mathbf{X}}  \tag{I,14}\\
\mathbf{V} & =\mathbb{E}^{0}-\mathbb{F}^{\mathrm{Obs}}+\mathbb{A} \overline{\mathbf{X}}  \tag{I,15}\\
& =-\mathbb{N}+\mathbb{A} \overline{\mathbf{X}} \tag{I,15'}
\end{align*}
$$

The least-squares criterion may be expressed as

$$
\begin{equation*}
\mathbb{V}^{\prime} \mathbb{P} \mathbb{V} \rightarrow \text { minimum }, \tag{I,16}
\end{equation*}
$$

from which one finds

$$
\begin{equation*}
(\partial / \partial \bar{X})(\mathbb{V} ' \mathbb{P} \mathbb{V})=\mathbb{A}^{\prime} \mathbb{P} \mathbb{V}=0 \tag{I,17}
\end{equation*}
$$

Combination of equations ( $I, 15^{\prime}$ ) and ( $I, 17$ ) give the normal equations

$$
\begin{equation*}
\mathbb{B} \bar{X}=\mathbb{Y} \tag{I,18}
\end{equation*}
$$

where

$$
\begin{equation*}
\mathbb{B}=\mathbb{A}^{\prime} \mathbb{P} \mathbb{A} \tag{I,19}
\end{equation*}
$$

and

$$
\begin{equation*}
\mathbf{Y}=\mathbb{A}^{\prime} \mathbb{P} \mathbb{N} . \tag{I,20}
\end{equation*}
$$

The solutions are

$$
\begin{equation*}
\bar{X}=\mathbb{B}^{-1} \mathbb{Y}, \tag{I,21}
\end{equation*}
$$

and the standard errors are

$$
\begin{align*}
\sigma\left(x_{i}\right) & =\left[\left(\mathbb{B}^{-1}\right)_{i i} \mathbb{N} \cdot \mathbb{P} \mathbb{V} / \mathbb{N}-m\right]^{\frac{1}{2}}  \tag{I,22}\\
& \left.=\left[\left(\mathbb{B}^{-1}\right)_{i i}\left(\mathbb{N}^{\prime}: \mathbb{P} \mathbb{N}-\overline{X^{\prime}} \cdot \mathbb{Y}\right) / \mathbb{N}-m\right)\right]^{\frac{1}{2}} \tag{I,23}
\end{align*}
$$

In the case of electron diffraction, $f\left(x_{1}, x_{2}, \cdots, x_{m}\right)$ may be identified with an intensity function, say $I_{E}(s)$, the parameters of which are $k^{\prime}$ (scaling factor), some of the $r_{i j} ' s$, and the $l_{i j}$ 's. Therefore, the columns of the $\mathbb{A}$ matrix are $\partial I_{E} / \partial k^{\prime}, \partial I_{E} / \partial r_{i j}, \cdots$, $\partial \mathrm{I}_{\mathrm{E}} / \partial \mathrm{r}_{\mathrm{kl}}, \partial \mathrm{I}_{\mathrm{E}} / \partial \mathrm{l}_{\mathrm{ij}}, \cdots, \partial \mathrm{I}_{\mathrm{E}} / \partial \mathrm{l}_{\mathrm{kl}}$, et cetera. The elements of the diagonal weight matrix, $\mathbb{P}$, are often calculated using the analytical expression

$$
\begin{equation*}
(\mathbb{P})_{i i}=\text { const } s_{i} \exp \left(-b s_{i}^{2}\right) \tag{I,24}
\end{equation*}
$$

which simply reflects general experience regarding the quality of the data.

## DETERMINATION OF MOLECULAR STRUCTURE

## Experimental

The electron diffraction photographs of gaseous nitrogen dioxide were taken with the Oslo sector apparatus (3, p. 232-238); the electron source being a hot cathode gun similar to that used in electron microscopes [see (14, p. 40-46; 20, p. 12-22) for discussions relating tothe performance characteristics of such electron guns and the general problem of resolution in electron diffraction cameras, respectively].

The preparation of the nitrogen dioxide sample proceeded essentially as follows. Powdered $\mathrm{Pb}\left(\mathrm{NO}_{3}\right)_{2}$ was dried at temperatures ranging from $110^{\circ}$ to $120^{\circ} \mathrm{C}$. The powder was then transferred to a pyrex tube and slowly heated in the presence of a stream of $\mathrm{O}_{2}$. The reaction proceeds according to the equation

$$
\begin{equation*}
2 \mathrm{~Pb}\left(\mathrm{NO}_{3}\right)_{2} \rightarrow 2 \mathrm{PbO}_{(\mathrm{s})}+4 \mathrm{NO}_{2(\mathrm{~g})}+\mathrm{O}_{2(\mathrm{~g})} \tag{I,25}
\end{equation*}
$$

The water vapor liberated during the heating process was condensed with a cold trap ( $5^{\circ}-20^{\circ} \mathrm{C}$ ). The nitrogen dioxide was passed over $\mathrm{PbO}_{2}$ and $\mathrm{Pb}_{2} \mathrm{O}_{5}$, and condensed in a dry ice bath. Finally, the nitrogen dioxide was purified by distillation.

Several photographic plates (Kodak B-40 lantern slide plates) were exposed at each of the three camera distances, $478.00,192.07$
and 120.00 mm , from which four plates per distance were subsequently selected for analysis (twelve plates in all); the exposure times ranged from about one-half minute to five minutes in duration.

The average nozzle temperature and electron wavelength for each of the runs were determined as $107^{\circ} \mathrm{C}$ and $0.06458 \AA$, respectively. The temperatures were read from a thermocouple placed in contact with the input gas nozzle a short distance from the tip. The wavelength associated with the electron beam was determined in separate experiments by diffraction from gold foil (8, p. 242).

The rotating sector, which must be used to even out the steeply falling background for photographic purposes, was spiral in shape (with a maximum radius of approximately 11 cm ) such that its angular opening was proportional to the cube of the radius save for very small $s$ values where the opening was larger in order to give a more uniform background. ${ }^{l}$ The mounting of the sector in the diffraction chamber was such that its rotational axis (perpendicular to the plane of the sector) coincided with the direction of the undiffracted electron beam; the distance between sector and photographic plate was approximately 16 mm . The sector described above acted effectively as an $\mathrm{s}^{3}$ screen (for the better part of the s range), which tended to offset the characteristic inverse square fall-off of intensity with distance from the
${ }^{1}$ Such a sector is usually referred to as an "r ${ }^{3}$ sector."
scattering point, and therefore, to accentuate the oscillating features of the diffraction pattern. In other words, without a sector, the photographic plate would be over exposed at smalls values and under exposed at large s values.

## Data Reduction

Though it is usual to refer to the experimental diffraction curve as that which corresponds to a suitable molecular intensity function, it is only the information contained on the photographic plates which can be properly referred to as the experimental data. The microdensitometery of the plates and the various mathematical operations performed on the experimental data, eventually leading to the isolation of a suitable molecular intensity function, constitute the data reduction process.

Exposed photographic plates from gaseous electron diffraction show well-defined rings such that as the scattering angle increases, the blackening of the photographic emulsion appears to pass through successive maximum and minimum values. It has been pointed out (41, p. 868) that these maxima and minima are not real, but correspond to small fluctuations in the density superimposed on a monotonically falling background (see discussion of sector).

The photographic plates from the nitrogen dioxide experiments were traced with a Leeds and Northrup recording microdensitometer
along a direction corresponding to a ring diameter, chosen to be as free as possible from photographic defects. During the tracing, the plates were oscillated about their centers in order to average out emulsion irregularities arising from graininess. This was accomplished by mounting a plate on an oscillating device which itself was mounted on the microdensitometer carriage. Since the diffraction pattern on the photographic plate was radially symmetric, the corresponding microdensitometer tracing consisted of two branches (left and right branch) separated by a narrow region corresponding to the position of the beam stop image which coincided with that of the undiffracted beam.

In practice, two traces corresponding to two different microdensitometer carriage speeds and amplifier gains ${ }^{1}$ were actually made of a given plate. The slower carriage speed and higher amplifier gain had the advantage of spreading out and magnifying the individual undulations and hence facilitating the reading off of the photographic densities. The traces clearly showed the desired broad maxima and minima, which became progressively weaker as the scattering angle increased, and less easy to detect in the presence of the low level

[^4]noise present in the traces. In addition to this noise, occasional spike-like absorption minima (equivalent to transmission maxima) occurred in the traces and were credited to dust on the surface of the photographic plate during the diffraction experiment and to emulsion defects.

The procedure employed in reading photographic densities from a trace involved the following steps.

First, a continuous smooth pencil line was drawn on each branch of a trace in an attempt to visually average out the effect of noise in the recorded signal. When the spikes described above were encountered, the line was drawn so as to correspond to the curvature of the trace on each side of the spike. A center line corresponding to zero scattering angle was then located on the amplified trace by averaging the center positions between corresponding maxima and minima on each of the two branches. The effective position of a given maximum or minimum was located by constructing tangents to the peak (one on the up side and one on the down side), and then locating the point of intersection of the se two tangents. This tangent technique was also employed in locating the effective peak positions on the unamplified trace.

Second, an s scale, graduated in one-quarter s units, was
placed along the bottom of the amplified trace. ${ }^{l}$ Since the amplified trace was recorded at a chart speed greater than that of the corresponding carriage speed, it was necessary to relate distances on the amplified trace to those on the plate. This was done by simply tracing an accurately calibrated, etched glass scale under the same conditions used with the diffraction plates. The result (often called the 'paper factor') was $x_{T} / x_{P}=5.2350$. The value of the paper factor actually used in calculating the $\mathrm{x}_{\mathrm{T}}$ 's was 5.2415 , which was the value determined from the calibration trace in the Oslo laboratory before mailing to Oregon. The discrepancy between these two values was probably due to shrinkage of the chart paper caused by differences in humidity. This discrepancy was eventually taken account of by multiplying the final distance parameters of nitrogen dioxide by the factor $1.0012=5.2415 / 5.2350$. A correction to the mean amplitudes is also required in principle, however it is so small in value that it was neglected. ${ }^{2}$
${ }^{1}$ Since there were two branches per trace, each trace required two s scales using the previously determined center line as a common zero point relative to s. Obviously, the s scales differed in spacing and range for the different camera distances.
${ }^{2}$ For example the correction is about $2 \times 10^{-6} \AA$ for $1(\mathrm{~N}-\mathrm{O})$ :

$$
\begin{aligned}
& I \propto I_{o} \exp \left(-1^{2} s^{2} / 2\right) \\
& 0=-s^{2} \mathrm{dl}-\mathrm{sl}^{2} \mathrm{ds} \\
& \mathrm{dl}=-\mathrm{l}^{2}(\mathrm{ds} / \mathrm{s})=-(0.038)^{2}\left(1.2 \times 10^{-3}\right)
\end{aligned}
$$

The third and final step of this procedure involved the actual reading of the photographic densities from the microdensitometer traces. Since the absorption of light by the photographic emulsion follows the exponential law

$$
\begin{equation*}
I(\text { dens }) / I_{0}(\text { dens })=\exp (-\mu D) \tag{I,26}
\end{equation*}
$$

it was convenient to use a logarithmically scaled "T" square to read the photographic densities from the traces. The scale of the "T" square was in density units,

$$
\begin{equation*}
D=\log \left[I_{0}(\text { dens }) / I(\operatorname{dens})\right] \tag{I,27}
\end{equation*}
$$

with the zero and infinity points at positions corresponding to the edges of the chart paper. It was necessary, of course, to scale the readings obtained from the amplified trace to the actual densities (D) as defined in equation ( $\mathrm{I}, 26$ ). Further, since the functional relationship of exposure (scattered electron intensity x time) ${ }^{1}$ and density is known, a determination of the desired scattered electron intensity is possible. The scaling procedure was as follows. The only essential difference between the unamplified and amplified traces was that of amplifier gain. Clearly one correction to the apparent density (as read from the amplified trace) must consist of determining the increased amplification of the amplified trace in "T" square density units. This was accomplished by measuring the average difference
${ }^{1} E=I t$ is termed the reciprocity law.
in readings between corresponding maxima and minima on the unamplified and amplified traces, and then adding this term to the apparent density reading of the amplified trace. A second minor correction term was also necessary because of slight differences between the scale of the " T " square and the 0 to 100 percent transmission scale of the unamplified traces. This term was either subtracted or added to the apparent density described above, depending on whether the 100 percent transmission line of the "T" square fell above or below that of the unamplified trace.

An algebraic formulation of this procedure is as follows (see Figure 1 for the meaning of the various symbols). Let

$$
\begin{equation*}
D=\log \left[I_{o}^{\prime}(\text { dens }) / I^{\prime}(\text { dens })\right]=\log \left[I_{0}^{\prime \prime}(\text { dens }) / I^{\prime \prime}(\text { dens })\right] \tag{I,28}
\end{equation*}
$$

and

$$
\begin{equation*}
D^{\prime}=\log \left[I_{0}(\text { dens }) / I^{\prime}(\text { dens })\right] \tag{I,29}
\end{equation*}
$$

then

$$
\begin{equation*}
\Delta \mathrm{D}=\mathrm{D}-\mathrm{D}^{\prime}=\log \left[\mathrm{I}_{\mathrm{o}}^{\prime}(\operatorname{den} s) / I^{\prime}(\operatorname{den} s)\right]-\log \left[I_{\mathrm{o}}(\operatorname{den} s) / I^{\prime}(\operatorname{den} s)\right] \tag{I,30}
\end{equation*}
$$

or

$$
\begin{equation*}
\Delta D=\log \left[I_{0}^{\prime \prime}(\text { dens }) / I^{\prime \prime}(\text { dens })\right]-\log \left[I_{0}(\text { den } s) / I^{\prime}(\text { dens })\right] \tag{I,30'}
\end{equation*}
$$

Rearrangement of equation ( $\mathrm{I}, 30^{\prime}$ ) yields

$$
\begin{equation*}
\Delta D=\log \left[I^{\prime}(\operatorname{den} s) / I^{\prime \prime}(\operatorname{den} s)\right]-\log \left[I_{0}(\operatorname{den} s) / I_{o}^{\prime \prime \prime}(\operatorname{den} s)\right] \tag{I,31}
\end{equation*}
$$

where

$$
\begin{align*}
\log \left[I^{\prime}(\text { dens }) / I^{\prime \prime}(\text { dens })\right]= & \log \left[I_{o}(\text { dens }) / I^{\prime \prime}(\text { dens })\right] \\
& -\log \left[I_{0}(\text { dens }) / I^{\prime}(\text { dens })\right] \tag{I,32}
\end{align*}
$$

Letting $\Delta D_{1}=\log \left[I^{\prime}(\right.$ dens $) / I^{\prime \prime}($ dens $\left.)\right]$ and $\Delta D_{2}=\log \left[I_{o}\left(\right.\right.$ dens $/ I_{o}^{\prime \prime \prime}($ dens $\left.)\right]$, then

$$
\begin{equation*}
\Delta \mathrm{D}=\Delta \mathrm{D}_{1}-\Delta \mathrm{D}_{2} \tag{I,33}
\end{equation*}
$$

or

$$
\begin{equation*}
D=D^{\prime}+\Delta D_{1}-\Delta D_{2} . \tag{I,34}
\end{equation*}
$$

$\Delta D_{1}$ and $\Delta D_{2}$ may be identified with the first and second corrections, respectively, as discussed in the previous paragraph.

The recorded diffraction patterns covered the following scattering ranges:

$$
\begin{aligned}
& h_{\mathrm{a}} ; 2.50 \leq \mathrm{s} \leq 20.75 \\
& \mathrm{~h}_{\mathrm{b}} ; 10.25 \leq \mathrm{s} \leq 42.00 \\
& \mathrm{~h}_{\mathrm{c}} ; 18.50 \leq \mathrm{s} \leq 49.75 .
\end{aligned}
$$

Following the reading of the densities from the plates, as described above, the densities were corrected for non-linearity of photographic response according to the relation ${ }^{1}$

$$
\begin{equation*}
I_{p}=\gamma(D+\delta) \tag{I,35}
\end{equation*}
$$

The values of $\delta$ actually used in this work (see Table 10) were obtained from the Oslo laboratory. ${ }^{2} \delta$ was taken as zerofor $D<0.62$,
${ }^{1}$ The proportionality constant $\gamma$ (in units of reciprocal time) was arbitrarily taken as unity.
${ }^{2}$ The Oslo calibration of photographic densities with electron intensities was based on a series of investigations extending over a period of some fourteen years, employing the procedure developed by Karle and Karle (27, p. 961).
for densities less than this value, the density-exposure curve was found to be linear. All twelve of the photographic plates used we re sufficiently light in exposure that only data occurring in the following scattering ranges were actually blackness corrected: ${ }^{1}$

$$
\begin{aligned}
& h_{b} ; \quad 10.25 \leq s \leq 18.00 \\
& h_{c} ; \quad 18.50 \leq s \leq 35.00 .
\end{aligned}
$$

The relevancy of this fact will be seen later in the discussion of uncertainties in the final mean square vibrational amplitudes.

As a check on the Oslo blackness correction, a blackness correction was constructed in this laboratory using two plates made at the 478 mm distance. As in the Oslo correction, the method of Karle and Karle (27, p. 961) was employed in this analysis. The applicability of this method rests on the validity of the reciprocity law

$$
\begin{equation*}
E=I t \tag{.1,36}
\end{equation*}
$$

for fast electrons. From equation (I. 36), it is seen that it is possible to interpret the difference in two exposures as due to differences in electron intensity at constant time. This interpretation, combined with the assumption that D is proportional to I for $\mathrm{D} \leq 0.25$ (for contrast lantern slide plates), constitute the basis of the method.

A comparison of the two corrections (Oregon and Oslo)
${ }^{l}$ The 478 mm plates did not require blackness correcting.
indicated that $\delta$ (Oregon) was somewhat greater than $\delta$ (Oslo) [for example, $\delta($ Oregon $)-\delta($ Oslo $) \simeq 0.010$ density units at $D=0.480]$. This difference may or may not be significant; but because the two plates used in deriving the Oregon correction did not differ quite enough in density for optimal results, and because the blackness correction in any event was not great, it was decided to use the Oslo correction.

The $I_{p}(s)$ (or D) data (see Tables 2, 3, and 4) were plotted on large-scale graph paper in order to locate possible reading errors. A composite function for each of the camera distances was then obtained by summing the $I_{p}$ data from each of the four plates at corresponding points of $s$ :

$$
\begin{equation*}
I_{p}^{k}(s)=\sum_{i=1}^{4} I_{p}^{k(i)}(s) \tag{I,37}
\end{equation*}
$$

This composite intensity function is related to the total scattered intensity per unit solid angle $\left[I_{t}^{k}(s)\right]$ by the equation

$$
\begin{equation*}
I_{p}^{k}(s)=I_{t}^{k}(s) g(\theta) \tag{I,38}
\end{equation*}
$$

where $g(\theta)$ incorporates the effect of the sector and that of using a flat plate perpendicular to the undiffracted beam instead of a cylindrical film with an axis perpendicular to the undiffracted beam and a surface everywhere equidistant from the scattering point. Recalling the screening effect of the rotating sector, it is clear that one part of $g(\theta)$ will take the form $a\left(r_{s}\right)=\rho r_{s}^{3}$. The second factor of $g(\theta)$ is
$\cos ^{3} 2 \theta$. Two powers of this factor are derived from the inverse fall-off of intensity with distance from the scattering point, and one power from the angle of inclination of the element of area on the flat plate with respect to the scattered electron rays striking it. Equation $(1,38)$ thus becomes

$$
\begin{equation*}
I_{t}^{k}(s)=I_{p}^{k}(s) / a\left(r_{s}\right) \cos ^{3} 2 \theta \tag{I.39}
\end{equation*}
$$

For the purpose of extracting the molecular sensitive part of the scattered intensity, it is convenient to multiply both sides of equation (I, 39) by $s^{4}$, giving

$$
\begin{equation*}
s^{4} I_{t}^{k}(s)=s^{4} I_{p}^{k}(s) / a\left(r_{s}\right) \cos ^{3} 2 \theta \tag{I,40}
\end{equation*}
$$

For each camera distance, $\mathrm{s}^{4} \mathrm{I}_{\mathrm{t}}^{\mathrm{k}}(\mathrm{s})$ curves were obtained by performing the multiplications indicated in equation (I, 40) and plotted on large-scale graph paper. Values of the calibration function $a\left(r_{s}\right)$ were obtained from the Oslo Laboratory. ${ }^{1}$ It would now seem that the desired molecular intensity function $I_{m}^{k}(s)$ could be obtained by subtracting the last two terms in equation ( $\mathrm{I}, 1$ ) from $\mathrm{s}^{4} \mathrm{I}_{\mathrm{t}}^{\mathrm{k}}(\mathrm{s})$; these two terms constitute the theoretical background and can be calculated. As has been pointed out, however, the theory of incoherent scattering is on poor ground and, even more important, there inevitably exists on any exposed plate a superposed experimental background derived
 used. These values correspond to a value of $\lambda$ equal to $0.06449 \AA$; values calculated with $\lambda_{\text {exp }}=0.06458$ would differ inconsequentially from these.
from apparatus scattering. In practice, therefore, since little is known about the apparatus background other than it is monatonically declining with increasing angle, one simply draws a background curve through the undulations of the experimental intensity and subtracts it. The result is the desired function,

$$
\begin{equation*}
I_{m}^{k}(s)=s^{4} I_{t}^{k}(s)-B_{t}^{k}(s) \tag{I,41}
\end{equation*}
$$

The initial background often contains errors which manifest themselves by negative values of $r D(r)$ calculated from $I_{m}(s)$, or small peaks in $r D(r)$ at $r<1.00 \AA$. These errors are usually corrected by changing the background. Throughout this work, experimental background functions were used instead of theoretical functions.

Following subtraction of the background, the three $I_{m}^{k}(s)$ functions were placed on a common amplitude scale by comparing corresponding maxima and minima in the following overlap regions:

$$
\begin{array}{ll}
\mathrm{I}_{\mathrm{m}}^{\mathrm{a}}(\mathrm{~s}) \text { and } \mathrm{I}_{\mathrm{m}}^{\mathrm{b}}(\mathrm{~s}) ; & 10.25 \leq \mathrm{s} \leq 20.75 \\
\mathrm{I}_{\mathrm{m}}^{\mathrm{b}}(\mathrm{~s}) \text { and } \mathrm{I}_{\mathrm{m}}^{\mathrm{c}}(\mathrm{~s}) ; & 28.75 \leq \mathrm{s} \leq 42.00
\end{array}
$$

A single composite function, $\mathrm{I}_{\mathrm{m}}^{\mathrm{T}}(\mathrm{s})$, was then obtained by combining ${ }^{1}$ $\mathrm{I}_{\mathrm{m}}^{\mathrm{a}}(\mathrm{s}), \mathrm{I}_{\mathrm{m}}^{\mathrm{b}}(\mathrm{s})$ and $\mathrm{I}_{\mathrm{m}}^{\mathrm{c}}(\mathrm{s})$ now normalized as follows:
${ }^{1}$ The data available from the $I_{m}^{c}$ (s) curve in the range $18.50 \leq \mathrm{s}<28.75$, was not used in forming the composite curve $\mathrm{I}_{\mathrm{m}}^{\mathrm{T}}$ (s).

$$
\begin{aligned}
& 2.50 \leq \mathrm{s} \leq 10.00 ; \mathrm{I}_{\mathrm{m}}^{\mathrm{T}}(\mathrm{~s})=\mathrm{I}_{\mathrm{m}}^{\mathrm{a}}(\mathrm{~s}) \\
& 10.25 \leq \mathrm{s} \leq 20.75 ; \mathrm{I}_{\mathrm{m}}^{\mathrm{T}}(\mathrm{~s})=\mathrm{t}(\mathrm{~s}) \mathrm{I}_{\mathrm{m}}^{\mathrm{a}}(\mathrm{~s})+\mathrm{u}(\mathrm{~s}) \mathrm{I}_{\mathrm{m}}^{\mathrm{b}}(\mathrm{~s}) \\
& 21.00 \leq \mathrm{s} \leq 28.50 ; \mathrm{I}_{\mathrm{m}}^{\mathrm{T}}(\mathrm{~s})=\mathrm{I}_{\mathrm{m}}^{\mathrm{b}}(\mathrm{~s}) \\
& 28.75 \leq \mathrm{s} \leq 42.00 ; \mathrm{I}_{\mathrm{m}}^{\mathrm{T}}(\mathrm{~s})=\mathrm{v}(\mathrm{~s}) \mathrm{I}_{\mathrm{m}}^{\mathrm{b}}(\mathrm{~s})+\mathrm{w}(\mathrm{~s}) \mathrm{I}_{\mathrm{m}}^{\mathrm{c}}(\mathrm{~s}) \\
& 42.25 \leq \mathrm{s} \leq 49.75 ; \mathrm{I}_{\mathrm{m}}^{\mathrm{T}}(\mathrm{~s})=\mathrm{I}_{\mathrm{m}}^{\mathrm{c}}(\mathrm{~s}) .
\end{aligned}
$$

The weighting factors $t(s), u(s), v(s)$ and $w(s)$ were obtained from the $I_{p}^{k}(s)$ data. The overall range of the composite $I_{m}^{T}(s)$ was $2.50 \leq s \leq 49.75$.

The composite curve $I_{m}^{T}(s)$ resulting from the procedures just described is in theory represented by the expression

$$
\begin{aligned}
& s I_{m}^{T}(s)=k^{\prime} \sum_{i, j}^{1} n_{i j}(Z-F)_{i}(Z-f)_{j} r_{i j}^{-1} \\
& \quad \cos \left|\Delta \eta_{i j}\right| \exp \left(-l_{i j} s^{2} / 2\right) \sin \left(r_{i j} s\right),(I, 42)
\end{aligned}
$$

which is, in fact, equation (I, 2) multiplied by $s^{5}$. In order to replace the variable coefficients of $\mathrm{I}_{\mathrm{m}}^{\mathrm{T}}(\mathrm{s})$ in equation ( $\mathrm{I}, 42$ ) by essentially constant coefficients, as is necessary for obtaining an easily interpreted radial distribution curve, the modified molecular intensity function $I_{E}^{T}(s) E_{x p}$ was calculated according to the equation

$$
\begin{equation*}
I_{E}^{T}(s)_{\operatorname{Exp}}=s I_{m}^{T}(s) Z_{N} Z_{O} /(Z-F)_{N}(Z-F)_{O} \tag{I,43}
\end{equation*}
$$

The values of $\mathrm{F}_{\mathrm{N}}(\mathrm{s})$ and $\mathrm{F}_{\mathrm{O}}(\mathrm{s})$ were obtained by combining those published by Hoerni and Ibers (21, p. 745) with those of Viervoll and Ögrim (43, p. 279). In the former case the $F_{i}(s)$ 's were computed from Hartree-Fock radial wave functions, and in the latter an
interpolation method was used to extend the calculations of James and Brindley (25, p. 81-111) to s equal to 30. Since the nitrogen dioxide data extended well-beyond $s=30$, it was necessary to extrapolate the $F_{i}$ curves to obtain values in this region. The values of $(Z-F / Z)_{O}$ and $(Z-F / Z)_{N}$ used are given in Table 14. Values of $\mathrm{I}_{\mathrm{E}}^{\mathrm{T}}(\mathrm{s})_{\operatorname{Exp}}$ are given in Table 5 and the curve is ploted in Figure 2.

Reference to equations ( $\mathrm{I}, 42$ ) and ( $\mathrm{I}, 43$ ) reveals that $\mathrm{I}_{\mathrm{E}}^{\mathrm{T}}(\mathrm{s}) \operatorname{Exp}$ for nitrogen dioxide corresponds to the theoretical scattering equation (if the relatively important $\cos \left|\Delta \eta_{i}\right|$ term is ignored ${ }^{1}$ )

$$
\begin{aligned}
& \mathrm{I}_{\mathrm{E}}^{\mathrm{T}}(\mathrm{~s})_{\text {Theor }}=\mathrm{k}^{\prime}\left[2 \mathrm{Z}_{\mathrm{N}^{Z}} \mathrm{O}^{\mathrm{r}} \mathrm{~N}^{-1}-\mathrm{O} \exp \left(-1 \mathrm{~N}_{\left.-\mathrm{O}^{s^{2}} / 2\right) \sin (\mathrm{sr}}^{\mathrm{N}-\mathrm{O})}\right.\right.
\end{aligned}
$$

The coefficient $Z_{N} Z_{O}(Z-F)_{\mathrm{O}} /(\mathrm{Z}-\mathrm{F})_{\mathrm{N}}$ is essentially constant; Table 15 shows that it is approximately equal to $Z_{O}^{2}$ for $s \geq 7$.00. An $\mathrm{I}_{\mathrm{E}}^{\mathrm{T}}(\mathrm{s})$ Theor curve was calculated according to equation (I, 44) using the final refined parameter values (Table 22) and is shown in Figure 2 and tabulated in Table 5. The agreement between the experimental and theoretical curves is good.

In addition to the final composite intensity function $I_{E}^{T}(s) \operatorname{Exp}^{\mathrm{T}}$ several other $I_{E}(s) \operatorname{Exp}$ curves were calculated which included (1) only data from plates taken at a single camera distance and (2) data

[^5]taken from single plates at a single camera distance. The purpose of these curves was to help with an understanding of the errors associated with the parameter values determined. The various curves and ranges of data they include are:
\[

$$
\begin{aligned}
& \mathrm{I}_{\mathrm{E}}^{\mathrm{a}}(\mathrm{~s}) ; \quad 2.50 \leq \mathrm{s} \leq 20.75 \\
& \mathrm{I}_{\mathrm{E}}^{\mathrm{b}}(\mathrm{~s}) ; 10.25 \leq \mathrm{s} \leq 42.00 \\
& \mathrm{I}_{\mathrm{E}}^{\mathrm{c}}(\mathrm{~s}) ; 28.75 \leq \mathrm{s} \leq 49.75 \text { and } 18.50 \leq \mathrm{s} \leq 49.75 \\
& \mathrm{I}_{\mathrm{E}}^{\mathrm{a}(1)}(\mathrm{s}), \mathrm{I}_{\mathrm{E}}^{\mathrm{a}(2)}(\mathrm{s}), \mathrm{I}_{\mathrm{E}}^{\mathrm{a}(3)}(\mathrm{s}), \mathrm{I}_{\mathrm{E}}^{\mathrm{a}(4)}(\mathrm{s}) ; \quad 2.50 \leq \mathrm{s} \leq 20.75 \\
& \mathrm{I}_{\mathrm{E}}^{\mathrm{b}(1)}(\mathrm{s}), \mathrm{I}_{\mathrm{E}}^{\mathrm{b}(2)}(\mathrm{s}), \mathrm{I}_{\mathrm{E}}^{\mathrm{b}(3)}(\mathrm{s}), \mathrm{I}_{\mathrm{E}}^{\mathrm{b}(4)}(\mathrm{s}) ; 10.25 \leq \mathrm{s} \leq 42.00 .
\end{aligned}
$$
\]

The curves described above are given in Tables 6, 7, and 8 and plotted ${ }^{1}$ in Figure 3.

## Radial Distribution Function and Preliminary Structure

The final radial distribution function $r D^{\prime}(r)_{\operatorname{Exp}}$ [see equation (I, 11)], from the modified experimental molecular intensity curve $I_{E}^{T}(s)_{E x p}(\Delta s=0.25)$ was calculated according to the equation

$$
\mathrm{s}=49.75
$$

$$
\begin{equation*}
r D^{\prime}(r)_{\operatorname{Exp}}=\sum_{s=0} I_{E}^{T}(s) \operatorname{Exp} \exp \left(-0.001 s^{2}\right) \sin (r s) \tag{I,45}
\end{equation*}
$$

the intensity data in the range $0 \leq s \leq 2.25$ was calculated from a theoretical curve according to equation (I, 44). The experimental radial distribution curve (values are given in Table 9 and the curve

[^6]is shown in Figure 4) shows two strong peaks attributed to the $\mathrm{N}-\mathrm{O}$ and $O \cdots$ distances at about 1.2 and $2.2 \AA$, respectively. Careful analysis of these peaks gave the following preliminary values for the distance and amplitude parameters:
\[

$$
\begin{aligned}
& \mathrm{r}(\mathrm{~N}-\mathrm{O})=1.20_{1} \AA, 1(\mathrm{~N}-\mathrm{O})=0.038_{5} \AA \\
& \mathrm{r}(\mathrm{O} \cdot \mathrm{O})=2.21_{0} \AA, 1(\mathrm{O} \cdot \mathrm{O})=0.0438 \AA .
\end{aligned}
$$
\]

For comparison, a theoretical radial distribution curve calculated using the final refined parameter values (Table 22) is shown in Figure 4 and tabulated in Table 9. The calculation was carried out according to the equation

$$
\begin{align*}
& r D^{\prime}(r)_{\text {Theor }}=k^{\prime \prime} \sum_{i, j}^{r} n_{i j} Z_{i} Z_{j} r_{i j}^{-1}\left(l_{i j}^{2}+.002\right)^{-\frac{1}{2}} \\
& x \exp \left[-\left(r-r_{i j}\right)^{2} /\left(21_{i j}^{2}+.004\right)\right], \tag{I,46}
\end{align*}
$$

where the scale factor $\mathrm{k}^{\prime \prime}$ was determined from the peak heights in $r D^{\prime}(r)_{E_{x p}}$. The agreement between the experimental and theoretical curves is good.

Least-Squares Refinements

A large number of refinements, employing the Alwac III-E digital computer, were carried out according to the procedures
already described. The results of several of these refinements are summarized in Tables 16 through 19. In each refinement the starting model was obtained from the $r D^{\prime}(r) E_{x p}$ curve. The information to be deduced from these tables will be discussed in the following paragraphs.

## Non-Systematic Errors

The error matrix, $\mathbb{M}$, derived from least-squares refinement is given by

$$
\begin{equation*}
\mathbb{M}=\bar{s}^{2} \mathbb{D} \mathbb{B}^{-1} \mathbb{D}^{1}, \tag{I,47}
\end{equation*}
$$

where the transformation matrix $\mathbb{D}$ is obtained from

$$
\begin{equation*}
\mathbb{U}=\mathbb{D} \mathbb{X} . \tag{I,48}
\end{equation*}
$$

In the nitrogen dioxide case, the only additional parameter of interest is the bond angle: equation ( $\mathrm{I}, 48$ ) thus becomes

$$
\left[\begin{array}{l}
\mathrm{r}(\mathrm{~N}-\mathrm{O})  \tag{I,48'}\\
\mathrm{r}(\mathrm{O} \cdot \mathrm{O}) \\
<(\mathrm{O}-\mathrm{N}-\mathrm{O}) \\
1(\mathrm{~N}-\mathrm{O}) \\
1(\mathrm{O} \cdot \mathrm{O})
\end{array}\right]=\mathbb{D}\left[\begin{array}{l}
\mathrm{r}(\mathrm{~N}-\mathrm{O}) \\
\mathrm{r}(\mathrm{O} \cdots \mathrm{O}) \\
1(\mathrm{~N}-\mathrm{O}) \\
1(\mathrm{O} \cdots \mathrm{O})
\end{array}\right]
$$

and $\mathbb{D}$ is easily seen to be given by
${ }^{1}$ Additional refinements were carried out investigating the effect on the parameter values of such things as the various background corrections, selection of suitable s ranges for separate composites, determination of the overlap ranges, et cetera.

$$
\mathbb{D}=\left[\begin{array}{cccc}
1 & 0 & 0 & 0  \tag{I,49}\\
0 & 1 & 0 & 0 \\
a^{\prime} & b^{\prime} & 0 & 0 \\
0 & 0 & 1 & 0 \\
0 & 0 & 0 & 1
\end{array}\right]
$$

Combining the parameter values given in the first column of Table 19 with the corresponding $\bar{s}^{2} \mathbb{B}^{-1}$ matrix, $\mathbb{M}$ was evaluated ${ }^{l}$ and is shown in Table 20. The off-diagonal elements, $(\mathbb{M})_{i j}$, of this matrix are the average products of the errors $\sigma_{i}^{L S}$ and $\sigma_{j}^{L S}$ (often denoted ${ }^{2}$ by $\left.\rho_{i j} \sigma_{i}^{L S} \sigma_{j}^{L S}\right)$; the square roots of the diagonal elements, $(\mathbb{M})_{i i}$, are the standard error $\left(\sigma_{i}^{L S}\right)$ associated with each parameter.

Though the error matrix, $\mathbb{M}$, provides a means of estimating the random errors arising from the discrepancy of the composite observations from the theoretical modified molecular intensity curve [equation (I, 44)], Morino ${ }^{3}$ has pointed out that another source of nonsystematic error arises from variations in the most probable parameters as obtained from the individual photographic plates for a given camera distance (see Table 17). For the parameters $r(N-O)$,

$$
\begin{align*}
& { }^{1} \text { From equations ( } I, 47 \text { ) and (I, 49), the error, } \\
& (\mathbb{M})_{<O-N-O,<O-N-O} \text { is defined by } \\
& \bar{s}^{2}\left[\left(a^{\prime}\right)^{2}\left(\mathbb{B}^{-1}\right) r_{r_{N-O}, r_{N-O}}+2 a^{\prime} b^{\prime}\left(\mathbb{B}^{-1}\right)_{r_{N-O}}, r_{O} \ldots \mathrm{O}\right. \\
& +\left(b^{\prime}\right)^{2}\left(\mathbb{B}^{-1}\right)_{r_{O} \ldots O}, r_{O} \ldots O \quad . \tag{I,50}
\end{align*}
$$

$2_{\rho_{i j}}$ is usually referred to as the correlation coefficient.
${ }^{3}$ Morino, Yonezo. Private communication. Tokyo, Japan. University of Tokyo, 1964.
$r(O, O), 1(\mathrm{~N}-\mathrm{O})$ and $1(\mathrm{O} \cdot \mathrm{O}), \sigma_{2}\left(\mathrm{x}_{\mathrm{j}}\right)^{2}$ was estimated as follows. Let

$$
\begin{equation*}
\sigma_{2}^{a(i)}\left(x_{j}\right)=x_{j}^{a}-x_{j}^{a(i)} \tag{I,5l}
\end{equation*}
$$

and

$$
\begin{equation*}
\sigma_{2}^{b(i)}\left(x_{j}\right)=x_{j}^{b}-x_{j}^{b(i)} . \tag{I,51'}
\end{equation*}
$$

The final values of $\sigma_{2}\left(x_{j}\right)$ were then calculated as

$$
\begin{align*}
\sigma_{2}\left(x_{j}\right)^{2}=(1 / 8-1)(0.365 & \sum_{i=1}^{4}\left[\sigma_{2}^{a(i)}\left(x_{j}\right)\right]^{2} \\
& \left.+0.635 \sum_{i=1}^{4}\left[\sigma_{2}^{b(i)}\left(x_{j}\right)\right]^{2}\right), \tag{I,52}
\end{align*}
$$

where the weights 0.365 and 0.635 were obtained by consideration of the total s ranges contributed by each of the two camera distances ( 478 and 192 mm ) relative to $\mathrm{I}_{\mathrm{E}}^{\mathrm{T}} \mathrm{s}_{\mathrm{Exp}}$. The additional information that might have been obtained by a similar analysis of the 120 mm plates did not seem justified. The corresponding standard deviation for the bond angle was estimated ${ }^{1}$ as

$$
\begin{equation*}
\sigma_{2}(<\mathrm{O}-\mathrm{N}-\mathrm{O})^{2}=\left(\mathrm{a}^{\prime}\right)^{2} \sigma_{2}\left(\mathrm{r}_{\mathrm{N}-\mathrm{O}}\right)^{2}+\left(\mathrm{b}^{\prime}\right)^{2} \sigma_{2}\left(\mathrm{r}_{\mathrm{O}} \ldots \mathrm{O}\right)^{2} \tag{I,53}
\end{equation*}
$$

## Systematic Errors

Uncertainties arising from the measurement of camera

[^7]distance, electron wavelength and the position coordinate (uncertainty $\Delta \mathrm{x}_{\mathrm{T}}$ in the designation of the correct obscissa for a predetermined s scale) principally effect the size of the molecule and are negligible in their effect on the vibrational amplitudes. In terms of interatomic distances, the error associated with the first two of these parameters ( h and $\lambda$ ) can be estimated as follows. Recalling that $\mathrm{s}=4 \pi \lambda^{-1} \sin \theta$ where $\sin \theta=x_{p} /\left(h^{2}+x_{p}^{2}\right)^{\frac{1}{2}}$,
\[

$$
\begin{equation*}
-\mathrm{ds} / \mathrm{s}=\left[\mathrm{d} \lambda / \lambda+\mathrm{hdh} /\left(\mathrm{h}^{2}+\mathrm{x}_{\mathrm{p}}^{2}\right)\right] . \tag{I,54}
\end{equation*}
$$

\]

Since, for a given ring spacing

$$
\begin{equation*}
s \propto r_{i j}^{-1} \tag{I,55}
\end{equation*}
$$

then

$$
\begin{equation*}
\mathrm{ds} / \mathrm{s}=-\mathrm{dr} \mathrm{r}_{\mathrm{ij}} / \mathrm{r}_{\mathrm{ij}}, \tag{1,56}
\end{equation*}
$$

and combining equations ( $I, 54$ ) and ( $I, 56$ ), we obtain

$$
\begin{equation*}
d r_{i j} / r_{i j}=\left[d \lambda / \lambda+h d h /\left(h^{2}+x_{p}^{2}\right)\right] . \tag{I,57}
\end{equation*}
$$

Setting $x_{p}$ equal to zero and noting that $\lambda$ and $h$ are independent parameters, the desired estimate is given by

$$
\begin{equation*}
d r_{i j}^{\prime}=\left[(\mathrm{d} \lambda / \lambda)^{2}+(\mathrm{dh} / \mathrm{h})^{2}\right]^{\frac{1}{2}} r_{i j} . \tag{I,58}
\end{equation*}
$$

Using the values ${ }^{l} \lambda \pm d \lambda=0.06458 \pm .00002 \AA$ and $h \pm d h=263.3$ $\pm 0.1 \mathrm{~mm}$ (obtained by simple averaging of 478,192 , and 120 mm camera distances), equation ( $\mathrm{I}, 58$ ) gives a value of $0.0005 \mathrm{r}_{\mathrm{ij}}$ for

[^8]drij which agrees with the corresponding estimate given by Hedberg and Iwasaki (16, p. 592-593). In comparison, the error in the position coordinate can be neglected.

Uncertainties in the blackness correction and the atomic form factors affect largely the vibrational amplitudes. This error has been estimated as $0.021_{\mathrm{ij}}$ (16, p. 593). Since this investigation sought to establish the reliability of these amplitudes, the significance of the earlier remarks pertaining to the fact that only a very small fraction of the densities used required a correction for blackness, should now be clear.

If the data on which the determinations are based are not all independent, the error estimates $\sigma_{L S}$ are too small for all parameters. Very little is known about correlation among the data, but a rough, plausible guess might be that about one-half the observations are independent; this estimate would lead to standarderrors $\sigma$ LS greater by about $2^{\frac{1}{2}}$ than those calculated.

No attempt was made to estimate the systematic errors arising from uncertainties in the sector correction ${ }^{l}$ and in the experimental background, finite size of scattering region, deflection of the electrons resulting from interaction with the magnetic field of the earth which would give asymmetric rings, and the effect of

[^9]anharmonicity.

## Overall Standard Errors

The overall standard errors for the final structural parameters were estimated as follows: ${ }^{1}$

1. $\quad \sigma_{\mathrm{T}}\left(\mathrm{r}_{\mathrm{ij}}\right)=\left[2 \sigma_{\mathrm{LS}}\left(\mathrm{r}_{\mathrm{ij}}\right)^{2}+\sigma_{2}\left(\mathrm{r}_{\mathrm{ij}}\right)^{2}+\left(0.0005 \mathrm{r}_{\mathrm{ij}}\right)^{2}\right]^{\frac{1}{2}}$
2. $\sigma_{\mathrm{T}}(<\mathrm{O}-\mathrm{N}-\mathrm{O})=\left[2 \sigma_{\mathrm{LS}}(<\mathrm{O}-\mathrm{N}-\mathrm{O})^{2}+\sigma_{2}(<\mathrm{O}-\mathrm{N}-\mathrm{O})^{2}\right]^{\frac{1}{2}}$
3. $\sigma_{\mathrm{T}}\left(\mathrm{l}_{\mathrm{ij}}\right)=\left[2 \sigma_{\mathrm{LS}}\left(1_{\mathrm{ij}}\right)^{2}+\sigma_{2}\left({ }_{\mathrm{ij}}\right)^{2}+\left(0.021_{\mathrm{ij}}\right)^{2}\right]^{\frac{1}{2}}$.

The complete error analysis is summarized in Table 21, it should be noted that if the random errors $\sigma_{L S}$ and $\sigma_{2}$ were not assumed to be independent (that is, if the observations on several photographic plates did not belong to a single statistical population), it would seem appropriate to only include the larger of the two in evaluating $\sigma_{T}$. Further, it might very well be that $\sigma_{2}$ reflects the presence of hidden systematic errors in the individual observations. The results in Table 21 thus represent conservative estimates.
${ }^{1}$ The factor two associated with the term $2 \sigma_{\text {LS }}^{2}$ arises from considerations of data correlation discussed earlier. The value $1.0012 \mathrm{r}_{\mathrm{ij}}$ was used in evaluating the term $\left(0.0005 \mathrm{r}_{\mathrm{ij}}\right)^{2}$.

## Final Results


#### Abstract

The final values ${ }^{1}$ of the structural parameters (including estimated standard errors) are given in Table 22. These values were derived from those given in the first column in Table 19 and the $r_{i j}$ parameters have been multiplied by 1.0012 . The comparison of these results with the corresponding microwave work (5, p. 10401043) is pleasing. It should be noted that in neither case do the parameters represent true equilibrium values (2, p. 1219-1222; 23, p. 2961-2963; 29, 1945-1949; 37, p. 644-648; 38, p. 1108-1109), though the microwave parameters represent a closer approximation than those of electron diffraction.


[^10]
## PART II

QUADRATIC POTENTIAL CONSTANTS

## POTENTIAL CONSTANT INVESTIGATION

List of Symbols (In order of appearance in Part II of the text) ${ }^{1}$

| n | p.d. |
| :---: | :---: |
| $\Delta \mathrm{r}_{1}$ | internal bond stretching coordinate. |
| $\Delta r_{2}$ | same as $\Delta \mathrm{r}_{1}$. |
| $\Delta \mathrm{a}$ | internal valence angle bending coordinate. |
| $\Delta r_{3}$ | internal non-bonded stretching coordinate. |
| $r_{X}^{e}-Y$ | equilibrium bond distance in non-linear $\mathrm{XY}_{2}$ molecule. |
| $<\mathrm{Y}-\mathrm{X}-\mathrm{Y}$ | equilibrium valence angle in non-linear $\mathrm{XY}_{2}$ molecule. |
| $\mathrm{r}_{\mathrm{Y}}^{\mathrm{e}} \ldots \mathrm{Y}$ | $\begin{aligned} & \text { equilibrium non-bonded distance in non-linear } \mathrm{XY}_{2} \\ & \text { molecule. } \end{aligned}$ |
| t | $\mathrm{t}=\mathrm{r}_{\mathrm{X}-\mathrm{Y}}^{\mathrm{e}} \sin (<\mathrm{Y}-\mathrm{X}-\mathrm{Y}) / \mathrm{r}_{\mathrm{Y}}^{\mathrm{e}} \ldots \mathrm{Y} .$ |
| u | $u=r_{X-Y}^{e}[1-\cos (<Y-X-Y)] / r_{Y}^{e} \ldots Y^{e} .$ |
| $\mathrm{r}_{\mathrm{ij}}$ | p.d. |
| $1_{i j}$ | p.d. |
| $\mathrm{r}_{\mathrm{ij}}^{\mathrm{i}}$ | p.d. |
| $\mathrm{r}_{\mathrm{ij}}^{\mathrm{e}}$ | p.d. |
| R | column matrix of internal coordinate set. |
| \$ | column matrix of symmetry coordinate set. |

Q column matrix of normal coordinate set.
$\overline{\mathbf{V}} \quad \operatorname{transformation~matrix}$ from $\mathbf{S}$ to $\mathbf{R} . \quad \mathbf{R}=\overline{\mathbf{V}} \mathbf{S}$.
$\mathbb{L} \quad \operatorname{tran}$ formation matrix from $\mathbf{Q}$ to $\mathbf{S} . \quad \mathbf{S}=\mathbf{L} \mathbf{Q}$.
$G_{S} \quad$ symmetrized $\mathbb{G}$ matrix.
$\mathbb{F}_{S} \quad$ symmetrized $\mathbb{F}$ matrix.
${ }^{v}{ }_{k} \quad$ frequency of $k$ th vibrational mode.
$\wedge$

X
column matrix of Cartesian displacement coordinates.
$\bar{A}$
transformation matrix from $\mathbb{R}$ to $X . X=\bar{A} \mathbb{R}$.
$\bar{M}$
diagonal matrix of the atomic masses.
$G_{R} \quad$ internal $G$ matrix. $\quad G_{R}=\overline{\mathbf{V}} G_{S} \overline{\mathbb{V}}^{\prime}$.
$\mathbb{E}$
unit matrix. $(\mathbb{E})_{i j}=\delta_{i j}$.
$\Delta \quad$ diagonal matrix of the mean-square amplitudes of normal vibration. $\Delta=\left\langle\mathbb{Q} \mathbb{Q}^{\prime}\right\rangle$.
h
k
p.d.

T
absolute temperature ( ${ }^{\circ} \mathrm{K}$ ).
$\underline{\Sigma}_{\mathrm{R}} \quad$ the mean-square vibrational amplitude matrix in internal coordinates.
$r^{\mathbf{e}} \quad$ same as $\mathrm{r}_{\mathrm{N}-\mathrm{O}}^{\mathrm{e}}$.

$$
\begin{aligned}
& \mathrm{S}_{1} \quad \mathrm{~S}_{1}=\left(\Delta \mathrm{r}_{2}+\Delta \mathrm{r}_{2}\right) / 2^{\frac{1}{2}} . \\
& S_{2} \quad S_{2}=r^{e} \Delta a \text {. } \\
& \mathrm{S}_{3} \quad \mathrm{~S}_{3}=\left(\Delta \mathrm{r}_{1}-\Delta \mathrm{r}_{2}\right) / 2^{\frac{1}{2}} \text {. } \\
& \Delta \mathrm{r} \quad \Delta \mathrm{r}=\Delta \mathrm{r}_{1} \text { or } \Delta \mathrm{r}_{2} . \\
& \text { a equilibrium } \mathrm{O}-\mathrm{N}-\mathrm{O} \text { angle. } \\
& F_{11} \quad F_{11}=f_{r}+f_{r r} . \\
& F_{12} \quad F_{12}=2^{\frac{1}{2}}{ }_{\mathrm{r} 0} \text {. } \\
& \mathrm{F}_{22} \quad \mathrm{~F}_{22}=\mathrm{f}_{\mathrm{a}} \text {. } \\
& \mathrm{F}_{33} \quad \mathrm{~F}_{33}=\mathrm{f}_{\mathrm{r}}-\mathrm{f}_{\mathrm{rr}} . \\
& \mu_{i} \quad \mu_{i}=m_{i}^{-1} \text { where } m_{i} \text { is the mass of the ith atom. } \\
& G_{11} \quad G_{11}=2 \mu_{N} \cos ^{2}(a / 2)+\mu_{\mathrm{O}} \text {. } \\
& G_{12} \quad G_{12}=-2^{3 / 2} \mu_{N} \sin (a / 2) \cos (a / 2) \text {. } \\
& G_{22} \quad G_{22}=2\left[2 \mu_{N} \sin ^{2}(a / 2)+\mu_{O}\right] \text {. } \\
& G_{33} \quad G_{33}=G_{22} / 2 . \\
& \beta \quad \beta=F_{11} F_{22}-F_{12}^{2} . \\
& \bar{\gamma} \quad \bar{\gamma}=G_{11} G_{22}-G_{12}^{2} . \\
& \mathbb{C} \quad \mathbb{C}=\mathbb{F}^{-1} \text {. } \\
& \mathbb{K} \quad \mathbb{K}=G^{-1} \text {. } \\
& \phi \quad \phi=\lambda^{-1} \text {. } \\
& \mathbb{C}_{S} \quad \mathbb{C}_{S}=\mathbb{E}_{S}^{-1} . \\
& \mathrm{C}_{11} \quad \mathrm{C}_{11}=\mathrm{F}_{22} / \beta \text {. } \\
& \mathrm{C}_{12} \quad \mathrm{C}_{12}=-\mathrm{F}_{22} / \beta \text {. } \\
& \mathrm{C}_{22} \quad \mathrm{C}_{22}=\mathrm{F}_{11} / \beta \text {. }
\end{aligned}
$$

$\mathrm{C}_{33} \quad \mathrm{C}_{33}=\mathrm{F}_{33}^{-1}$.
$v_{i} \quad$ observed fundamental frequency of the ith vibrational mode.
$\omega_{i} \quad$ harmonic frequency of the ith vibrational mode. $\mathbb{P}_{\text {Ot }} \quad$ diagonal weight matrix used in least-squares determination of symmetrized compliance constants.
$f_{i} \quad$ ith internal potential constant.
$\sigma\left(f_{i}\right) \quad$ estimated error in $f_{i}$ due to uncertainties in $1_{\mathrm{N}-\mathrm{O}}$ and $^{1} \mathrm{O} \ldots \mathrm{O}$.

$$
\begin{array}{cc}
\sigma_{T}\left(1_{i j}\right) & \text { p.d. } \\
\sigma_{L S}\left(1_{i j}\right) & \text { p.d. }
\end{array}
$$

## Molecular Potential Functions

In the harmonic approximation, a non-linear polyatomic molecule can be viewed as an aggregation of $3 n-6$ ( $3 n-5$ for a linear molecule) independent simple harmonic oscillators. As internal coordinates one normally selects either "valence" or "central force" coordinates [various choices are possible (46, p. 223)]. The former set consists of bond distance and bond angle displacements from equilibrium and the latter solely of internuclear distance displacements. For example, for a non-linear $X Y_{2}$ molecule the valence force coordinates would be the two equivalent $X-Y$ stretches and the Y-X - Y angle distortion, which may be denoted by $\Delta r_{1}, \Delta r_{2}$ and $\Delta a^{l}$, respectively; the corresponding central force coordinates would then be $\Delta r_{1}$ and $\Delta r_{2}$ and the $Y \cdots Y$ distance displacement $\Delta r_{3} \cdot B y$ geometric means, it is easily shown that (assuming small displacements)

$$
\Delta r_{3}=\left(\Delta r_{1}+\Delta r_{2}\right) \sin (<Y-X-Y / 2)+r_{X-Y}^{e} \Delta a \cos (<Y-X-Y / 2)
$$ With the coordinates defined above one may consider many vibrational models. Some of the more common are the simple central force, simple valence force, generalized central force, generalized valence force, and the Urey-Bradley force field which may be

[^11]abbreviated by SCF, SVF, GCF, GVF, and UBF, respectively. For a bent $\mathrm{XY}_{2}$ molecule the vibrational potentials corresponding to these models have the forms (in the harmonic approximation)
\[

$$
\begin{align*}
\mathrm{SCF} ; & 2 \mathrm{~V}=\mathrm{A}_{\mathrm{r}}\left[\left(\Delta \mathrm{r}_{1}\right)^{2}+\left(\Delta \mathrm{r}_{2}\right)^{2}\right]+\mathrm{A}_{\mathrm{r}^{\prime}}\left(\Delta \mathrm{r}_{3}\right)^{2},  \tag{II,2}\\
\mathrm{SVF} ; 2 \mathrm{~V} & =\mathrm{B}_{\mathrm{r}}\left[\left(\Delta \mathrm{r}_{1}\right)^{2}+\left(\Delta \mathrm{r}_{2}\right)^{2}\right]+\mathrm{B}_{\mathrm{a}}\left(\mathrm{r}_{\mathrm{X}-\mathrm{Y}}^{\mathrm{e}} \Delta \mathrm{a}\right)^{2},  \tag{II,3}\\
\mathrm{GCF} ; & 2 \mathrm{~V}=\mathrm{D}_{\mathrm{r}}\left[\left(\Delta \mathrm{r}_{1}\right)^{2}+\left(\Delta \mathrm{r}_{2}\right)^{2}\right]+\mathrm{D}_{\mathrm{r}^{\prime}}\left(\Delta \mathrm{r}_{3}\right)^{2} \\
& +2 \mathrm{D}_{\mathrm{rr}}\left(\Delta \mathrm{r}_{1} \Delta \mathrm{r}_{2}\right)+2 \mathrm{D}_{\mathrm{rr}^{\prime}}\left(\Delta \mathrm{r}_{1}+\Delta \mathrm{r}_{2}\right) \Delta \mathrm{r}_{3},  \tag{II,4}\\
\mathrm{GVF} ; & 2 \mathrm{~V}=\mathrm{H}_{\mathrm{r}}\left[\left(\Delta \mathrm{r}_{1}\right)^{2}+\left(\Delta \mathrm{r}_{2}\right)^{2}\right]+\mathrm{H}_{\mathrm{a}}\left(\mathrm{r}_{\mathrm{X}-\mathrm{Y}}^{\mathrm{e}} \Delta \mathrm{a}\right)^{2} \\
& +2 \mathrm{H}_{\mathrm{rr}}\left(\Delta \mathrm{r}_{1} \Delta \mathrm{r}_{2}\right)+2 \mathrm{H}_{\mathrm{ra}}\left(\Delta \mathrm{r}_{1}+\Delta \mathrm{r}_{2}\right) \mathrm{r}_{\mathrm{X}-\mathrm{Y}}^{\mathrm{e}} \Delta \mathrm{a} \tag{II,5}
\end{align*}
$$
\]

UBF; $2 \mathrm{~V}=\left(\mathrm{K}+\mathrm{t}^{2} \mathrm{~F}^{\prime}+\mathrm{u}^{2} \mathrm{~F}\right)\left[\left\{\Delta \mathrm{r}_{1}\right)^{2}+\left(\Delta \mathrm{r}_{2}\right)^{2}\right]+\left(\mathrm{H}-\mathrm{u}^{2} \mathrm{~F}^{\prime}+\mathrm{t}^{2} \mathrm{~F}\right)\left(\mathrm{r}_{\mathrm{X}}^{\mathrm{e}} \mathrm{Y}-\Delta \mathrm{c}\right)^{2}$

$$
+2\left(-\mathrm{t}^{2} \mathrm{~F}^{t}+\mathrm{u}^{2} \mathrm{~F}\right) \Delta \mathrm{r}_{1} \Delta \mathrm{r}_{2}+2 \mathrm{tu}\left(\mathrm{~F}^{\prime}+\mathrm{F}\right)\left(\Delta \mathrm{r}_{1}+\Delta \mathrm{r}_{2}\right) \mathrm{r}_{\mathrm{X} . . \mathrm{Y}}^{\mathrm{e}} \Delta \mathrm{c} .(\mathrm{II}, 6)
$$

In equation (II, 6), K and H denote the stretching and bending potential constants and F and $\mathrm{F}^{\prime}$, the repulsive potential constants between non-bonded atoms. $F^{\prime}$ is often approximated as $-(1 / 10) F$, which follows from taking the potential energy proportional to $(\mathrm{r} \underset{\mathrm{Y}}{\mathrm{e}} \ldots \mathrm{Y})^{-9}$. Furthermore, the potential constants defined in equations (Ii, 4), (II, 5) and (II, 6) can be simply related. Equating corresponding coefficients in equations (II, 5) and (II, 6),

$$
\begin{align*}
& \mathrm{H}_{\mathrm{r}}=\mathrm{K}+\mathrm{t}^{2} \mathrm{~F}^{\prime}+\mathrm{u}^{2} \mathrm{~F}, \\
& \mathrm{H}_{\mathrm{a}}=\mathrm{H}-\mathrm{u}^{2} \mathrm{~F}^{\prime}+\mathrm{t}^{2} \mathrm{~F}, \\
& \mathrm{H}_{\mathrm{rr}}=-\mathrm{t}^{2} \mathrm{~F}^{\prime}+\mathrm{u}^{2} \mathrm{~F},  \tag{II,7}\\
& \mathrm{H}_{\mathrm{ra}}=\operatorname{tu}\left(\mathrm{F}^{\prime}+\mathrm{F}\right) .
\end{align*}
$$

Since the potential and kinetic energy expressions must be invariant with respect to the coordinate system, one has
$H_{r}=D_{r}+2 D_{r r^{\prime}} \sin (<Y-X-Y / 2)+D_{r^{\prime}} \sin ^{2}(<Y-X-Y / 2)$, $H_{a}=D_{r}, \cos ^{2}(<Y-X-Y / 2)$,
$H_{r r}=D_{r r}+2 D_{r r^{\prime}} \sin (<Y-X-Y / 2)+D_{r^{\prime}} \sin ^{2}(<Y-X-Y / 2)$,
$H_{r a}=D_{r r}, \cos \left(\langle Y-X-Y / 2)+D_{r}, \cos (\langle Y-X-Y / 2) \sin (<Y-X-Y / 2)\right.$.
Finally, a comparison of equations (II, 7), and (II, 8) gives
$K+t^{2} F^{\prime}+u^{2} F=D_{r}+2 D_{r r^{\prime}} \sin (<Y-X-Y / 2)+D_{r^{\prime}} \sin ^{2}(<Y-X-Y / 2)$, $H-u^{2} F^{\prime}+t^{2} F=D_{r^{\prime}} \cos ^{2}(<Y-X-Y / 2)$,
$-\mathrm{t}^{2} \mathrm{~F}^{\prime}+\mathrm{u}^{2} \mathrm{~F}=\mathrm{D}_{\mathrm{rr}}+2 \mathrm{D}_{\mathrm{r} \mathrm{r}^{\prime}} \sin (<\mathrm{Y}-\mathrm{X}-\mathrm{Y} / 2)+\mathrm{D}_{\mathrm{r}^{\prime}} \sin ^{2}(<\mathrm{Y}-\mathrm{X}-\mathrm{Y} / 2)$, $\operatorname{tu}\left(\mathrm{F}^{\prime}+\mathrm{F}\right)=\mathrm{D}_{\mathrm{rr}} \mathrm{r}^{\prime} \cos (<\mathrm{Y}-\mathrm{X}-\mathrm{Y} / 2)+\mathrm{D}_{\mathrm{r}}, \cos (<\mathrm{Y}-\mathrm{X}-\mathrm{Y} / 2) \sin (<\mathrm{Y}-\mathrm{X}-\mathrm{Y} / 2)$.

Since the applicability of these models has been discussed by many authors [see (19, p. 142-191; 40, p. 57-59; 49, p. 169-182) and bibliographies therein cited], it suffices to mention here that the usual problem met in evaluating all the potential constants of the GCF or GVF is that generally there is insufficient data from spectroscopy alone: for example, for a bent $X Y_{2}$ molecule, there are three frequencies and four generalized quadratic potential constants. Isotopic substitution provides a solution to this problem, but this method is not always easy or satisfactory.

Potential and Compliance Constants of Nitrogen Dioxide from MeanSquare Amplitudes and Vibrational Frequencies

The early work of James (26, p. 737-754) established the connection between molecular vibration and the intensity of scattering from molecules. Although this work was specifically concerned with $x-r a y$ scattering, the results are also applicable to electrons, and have been successfully applied to the interpretation of electron diffraction patterns for many years. Recently, a good deal of attention has been devoted to exploring the connection between amplitudes of vibration, frequencies of vibration, and force constants [ see (10, p. 1-200; 11, p. 1121-1122; 22, p. 594-598; 33, p. 395; 34, p. 726733; 35, p. 1927-1933; 36, p. 737-747; 37, p. 643-652) and bibliographies therein cited]; the work by James provides the theoretical backbone for the interpretation of the diffraction results. It is the intention here to present only an outline of those ideas and equations needed to relate potential constants to mean amplitudes and normal frequencies of vibration.

Morino and Hirota (36, p. 737-747) distinguish three types of generalized vibrational amplitudes with respect to a specific atom pair ( $i, j$ ) in a molecule. Let the coordinates $x_{1}, x_{2}$ and $x_{3}$ denote the Cartesian axes parallel and perpendicular, respectively, to $r_{i j}$; then $\Delta \mathrm{x}_{1}, \Delta \mathrm{x}_{2}$ and $\Delta \mathrm{x}_{3}$ will denote the net displacement coordinates
of the $i$, $j$ atomic pair along each of these axial directions. The various amplitudes are then defined as follows:
$<\Delta x_{1}^{2}>$; the mean-square parallel amplitude,
$<\Delta \mathrm{x}_{2}^{2}>,<\Delta \mathrm{x}_{3}^{2}>$; the mean-square perpendicular amplitudes,
$\left.\left.<\Delta x_{1} \Delta x_{2}\right\rangle,\left\langle\Delta x_{2} \Delta x_{3}\right\rangle,<\Delta x_{2} \Delta x_{1}\right\rangle$; the mean cross products.
It has been shown $(36$, p. 743 ) that symmetry considerations allow one to conclude that for a non-linear $X Y_{2}$ molecule the only non-zero amplitudes for the atomic pair $Y-X$ are $<\Delta X_{1}^{2}>$ and $<\Delta x_{1} \Delta x_{2}>$, and for $Y \cdots Y,<\Delta x_{l}^{2}>$; the diagram shows the orientation of coordinates.


Now, in the usual definition (10, p. l) of the mean amplitude of vibration for an atom pair $i, j$ one has

$$
\begin{equation*}
l_{i j}=\left\langle\left(r_{i j}^{i}-r_{i j}^{e}\right)^{2}>^{\frac{1}{2}}\right. \tag{II,10}
\end{equation*}
$$

As a first approximation $l_{i j}$ is equivalent to the square root of the mean-square parallel amplitude discussed earlier. That is,
$r_{i j}^{i}-r_{i j}^{e}=\sum_{k=1}^{3}\left(\partial r_{i j}^{i} / \partial x_{k}\right)_{e} \Delta x_{k}+$ higher order terms $=\sum_{k=1}^{3}\left(x_{k} / r_{i j}^{e}\right) \Delta x_{k}$ + higher order terms; neglecting the higher order terms, squaring and averaging gives equation (II, l0). The various relationships defining the basic framework of the potential constant calculation may
be summarized as follows.
Let the column matrices $\mathbb{R}, \mathbf{S}$, and $\mathbf{Q}$ represent respectively sets of internal coordinates, symmetry coordinates, and the normal coordinates. The relations between these sets of coordinates are

$$
\begin{equation*}
\mathbf{R}=\overline{\mathbf{V}} \mathbf{S} \tag{II,11}
\end{equation*}
$$

and

$$
\begin{equation*}
\mathbf{S}=\mathbb{L} \mathbb{Q} . \tag{II,12}
\end{equation*}
$$

The matrix $L$ is determined by the equations (47, p. 1047-1052;
48, p. 76-84)

$$
\begin{align*}
& \mathbf{G}_{S} \mathbb{F}_{S} \mathbf{L}=\mathbb{L} \mathbb{\Lambda},  \tag{II,13}\\
& \mathbf{L}^{\prime} \mathbb{E}_{S} \mathbf{L}=\mathbb{1}, \tag{II,14}
\end{align*}
$$

and

$$
\begin{equation*}
\mathbb{L} \mathbb{L}^{\prime}=\mathbb{G}_{S} \tag{II,15}
\end{equation*}
$$

The matrix $\mathbb{E}_{S}$, of course, is defined in terms of the potential energy

$$
\begin{equation*}
2 V=S^{\prime} \mathbb{F}_{S} \mathbf{S} \tag{II,16}
\end{equation*}
$$

The matrix $\mathbb{G}_{S}$ is connected to the kinetic energy, as may be seen by the following equations:

$$
\mathbb{X}=\overline{\mathbb{A}} \mathbb{R}
$$

$$
\begin{align*}
2 T & =\dot{\mathbb{X}} \cdot \overline{\mathbb{M}} \dot{\mathbf{X}} \\
& =\mathbb{R}^{\prime} \overline{\mathbb{A}} \cdot \overline{\mathbb{M}} \overline{\mathbb{A}} \dot{\mathbb{R}} \\
& =\dot{\mathbb{R}}^{\prime} \cdot G_{R}^{-1} \dot{\mathbb{R}} \\
& =\dot{\mathbb{S}} \cdot \overline{\mathbb{N}} \cdot \mathbb{G}_{\mathrm{R}}^{-1} \overline{\mathbb{V}} \dot{\mathbb{S}} \\
& =\dot{\mathbb{S}} \cdot \mathbb{G}_{S}^{-1} \dot{\mathbb{S}} . \tag{II,18}
\end{align*}
$$

The matrix $\Lambda$ is a diagonal matrix the elements of which are given by

$$
\begin{equation*}
\lambda_{\mathrm{k}}=4 \pi^{2} v_{\mathrm{k}}^{2} ; \tag{II,19}
\end{equation*}
$$

they are related to the $G$ and $\mathbb{F}$ matrices by the secular equations (47, p. 1047-1052)

$$
\begin{equation*}
\mathbf{G}_{S} \mathbb{F}_{S}-\lambda \mathbb{E} \mid=0 \tag{II,20}
\end{equation*}
$$

and

$$
\begin{equation*}
\mathbf{G}_{\mathrm{R}} \mathbb{E}_{\mathrm{R}}-\lambda \mathbb{E} \mid=0 \tag{II,21}
\end{equation*}
$$

The mean square amplitudes of a normal vibration defined by the diagonal matrix

$$
\begin{equation*}
\left\langle\boldsymbol{Q} \mathbf{Q}^{\prime}\right\rangle=\left\langle\mathbf{Q}^{2}\right\rangle^{1}=\Delta \tag{II,22}
\end{equation*}
$$

and in the harmonic approximation are given by (6, p. 309; 26,
p. 737-754)

$$
\begin{equation*}
<\mathrm{Q}_{\mathrm{k}}^{2}>=\mathrm{h} / 8 \pi^{2} v_{\mathrm{k}} \operatorname{coth}\left(\mathrm{~h} v_{\mathrm{k}} / 2 \mathrm{kT}\right) \tag{II,23}
\end{equation*}
$$

The mean square vibrational matrix in internal coordinates $\left(\Sigma_{R}\right)$
(34, p. 726-727) is given by
${ }^{l}<Q^{\prime}>$ is diagonal due to the non-mixing character of the normal coordinates.

$$
\begin{aligned}
& \Sigma_{R}=\left\langle\mathbb{R} R^{\prime}\right\rangle=\left\langle\overline{\mathbf{v}} \mathbb{L} Q Q^{\prime} \mathbb{L}^{\prime} \overline{\mathbf{v}}^{\prime}\right\rangle \\
& =\overline{\mathbf{V}} \mathbb{L}\left\langle\mathbb{Q} \mathbb{Q}^{\prime}\right\rangle \mathbb{L}^{\prime} \overline{\mathbf{V}}^{\prime}=\overline{\mathbf{V}} \mathbb{L} \Delta \mathbb{L}^{\prime} \overline{\mathbb{V}}^{\prime} .
\end{aligned}
$$

The solution to the vibrational problem is contained in equations (II, 13) and (II, 24). The $\mathbb{V}$ and $\mathbf{G}$ matrices can be written down by inspection, and by eliminating the $\mathbb{L}$ matrix elements from the se two equations [with the aid of the normalization conditions expressed in equations (II, 14) and (II, 15)] one obtains expressions for the potential constants in terms of the measured mean-square vibrational amplitudes and vibrational frequencies.

For nitrogen dioxide the general quadratic potential function in terms of the internal valence force coordinates, $\Delta r_{1}, \Delta r_{2}$, and $\mathrm{r}^{\mathrm{e}} \Delta a$ is [see equation (II, 5)]

$$
\begin{align*}
2 V=f_{r}\left[\left(\Delta r_{1}\right)^{2}+\left(\Delta r_{2}\right)^{2}\right] & +2 f_{r r}\left(\Delta r_{1} \Delta r_{2}\right)+f_{a}\left(r^{e} \Delta a\right)^{2} \\
& +2 f_{r a}\left(\Delta r_{1}+\Delta r_{2}\right) r^{e} \Delta a \tag{II,25}
\end{align*}
$$

The molecular point group of nitrogen dioxide is $C_{2 v}$. The symmetry species (49, p. 146-162) as obtained by standard procedures are

$$
\begin{align*}
\Gamma\left(\mathrm{NO}_{2}\right) & =\Gamma(r)+\Gamma(a) \\
& =\left(\mathrm{A}_{1}+\mathrm{B}_{1}\right)+\mathrm{A}_{1} \\
& =2 \mathrm{~A}_{1}+\mathrm{B}_{1}, \tag{II,26}
\end{align*}
$$

where $A_{l}$ and $B_{1}$ denote symmetric and antisymmetric modes, respectively. The selection rules thus predict two infrared and Raman active $A_{1}$ modes (symmetric stretch and bend, respectively) and one active $B_{1}$ mode (antisymmetric stretch) for nitrogen dioxide.

Representing the column matrices $\mathbb{R}$ and $\mathbf{S}$ as

$$
\begin{equation*}
\mathbb{R}=\left\{\Delta \mathrm{r}_{1}, \mathrm{r}^{\mathrm{e}} \Delta \mathrm{a}, \Delta \mathrm{r}_{2}\right\} \tag{II,27}
\end{equation*}
$$

and

$$
\begin{equation*}
\mathbf{s}=\left\{\mathrm{s}_{1}, \mathrm{~s}_{2}, \mathrm{~s}_{3}\right\} \tag{II,28}
\end{equation*}
$$

the transformation matrix $\overline{\mathbf{V}}$ can be obtained as follows. Let the subscripts 1 and 2 denote the totally symmetric $N-O$ stretch and $<\mathrm{O}-\mathrm{N}-\mathrm{O}$ bend, respectively, and the subscript 3 , the antisymmetric N-O stretch. Then the symmetry coordinates are given by (42,
p. 902)

$$
\begin{align*}
& S_{1}=S_{r}^{\left(A_{1}\right)}=2^{-\frac{1}{2}}\left(\Delta r_{1}+\Delta r_{2}\right)  \tag{II,29}\\
& S_{2}=S_{a}^{\left(A_{1}\right)}=r^{e} \Delta a \tag{II,30}
\end{align*}
$$

and

$$
\begin{equation*}
S_{3}=S_{r}^{\left(B_{1}\right)}=2^{-\frac{1}{2}}\left(\Delta r_{1}-\Delta r_{2}\right) \tag{II,31}
\end{equation*}
$$

The orthogonality of $\overline{\mathbf{V}}$ is easily demonstrated in this case. Since an orthogonal transformation leaves the sum of squares of both sets of coordinates invariant, the following relationship should and does exist:

$$
\begin{equation*}
\left(\Delta \mathrm{r}_{1}\right)^{2}+\left(\Delta \mathrm{r}_{2}\right)^{2}+\left(\mathrm{r}^{\mathrm{e}} \Delta \mathrm{a}\right)^{2}=\mathrm{s}_{1}^{2}+\mathrm{s}_{2}^{2}+\mathrm{s}_{3}^{2} \tag{II,32}
\end{equation*}
$$

Hence, $\overline{\mathbb{V}}^{-1}=\overline{\mathbb{V}}^{\prime}$ and we have

$$
\overline{\mathbb{V}}=\left[\begin{array}{ccc}
2^{-\frac{1}{2}} & 0 & 2^{-\frac{1}{2}}  \tag{II,33}\\
& 1 & 0 \\
& & -2^{-\frac{1}{2}}
\end{array}\right]
$$

One may now write the column matrix $Q$ as

$$
\begin{equation*}
Q=\left\{Q_{1}, Q_{2}, Q_{3}\right\}=\left\{Q_{r}^{\left(\mathrm{A}_{1}\right)}, Q_{a}^{\left(\mathrm{A}_{1}\right)}, Q_{r}^{\left(\mathrm{B}_{1}\right)}\right\}, \tag{II,34}
\end{equation*}
$$

the transformation matrix $\mathbb{L}$ [see equation (II, 12)] as

$$
\mathbb{L}=\left[\begin{array}{lll}
L_{11} & L_{12} & 0  \tag{II,35}\\
L_{21} & L_{22} & 0 \\
0 & 0 & L_{33}
\end{array}\right]
$$

and the mean-square normal coordinate matrix, $\Delta$ [see equation (II, 22)], as

$$
\Delta=\left[\begin{array}{lll}
\Delta_{1} & 0 & 0  \tag{II,36}\\
& \Delta_{2} & 0 \\
& & \Delta_{3}
\end{array}\right]
$$

From the expression for $\Sigma_{R}$ [equation (II, 24)] we can relate the mean-square vibrational amplitudes $1_{\mathrm{N}-\mathrm{O}}^{2}$ and $\mathrm{l}_{\mathrm{O}}^{2} \ldots \mathrm{O}$ to the elements of the $\overline{\mathbf{V}}, L$ and $\Delta$ matrices as follows. Using the first expression in equation (II, 24)

$$
<\mathbb{R} \mathbb{R}^{\prime}>=\left[\begin{array}{ccc}
1_{N-O}^{2} & \mathrm{r}^{\mathrm{e}}<\Delta \mathrm{r} \Delta \mathrm{a}> & <\Delta \mathrm{r}_{1} \Delta \mathrm{r}_{2}>  \tag{II,37}\\
& \left(\mathrm{r}^{\mathrm{e}}\right)^{2}<\Delta \mathrm{a}^{2}> & \mathrm{r}^{\mathrm{e}}<\Delta \mathrm{r} \Delta a> \\
& & \mathrm{l}_{\mathrm{N}-\mathrm{O}}^{2}
\end{array}\right]
$$

from which

$$
\left[\begin{array}{rl}
\overline{\mathbf{V}} \mathbb{L} \Delta_{\mathbf{L}^{\prime}} \overline{\mathbb{V}}^{\prime}= \\
\left.2^{1}\left(\Delta_{1} L_{11}+\Delta_{2} L_{12}^{2}+\Delta_{3} L_{33}^{2}\right), 2^{\frac{1}{2}} \Delta_{1} L_{11} L_{12}+\Delta_{2} L_{1} 2_{22}\right) & 2^{-1}\left(\Delta_{1} L_{11}^{2}+\Delta_{2} L_{12}^{2}-\Delta_{3} L_{33}^{2}\right)  \tag{II,38}\\
\Delta_{1} L_{21}^{2}+\Delta_{2} L_{22}^{2} & , 2^{-\frac{1}{4}\left(\Delta_{1} L_{11} L_{12}+\Delta_{2} L_{12} L_{22}\right)} \\
& 2^{-1}\left(\Delta_{1} L_{11}^{2}+\Delta_{2} L_{12}^{2}+\Delta_{3} L_{33}^{2}\right)
\end{array}\right] .
$$

If one squares both sides of equation (II, 1) and takes the time average

$$
\begin{aligned}
1_{\mathrm{O}}^{2} \cdots \mathrm{O} & =\left\langle\Delta \mathrm{r}_{3}^{2}\right\rangle=2\left(1_{\mathrm{N}-\mathrm{O}}^{2}+\left\langle\Delta \mathrm{r}_{1} \Delta \mathrm{r}_{2}\right\rangle\right) \sin ^{2}(\mathrm{a} / 2) \\
& \left.+\left(\mathrm{r}^{\mathrm{e}}\right)^{2}<\Delta \mathrm{a}^{2}>\cos ^{2}(\mathrm{a} / 2)+2 \mathrm{r}^{\mathrm{e}}<\Delta \mathrm{r} \Delta \mathrm{a}\right\rangle \sin a .
\end{aligned}
$$

Combining equations (II, 37), (II, 38) and (II, 39), one obtains

$$
\begin{equation*}
1_{\mathrm{N}-\mathrm{O}}^{2}=2^{-1}\left(\Delta_{1} L_{11}^{2}+\Delta_{2} L_{22}^{2}+\Delta_{3} L_{33}^{2}\right) \tag{II.40}
\end{equation*}
$$

and

$$
\begin{align*}
1_{\mathrm{O}}^{2} \ldots \mathrm{O}=2\left(\Delta_{1} \mathrm{~L}_{11}^{2}\right. & \left.+\Delta_{2} \mathrm{~L}_{12}^{2}\right) \sin ^{2}(\mathrm{a} / 2)+\left(\Delta_{1} \mathrm{~L}_{21}^{2}+\Delta_{2} \mathrm{~L}_{22}^{2}\right) \cos ^{2}(\mathrm{a} / 2) \\
& +2^{\frac{1}{2}}\left(\Delta_{1} L_{11} L_{21}+\Delta_{2} L_{12} L_{22}\right) \sin a . \tag{II,41}
\end{align*}
$$

The $\mathbb{F}_{S}$ and $\mathbb{G}_{S}$ matrices may be written down immediately
(42, p. 902)

$$
\mathrm{F}_{\mathrm{S}}=\left[\begin{array}{ccc}
\mathrm{f}_{\mathrm{r}}+\mathrm{f}_{\mathrm{rr}} & 2^{\frac{1}{2}} \mathrm{f}_{\mathrm{ra}} & 0  \tag{II,42}\\
& \mathrm{f}_{\mathrm{a}} & 0 \\
& & \mathrm{f}_{\mathrm{r}}-\mathrm{f}_{\mathrm{rr}}
\end{array}\right]=\left[\begin{array}{ccc}
\mathrm{F}_{11} & \mathrm{~F}_{12} & 0 \\
& \mathrm{~F}_{22} & \\
& & \mathrm{~F}_{33}
\end{array}\right]
$$

and

$$
\begin{align*}
& \mathbb{G}_{S}=\left[\begin{array}{lll}
2 \mu_{N} \cos ^{2}(a / 2)+\mu_{O}, & -2^{3 / 2} \mu_{N} \sin (a / 2) \cos (\alpha / 2, & 0 \\
& 2\left(2 \mu_{N} \sin ^{2}(a / 2)+\mu_{O}\right. & \\
& & 2 \mu_{N} \sin ^{2}(a / 2)+\mu_{O}
\end{array}\right] \\
& =\left[\begin{array}{ccc}
G_{11} & G_{12} & 0 \\
& G_{22} & 0 \\
& & G_{33}
\end{array}\right] . \tag{II,43}
\end{align*}
$$

Solving equation (II, 14) for $\mathbb{F}_{S}^{-1}$, one obtains

$$
\begin{equation*}
\mathbb{F}_{S}^{-1}=\mathbb{L} \mathbb{A}^{-1} \mathbb{L}^{1} \tag{II,44}
\end{equation*}
$$

Since

$$
\mathbb{F}_{S}^{-1}=\left[\begin{array}{ccc}
F_{22} / \beta & -F_{12} / \beta & 0  \tag{II,45}\\
& F_{11} / \beta & 0 \\
& & F_{33}^{-1}
\end{array}\right]
$$

and

$$
\mathbb{N}^{-1}=\left[\begin{array}{ccc}
1 / \lambda_{1} & 0 & 0  \tag{II,46}\\
& 1 / \lambda_{2} & 0 \\
& & 1 / \lambda_{3}
\end{array}\right]
$$

one obtains with equations (II, 35) and (II, 43),

$$
\left[\begin{array}{lll}
G_{11} & G_{12} & 0 \\
& G_{22} & 0 \\
& & G_{33}
\end{array}\right]=\left[\begin{array}{ccc}
L_{11}^{2}+L_{12}^{2} & L_{11} L_{21}+L_{12} L_{22} & 0 \\
& L_{21}^{2}+L_{22}^{2} & 0 \\
& & L_{33}^{2}
\end{array}\right] \text { (II, 47) }
$$

and

$$
\begin{aligned}
& {\left[\begin{array}{ccc}
F_{22} / \beta & -F_{12} / \beta & 0 \\
& F_{11} / \beta & 0 \\
& & F_{33}^{-1}
\end{array}\right]} \\
& =\left[\begin{array}{llll}
L_{11}^{2} \lambda_{1}^{-1}+L_{12}^{2} \lambda_{2}^{-1}, & L_{11} L_{21} \lambda_{1}^{-1}+L_{12} L_{22^{\lambda^{-1}}}, & 0 \\
& L_{21}^{2} \lambda_{1}^{-1}+L_{22}^{2} \lambda_{2}^{-1} & 0 \\
& & 0 & \\
& & L_{33}^{2} \lambda_{3}^{-1}
\end{array}\right] . \text { (II, 48) }
\end{aligned}
$$

The solution of equation (II, 20) can be written down by inspection (30, p. 3) giving

$$
\begin{equation*}
\lambda_{1}+\lambda_{2}=G_{11} F_{11}+G_{22} F_{22}+2 G_{12} F_{22}, \tag{II,49}
\end{equation*}
$$

$$
\begin{equation*}
\lambda_{1} \lambda_{2}=\beta\left(G_{11} G_{22}-G_{12}^{2}\right)=\beta \bar{\gamma}, \tag{II,50}
\end{equation*}
$$

and

$$
\begin{equation*}
\lambda_{3}=G_{33} F_{33} \tag{II,51}
\end{equation*}
$$

Combining equations (II, 47) and (II, 48), one obtains

$$
\begin{align*}
& L_{11}^{2}=\left[\lambda_{1} / \beta\left(\lambda_{1}-\lambda_{2}\right)\right]\left(-\lambda_{2} F_{22}+\beta G_{11}\right)  \tag{II,52}\\
& L_{22}^{2}=\left[\lambda_{2} / \beta\left(\lambda_{1}-\lambda_{2}\right)\right]\left(\lambda_{1} F_{11}-\beta G_{22}\right)  \tag{II,53}\\
& L_{33}^{2}=G_{33}=\lambda_{3} / F_{33}  \tag{II,54}\\
& L_{12}^{2}=\left[\lambda_{2} / \beta\left(\lambda_{1}-\lambda_{2}\right)\right]\left(\lambda_{1} F_{22}-\beta G_{11}\right)  \tag{II,55}\\
& L_{21}^{2}=\left[\lambda_{1} / \beta\left(\lambda_{1}-\lambda_{2}\right)\right]\left(-\lambda_{2} F_{11}+\beta G_{22}\right)  \tag{II,56}\\
& L_{11} L_{21}=\left[\lambda_{1} / \beta\left(\lambda_{1}-\lambda_{2}\right)\right]\left(\lambda_{2} F_{12}+\beta G_{12}\right)  \tag{II,57}\\
& L_{12} L_{22}=\left[-\lambda_{2} / \beta\left(\lambda_{1}-\lambda_{2}\right)\right]\left(\lambda_{1} F_{12}+\beta G_{12}\right) \tag{II,58}
\end{align*}
$$

Finally, by condensing the various relationships one has

$$
\begin{align*}
& 1_{N-O}^{2}=A_{1} F_{22}+A_{2}\left(F_{11} F_{22}-F_{12}^{2}\right)+A_{3}  \tag{II,59}\\
& 1_{O}^{2} \ldots O=A_{4} F_{22}+A_{5} F_{11}+A_{6} F_{12}+A_{7},  \tag{II,60}\\
& A_{8}=A_{9} F_{22}+A_{10} F_{11}+A_{11} F_{12} \tag{II,61}
\end{align*}
$$

and

$$
\begin{equation*}
F_{33}=\lambda_{3} / G_{33} \tag{II,62}
\end{equation*}
$$

where

$$
A_{1}=\bar{c} f / 2 g, A_{2}=G_{11} \bar{b} \bar{c} / 2 d g, A_{3}=G_{33} e / 2, A_{4}=2 \bar{i} \sin ^{2}(a / 2)
$$

$$
A_{5}=\bar{i} \cos ^{2}(a / 2), A_{6}=-2^{3 / 2} \bar{i} \sin (a / 2) \cos (a / 2)
$$

$$
A_{7}=(\bar{b} / g)\left[2 G_{11} \sin ^{2} a / 2+\left(G_{22} \cos a / 2+2^{3 / 2} G_{12} \sin a / 2\right) \cos a / 2\right]
$$

$$
\begin{equation*}
A_{8}=\bar{h}, A_{9}=G_{22}, A_{10}=G_{11}, A_{11}=2 G_{12} \tag{II,63}
\end{equation*}
$$

with

$$
\begin{gather*}
\bar{b}=\Delta_{1} \lambda_{1}-\Delta_{2} \lambda_{2}, \bar{c}=\bar{\gamma}, d=\lambda_{1} \lambda_{2}, \quad e=\Delta_{3}, f=\Delta_{2}-\Delta_{2}, \\
g=\lambda_{1}-\lambda_{2}, \bar{h}=\lambda_{1}+\lambda_{2}, \quad \bar{i}=\bar{c} f / g=2 A_{1} . \tag{II,64}
\end{gather*}
$$

Since equation (II, 59) is quadratic in $\mathrm{F}_{12}$, two sets of solutions are possible. The most physically reasonable is selected.

During the course of this work J. C. Decius (12, p. 241-248) introduced the notion of a compliance matrix. With this approach the secular equation takes the form

$$
\begin{equation*}
|\mathbb{C} \mathbb{K}-\phi \mathbb{E}|=0 \tag{II,65}
\end{equation*}
$$

where $\mathbb{K}=\mathbb{G}^{-1}, \mathbb{C}=\mathbb{F}^{-1}$, and $\phi=\lambda^{-1}$. Since this paper describes the determination of compliance constants from normal frequencies and mean-square amplitudes (or centrifugal distortion data), treating among other molecules, nitrogen dioxide as an example, ${ }^{1}$ no attempt will be made here to duplicate this development. Since the compliance constants to be reported in this thesis correspond to the inverse of the $\mathbb{F}_{S}$ matrix defined in equation (II, 45), the symmetrized compliance matrix $\mathbb{C}_{S}$ (defined in terms of valence force symmetry coordinates) will take the form

[^12]\[

\mathbb{C}_{S}=\left[$$
\begin{array}{ccc}
\mathrm{C}_{11} & \mathrm{C}_{12} & 0  \tag{II,66}\\
& \mathrm{C}_{22} & 0 \\
& & \mathrm{C}_{33}
\end{array}
$$\right]=\left[$$
\begin{array}{ccc}
\mathrm{F}_{22} / \beta & -\mathrm{F}_{12} / \beta & 0 \\
& \mathrm{~F}_{11} / \beta & 0 \\
& & \mathrm{~F}_{33}^{-1}
\end{array}
$$\right]
\]

The compliance matrix of nitrogen dioxide reported by Decius is defined in terms of central force coordinates, it differs numerically from $\mathbb{C}_{S}$ of equation (II, 66).

## Computation of Potential and Compliance Constants

The numerical solutions of equations (II, 59) - (II, 61) were obtained by the use of the university Alwac III-E digital computer. Since the computer program is rather specialized (non-linear $\mathrm{XY}_{2}$ molecules), it will not be reproduced here though a brief description will be given. The vibrational frequencies (l, p. 413-427) used are given ${ }^{1}$ in Table 24. The computer output gave elliptical contours (22, p. 596-598) corresponding to the observed values of $1_{N-O}$ and ${ }^{1}$ O... O' respectively, such that on each of the two contours (corresponding to $l_{N-O}$ and $l_{\mathrm{O}} \cdots \mathrm{O}^{\text {}}$ ), all real combinations of the symmetrized potential constants $F_{11}, F_{22}$ and $F_{12}$ were represented. Systematic investigation of the output contours identified their approximate intersections (ideally, there are two of them); the se

[^13]intersections were subsequently calculated exactly. Since the intersections represented two combinations of symmetrized potential constants compatible with both electron diffraction and spectroscopic data, they are the solutions of equations (II, 59) - (II, 61). Figure 5 is a plot of these contours. Finally, the se solutions were transformed to the corresponding ones in terms of the internal potential constants $f_{r}, f_{r r}, f_{a}$ and $f_{r a}$ [see equation (II, 42)].

In addition to the potential constants obtained by the method described above, various combinations of frequencies (see Table 30a) and vibrational amplitudes were investigated using a newly devised least-squares program of $R$. Ottinger. ${ }^{1}$ The elements of the diagonal weight matrix used were given by

$$
\begin{equation*}
\left(\mathbb{P}_{O t}\right)_{v_{i}}=1 \quad \text { and }\left(\mathbb{P}_{O t}\right)_{l_{i j}^{2}}^{2}=2500 \tag{II,67}
\end{equation*}
$$

These results are expressed in terms of the symmetrized compliance constants defined in equation (II, 66).

Errors in the Internal Potential Constants Derived from the Intersections of Elliptical Contours

A complete error analysis should include uncertainties arising from the determination of the vibrational amplitudes, normal frequencies, interatomic distances, physical constants and the errors
${ }^{1}$ Ottinger, Robert. Private communication. Corvallis, Oregon. Oregon State University, 1964.
arising from the method of calculation employed. The effect in the potential constants arising from the uncertainties in the vibrational amplitudes were estimated as follows. Let $f_{i}$ denote one of the internal potential constants $f_{r}, f_{r r}, f_{a}$, and $f_{r a}$, then

$$
\begin{equation*}
\mathrm{f}_{\mathrm{i}}=\mathrm{f}_{\mathrm{i}}\left(\mathrm{r}_{\mathrm{N}-\mathrm{O}}, \mathrm{r}_{\mathrm{O}} \ldots \mathrm{O}^{\prime} \mathrm{l}_{\mathrm{N}-\mathrm{O}}, \mathrm{l}_{\mathrm{O}} \ldots \mathrm{O}^{\prime} v_{1}, v_{2}, v_{3}\right) \tag{II,68}
\end{equation*}
$$

Further, let $\sigma_{\left(f_{i}\right)}$ be defined as

$$
\begin{align*}
& \left.2 q_{f_{i}}\right)=f_{i}\left[r_{\mathrm{N}-\mathrm{O}}, \mathrm{r}_{\mathrm{O}} \ldots \mathrm{O}^{,} \mathrm{l}_{\mathrm{N}-\mathrm{O}}+\mathrm{m}_{\mathrm{T}}\left(\mathrm{l}_{\mathrm{N}-\mathrm{O}}\right), \mathrm{l}_{\mathrm{O}} \ldots \mathrm{O}+{ }_{\mathrm{n}} \sigma_{\mathrm{T}}\left(\mathrm{l}_{\mathrm{O}} \ldots \mathrm{O}\right), v_{1}, v_{2}, v_{3}\right] \\
& -\mathrm{f}_{\mathrm{i}}\left(\mathrm{r}_{\mathrm{N}-\mathrm{O}}, \mathrm{r}_{\mathrm{O}} \ldots \mathrm{O}^{\left., 1_{\mathrm{N}-\mathrm{O}}, \mathrm{l}_{\mathrm{O}} \ldots \mathrm{O}, v_{1}, v_{2}, v_{3}\right) .}\right. \tag{II,69}
\end{align*}
$$

It is clear that $\sigma_{\left(f_{i}\right)}$ (as a very rough approximation) will reflect the uncertainty in $f_{i}$ arising from those in the vibrational amplitudes. The values of the coefficients $m$ and $n$ were obtained from the error matrix given in Table 24. The correlation between $l_{N-O}$ and ${ }^{1} \mathrm{O} \ldots \mathrm{O}$ is positive indicating that the error which increases one mean amplitude also increases the other, hence, $m$ and $n$ should have the same algebraic signs. Arbitrarily, $m$ was taken as two, and $n$ as one-half. The results are given in Tables ${ }^{1} 26$ a and 26 b .

No attempt was made to estimate the errors arising from the determination of normal frequencies, internuclear distances, and physical constants. From the form of equations (II-59) to (II-64), it was felt that these errors would be negligible by comparison to those

[^14]of the vibrational amplitudes.

Errors in the Symmetrized Compliance Constants Obtained from
Least-Squares Fitting

The only errors estimated here were the standard errors obtained from least-squares fitting (Table 30a). The significance of these errors is mainly that of indicating the compatibility of the vibrational amplitudes and the normal frequencies with respect to the compliance constants.

## Final Results

The constants used in the various calculations are given in Tables 23-25. The final results are given in Tables 27-30b. Comparison of the internal potential constants determined in this work with those obtained by isotopic spectroscopy (1, p. 413-427) shows the agreement to be good (Table 27). The comparison of the observed and calculated frequencies (derived from the final internal potential constants), as given in Table 29, is pleasing, especially so in the case of the $\omega_{i}$ 's. The comparison of the observed vibrational amplitudes from this work with those calculated by Cyvin (10, p. 117) from potential constants derived from isotopic spectroscopy, is
given in Table 29. Again the agreement ${ }^{1}$ is good. The numerous compliance constant results given in Tables 30 a and 30 b are discussed in the next section.
${ }^{1}$ Though the observed amplitudes and calculated ones correspond to two different temperatures ( $380^{\circ}$ and $298^{\circ} \mathrm{K}$, respectively), the temperature effect in this case is surely very small since the vibrational frequencies are high.

## SUMMARY

## Part I

The molecular geometry of nitrogen dioxide was determined. The parameter values of $\mathrm{r}_{\mathrm{N}-\mathrm{O}}$ ' $^{\mathrm{O}} \mathrm{O} \ldots \mathrm{O}$, and $<\mathrm{O}-\mathrm{N}-\mathrm{O}$ agree well with the corresponding microwave results (5, p. 1040-1043). Conservative estimates of standard errors lead to probable accuracies of $0.1,0.2$, and 0.5 percent for $\mathrm{r}_{\mathrm{N}-\mathrm{O}}{ }^{\prime} \mathrm{r}_{\mathrm{O}} \ldots \mathrm{O}$, and $<\mathrm{O}-\mathrm{N}-\mathrm{O}$, respectively. Corresponding conservative estimates for the root-mean-square amplitudes of vibration lead to seven percent for $1_{\mathrm{N}-\mathrm{O}}$ and 11 percent for $\mathrm{l}_{\mathrm{O}} \ldots \mathrm{O}$.

## Part II

The two sets of internal quadratic potential constants determined from $\left\{1_{\mathrm{N}-\mathrm{O}}, \mathrm{l}_{\mathrm{O}} \ldots \mathrm{O}^{\left., \mathrm{r}_{\mathrm{N}-\mathrm{O}}, \mathrm{r}_{\mathrm{O}} \ldots \mathrm{O}^{\prime} v_{1}, v_{2}, v_{3}\right\} \text { and from } .}\right.$ $\left\{1_{\mathrm{N}-\mathrm{O}}, \mathrm{l}_{\mathrm{O}} \cdots \mathrm{O}^{,} \mathrm{r}_{\mathrm{N}-\mathrm{O}}, \mathrm{r}_{\mathrm{O}} \ldots \mathrm{O}^{, \omega_{1}}, \omega_{2}, \omega_{3}\right\}$ agree well with those obtained from isotopic spectroscopy. The comparison of calculated and observed frequencies indicated that there is probably very little anharmonicity in the O..O motion. Further, the observed vibrational amplitudes agree well with those calculated by Cyvin.

The numerous least-squares fitting for symmetrized compliance constants indicated that (1) the results are essentially
insensitive to the bond angle ${ }^{1}$ parameter used within reasonable limits, (2) the off-diagonal compliance constants are quite sensitive to input data combinations, where the diagonal elements are not. The agreement between the various sets of compliance constants and internal potential constants suggest very strongly that vibrational amplitudes from electron diffraction (at least for small polyatomics composed of similar atoms) are compatible with spectroscopy data (vibrational frequencies) with respect to either potential or compliance constant determinations. This statement is further reinforced by the various comparisons of observed and calculated frequencies.

In conclusion, the reliability and consistency of the vibrational amplitudes from electron diffraction for potential or compliance constant determinations can be regarded as favorable, at least for small polyatomic molecules composed of similar atoms.

[^15]
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APPENDICES

APPENDIX I

TABLES

Table 1. Previous structure investigations of nitrogen dioxide.

| $\mathrm{r}_{\mathrm{N}-\mathrm{O}}, \AA$ | <O-N-O, deg. | Comments |
| :---: | :---: | :---: |
| $1.21 \pm .02$ | $130 \pm 2$ | eiectron diffraction (31). ${ }^{\text {(a) }}$ |
| $1.20 \pm .02$ | $132 \pm 3$ | electron diffraction (9). (a) |
| 1.21 | 141 | Spurr (50, p. 27) reanalyzed the electron diffraction data of Maxwell and Mosley (31). |
| 1. 28 | 154 | partial analysis of ultraviolet spectrum (15). |
| $1.188 \pm .004$ | $134.07 \pm .25$ | infrared (32). |
| $1.189 \pm .003$ | $133.95 \pm .10$ | calculated (45) from rotational data of Keller and Nielsen (28) and Moore (32). |
| $1.186 \pm .003$ | $133.53 \pm .15$ | electron diffraction. ${ }^{(b), 1}$ |
| 1. 197 | 134.25 | microwave (5). |

${ }^{\text {(a) }}$ Visual method (8, p. 250-254; 41, p. 867-881).
(b)

Sector-microphotometer method (27).
${ }^{1}$ Severinsson, Robert. Private communication. Oslo, Norway. Universitetets Kjemisk Institutt, 1955.

Table 2. Electron intensity incident on the photographic plate: $\mathrm{h}=478.00 \mathrm{~mm}$.

| s | $I_{p}^{a(1)}$ |  | $I_{p}^{a(2)}$ |  | $\mathrm{I}_{\mathrm{p}}^{\mathrm{a}(3)}$ |  | $\mathrm{I}_{\mathrm{p}}^{\mathrm{a(4)}}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | L | R | L | R | L | R | L | R |
| 2.50 | 0.4570 | 0.5110 | 0.3820 | 0.4240 | 0.5050 | 0.5490 | 0.4220 | 0.4500 |
| 2.75 | 0.4470 | 0.4920 | 0.3730 | 0.4100 | 0.4930 | 0.5310 | 0.4110 | 0.4370 |
| 3.00 | 0.4370 | 0.4780 | 0.3640 | 0.3960 | 0.4820 | 0.5160 | 0.4030 | 0.4240 |
| 3.25 | 0.4310 | 0.4670 | 0.3580 | 0.3850 | 0.4710 | 0.5020 | 0.3960 | 0.4120 |
| 3.50 | 0.4170 | 0.4530 | 0.3490 | 0.3720 | 0.4620 | 0.4900 | 0.3880 | 0.4010 |
| 3.75 | 0.4060 | 0.4370 | 0.3390 | 0.3590 | 0.4480 | 0.4720 | 0.3770 | 0.3880 |
| 4.00 | 0.3920 | 0.4230 | 0.3270 | 0.3460 | 0.4340 | 0.4540 | 0.3620 | 0.3750 |
| 4.25 | 0.3820 | 0.4130 | 0.3200 | 0.3340 | 0.4250 | 0.4420 | 0.3530 | 0.3650 |
| 4.50 | 0.3840 | 0.4120 | 0.3200 | 0.3330 | 0.4250 | 0.4420 | 0.3500 | 0.3630 |
| 4.75 | 0.3930 | 0.4210 | 0.3270 | 0.3410 | 0.4360 | 0.4520 | 0.3610 | 0.3730 |
| 5.00 | 0.4120 | 0.4400 | 0.3440 | 0.3540 | 0.4540 | 0.4730 | 0.3780 | 0.3900 |
| 5.25 | 0.4350 | 0.4650 | 0.3640 | 0.3740 | 0.4790 | 0.4960 | 0.3980 | 0.4120 |
| 5.50 | 0.4580 | 0.4880 | 0.3870 | 0.3970 | 0.5050 | 0.5240 | 0.4220 | 0.4360 |
| 5.75 | 0.4780 | 0.5120 | 0.4040 | 0.4160 | 0.5280 | 0.5470 | 0.4420 | 0.4550 |
| 6.00 | 0.4900 | 0.5250 | 0.4140 | 0.4290 | 0.5440 | 0.5620 | 0.4550 | 0.4670 |
| 6.25 | 0.4910 | 0.5290 | 0.4170 | 0.4320 | 0.5480 | 0.5630 | 0.4590 | 0.4710 |
| 6.50 | 0.4820 | 0.5220 | 0.4110 | 0.4250 | 0.5410 | 0.5550 | 0.4520 | 0.4630 |
| 6.75 | 0.4670 | 0.5100 | 0.3990 | 0.4120 | 0.5250 | 0.5360 | 0.4350 | 0.4510 |
| 7.00 | 0.4470 | 0.4890 | 0.3830 | 0.3950 | 0.5050 | 0.5150 | 0.4180 | 0.4310 |
| 7.25 | 0.4180 | 0,4620 | 0.3590 | 0.3690 | 0.4800 | 0.4840 | 0.3920 | 0.4050 |
| 7.50 | 0.3950 | 0.4370 | 0.3340 | 0.3450 | 0.4520 | 0.4550 | 0.3670 | 0.3820 |
| 7.75 | 0.3730 | 0.4160 | 0.3170 | 0.3240 | 0.4280 | 0.4280 | 0.3490 | 0.3630 |
| 8.00 | 0.3560 | 0.3970 | 0.3020 | 0.3080 | 0.4090 | 0.4060 | 0.3320 | 0.3470 |
| 8.25 | 0.3420 | 0.3860 | 0.2920 | 0.2960 | 0.3990 | 0.3900 | 0.3210 | 0.3340 |

Table 2 (continued).

| s | $I_{p}^{a(1)}$ |  | $\mathrm{I}_{\mathrm{p}}^{\mathrm{a}(2)}$ |  | $I_{p}^{a(3)}$ |  | $I_{p}^{a(4)}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | L | R | L | R | L | R | L | R |
| 8.50 | 0.3350 | 0.3780 | 0.2850 | 0.2880 | 0.3920 | 0.3800 | 0.3140 | 0.3270 |
| 8.75 | 0.3280 | 0.3720 | 0.2790 | 0.2830 | 0.3850 | 0.3730 | 0.3090 | 0.3220 |
| 9.00 | 0.3230 | 0.3690 | 0.2770 | 0.2760 | 0.3810 | 0.3570 | 0.3030 | 0.3200 |
| 9.25 | 0.3190 | 0.3660 | 0.2740 | 0.2730 | 0.3770 | 0.3620 | 0.3010 | 0.3180 |
| 9.50 | 0.3160 | 0.3650 | 0.2710 | 0.2690 | 0.3740 | 0.3580 | 0.2970 | 0.3160 |
| 9.75 | 0.3130 | 0.3630 | 0.2680 | 0.2650 | 0.3730 | 0.3530 | 0.2940 | 0.3130 |
| 10.00 | 0.3110 | 0.3600 | 0.2670 | 0.2640 | 0.3720 | 0.3510 | 0.2920 | 0.3110 |
| 10.25 | 0.3080 | 0.3590 | 0.2660 | 0.2620 | 0.3720 | 0.3500 | 0.2910 | 0.3100 |
| 10.50 | 0.3070 | 0.3630 | 0.2680 | 0.2620 | 0.3720 | 0.3510 | 0.2920 | 0.3110 |
| 10.75 | 0.3110 | 0.3670 | 0.2690 | 0.2650 | 0.3770 | 0.3530 | 0.2930 | 0.3130 |
| 11.00 | 0.3130 | 0.3710 | 0.2720 | 0.2680 | 0.3800 | 0.3580 | 0.2980 | 0.3150 |
| 11.25 | 0.3170 | 0.3760 | 0.2750 | 0.2710 | 0.3850 | 0.3610 | 0.3000 | 0.3190 |
| 11.50 | 0.3160 | 0.3800 | 0.2760 | 0.2720 | 0.3880 | 0.3620 | 0.3010 | 0.3220 |
| 11.75 | 0.3150 | 0.3810 | 0.2770 | 0.2720 | 0.3900 | 0.3630 | 0.3000 | 0.3210 |
| 12.00 | 0.3110 | 0.3800 | 0.2740 | 0.2700 | 0.3850 | 0.3590 | 0.2960 | 0.3180 |
| 12.25 | 0.3040 | 0.3750 | 0.2670 | 0.2630 | 0.3790 | 0.3520 | 0.2890 | 0.3120 |
| 12.50 | 0.2950 | 0.3660 | 0.2600 | 0.2560 | 0.3680 | 0.3420 | 0.2800 | 0.3040 |
| 12.75 | 0.2860 | 0.3570 | 0.2520 | 0.2470 | 0.3570 | 0.3310 | 0.2700 | 0.2940 |
| 13.00 | 0.2750 | 0.3480 | 0.2420 | 0.2360 | 0.3450 | 0.3190 | 0.2580 | 0.2840 |
| 13.25 | 0.2660 | 0.3380 | 0.2350 | 0.2290 | 0.3340 | 0.3080 | 0.2500 | 0.2750 |
| 13.50 | 0.2610 | 0.3330 | 0.2300 | 0.2220 | 0.3270 | 0.2990 | 0.2430 | 0.2700 |
| 13.75 | 0.2560 | 0.3290 | 0.2290 | 0.2170 | 0.3230 | 0.2940 | 0.2400 | 0.2640 |
| 14.00 | 0.2530 | 0.3270 | 0.2270 | 0.2150 | 0.3220 | 0.2900 | 0.2370 | 0.2630 |
| 14.25 | 0.2520 | 0.3270 | 0.2270 | 0.2130 | 0.3200 | 0.2880 | 0.2370 | 0.2630 |

Table 2 (continued).

|  | $\mathrm{I}_{\mathrm{p}}^{\mathrm{a}(\mathrm{l})}$ |  | $\mathrm{I}_{\mathrm{p}}^{\mathrm{a}(2)}$ |  | $\mathrm{I}_{\mathrm{p}}^{\mathrm{a}(3)}$ |  | $I_{p}^{a(4)}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| s | L | R | L | R | L | R | L | R |
| 14.50 | 0.2520 | 0.3280 | 0.2290 | 0.2130 | 0.3220 | 0.2900 | 0.2370 | 0.2630 |
| 14.75 | 0.2530 | 0.3290 | 0.2310 | 0.2130 | 0.3230 | 0.2900 | 0.2370 | 0.2650 |
| 15.00 | 0.2530 | 0.3310 | 0.2320 | 0.2140 | 0.3240 | 0.2910 | 0.2390 | 0.2670 |
| 15.25 | 0.2530 | 0.3320 | 0.2330 | 0.2140 | 0.3240 | 0.2920 | 0.2390 | 0.2690 |
| 15.50 | 0.2540 | 0.3330 | 0.2340 | 0.2140 | 0.3240 | 0.2910 | 0.2370 | 0.2700 |
| 15.75 | 0.2540 | 0.3340 | 0.2350 | 0.2150 | 0.3250 | 0.2910 | 0.2370 | 0.2710 |
| 16.00 | 0.2550 | 0.3350 | 0.2380 | 0.2160 | 0.3260 | 0.2910 | 0.2370 | 0.2720 |
| 16.25 | 0.2550 | 0.3370 | 0.2390 | 0.2160 | 0.3260 | 0.2910 | 0.2370 | 0.2730 |
| 16.50 | 0.2540 | 0.3400 | 0.2400 | 0.2170 | 0.3280 | 0.2910 | 0.2380 | 0.2740 |
| 16.75 | 0.2550 | 0.3410 | 0.2420 | 0.2170 | 0.3290 | 0.2920 | 0.2370 | 0.2770 |
| 17.00 | 0.2550 | 0.3420 | 0.2430 | 0.2180 | 0.3300 | 0.2920 | 0.2370 | 0.2760 |
| 17.25 | 0.2550 | 0.3430 | 0.2430 | 0.2170 | 0.3290 | 0.2890 | 0.2360 | 0.2760 |
| 17.50 | 0.2520 | 0.3430 | 0.2420 | 0.2160 | 0.3280 | 0.2880 | 0.2350 | 0.2760 |
| 17.75 | 0.2490 | 0.3420 | 0.2390 | 0.2130 | 0.3270 | 0.2850 | 0.2320 | 0.2740 |
| 18.00 | 0.2450 | 0.3400 | 0.2360 | 0.2100 | 0.3220 | 0.2800 | 0.2270 | 0.2710 |
| 18.25 | 0.2410 | 0.3360 | 0.2330 | 0.2060 | 0.3170 | 0.2740 | 0.2220 | 0.2670 |
| 18.50 | 0.2360 | 0.3320 | 0.2280 | 0.2010 | 0.3120 | 0.2670 | 0.2190 | 0.2620 |
| 18.75 | 0.2320 | 0.3300 | 0.2250 | 0.1980 | 0.3070 | 0.2630 | 0.2120 | 0.2580 |
| 19.00 | 0.2270 | 0.3270 | 0.2220 | 0.1950 | 0.3030 | 0.2590 | 0.2110 | 0.2560 |
| 19.25 | 0.2260 | 0.3250 | 0.2210 | 0.1930 | 0.3000 | 0.2570 | 0.2100 | 0.2530 |
| 19.50 | 0.2250 | 0.3240 | 0.2210 | 0.1920 | 0.2990 | 0.2560 | 0.2100 | 0.2520 |
| 19.75 | 0.2250 | 0.3240 | 0.2210 | 0.1920 | 0.2980 | 0.2560 | 0.2080 | 0.2520 |
| 20.00 | 0.2260 | 0.3260 | 0.2220 | 0.1930 | 0.2990 | 0.2580 | 0.2100 | 0.2540 |
| 20.25 | 0.2270 | 0.3280 | 0.2220 | 0.1940 | 0.3010 | 0.2590 | 0.2110 | 0.2550 |

Table 2 (continued).

| s | $\mathrm{I}_{\mathrm{p}}^{\mathrm{a}(1)}$ |  | $\mathrm{I}_{\mathrm{p}}^{\mathrm{a}(2)}$ |  | $\mathrm{I}_{\mathrm{p}}^{\mathrm{a}(3)}$ |  | $\mathrm{I}_{\mathrm{p}}^{\mathrm{a}(4)}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | L | R | L | R | L | R | L | R |
| 20.50 | 0.2280 | 0.3300 | 0.2240 | 0.1950 | 0.3030 | 0.2600 | 0.2120 | 0.2560 |
| 20.75 | 0.2310 | 0.3310 | 0.2240 | 0.1960 | 0.3050 | 0.2620 | 0.2120 | 0.2570 |

L Left branch
R Right branch

Table 3. Electron intensity incident on the photographic plate: $\mathrm{h}=192.07 \mathrm{~mm}$.

| $s$ | $\mathrm{I}_{\mathrm{p}}^{\mathrm{b}(1)}$ |  | $I_{p}^{b(2)}$ |  | $\mathrm{I}_{\mathrm{p}}^{\mathrm{b}(3)}$ |  | $I_{p}^{b(4)}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | L | R | L | R | L | R | L | R |
| 10.25 | 0.9401 | 1.0580 | 1.0959 | 1.2336 | 0.9249 | 1.0681 | 0.9356 | 1.0879 |
| 10.50 | 0.9200 | 1.0389 | 1.0658 | 1.2009 | 0.9031 | 1.0325 | 0.9103 | 1.0619 |
| 10.75 | 0.8998 | 1.0188 | 1.0514 | 1.1853 | 0.8870 | 1.0111 | 0.8902 | 1.0429 |
| 11.00 | 0.8868 | 1.0076 | 1.0311 | 1.1660 | 0.8740 | 0.9951 | 0.8786 | 1.0338 |
| 11.25 | 0.8739 | 0.9890 | 1.0150 | 1.1481 | 0.8636 | 0.9830 | 0.8670 | 1.0211 |
| 11.50 | 0.8621 | 0.9707 | 1.0027 | 1.1320 | 0.8520 | 0.9708 | 0.8485 | 1.0050 |
| 11.75 | 0.8402 | 0.9522 | 0.9780 | 1.1050 | 0.8335 | 0.9461 | 0.8322 | 0.9803 |
| 12.00 | 0.8177 | 0.9222 | 0.9538 | 1.0682 | 0.8083 | 0.9103 | 0.8097 | 0.9500 |
| 12.25 | 0.7839 | 0.8809 | 0.9118 | 1.0274 | 0.7780 | 0.8750 | 0.7859 | 0.9091 |
| 12.50 | 0.7409 | 0.8402 | 0.8796 | 0.9780 | 0.7398 | 0.8311 | 0.7441 | 0.8659 |
| 12.75 | 0.7080 | 0.8050 | 0.8360 | 0.9294 | 0.7050 | 0.7939 | 0.7110 | 0.8211 |
| 13.00 | 0.6719 | 0.7560 | 0.7904 | 0.8820 | 0.6728 | 0.7482 | 0.6760 | 0.7759 |
| 13.25 | 0.6384 | 0.7184 | 0.7518 | 0.8244 | 0.6383 | 0.7133 | 0.6443 | 0.7377 |
| 13.50 | 0.6090 | 0.6977 | 0.7259 | 0.7960 | 0.6110 | 0.6873 | 0.6150 | 0.7163 |
| 13.75 | 0.5900 | 0.6770 | 0.7008 | 0.7739 | 0.5920 | 0.6568 | 0.5920 | 0.6903 |
| 14.00 | 0.5760 | 0.6575 | 0.6905 | 0.7550 | 0.5790 | 0.6514 | 0.5790 | 0.6790 |
| 14.25 | 0.5670 | 0.6494 | 0.6780 | 0.7462 | 0.5720 | 0.6413 | 0.5740 | 0.6698 |
| 14.50 | 0.5600 | 0.6433 | 0.6728 | 0.7354 | 0.5660 | 0.6373 | 0.5670 | 0.6616 |
| 14.75 | 0.5560 | 0.6363 | 0.6677 | 0.7290 | 0.5630 | 0.6302 | 0.5600 | 0.6544 |
| 15.00 | 0.5510 | 0.6312 | 0.6626 | 0.7207 | 0.5590 | 0.6251 | 0.5560 | 0.6494 |
| 15.25 | 0.5460 | 0.6231 | 0.6565 | 0.7143 | 0.5550 | 0.6221 | 0.5510 | 0.6433 |
| 15.50 | 0.5420 | 0.6170 | 0.6504 | 0.7090 | 0.5490 | 0.6160 | 0.5450 | 0.6352 |
| 15.75 | 0.5360 | 0.6100 | 0.6443 | 0.7009 | 0.5470 | 0.6070 | 0.5410 | 0.6292 |
| 16.00 | 0.5320 | 0.6060 | 0.6413 | 0.6935 | 0.5420 | 0.6040 | 0.5350 | 0.6231 |

Table 3 (continued).

| s | $\mathrm{I}_{\mathrm{p}}^{\mathrm{b}(1)}$ |  | $\overline{I_{\mathrm{p}}^{\mathrm{b}(2)}}$ |  | $\mathrm{I}_{\mathrm{p}}^{\mathrm{b}(3)}$ |  | $I_{p}^{b(4)}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | L | R | L | R | L | R | L | R |
| 16.25 | 0.5280 | 0.5990 | 0.6362 | 0.6872 | 0.5380 | 0.6000 | 0.5310 | 0.6180 |
| 16.50 | 0.5240 | 0.5940 | 0.6302 | 0.6831 | 0.5330 | 0.5960 | 0.5310 0.5270 | 0.6180 |
| 16.75 | 0.5190 | 0.5920 | 0.6272 | 0.6811 | 0.5290 | 0.5920 | 0.5230 | 0.6110 |
| 17.00 | 0.5160 | 0.5880 | 0.6211 | 0.6770 | 0.5280 | 0.5860 | 0.5180 | 0.6070 |
| 17.25 | 0.5110 | 0.5810 | 0.6130 | 0.6719 | 0.5210 | 0.5810 | 0.5140 | 0.6000 |
| 17.50 | 0.5040 | 0.5750 | 0.6070 | 0.6616 | 0.5140 | 0.5740 | 0.5090 | 0.5910 |
| 17.75 18.00 | 0.4970 | 0.5610 | 0.5930 | 0.6474 | 0.5030 | 0.5630 | 0.5000 | 0.5790 |
| 18.00 18.25 | 0.4870 | 0.5460 | 0.5840 | 0.6322 | 0.4940 | 0.5510 | 0.4890 | 0.5640 |
| 18.25 18.50 | 0.4740 | 0.5310 | 0.5700 | 0.6170 | 0.4800 | 0.5360 | 0.4770 | 0.5490 |
| 18.50 18.75 | 0.4630 0.4510 | 0.5180 | 0.5520 | 0.6010 | 0.4670 | 0.5210 | 0.4640 | 0.5330 |
| 19.00 | 0.4420 | 0.4920 | 0.5370 0.5250 | 0.5870 0.5720 | 0.4590 | 0.5060 | 0.4530 | 0.5190 |
| 19.25 | 0.4360 | 0.4860 | 0.5350 0.5170 | 0.58720 0.5630 | 0.4460 0.4410 | 0.4960 | 0.4440 | 0.5090 |
| 19.50 | 0.4310 | 0.4810 | 0.5130 | 0.5570 | 0.4370 | 0.4960 | 0.4360 0.4320 | 0.5030 |
| 19.75 | 0.4300 | 0.4810 | 0.5110 | 0.5540 | 0.4350 | 0.4820 | 0.4310 | 0.4950 |
| 20.00 | 0.4290 | 0.4800 | 0.5110 | 0.5530 | 0.4350 | 0.4830 | 0.4300 | 0.4960 |
| 20.25 | 0.4300 | 0.4800 | 0.5120 | 0.5560 | 0.4360 | 0.4850 | 0.4320 | 0.4970 |
| 20.50 | 0.4310 | 0.4800 | 0.5140 | 0.5560 | 0.4370 | 0.4850 | 0.4330 | 0.4970 |
| 20.75 | 0.4310 | 0.4790 | 0.5150 | 0.5570 | 0.4370 | 0.4840 | 0.4340 | 0.4950 |
| 21.00 | 0.4310 | 0.4790 | 0.5150 | 0.5550 | 0.4390 | 0.4830 | 0.4340 | 0.4940 |
| 21.25 | 0.4300 | 0.4760 | 0.5140 | 0.5520 | 0.4390 | 0.4830 | 0.4320 | 0.4940 |
| 21.50 | 0.4270 | 0.4740 | 0.5120 | 0.5480 | 0.4380 | 0.4810 | 0.4330 | 0.4890 |
| 21.75 | 0.4260 | 0.4700 | 0.5100 | 0.5450 | 0.4360 | 0.4760 | 0.4310 | 0.4850 |
| 22.00 | 0.4240 | 0.4670 | 0.5090 | 0.5380 | 0.4360 | 0.4740 | 0.4290 | 0.4800 |

Table 3 (continued).

| s | $\overline{I_{p}^{b(1)}}$ |  | $\mathrm{I}_{\mathrm{p}}^{\mathrm{b}(2)}$ |  | $\mathrm{I}_{\mathrm{p}}^{\mathrm{b}(3)}$ |  | $I_{p}^{b(4)}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | L | R | L | R | L | R | L | R |
| 22.25 | 0.4200 | 0.4640 | 0.5070 | 0.5350 | 0.4340 | 0.4690 | 0.4260 | 0.4780 |
| 22.50 | 0.4170 | 0.4600 | 0.5030 | 0.5300 | 0.4310 | 0.4650 | 0.4250 | 0.4730 |
| 22.75 | 0.4140 | 0.4560 | 0.4990 | 0.5240 | 0.4280 | 0.4610 | 0.4230 | 0.4690 |
| 23.00 | 0.4110 | 0.4510 | 0.4930 | 0.5200 | 0.4250 | 0.4560 | 0.4200 | 0.4640 |
| 23.25 | 0.4060 | 0.4460 | 0.4870 | 0.5130 | 0.4210 | 0.4510 | 0.4140 | 0.4590 |
| 23.50 | 0.4000 | 0.4380 | 0.4820 | 0.5040 | 0.4150 | 0.4460 | 0.4090 | 0.4490 |
| 23.75 | 0.3940 | 0.4310 | 0.4740 | 0.4950 | 0.4110 | 0.4380 | 0.4040 | 0.4430 |
| 24.00 | 0.3890 | 0.4240 | 0.4670 | 0.4880 | 0.4040 | 0.4310 | 0.3980 | 0.4360 |
| 24.25 | 0.3810 | 0.4170 | 0.4600 | 0.4820 | 0.3980 | 0.4260 | 0.3920 | 0.4300 |
| 24.50 | 0.3780 | 0.4120 | 0.4560 | 0.4770 | 0.3930 | 0.4200 | 0.3890 | 0.4240 |
| 24.75 | 0.3750 | 0.4100 | 0.4520 | 0.4710 | 0.3910 | 0.4160 | 0.3850 | 0.4210 |
| 25.00 | 0.3730 | 0.4060 | 0.4500 | 0.4680 | 0.3900 | 0.4130 | 0.3840 | 0.4180 |
| 25.25 | 0.3710 | 0.4060 | 0.4490 | 0.4670 | 0.3880 | 0.4120 | 0.3810 | 0.4160 |
| 25.50 | 0.3710 | 0.4060 | 0.4510 | 0.4670 | 0.3890 | 0.4120 | 0.3820 | 0.4170 |
| 25.75 | 0.3720 | 0.4070 | 0.4540 | 0.4690 | 0.3890 | 0.4140 | 0.3820 | 0.4180 |
| 26.00 | 0.3730 | 0.4080 | 0.4550 | 0.4680 | 0.3900 | 0.4140 | 0.3830 | 0.4190 |
| 26.25 | 0.3720 | 0.4080 | 0.4560 | 0.4680 | 0.3890 | 0.4140 | 0.3810 | 0.4190 |
| 26.50 | 0.3730 | 0.4080 | 0.4580 | 0.4660 | 0.3890 | 0.4150 | 0.3810 | 0.4180 |
| 26.75 | 0.3710 | 0.4080 | 0.4560 | 0.4660 | 0.3880 | 0.4150 | 0.3800 | 0.4170 |
| 27.00 | 0.3700 | 0.4070 | 0.4540 | 0.4640 | 0.3860 | 0.4130 | 0.3780 | 0.4150 |
| 27.25 | 0.3670 | 0.4030 | 0.4530 | 0.4610 | 0.3830 | 0.4110 | 0.3760 | 0.4120 |
| 27.50 | 0.3650 | 0.3990 | 0.4500 | 0.4580 | 0.3790 | 0.4090 | 0.3740 | 0.4090 |
| 27.75 | 0.3610 | 0.3960 | 0.4470 | 0.4540 | 0.3770 | 0.4060 | 0.3710 | 0.4060 |
| 28.00 | 0.3590 | 0.3950 | 0.4450 | 0.4500 | 0.3740 | 0.4030 | 0.3700 | 0.4030 |

Table 3 (continued).

| s | $\mathrm{I}_{\mathrm{p}}^{\mathrm{b}(1)}$ |  | $\mathrm{I}_{\mathrm{p}}^{\mathrm{b}(2)}$ |  | $\mathrm{I}_{\mathrm{p}}^{\mathrm{b}(3)}$ |  | $\mathrm{I}_{\mathrm{p}}^{\mathrm{b}(4)}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | L | R | L | R | L | R | L | R |
| 28.25 | 0.3560 | 0.3920 | 0.4420 | 0.4470 | 0.3710 | 0.4010 | 0.3670 | 0.4000 |
| 28.50 | 0.3540 | 0.3870 | 0.4380 | 0.4420 | 0.3680 | 0.3970 | 0.3630 | 0.3950 |
| 28.75 | 0.3510 | 0.3840 | 0.4360 | 0.4390 | 0.3650 | 0.3940 | 0.3590 | 0.3920 |
| 29.00 | 0.3480 | 0.3800 | 0.4320 | 0.4340 | 0.3630 | 0.3920 | 0.3560 | 0.3890 |
| 29.25 | 0.3450 | 0.3760 | 0.4270 | 0.4300 | 0.3600 | 0.3880 | 0.3530 | 0.3840 |
| 29.50 | 0.3410 | 0.3720 | 0.4240 | 0.4250 | 0.3570 | 0.3850 | 0.3490 | 0.3800 |
| 29.75 | 0.3380 | 0.3680 | 0.4200 | 0.4210 | 0.3530 | 0.3810 | 0.3460 | 0.3780 |
| 30.00 | 0.3360 | 0.3650 | 0.4170 | 0.4170 | 0.3500 | 0.3790 | 0.3430 | 0.3750 |
| 30.25 | 0.3320 | 0.3620 | 0.4150 | 0.4140 | 0.3460 | 0.3770 | 0.3400 | 0.3720 |
| 30.50 | 0.3310 | 0.3600 | 0.4140 | 0.4130 | 0.3440 | 0.3760 | 0.3380 | 0.3710 |
| 30.75 | 0.3310 | 0.3600 | 0.4150 | 0.4120 | 0.3420 | 0.3750 | 0.3380 | 0.3690 |
| 31.00 | 0.3300 | 0.3590 | 0.4160 | 0.4120 | 0.3420 | 0.3750 | 0.3380 | 0.3690 |
| 31.25 | 0.3310 | 0.3600 | 0.4160 | 0.4120 | 0.3410 | 0.3750 | 0.3370 | 0.3680 |
| 31.50 | 0.3310 | 0.3590 | 0.4170 | 0.4130 | 0.3410 | 0.3750 | 0.3370 | 0.3680 |
| 31.75 | 0.3300 | 0.3600 | 0.4170 | 0.4120 | 0.3420 | 0.3760 | 0.3380 | 0.3690 |
| 32.00 | 0.3300 | 0.3600 | 0.4160 | 0.4120 | 0.3410 | 0.3750 | 0.3370 | 0.3680 |
| 32.25 | 0.3290 | 0.3580 | 0.4150 | 0.4100 | 0.3410 | 0.3730 | 0.3380 | 0.3650 |
| 32.50 | 0.3280 | 0.3560 | 0.4140 | 0.4080 | 0.3400 | 0.3720 | 0.3360 | 0.3630 |
| 32.75 | 0.3260 | 0.3550 | 0.4120 | 0.4060 | 0.3370 | 0.3710 | 0.3340 | 0.3610 |
| 33.00 | 0.3250 | 0.3510 | 0.4090 | 0.4030 | 0.3350 | 0.3690 | 0.3320 | 0.3580 |
| 33.25 | 0.3230 | 0.3500 | 0.4070 | 0.4010 | 0.3320 | 0.3660 | 0.3290 | 0.3560 |
| 33.50 | 0.3210 | 0.3480 | 0.4040 | 0.3980 | 0.3280 | 0.3640 | 0.3260 | 0.3530 |
| 33.75 | 0.3180 | 0.3450 | 0.4000 | 0.3950 | 0.3280 | 0.3620 | 0.3240 | 0.3500 |
| 34.00 | 0.3160 | 0.3420 | 0.3990 | 0.3920 | 0.3240 | 0.3610 | 0.3220 | 0.3480 |

Table 3 (continued).

|  | $I_{p}^{b(1)}$ |  | $\mathrm{I}_{\mathrm{p}}^{\mathrm{b}(2)}$ |  | $I_{p}^{b(3)}$ |  | $\mathrm{I}_{\mathrm{p}}^{\mathrm{b}(4)}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| S | L | R | L | R | L | R | L | R |
| 34.25 | 0.3150 | 0.3410 | 0.3950 | 0.3900 | 0.3230 | 0.3590 | 0.3200 | 0.3450 |
| 34.50 | 0.3140 | 0.3370 | 0.3940 | 0.3870 | 0.3210 | 0.3570 | 0.3200 | 0.3430 |
| 34.75 | 0.3120 | 0.3340 | 0.3920 | 0.3850 | 0.3190 | 0.3550 | 0.3180 | 0.3390 |
| 35.00 | 0.3110 | 0.3330 | 0.3900 | 0.3820 | 0.3180 | 0.3540 | 0.3160 | 0.3370 |
| 35.25 | 0.3100 | 0.3300 | 0.3890 | 0.3810 | 0.3170 | 0.3510 | 0.3140 | 0.3350 |
| 35.50 | 0.3080 | 0.3290 | 0.3870 | 0.3770 | 0.3140 | 0.3500 | 0.3120 | 0.3330 |
| 35.75 | 0.3060 | 0.3280 | 0.3850 | 0.3760 | 0.3130 | 0.3480 | 0.3110 | 0.3310 |
| 36.00 | 0.3050 | 0.3270 | 0.3830 | 0.3740 | 0.3110 | 0.3470 | 0.3100 | 0.3300 |
| 36.25 | 0.3040 | 0.3270 | 0.3820 | 0.3730 | 0.3110 | 0.3470 | 0.3090 | 0.3280 |
| 36.50 | 0.3040 | 0.3260 | 0.3830 | 0.3720 | 0.3100 | 0.3470 | 0.3090 | 0.3270 |
| 36.75 | 0.3040 | 0.3250 | 0.3830 | 0.3720 | 0.3090 | 0.3470 | 0.3090 | 0.3270 |
| 37.00 | 0.3030 | 0.3250 | 0.3820 | 0.3720 | 0.3090 | 0.3480 | 0.3080 | 0.3270 |
| 37.25 | 0.3020 | 0.3250 | 0.3820 | 0.3720 | 0.3080 | 0.3480 | 0.3080 | 0.3280 |
| 37.50 | 0.3020 | 0.3240 | 0.3800 | 0.3710 | 0.3090 | 0.3470 | 0.3070 | 0.3260 |
| 37.75 | 0.3010 | 0.3230 | 0.3790 | 0.3690 | 0.3080 | 0.3470 | 0.3070 | 0.3250 |
| 38.00 | 0.3000 | 0.3220 | 0.3780 | 0.3670 | 0.3070 | 0.3460 | 0.3050 | 0.3240 |
| 38.25 | 0.2990 | 0.3200 | 0.3770 | 0.3640 | 0.3060 | 0.3440 | 0.3040 | 0.3230 |
| 38.50 | 0.2970 | 0.3180 | 0.3740 | 0.3620 | 0.3040 | 0.3430 | 0.3020 | 0.3210 |
| 38.75 | 0.2950 | 0.3160 | 0.3720 | 0.3610 | 0.3010 | 0.3410 | 0.3000 | 0.3200 |
| 39.00 | 0.2940 | 0.3140 | 0.3700 | 0.3590 | 0.3000 | 0.3400 | 0.2990 | 0.3190 |
| 39.25 | 0.2920 | 0.3120 | 0.3670 | 0.3570 | 0.2990 | 0.3380 | 0.2970 | 0.3170 |
| 39.50 | 0.2910 | 0.3100 | 0.3660 | 0.3550 | 0.2980 | 0.3370 | 0.2960 | 0.3150 |
| 39.75 | 0.2900 | 0.3080 | 0.3650 | 0.3540 | 0.2960 | 0.3360 | 0.2950 | 0.3140 |
| 40.00 | 0.2900 | 0.3070 | 0.3640 | 0.3520 | 0.2950 | 0.3340 | 0.2940 | 0.3130 |

Table 3 (continued).

| s | $\overline{I_{\mathrm{p}}^{\mathrm{b}(1)}}$ |  | $\mathrm{I}_{\mathrm{p}}^{\mathrm{b}(2)}$ |  | $I_{p}^{b(3)}$ |  | $\mathrm{I}_{\mathrm{p}}^{\mathrm{b}}$ (4) |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | L | R | L | R | L | R | L | R |
| 40.25 | 0.2890 | 0.3070 | 0.3630 | 0.3500 | 0.2940 | 0.3330 | 0.2930 | 0.3120 |
| 40.50 | 0.2880 | 0.3060 | 0.3620 | 0.3490 | 0.2920 | 0.3330 | 0.2930 | 0.3110 |
| 40.75 | 0.2870 | 0.3040 | 0.3620 | 0.3470 | 0.2910 | 0.3330 | 0.2930 | 0.3110 |
| 41.00 | 0.2860 | 0.3030 | 0.3620 | 0.3460 | 0.2890 | 0.3330 | 0.2920 | 0.3110 |
| 41.25 | 0.2850 | 0.3020 | 0.3620 | 0.3450 | 0.2890 | 0.3310 | 0.2910 | 0.3100 |
| 41.50 | 0.2850 | 0.3020 | 0.3610 | 0.3450 | 0.2880 | 0.3310 | 0.2890 | 0.3090 |
| 41.75 | 0.2850 | 0.3010 | 0.3600 | 0.3440 | 0.2880 | 0.3310 | 0.2890 | 0.3090 |
| 42.00 | 0.2840 | 0.3010 | 0.3590 | 0.3430 | 0.2870 | 0.3310 | 0.2880 | 0.3090 |

L Left branch
R Right branch

Table 4. Electron intensity incident on the photographic plate: $\mathrm{h}=120.00 \mathrm{~mm}$.

|  | $\mathrm{I}_{\mathrm{p}}^{\mathrm{c}(1)}$ |  | $\mathrm{I}_{\mathrm{p}}^{\mathrm{c}(2)}$ |  | $I_{p}^{c(3)}$ |  | $I_{p}^{c(4)}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| s | L | R | L | R | L | R | L | R |
| 18.50 | 1.0997 | 1.2665 | 0.8618 | 0.9983 | 0.8293 | 0.9454 | 0.8108 | 0.9092 |
| 18.75 | 1.0695 | 1.2320 | 0.8308 | 0.9628 | 0.8009 | 0.9106 | 0.7860 | 0.8856 |
| 19.00 | 1.0249 | 1.1837 | 0.8102 | 0.9265 | 0.7729 | 0.8788 | 0.7617 | 0.8612 |
| 19.25 | 0.9926 | 1.1495 | 0.7865 | 0.8991 | 0.7466 | 0.8522 | 0.7380 | 0.8394 |
| 19.50 | 0.9681 | 1.1265 | 0.7709 | 0.8861 | 0.7348 | 0.8362 | 0.7250 | 0.8188 |
| 19.75 | 0.9498 | 1.1090 | 0.7600 | 0.8745 | 0.7241 | 0.8247 | 0.7135 | 0.8097 |
| 20.00 | 0.9474 | 1.0957 | 0.7502 | 0.8641 | 0.7199 | 0.8190 | 0.7041 | 0.7995 |
| 20.25 | 0.9377 | 1.0891 | 0.7458 | 0.8572 | 0.7136 | 0.8156 | 0.7020 | 0.7950 |
| 20.50 | 0.9245 | 1.0852 | 0.7426 | 0.8526 | 0.7085 | 0.8099 | 0.6925 | 0.7905 |
| 20.75 | 0.9125 | 1.0721 | 0.7373 | 0.8468 | 0.7033 | 0.8065 | 0.6916 | 0.7826 |
| 21.00 | 0.9054 | 1.0630 | 0.7297 | 0.8399 | 0.6981 | 0.7964 | 0.6843 | 0.7748 |
| 21.25 | 0.8960 | 1.0527 | 0.7244 | 0.8330 | 0.6908 | 0.7930 | 0.6812 | 0.7671 |
| 21.50 | 0.8854 | 1.0337 | 0.7171 | 0.8239 | 0.6845 | 0.7806 | 0.6709 | 0.7584 |
| 21.75 | 0.8737 | 1.0262 | 0.7098 | 0.8114 | 0.6763 | 0.7717 | 0.6617 | 0.7497 |
| 22.00 | 0.8622 | 1.0098 | 0.7025 | 0.8012 | 0.6701 | 0.7630 | 0.6556 | 0.7389 |
| 22.25 | 0.8541 | 0.9975 | 0.6942 | 0.7910 | 0.6630 | 0.7532 | 0.6454 | 0.7303 |
| 22.50 | 0.8484 | 0.9815 | 0.6848 | 0.7787 | 0.6517 | 0.7455 | 0.6384 | 0.7187 |
| 22.75 | 0.8334 | 0.9693 | 0.6745 | 0.7676 | 0.6426 | 0.7380 | 0.6273 | 0.7093 |
| 23.00 | 0.8220 | 0.9547 | 0.6612 | 0.7611 | 0.6366 | 0.7295 | 0.6222 | 0.6989 |
| 23.25 | 0.8050 | 0.9414 | 0.6500 | 0.7458 | 0.6265 | 0.7136 | 0.6121 | 0.6833 |
| 23.50 | 0.7914 | 0.9197 | 0.6389 | 0.7297 | 0.6163 | 0.7001 | 0.5961 | 0.6740 |
| 23.75 | 0.7735 | 0.8971 | 0.6257 | 0.7139 | 0.5973 | 0.6908 | 0.5871 | 0.6597 |
| 24.00 | 0.7604 | 0.8772 | 0.6166 | 0.6973 | 0.5883 | 0.6763 | 0.5731 | 0.6485 |
| 24.25 | 0.7440 | 0.8576 | 0.6046 | 0.6848 | 0.5763 | 0.6609 | 0.5621 | 0.6303 |

Table 4 (continued)

| s | $I_{p}^{c(1)}$ |  | $\mathrm{I}_{\mathrm{p}}^{\mathrm{c}(2)}$ |  | $I_{p}^{c(3)}$ |  | $I_{p}^{c(4)}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | L | R | L | R | L | R | L | R |
| 24.50 | 0.7280 | 0.8392 | 0.5966 | 0.6714 | 0.5683 | 0.6477 | 0.5551 | 0.6212 |
| 24.75 | 0.7185 | 0.8266 | 0.5866 | 0.6632 | 0.5623 | 0.6386 | 0.5451 | 0.6131 |
| 25.00 | 0.7070 | 0.8186 | 0.5836 | 0.6561 | 0.5563 | 0.6335 | 0.5391 | 0.6071 |
| 25.25 | 0.7029 | 0.8152 | 0.5805 | 0.6500 | 0.5543 | 0.6265 | 0.5341 | 0.6031 |
| 25.50 | 0.6987 | 0.8118 | 0.5776 | 0.6500 | 0.5523 | 0.6245 | 0.5321 | 0.6011 |
| 25.75 | 0.6977 | 0.8084 | 0.5776 | 0.6429 | 0.5503 | 0.6234 | 0.5331 | 0.6001 |
| 26.00 | 0.6946 | 0.8061 | 0.5756 | 0.6409 | 0.5513 | 0.6224 | 0.5331 | 0.5971 |
| 26.25 | 0.6935 | 0.8050 | 0.5736 | 0.6399 | 0.5503 | 0.6214 | 0.5301 | 0.5951 |
| 26.50 | 0.6914 | 0.8027 | 0.5726 | 0.6369 | 0.5463 | 0.6163 | 0.5271 | 0.5911 |
| 26.75 | 0.6862 | 0.7936 | 0.5706 | 0.6328 | 0.5413 | 0.6113 | 0.5261 | 0.5861 |
| 27.00 | 0.6810 | 0.7846 | 0.5656 | 0.6278 | 0.5343 | 0.6063 | 0.5201 | 0.5821 |
| 27.25 | 0.6707 | 0.7768 | 0.5596 | 0.6196 | 0.5293 | 0.5983 | 0.5131 | 0.5711 |
| 27.50 | 0.6556 | 0.7713 | 0.5526 | 0.6136 | 0.5263 | 0.5923 | 0.5081 | 0.5671 |
| 27.75 | 0.6533 | 0.7614 | 0.5466 | 0.6086 | 0.5193 | 0.5863 | 0.5031 | 0.5621 |
| 28.00 | 0.6453 | 0.7560 | 0.5416 | 0.6046 | 0.5143 | 0.5803 | 0.4981 | 0.5581 |
| 28.25 | 0.6382 | 0.7473 | 0.5346 | 0.5946 | 0.5083 | 0.5723 | 0.4911 | 0.5531 |
| 28.50 | 0.6301 | 0.7397 | 0.5296 | 0.5896 | 0.5013 | 0.5673 | 0.4861 | 0.5461 |
| 28.75 | 0.6230 | 0.7333 | 0.5236 | 0.5846 | 0.4963 | 0.5613 | 0.4821 | 0.5401 |
| 29.00 | 0.6179 | 0.7226 | 0.5186 | 0.5796 | 0.4903 | 0.5523 | 0.4761 | 0.5351 |
| 29.25 | 0.6099 | 0.7174 | 0.5136 | 0.5716 | 0.4843 | 0.5483 | 0.4701 | 0.5301 |
| 29.50 | 0.6059 | 0.7091 | 0.5096 | 0.5656 | 0.4783 | 0.5433 | 0.4671 | 0.5221 |
| 29.75 | 0.5969 | 0.7018 | 0.5036 | 0.5606 | 0.4733 | 0.5363 | 0.4571 | 0.5171 |
| 30.00 | 0.5909 | 0.6945 | 0.4996 | 0.5516 | 0.4703 | 0.5313 | 0.4531 | 0.5121 |
| 30.25 | 0.5859 | 0.6883 | 0.4966 | 0.5506 | 0.4673 | 0.5283 | 0.4471 | 0.5081 |

Table 4 (continued).

| s | $\mathrm{I}_{\mathrm{p}}^{\mathrm{c}(1)}$ |  | $\mathrm{I}_{\mathrm{p}}^{\mathrm{c}(2)}$ |  | $\mathrm{I}_{\mathrm{p}}^{\mathrm{c}(3)}$ |  | $\mathrm{I}_{\mathrm{p}}^{\mathrm{C}}(4)$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | L | R | L | R | L | R | L | R |
| 30.50 | 0.5809 | 0.6831 | 0.4946 | 0.5466 | 0.4663 | 0.5223 | 0.4471 | 0.5041 |
| 30.75 | 0.5776 | 0.6779 | 0.4926 | 0.5446 | 0.4623 | 0.5213 | 0.4451 | 0.5021 |
| 31.00 | 0.5769 | 0.6758 | 0.4916 | 0.5436 | 0.4623 | 0.5203 | 0.4431 | 0.5011 |
| 31.25 | 0.5759 | 0.6789 | 0.4906 | 0.5426 | 0.4613 | 0.5183 | 0.4431 | 0.5001 |
| 31.50 | 0.5749 | 0.6789 | 0.4906 | 0.5396 | 0.4593 | 0.5173 | 0.4421 | 0.4981 |
| 31.75 | 0.5719 | 0.6789 | 0.4896 | 0.5406 | 0.4583 | 0.5163 | 0.4401 | 0.4871 |
| 32.00 | 0.5699 | 0.6748 | 0.4876 | 0.5396 | 0.4573 | 0.5163 | 0.4391 | 0.4961 |
| 32.25 | 0.5649 | 0.6717 | 0.4856 | 0.5356 | 0.4553 | 0.5113 | 0.4381 | 0.4941 |
| 32.50 | 0.5619 | 0.6587 | 0.4826 | 0.5336 | 0.4523 | 0.5113 | 0.4351 | 0.4901 |
| 32.75 | 0.5599 | 0.6655 | 0.4796 | 0.5316 | 0.4493 | 0.5063 | 0.4321 | 0.4851 |
| 33.00 | 0.5549 | 0.6605 | 0.4756 | 0.5276 | 0.4443 | 0.5013 | 0.4301 | 0.4821 |
| 33.25 | 0.5489 | 0.6544 | 0.4706 | 0.5226 | 0.4423 | 0.4943 | 0.4221 | 0.4781 |
| 33.50 | 0.5449 | 0.6503 | 0.4666 | 0.5186 | 0.4393 | 0.4903 | 0.4211 | 0.4751 |
| 33.75 | 0.5419 | 0.6422 | 0.4616 | 0.5156 | 0.4343 | 0.4873 | 0.4141 | 0.4721 |
| 34.00 | 0.5369 | 0.6382 | 0.4566 | 0.5126 | 0.4313 | 0.4813 | 0.4121 | 0.4661 |
| 34.25 | 0.5309 | 0.6324 | 0.4546 | 0.5096 | 0.4283 | 0.4763 | 0.4091 | 0.4631 |
| 34.50 | 0.5279 | 0.6281 | 0.4526 | 0.5066 | 0.4273 | 0.4723 | 0.4081 | 0.4591 |
| 34.75 | 0.5229 | 0.6250 | 0.4516 | 0.5026 | 0.4223 | 0.4693 | 0.4041 | 0.4551 |
| 35.00 | 0.5179 | 0.6220 | 0.4486 | 0.4996 | 0.4193 | 0.4663 | 0.4001 | 0.4511 |
| 35.25 | 0.5109 | 0.6159 | 0.4426 | 0.4976 | 0.4163 | 0.4613 | 0.3991 | 0.4471 |
| 35.50 | 0.5079 | 0.6119 | 0.4406 | 0.4936 | 0.4143 | 0.4583 | 0.3951 | 0.4451 |
| 35.75 | 0.5049 | 0.6079 | 0.4396 | 0.4916 | 0.4123 | 0.4553 | 0.3931 | 0.4411 |
| 36.00 | 0.5019 | 0.6049 | 0.4376 | 0.4906 | 0.4113 | 0.4543 | 0.3911 | 0.4401 |
| 36.25 | 0.4999 | 0.6029 | 0.4366 | 0.4886 | 0.4103 | 0.4533 | 0.3901 | 0.4371 |

Table 4 (continued).

| s | $\overline{I_{p}^{c(l)}}$ |  | $I_{p}^{c(2)}$ |  | $\mathrm{I}_{\mathrm{p}}^{\mathrm{c}(3)}$ |  | $\mathrm{I}_{\mathrm{p}}^{\mathrm{c}(4)}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | L | R | L | R | L | R | L | R |
| 36.50 | 0.4999 | 0.6009 | 0.4356 | 0.4896 | 0.4093 | 0.4533 | 0.3901 | 0.4381 |
| 36.75 | 0.4989 | 0.5999 | 0.4346 | 0.4886 | 0.4073 | 0.4513 | 0.3891 | 0.4361 |
| 37.00 | 0.4969 | 0.5979 | 0.4336 | 0.4876 | 0.4083 | 0.4503 | 0.3891 | 0.4351 |
| 37.25 | 0.4949 | 0.5959 | 0.4316 | 0.4876 | 0.4063 | 0.4483 | 0.3861 | 0.4321 |
| 37.50 | 0.4919 | 0.5939 | 0.4306 | 0.4846 | 0.4043 | 0.4463 | 0.3851 | 0.4331 |
| 37.75 | 0.4899 | 0.5909 | 0.4276 | 0.4836 | 0.4013 | 0.4463 | 0.3821 | 0.4301 |
| 38.00 | 0.4859 | 0.5879 | 0.4246 | 0.4806 | 0.3993 | 0.4423 | 0.3801 | 0.4281 |
| 38.25 | 0.4809 | 0.5839 | 0.4216 | 0.4786 | 0.3973 | 0.4403 | 0.3781 | 0.4251 |
| 38.50 | 0.4769 | 0.5799 | 0.4196 | 0.4756 | 0.3943 | 0.4373 | 0.3751 | 0.4231 |
| 38.75 | 0.4739 | 0.5759 | 0.4166 | 0.4736 | 0.3913 | 0.4343 | 0.3721 | 0.4211 |
| 39.00 | 0.4709 | 0.5729 | 0.4136 | 0.4706 | 0.3893 | 0.4323 | 0.3701 | 0.4181 |
| 39.25 | 0.4659 | 0.5669 | 0.4116 | 0.4666 | 0.3873 | 0.4293 | 0.3671 | 0.4161 |
| 39.50 | 0.4649 | 0.5639 | 0.4076 | 0.4646 | 0.3843 | 0.4263 | 0.3641 | 0.4141 |
| 39.75 | 0.4619 | 0.5619 | 0.4066 | 0.4616 | 0.3813 | 0.4243 | 0.3621 | 0.4121 |
| 40.00 | 0.4589 | 0.5599 | 0.4036 | 0.4597 | 0.3793 | 0.4223 | 0.3601 | 0.4101 |
| 40.25 | 0.4569 | 0.5579 | 0.4026 | 0.4586 | 0.3773 | 0.4203 | 0.3571 | 0.4091 |
| 40.50 | 0.4549 | 0.5559 | 0.3996 | 0.4566 | 0.3763 | 0.4203 | 0.3541 | 0.4071 |
| 40.75 | 0.4519 | 0.5549 | 0.3976 | 0.4546 | 0.3743 | 0.4173 | 0.3531 | 0.4051 |
| 41.00 | 0.4489 | 0.5539 | 0.3966 | 0.4536 | 0.3733 | 0.4153 | 0.3511 | 0.4041 |
| 41.25 | 0.4479 | 0.5479 | 0.3956 | 0.4526 | 0.3713 | 0.4143 | 0.3501 | 0.4031 |
| 41.50 | 0.4449 | 0.5469 | 0.3936 | 0.4516 | 0.3683 | 0.4143 | 0.3491 | 0.4021 |
| 41.75 | 0.4429 | 0.5439 | 0.3926 | 0.4516 | 0.3673 | 0.4143 | 0.3471 | 0.4021 |
| 42.00 | 0.4409 | 0.5429 | 0.3916 | 0.4496 | 0.3663 | 0.4133 | 0.3451 | 0.4011 |
| 42.25 | 0.4409 | 0.5429 | 0.3896 | 0.4496 | 0.3643 | 0.4113 | 0.3441 | 0.4001 |

Table 4 (continued)

|  | $\mathrm{I}_{\mathrm{p}}^{\mathrm{c}(1)}$ |  | $\mathrm{I}_{\mathrm{p}}^{\mathrm{c}(2)}$ |  | $I_{p}^{c(3)}$ |  | $\mathrm{I}_{\mathrm{P}}^{\mathrm{C}(4)}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| s | L | R | L | R | L | R | L | R |
| 42.50 | 0.4409 | 0.5429 | 0.3896 | 0.4496 | 0.3633 | 0.4113 | 0.3421 | 0.4001 |
| 42.75 | 0.4379 | 0.5429 | 0.3876 | 0.4486 | 0.3623 | 0.4113 | 0.3411 | 0.3971 |
| 43.00 | 0.4359 | 0.5429 | 0.3866 | 0.4466 | 0.3613 | 0.4093 | 0.3401 | 0.3971 |
| 43.25 | 0.4339 | 0.5399 | 0.3846 | 0.4456 | 0.3583 | 0.4083 | 0.3381 | 0.3971 |
| 43.50 | 0.4309 | 0.5349 | 0.3816 | 0.4446 | 0.3563 | 0.4063 | 0.3371 | 0.3951 |
| 43.75 | 0.4269 | 0.5329 | 0.3806 | 0.4416 | 0.3533 | 0.4053 | 0.3351 | 0.3931 |
| 44.00 | 0.4239 | 0.5309 | 0.3776 | 0.4406 | 0.3513 | 0.4043 | 0.3321 | 0.3921 |
| 44.25 | 0.4199 | 0.5299 | 0.3756 | 0.4396 | 0.3493 | 0.4033 | 0.3311 | 0.3911 |
| 44.50 | 0.4179 | 0.5269 | 0.3746 | 0.4376 | 0.3483 | 0.4023 | 0.3301 | 0.3891 |
| 44.75 | 0.4129 | 0.5249 | 0.3716 | 0.4356 | 0.3443 | 0.4023 | 0.3271 | 0.3871 |
| 45.00 | 0.4109 | 0.5239 | 0.3706 | 0.4336 | 0.3433 | 0.4013 | 0.3251 | 0.3871 |
| 45.25 | 0.4099 | 0.5209 | 0.3686 | 0.4336 | 0.3413 | 0.3993 | 0.3241 | 0.3851 |
| 45.50 | 0.4069 | 0.5199 | 0.3666 | 0.4316 | 0.3403 | 0.3963 | 0.3231 | 0.3831 |
| 45.75 | 0.4059 | 0.5189 | 0.3656 | 0.4306 | 0.3383 | 0.3933 | 0.3221 | 0.3821 |
| 46.00 | 0.4059 | 0.5169 | 0.3636 | 0.4296 | 0.3373 | 0.3913 | 0.3201 | 0.3821 |
| 46.25 | 0.4049 | 0.5159 | 0.3626 | 0.4276 | 0.3363 | 0.3903 | 0.3181 | 0.3811 |
| 46.50 | 0.4019 | 0.5159 | 0.3616 | 0.4276 | 0.3333 | 0.3883 | 0.3171 | 0.3801 |
| 46.75 | 0.3999 | 0.5159 | 0.3606 | 0.4266 | 0.3323 | 0.3883 | 0.3161 | 0.3781 |
| 47.00 | 0.3989 | 0.5159 | 0.3596 | 0.4246 | 0.3313 | 0.3883 | 0.3151 | 0.3791 |
| 47.25 | 0.3969 | 0.5139 | 0.3586 | 0.4246 | 0.3303 | 0.3883 | 0.3141 | 0.3781 |
| 47.50 | 0.3959 | 0.5119 | 0.3566 | 0.4236 | 0.3283 | 0.3873 | 0.3131 | 0.3771 |
| 47.75 | 0.3939 | 0.5129 | 0.3566 | 0.4226 | 0.3283 | 0.3873 | 0.3121 | 0.3771 |
| 48.00 | 0.3929 | 0.5119 | 0.3536 | 0.4226 | 0.3263 | 0.3863 | 0.3111 | 0.3771 |
| 48.25 | 0.3909 | 0.5119 | 0.3526 | 0.4216 | 0.3253 | 0.3863 | 0.3101 | 0.3761 |

Table 4 (continued).

| s | $\mathrm{I}_{\mathrm{p}}^{\mathrm{c}(1)}$ |  | $I_{p}^{c(2)}$ |  | $I_{p}^{c(3)}$ |  | $\mathrm{I}_{\mathrm{p}}^{\mathrm{c}(4)}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | L | R | L | R | L | R | L | R |
| 48.50 | 0.3889 | 0.5099 | 0.3516 | 0.4206 | 0.3243 | 0.3853 | 0.3081 | 0.3761 |
| 48.75 | 0.3879 | 0.5089 | 0.3506 | 0.4196 | 0.3233 | 0.3843 | 0.3071 | 0.3751 |
| 49.00 | 0.3849 | 0.5069 | 0.3496 | 0.4196 | 0.3203 | 0.3833 | 0.3051 | 0.3741 |
| 49.25 | 0.3819 | 0.5059 | 0.3486 | 0.4196 | 0.3193 | 0.3823 | 0.3051 | 0.3751 |
| 49.50 | 0.3809 | 0.5049 | 0.3466 | 0.4176 | 0.3183 | 0.3823 | 0.3031 | 0.3741 |
| 49.75 | 0.3789 | 0.5019 | 0.3446 | 0.4166 | 0.3163 | 0.3813 | 0.3011 | 0.3731 |

L Left branch
$R$ Right branch

Table 5. Experimental and theoretical $\mathrm{I}_{\mathrm{E}}^{\mathrm{T}}(\mathrm{s})$ curves.

| s | $\mathrm{I}_{\mathrm{E}}^{\mathrm{T}}(\mathrm{~s})_{\mathrm{Exp}}$ | $\mathrm{I}_{\mathrm{E}}^{\mathrm{T}}(\mathrm{~s})_{\text {Theor }}$ | s | $I_{E^{(s)}}^{\mathrm{T}} \mathrm{Exp}$ | $\mathrm{I}_{\mathrm{E}}^{\mathrm{T}}(\mathrm{~s})_{\text {Theor }}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 0.00 |  | 0.0 | 10.50 | -151.0 | -126.5 |
| 0.25 |  | 240.7 | 10.75 | -8.0 | 21.6 |
| 0.50 |  | 441.2 | 11.00 | 154.0 | 198.6 |
| 0.75 |  | 593.0 | 11.25 | 316.0 | 380.1 |
| 1.00 |  | 645.9 | 11.50 | 454.0 | 534.4 |
| 1.25 |  | 622.0 | 11.75 | 547.0 | 630.4 |
| 1.50 |  | 530.0 | 12.00 | 557.0 | 645.3 |
| 1.75 |  | 394.2 | 12.25 | 447.0 | 571.4 |
| 2.00 |  | 242.2 | 12.50 | 293.0 | 418.0 |
| 2.25 |  | 97.3 | 12.75 | 110.0 | 210.1 |
| 2.50 | -41.0 | -25.0 | 13.00 | -145.0 | -16.9 |
| 2.75 | -179.0 | -121.8 | 13.25 | -352.0 | -226.4 |
| 3.00 | -316.0 | -199.9 | 13.50 | -501.0 | -387.6 |
| 3.25 | -369.0 | -269.2 | 13.75 | -590.0 | -482.1 |
| 3.50 | -448.0 | -337.9 | 14.00 | -598.0 | -507.5 |
| 3.75 | -493.0 | -408.7 | 14.25 | -549.0 | -474.2 |
| 4.00 | -530.0 | -473.8 | 14.50 | -473.0 | -401.9 |
| 4.25 | -556.0 | -515.8 | 14.75 | -395.0 | -312.3 |
| 4.50 | -528.0 | -513.6 | 15.00 | -291.0 | -222.8 |
| 4.75 | -450.0 | -450.2 | 15.25 | -216.0 | -142.7 |
| 5.00 | -317.0 | -317.8 | 15.50 | -141.0 | -72.0 |
| 5.25 | -127.0 | -123.0 | 15.75 | -54.0 | -3.4 |
| 5.50 | 93.0 | 110.7 | 16.00 | 45.0 | 72.2 |
| 5.75 | 326.0 | 348.0 | 16.25 | 118.0 | 160.8 |
| 6.00 | 527.0 | 549.4 | 16.50 | 220.0 | 260.9 |
| 6.25 | 654.0 | 679.1 | 16.75 | 327.0 | 362.1 |
| 6.50 | 702.0 | 714.8 | 17.00 | 402.0 | 446.5 |
| 6.75 | 647.0 | 652.9 | 17.25 | 445.0 | 492.8 |
| 7.00 | 543.0 | 508.0 | 17.50 | 476.0 | 483.3 |
| 7.25 | 337.0 | 309.8 | 17.75 | 373.0 | 408.8 |
| 7.50 | 121.0 | 95.4 | 18.00 | 269.0 | 273.2 |
| 7.75 | -58.0 | -100.4 | 18.25 | 89.0 | 93.0 |
| 8.00 | -212.0 | -251.3 | 18.50 | -124.0 | -105.0 |
| 8.25 | -316.0 | -347.7 | 18.75 | -303.0 | -289.3 |
| 8.50 | -355.0 | -392.2 | 19.00 | -455.0 | -430.8 |
| 8.75 | -374.0 | -399.5 | 19.25 | -514.0 | -509.5 |
| 9.00 | -368.0 | -387. 4 | 19.50 | -514.0 | -517.7 |
| 9.25 | -354.0 | -370.0 | 19.75 | -459.0 | -461.8 |
| 9.50 | -347.0 | -353.5 | 20.00 | -367.0 | -358.3 |
| 9.75 | -327.0 | -334.0 | 20.25 | -244.0 | -230.0 |
| 10.00 | -288.0 | -298.8 | 20.50 | -116.0 | -99.6 |
| 10.25 | -231.0 | -233.1 | 20.75 | 5.0 | 15.3 |

Table 5 (continued).

| s | $\mathrm{I}_{\mathrm{E}}^{\mathrm{T}}(\mathrm{~s})_{\mathrm{Exp}}$ | $\mathrm{I}_{\mathrm{E}}^{\mathrm{T}}(\mathrm{~s})_{\mathrm{Theor}}$ | s | $\mathrm{I}_{\mathrm{E}}^{\mathrm{T}}(\mathrm{~s})_{\mathrm{Exp}}$ | $\mathrm{I}_{\mathrm{E}}^{\mathrm{T}}(\mathrm{~s})_{\text {Theor }}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 21.00 | 123.0 | 105.7 | 31.50 | 24.0 | 63.9 |
| 21.25 | 182.0 | 171.2 | 31.75 | 140.0 | 164.2 |
| 21.50 | 251.0 | 217.6 | 32.00 | 225.0 | 237.1 |
| 21.75 | 271.0 | 252.7 | 32.25 | 255.0 | 275.7 |
| 22.00 | 293.0 | 282.7 | 32.50 | 267.0 | 279.5 |
| 22.25 | 351.0 | 308.2 | 32.75 | 277.0 | 254.2 |
| 22.50 | 332.0 | 324.3 | 33.00 | 230.0 | 208.8 |
| 22.75 | 332.0 | 321.4 | 33.25 | 164.0 | 152.9 |
| 23.00 | 293.0 | 289.1 | 33.50 | 120.0 | 95.1 |
| 23.25 | 243.0 | 220.5 | 33.75 | 38.0 | 40.4 |
| 23.50 | 118.0 | 115.3 | 34.00 | -14.0 | -9.4 |
| 23.75 | -9.0 | -17.8 | 34.25 | -83.0 | -54.9 |
| 24.00 | -128.0 | -162.2 | 34.50 | -106.0 | -97.7 |
| 24.25 | -276.0 | -296.0 | 34.75 | -172.0 | -138.3 |
| 24.50 | -370.0 | -397.2 | 35.00 | -206.0 | -175.2 |
| 24.75 | -403.0 | -448.4 | 35.25 | -250.0 | -204.1 |
| 25.00 | -416.0 | -441.1 | 35.50 | -276.0 | -219.4 |
| 25.25 | -365.0 | -377.4 | 35.75 | -290.0 | -215.2 |
| 25.50 | -231.0 | -269.6 | 36.00 | -259.0 | -187.8 |
| 25.75 | -81.0 | -137.0 | 36.25 | -240.0 | -136.9 |
| 26.00 | 39.0 | -1.3 | 36.50 | -130.0 | -66.8 |
| 26.25 | 140.0 | 118.2 | 36.75 | -26.0 | 14.3 |
| 26.50 | 229.0 | 208.2 | 37.00 | 71.0 | 95.4 |
| 26.75 | 304.0 | 263.0 | 37.25 | 115.0 | 164.7 |
| 27.00 | 337.0 | 285.0 | 37.50 | 144.0 | 212.7 |
| 27.25 | 300.0 | 281.5 | 37.75 | 141.0 | 233.4 |
| 27.50 | 264.0 | 261.5 | 38.00 | 139.0 | 225.5 |
| 27.75 | 236.0 | 232.9 | 38.25 | 106.0 | 192.6 |
| 28.00 | 226.0 | 199.5 | 38.50 | 58.0 | 141.8 |
| 28.25 | 204.0 | 161.1 | 38.75 | 12.0 | 82.0 |
| 28.50 | 126.0 | 114.7 | 39.00 | -23.0 | 21.8 |
| 28.75 | 84.0 | 56.3 | 39.25 | -108.0 | -31.9 |
| 29.00 | 17.0 | -15.6 | 39.50 | -160.0 | -75.3 |
| 29.25 | -62.0 | -98.4 | 39.75 | -194.0 | -106.9 |
| 29.50 | -146.0 | -184.3 | 40.00 | -203.0 | -127.8 |
| 29.75 | -236.0 | -261. 4 | 40.25 | -205.0 | -139.6 |
| 30.00 | -296.0 | -316.3 | 40.50 | -184.0 | -144.0 |
| 30.25 | -328.0 | -337.1 | 40.75 | -184.0 | -141.3 |
| 30.50 | -318.0 | -317.2 | 41.00 | -168.0 | -131.2 |
| 30.75 | -274.0 | -256.7 | 41.25 | -147.0 | -112.1 |
| 31.00 | -179.0 | -163.3 | 41.50 | -112.0 | -83.2 |
| 31.25 | -69.0 | -50.8 | 41.75 | -68.0 | -44.4 |

Table 5 (continued).

| $s$ | $\mathrm{I}_{\mathrm{E}}^{\mathrm{T}}(\mathrm{s})_{\mathrm{E}}$ | $\mathrm{I}_{\mathrm{E}}^{\mathrm{T}}(\mathrm{s})_{\mathrm{Theor}}$ | s | $\mathrm{I}_{\mathrm{E}}^{\mathrm{T}}(\mathrm{s})_{\mathrm{Exp}}$ | $\mathrm{I}_{\mathrm{E}}^{\mathrm{T}}(\mathrm{s})_{\mathrm{Theor}}$ |
| :---: | ---: | ---: | ---: | ---: | ---: |
|  |  |  |  |  |  |
| 42.00 | -47.0 | 2.0 | 46.00 | -75.0 | -102.8 |
| 42.25 | 21.0 | 52.0 | 46.25 | -78.0 | -85.4 |
| 42.50 | 83.0 | 99.5 | 46.50 | -69.0 | -64.4 |
| 42.75 | 131.0 | 138.1 | 46.75 | -66.0 | -40.9 |
| 43.00 | 188.0 | 162.0 | 47.00 | 1.0 | -15.5 |
| 43.25 | 188.0 | 167.4 | 47.25 | 27.0 | 11.1 |
| 43.50 | 139.0 | 153.3 | 47.50 | 21.0 | 38.1 |
| 43.75 | 64.0 | 121.9 | 47.75 | 77.0 | 63.7 |
| 44.00 | 7.0 | 78.1 | 48.00 | 81.0 | 85.6 |
| 44.25 | 18.0 | 28.4 | 48.25 | 117.0 | 101.0 |
| 44.50 | -18.0 | -20.5 | 48.50 | 104.0 | 107.2 |
| 44.75 | -107.0 | -62.5 | 48.75 | 118.0 | 102.7 |
| 45.00 | -74.0 | -93.8 | 49.00 | 77.0 | 87.0 |
| 45.25 | -66.0 | -112.4 | 49.25 | 112.0 | 61.7 |
| 45.50 | -85.0 | -118.8 | 49.50 | 64.0 | 29.7 |
| 45.75 | -79.0 | -114.7 | 49.75 | 7.0 | -5.0 |
|  |  |  |  |  |  |

Table 6. Experimental $\mathrm{I}_{\mathrm{E}}^{\mathrm{a}}(\mathrm{s})$ and $\mathrm{I}_{\mathrm{E}}^{\mathrm{a}(\mathrm{i})}(\mathrm{s})$ curves $(\mathrm{h}=478.00 \mathrm{~mm})$.


Table 6 (continued).

| s | $\mathrm{I}_{\mathrm{E}}^{\mathrm{a}}(\mathrm{s})_{\operatorname{Exp}}$ | $I_{E}^{a(1)}(s)_{E x p}$ | $\mathrm{I}_{\mathrm{E}}^{\mathrm{a}(2)}(\mathrm{s})_{\operatorname{Exp}}$ | $\mathrm{I}_{\mathrm{E}}^{\mathrm{a}(3)}(\mathrm{s})_{\operatorname{Exp}}$ | $\mathrm{I}_{\mathrm{E}}^{\mathrm{a}(4)}(\mathrm{s})_{\mathrm{Exp}}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 13.00 | -124.0 | -69.2 | -77.8 | -96.8 | -75.5 |
| 13.25 | -333.0 | -196.0 | -169.0 | -242.0 | -182.0 |
| 13.50 | -485.0 | -263.0 | -258.0 | -351.0 | -263.0 |
| 13.75 | -585.0 | -328.0 | -299.0 | -406.0 | -322.0 |
| 14.00 | -607.0 | -351.0 | -321.0 | -416.0 | -334.0 |
| 14.25 | -576.0 | -327.0 | -314.0 | -407.0 | -300.0 |
| 14.50 | -495.0 | -291.0 | -277.0 | -326.0 | -273.0 |
| 14.75 | -390.0 | -231.0 | -224.0 | -261.0 | -214.0 |
| 15.00 | -292.0 | -179.0 | -181.0 | -195.0 | -141.0 |
| 15.25 | -225.0 | -145.0 | -153.0 | -151.0 | -100.0 |
| 15.50 | -148.0 | -82.7 | -110.0 | -107.0 | -71.4 |
| 15.75 | -57.0 | -34.2 | -56.1 | -45.6 | -26.5 |
| 16.00 | 43.0 | 19.5 | 19.7 | 13.2 | 17.0 |
| 16.25 | 118.0 | 76.8 | 59.4 | 62.0 | 61.1 |
| 16.50 | 236.0 | 133.0 | 97.8 | 139.0 | 127.0 |
| 16.75 | 363.0 | 196.0 | 180.0 | 224.0 | 200.0 |
| 17.00 | 438.0 | 234.0 | 241.0 | 286.0 | 221.0 |
| 17.25 | 474.0 | 274.0 | 256.0 | 279.0 | 244.0 |
| 17.50 | 494.0 | 260.0 | 261.0 | 305.0 | 272.0 |
| 17.75 | 436.0 | 229.0 | 207.0 | 296.0 | 239.0 |
| 18.00 | 304.0 | 167.0 | 149.0 | 199.0 | 158.0 |
| 18.25 | 113.0 | 62.1 | 62.8 | 67.1 | 48.2 |
| 18.50 | -101.0 | -54.1 | -67.4 | -79.7 | -46.0 |
| 18.75 | -293.0 | -140.0 | -154.0 | -198.0 | -203.0 |
| 19.00 | -441.0 | -258.0 | -231.0 | -307.0 | -232.0 |
| 19.25 | -528.0 | -303.0 | -268.0 | -372.0 | -281.0 |
| 19.50 | -535.0 | -325.0 | -268.0 | -375.0 | -279.0 |
| 19.75 | -514.0 | -309.0 | -242.0 | -371.0 | -290.0 |
| 20.00 | -395.0 | -255.0 | -191.0 | -303.0 | -201.0 |
| 20.25 | -290.0 | -197.0 | -154.0 | -233.0 | -146.0 |
| 20.50 | -163.0 | -138.0 | -82.7 | -153.0 | -85.3 |
| 20.75 | -24.0 | -45.7 | -31.3 | -41.7 | -31.3 |

Table 7. Experimental $\mathrm{I}_{\mathrm{E}}^{\mathrm{b}}(\mathrm{s})$ and $\mathrm{I}_{\mathrm{E}}^{\mathrm{b}(\mathrm{i})}(\mathrm{s})$ curves $(\mathrm{h}=192.07 \mathrm{~mm})$.

| s | $\mathrm{I}_{\mathrm{E}}^{\mathrm{b}}(\mathrm{s})_{\operatorname{Exp}}$ | $\mathrm{I}_{\mathrm{E}}^{\mathrm{b}(1)}(\mathrm{s})_{\mathrm{Exp}}$ | $\mathrm{I}_{\mathrm{E}}^{\mathrm{b}(2)}{ }_{(\mathrm{s})_{\operatorname{Exp}}}$ | $\mathrm{I}_{\mathrm{E}}^{\mathrm{b}(3)}(\mathrm{s})_{\operatorname{Exp}}$ | $\mathrm{I}_{\mathrm{E}}^{\mathrm{b}}(\mathrm{~s})(\mathrm{s})_{\operatorname{Exp}}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 10.25 | -226 | -658 | -768 | -520 | -560 |
| 10.50 | -168 | -390 | -586 | -395 | -390 |
| 10.75 | -7 | -10 | 0 | 5 | -7 |
| 11.00 | 155 | 439 | 426 | 405 | 474 |
| 11.25 | 300 | 768 | 834 | 818 | 869 |
| 11.50 | 451 | 1122 | 1308 | 1236 | 1174 |
| 11.75 | 543 | 1364 | 1533 | 1436 | 1405 |
| 12.00 | 552 | 1403 | 1572 | 1371 | 1438 |
| 12.25 | 433 | 1038 | 1189 | 1106 | 1192 |
| 12.50 | 262 | 564 | 823 | 627 | 699 |
| 12.75 | 89 | 219 | 254 | 215 | 228 |
| 13.00 | -166 | -455 | -457 | -396 | -389 |
| 13.25 | -370 | -909 | -1190 | -858 | -831 |
| 13.50 | -508 | -1237 | -1528 | -1263 | -1175 |
| 13.75 | -592 | -1404 | -1735 | -1455 | -1482 |
| 14.00 | -594 | -1490 | -1681 | -1484 | -1424 |
| 14.25 | -537 | -1354 | -1544 | -1376 | -1234 |
| 14.50 | -450 | -1149 | -1313 | -1142 | -1065 |
| 14.75 | -405 | -1016 | -1130 | -1013 | -983 |
| 15.00 | -291 | -753 | -854 | -749 | -690 |
| 15.25 | -207 | -594 | -615 | -492 | -484 |
| 15.50 | -134 | -390 | -370 | -343 | -352 |
| 15.75 | -50 | -221 | -154 | -146 | -113 |
| 16.00 | 46 | 55 | 142 | 118 | 88 |
| 16.25 | 118 | 197 | 326 | 308 | 277 |
| 16.50 | 204 | 396 | 564 | 490 | 501 |
| 16.75 | 290 | 602 | 872 | 656 | 712 |
| 17.00 | 385 | 852 | 1110 | 880 | 916 |
| 17.25 | 432 | 955 | 1253 | 969 | 1054 |
| 17.50 | 468 | 1066 | 1356 | 1039 | 1146 |
| 17.75 | 343 | 804 | 940 | 729 | 881 |
| 18.00 | 234 | 479 | 698 | 495 | 542 |
| 18.25 | 65 | 60 | 301 | 31 | 151 |
| 18.50 | -148 | -348 | -338 | -500 | -394 |
| 18.75 | -313 | -733 | -820 | -873 | -809 |
| 19.00 | -463 | -1109 | -1276 | -1267 | -1078 |
| 19.25 | -506 | -1188 | -1450 | -1320 | -1208 |
| 19.50 | -503 | -1191 | -1421 | -1289 | -1253 |
| 19.75 | -430 | -937 | -1256 | -1204 | -1042 |
| 20.00 | -339 | -770 | -1023 | -952 | -813 |
| 20.25 | -198 | -477 | -602 | -613 | -462 |
| 20.50 | -69 | -166 | -215 | -315 | -147 |

Table 7 (continued).

| s | $\mathrm{I}_{\mathrm{E}}^{\mathrm{b}}(\mathrm{~s})_{\operatorname{Exp}}$ | $\mathrm{I}_{\mathrm{E}}^{\mathrm{b}(1)}(\mathrm{s})_{\mathrm{E}}$ | $\mathrm{I}_{\mathrm{E}}^{\left.\mathrm{b}(2)^{(s)}\right)_{\mathrm{E}}}$ | $I_{E}^{b(3)}(s)$ | $\mathrm{L}_{\mathrm{E}}^{\mathrm{b}(4)_{(s)_{E x p}}}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 20.75 | 40 | 68 | 156 | -94 | 81 |
| 21.00 | 123 | 304 | 357 | 152 | 268 |
| 21.25 | 182 | 389 | 481 | 376 | 431 |
| 21.50 | 251 | 534 | 643 | 581 | 618 |
| 21.75 | 271 | 597 | 754 | 564 | 665 |
| 22.00 | 293 | 654 | 746 | 730 | 657 |
| 22.25 | 351 | 752 | 983 | 823 | 845 |
| 22.50 | 332 | 714 | 907 | 762 | 851 |
| 22.75 | 332 | 731 | 841 | 768 | 918 |
| 23.00 | 293 | 658 | 721 | 680 | 855 |
| 23.25 | 243 | 555 | 545 | 610 | 718 |
| 23.50 | 118 | 212 | 223 | 379 | 342 |
| 23.75 | -9 | -89 | -208 | 115 | 142 |
| 24.00 | -128 | -332 | -513 | -233 | -140 |
| 24.25 | -276 | -796 | -860 | -514 | -453 |
| 24.50 | -370 | -974 | -1066 | -839 | -669 |
| 24.75 | -403 | -959 | -1250 | -884 | -743 |
| 25.00 | -416 | -1039 | -1270 | -885 | -721 |
| 25.25 | -365 | -864 | -1065 | -775 | -684 |
| 25.50 | -231 | -594 | -674 | -468 | -308 |
| 25.75 | -81 | -244 | -150 | -132 | -4 |
| 26.00 | 38 | 94 | 115 | 146 | 347 |
| 26.25 | 140 | 335 | 491 | 372 | 545 |
| 26.50 | 229 | 605 | 725 | 629 | 726 |
| 26.75 | 304 | 773 | 918 | 973 | 908 |
| 27.00 | 337 | 939 | 1009 | 886 | 975 |
| 27.25 | 300 | 766 | 1016 | 804 | 916 |
| 27.50 | 264 | 655 | 942 | 684 | 882 |
| 27.75 | 236 | 530 | 853 | 656 | 834 |
| 28.00 | 226 | 615 | 790 | 551 | 878 |
| 28.25 | 204 | 549 | 750 | 523 | 821 |
| 28.50 | 126 | 414 | 530 | 369 | 582 |
| 28.75 | 91 | 319 | 536 | 270 | 438 |
| 29.00 | 23 | 118 | 236 | 230 | 311 |
| 29.25 | -65 | -66 | -46 | 32 | 72 |
| 29.50 | -161 | -321 | -285 | -113 | -186 |
| 29.75 | -236 | -527 | -531 | -391 | -256 |
| 30.00 | -298 | -641 | -745 | -516 | -420 |
| 30.25 | -360 | -861 | -803 | -676 | -560 |
| 30.50 | -328 | -829 | -670 | -649 | -510 |
| 30.75 | -262 | -584 | -403 | -626 | -396 |
| 31.00 | -175 | -500 | -92 | -416 | -166 |

Table 7 (continued)

| s | $\mathrm{I}_{\mathrm{E}}^{\mathrm{b}}(\mathrm{~s})_{\mathrm{Exp}}$ | ${ }^{(1)}(\mathrm{s})_{\operatorname{ExF}}$ | $\mathrm{I}_{\mathrm{E}}^{\mathrm{b}(2)}(\mathrm{s})_{\operatorname{Exp}} \mathrm{I}_{\mathrm{E}}^{\mathrm{b}(3)}(\mathrm{s})_{\operatorname{Exp}} \mathrm{I}_{\mathrm{E}}^{\mathrm{b}}(4)_{(\mathrm{s})_{\operatorname{Exp}}}$ |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 31.25 | -80 | -125 | 205 | -253 | -42 |
| 31.50 | 25 | 38 | 601 | -28 | 202 |
| 31.75 | 155 | 306 | 823 | 361 | 620 |
| 32.00 | 222 | 518 | 1011 | 435 | 723 |
| 32.25 | 256 | 567 | 1082 | 554 | 851 |
| 32.50 | 261 | 549 | 1091 | 610 | 775 |
| 32.75 | 259 | 581 | 1095 | 561 | 754 |
| 33.00 | 210 | 441 | 899 | 494 | 624 |
| 33.25 | 194 | 494 | 922 | 308 | 541 |
| 33.50 | 133 | 446 | 754 | 96 | 344 |
| 33.75 | 58 | 168 | 431 | 137 | 168 |
| 34.00 | 0 | -34 | 336 | -70 | 65 |
| 34.25 | -56 | -16 | 45 | -152 | -157 |
| 34.50 | -94 | -222 | -59 | -288 | -101 |
| 34.75 | -173 | -441 | -170 | -425 | -379 |
| 35.00 | -182 | -368 | -338 | -372 | -467 |
| 35.25 | -202 | -470 | -244 | -484 | -556 |
| 35.50 | -245 | -472 | -482 | -587 | -620 |
| 35.75 | -262 | -527 | -520 | -663 | -663 |
| 36.00 | -244 | -438 | -577 | -681 | -558 |
| 36.25 | -225 | -350 | -562 | -526 | -642 |
| 36.50 | -166 | -227 | -318 | -419 | -515 |
| 36.75 | -41 | 82 | 60 | -212 | -190 |
| 37.00 | 42 | 242 | 266 | 136 | -24 |
| 37.25 | 121 | 275 | 543 | 251 | 295 |
| 37.50 | 143 | 404 | 527 | 465 | 238 |
| 37.75 | 141 | 372 | 431 | 520 | 298 |
| 38.00 | 138 | 401 | 401 | 545 | 223 |
| 38.25 | 109 | 339 | 262 | 448 | 242 |
| 38.50 | 29 | 128 | -20 | 333 | 28 |
| 38.75 | -26 | -25 | -33 | 25 | -45 |
| 39.00 | -45 | -86 | -182 | 38 | -28 |
| 39.25 | -128 | -293 | -456 | -84 | -229 |
| 39.50 | -161 | -407 | -540 | -133 | -376 |
| 39.75 | -213 | -574 | -569 | -324 | -456 |
| 40.00 | -202 | -398 | -585 | -411 | -437 |
| 40.25 | -209 | -302 | -674 | -442 | -481 |
| 40.50 | -182 | -241 | -583 | -416 | -330 |
| 40.75 | -165 | -376 | -568 | -337 | -142 |
| 41.00 | -162 | -389 | -436 | -373 | -66 |
| 41.25 | -127 | -332 | -210 | -332 | -35 |
| 41.50 | -98 | -110 | -83 | -241 | -198 |

Table 7 (continued).

| s | $\mathrm{I}_{\mathrm{E}}^{\mathrm{b}}(\mathrm{s})_{\operatorname{Exp}}$ | $\mathrm{I}_{\mathrm{E}}^{\mathrm{b}(1)}(\mathrm{s})_{\operatorname{Exp}} \mathrm{I}_{\mathrm{E}}^{\mathrm{b}}{ }^{(2)}(\mathrm{s})_{\operatorname{Exp}} \mathrm{I}_{\mathrm{E}}^{\mathrm{b}(3)}(\mathrm{s})_{\operatorname{Exp}} \mathrm{I}_{\mathrm{E}}^{\mathrm{b}}(4)(\mathrm{s})_{\operatorname{Exp}}$ |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 41.75 | -38 | 30 | -35 | 13 | 48 |
| 42.00 | -26 | 97 | -70 | 78 | 89 |

Table 8. Experimental $\mathrm{I}_{\mathrm{E}}^{\mathrm{C}}(\mathrm{s})$ curve $(\mathrm{h}=120.00 \mathrm{~mm})$.

| s | $\mathrm{I}_{\mathrm{E}}^{\mathrm{c}}(\mathrm{s})_{\operatorname{Exp}}$ | s | $\mathrm{I}_{\mathrm{E}}^{\mathrm{C}}(\mathrm{s})_{\operatorname{Exp}}$ | s | $\mathrm{I}_{\mathrm{E}}^{\mathrm{C}}(\mathrm{s})_{\operatorname{Exp}}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 18.50 | 134.0 | 29.00 | 12.0 | 39.50 | -150.0 |
| 18.75 | -23.0 | 29.25 | -59.0 | 39.75 | -172.0 |
| 19.00 | -207.0 | 29.50 | -137.0 | 40.00 | -195.0 |
| 19.25 | -351.0 | 29.75 | -236.0 | 40.25 | -193.0 |
| 19.50 | -361.0 | 30.00 | -294.0 | 40.50 | -176.0 |
| 19.75 | -336.0 | 30.25 | -306.0 | 40.75 | -189.0 |
| 20.00 | -228.0 | 30.50 | -311.0 | 41.00 | -164.0 |
| 20.25 | -123.0 | 30.75 | -282.0 | 41.25 | -153.0 |
| 20.50 | -55.0 | 31.00 | -181.0 | 41.50 | -113.0 |
| 20.75 | 50.0 | 31.25 | -61.0 | 41.75 | -81.0 |
| 21.00 | 142.0 | 31.50 | 24.0 | 42.00 | -54.0 |
| 21.25 | 225.0 | 31.75 | 145.0 | 42.25 | 21.0 |
| 21.50 | 236.0 | 32.00 | 227.0 | 42.50 | 83.0 |
| 21.75 | 281.0 | 32.25 | 254.0 | 42.75 | 131.0 |
| 22.00 | 331.0 | 32.50 | 270.0 | 43.00 | 188.0 |
| 22.25 | 401.0 | 32.75 | 289.0 | 43.25 | 188.0 |
| 22.50 | 359.0 | 33.00 | 243.0 | 43.50 | 139.0 |
| 22.75 | 327.0 | 33.25 | 141.0 | 43.75 | 64.0 |
| 23.00 | 356.0 | 33.50 | 110.0 | 44.00 | 7.0 |
| 23.25 | 272.0 | 33.75 | 24.0 | 44.25 | 18.0 |
| 23.50 | 160.0 | 34.00 | -24.0 | 44.50 | -18.0 |
| 23.75 | 9.0 | 34.25 | -100.0 | 44.75 | -107.0 |
| 24.00 | -95.0 | 34.50 | -111.0 | 45.00 | -74.0 |
| 24.25 | -260.0 | 34.75 | -168.0 | 45.25 | -66.0 |
| 24.50 | -412.0 | 35.00 | -220.0 | 45.50 | -85.0 |
| 24.75 | -444.0 | 35.25 | -280.0 | 45.75 | -79.0 |
| 25.00 | -415.0 | 35.50 | -292.0 | 46.00 | -75.0 |
| 25.25 | -370.0 | 35.75 | -305.0 | 46.25 | -78.0 |
| 25.50 | -276.0 | 36.00 | -263.0 | 46.50 | -69.0 |
| 25.75 | -135.0 | 36.25 | -245.0 | 46.75 | -66.0 |
| 26.00 | 10.0 | 36.50 | -97.0 | 47.00 | 1.0 |
| 26.25 | 166.0 | 36.75 | -7.0 | 47.25 | 27.0 |
| 26.50 | 267.0 | 37.00 | 99.0 | 47.50 | 21.0 |
| 26.75 | 327.0 | 37.25 | 117.0 | 47.75 | 77.0 |
| 27.00 | 309.0 | 37.50 | 152.0 | 48.00 | 80.0 |
| 27.25 | 235.0 | 37.75 | 149.0 | 48.25 | 117.0 |
| 27.50 | 240.0 | 38.00 | 147.0 | 48.50 | 104.0 |
| 27.75 | 182.0 | 38.25 | 111.0 | 48.75 | 118.0 |
| 28.00 | 183.0 | 38.50 | 87.0 | 49.00 | 77.0 |
| 28.25 | 119.0 | 38.75 | 47.0 | 49.25 | 112.0 |
| 28.50 | 92.0 | 39.00 | 2.0 | 49.50 | 64.0 |
| 28.75 | 78.0 | 39.25 | -85.0 | 49.75 | -7.0 |

Table 9. Experimental and theoretical rD $D^{\prime}(r)$ curves.

| r | ${ }^{r D^{\prime}(r)} E_{\mathrm{xp}}$ | $\mathrm{ra}^{\prime}(\mathrm{r})_{\text {Theor }}$ | r | $\mathrm{rD}^{\prime}(\mathrm{r}) \mathrm{E}_{\mathrm{xp}}$ | $\mathrm{rD}^{\prime}(\mathrm{r})$ Theor |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 0.00 | 0.0 | 0.0 | 1.68 | 0.4 | 0.0 |
| 0.04 | -9.9 | 0.0 | 1.72 | 2.5 | 0.0 |
| 0.08 | -13.1 | 0.0 | 1.76 | 3.2 | 0.0 |
| 0.12 | -13.7 | 0.0 | 1.80 | 2.0 | 0.0 |
| 0.16 | -16.7 | 0.0 | 1.84 | 0.4 | 0.0 |
| 0.20 | -15.6 | 0.0 | 1.88 | -0.9 | 0.0 |
| 0.24 | -2.1 | 0.0 | 1.92 | -1.4 | 0.0 |
| 0.28 | 12.8 | 0.0 | 1.96 | -2.1 | 0.0 |
| 0.32 | 13.8 | 0.0 | 2.00 | -3.3 | 0.3 |
| 0.36 | 5.5 | 0.0 | 2.04 | -2.5 | 2.1 |
| 0.40 | -0.1 | 0.0 | 2.08 | 4.5 | 8.7 |
| 0.44 | -3.9 | 0.0 | 2.12 | 20.9 | 24.9 |
| 0.48 | -10.1 | 0.0 | 2.16 | 44.1 | 48.4 |
| 0.52 | -15.4 | 0.0 | 2.20 | 60.3 | 64.5 |
| 0.56 | -16.8 | 0.0 | 2.24 | 54.5 | 58.8 |
| 0.60 | -15.3 | 0.0 | 2.28 | 30.9 | 36.6 |
| 0.64 | -12.4 | 0.0 | 2.32 | 9.2 | 15.6 |
| 0.68 | -9.3 | 0.0 | 2.36 | -0.6 | 4.5 |
| 0.72 | -4.3 | 0.0 | 2.40 | -3.8 | 0.9 |
| 0.76 | 2.4 | 0.0 | 2.44 | -5.4 | 0.1 |
| 0.80 | 6.0 | 0.0 | 2.48 | -5.4 | 0.0 |
| 0.84 | 5.7 | 0.0 | 2.52 | -4.7 | 0.0 |
| 0.88 | 6.1 | 0.0 | 2.56 | -4.1 | 0.0 |
| 0.92 | 6.6 | 0.0 | 2.60 | -2.9 | 0.0 |
| 0.96 | 4.9 | 0.1 | 2.64 | -1.4 | 0.0 |
| 1.00 | 3.8 | 0.7 | 2.68 | -0.8 | 0.0 |
| 1.04 | 6.6 | 5.5 | 2.72 | -0.7 | 0.0 |
| 1.08 | 27.8 | 28.1 | 2.76 | 0.0 | 0.0 |
| 1.12 | 94.5 | 90.2 | 2.80 | 0.3 | 0.0 |
| 1.16 | 192.6 | 182.4 | 2.84 | 0.0 | 0.0 |
| 1.20 | 243.8 | 232.3 | 2.88 | 0.3 | 0.0 |
| 1.24 | 197.0 | 186.1 | 2.92 | 1.5 | 0.0 |
| 1.28 | 101.5 | 93.9 | 2.96 | 1.3 | 0.0 |
| 1.32 | 34.8 | 29.8 | 3.00 | -0.4 | 0.0 |
| 1.36 | 11.9 | 6.0 | 3.04 | -0.5 | 0.0 |
| 1.40 | 5.5 | 0.7 | 3.08 | 1.2 | 0.0 |
| 1.44 | 2.2 | 0.1 | 3.12 | 1.6 | 0.0 |
| 1.48 | 3.0 | 0.0 | 3.16 | 0.8 | 0.0 |
| 1.52 | 4.8 | 0.0 | 3.20 | 1.4 | 0.0 |
| 1.56 | 4.1 | 0.0 | 3.24 | 2.8 | 0.0 |
| 1.60 | 1.4 | 0.0 | 3.28 | 2.4 | 0.0 |
| 1.64 | -0.5 | 0.0 | 3.32 | 0.7 | 0.0 |

Table 9 (continued).

| $r$ | $r D^{\prime}(r)_{\text {Exp }}$ | $r D^{\prime}(r)$ Theor | $r$ | $r D^{\prime}(r)_{\operatorname{Exp}}$ | $r D^{\prime}(r)$ Theor |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |
| 3.36 | -0.3 | 0.0 | 4.20 | -1.1 | 0.0 |
| 3.40 | -0.1 | 0.0 | 4.24 | -0.3 | 0.0 |
| 3.44 | 0.0 | 0.0 | 4.28 | -0.3 | 0.0 |
| 3.48 | -0.1 | 0.0 | 4.32 | -1.3 | 0.0 |
| 3.52 | 0.1 | 0.0 | 4.36 | -1.6 | 0.0 |
| 3.56 | 1.1 | 0.0 | 4.40 | -0.9 | 0.0 |
| 3.60 | 2.0 | 0.0 | 4.44 | -0.1 | 0.0 |
| 3.64 | 1.7 | 0.0 | 4.48 | 0.1 | 0.0 |
| 3.68 | 0.5 | 0.0 | 4.52 | 0.1 | 0.0 |
| 3.72 | -0.1 | 0.0 | 4.56 | -0.1 | 0.0 |
| 3.76 | -0.1 | 0.0 | 4.60 | -0.7 | 0.0 |
| 3.80 | -0.1 | 0.0 | 4.64 | -1.1 | 0.0 |
| 3.84 | 0.1 | 0.0 | 4.68 | -0.7 | 0.0 |
| 3.88 | 0.3 | 0.0 | 4.72 | -0.5 | 0.0 |
| 3.92 | 0.9 | 0.0 | 4.76 | -0.9 | 0.0 |
| 3.96 | 1.3 | 0.0 | 4.80 | -1.1 | 0.0 |
| 4.00 | 0.8 | 0.0 | 4.84 | -0.7 | 0.0 |
| 4.04 | -0.2 | 0.0 | 4.88 | -0.4 | 0.0 |
| 4.08 | -0.7 | 0.0 | 4.92 | -0.1 | 0.0 |
| 4.12 | -0.8 | 0.0 | 4.96 | -0.4 | 0.0 |
| 4.16 | -1.2 | 0.0 | 5.00 | 0.0 | 0.0 |
|  |  |  |  |  |  |

Table 10. Blackness correction table (Oslo).

| D | $\delta$ | D | $\delta$ | D | $\delta$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 0.6200 | . 0001 | 1.0400 | . 0624 | 1.4600 | . 2726 |
| 0.6300 | . 0002 | 1.0500 | . 0658 | 1.4700 | . 2790 |
| 0.6400 | . 0003 | 1.0600 | . 0693 | 1.4800 | . 2854 |
| 0.6500 | . 0004 | 1.0700 | . 0728 | 1.4900 | . 2919 |
| 0.6600 | . 0006 | 1.0800 | . 0764 | 1.5000 | . 2984 |
| 0.6700 | . 0008 | 1.0900 | . 0800 | 1.5100 | . 3050 |
| 0.6800 | . 0011 | 1.1000 | . 0838 | 1.5200 | . 3117 |
| 0.6900 | . 0015 | 1.1100 | . 0879 | 1.5300 | . 3185 |
| 0.7000 | . 0019 | 1.1200 | . 0921 | 1.5400 | . 3253 |
| 0.7100 | . 0023 | 1.1300 | . 0964 | 1.5500 | . 3321 |
| 0.7200 | . 0027 | 1.1400 | . 1007 | 1.5600 | . 3390 |
| 0.7300 | . 0034 | 1.1500 | . 1051 | 1.5700 | . 3460 |
| 0.7400 | . 0041 | 1.1600 | . 1095 | 1.5800 | . 3531 |
| 0.7500 | . 0050 | 1.1700 | . 1141 | 1.5900 | . 3602 |
| 0.7600 | . 0059 | 1.1800 | . 1187 | 1.6000 | . 3674 |
| 0.7700 | . 0069 | 1.1900 | . 1235 | 1.6100 | . 3747 |
| 0.7800 | . 0081 | 1.2000 | . 1283 | 1.6200 | . 3821 |
| 0.7900 | . 0094 | 1.2100 | . 1331 | 1.6300 | . 3895 |
| 0.8000 | . 0107 | 1.2200 | . 1380 | 1.6400 | . 3969 |
| 0.8100 | . 0121 | 1.2300 | . 1429 | 1.6500 | . 4043 |
| 0.8200 | . 0135 | 1.2400 | . 1479 | 1.6600 | . 4119 |
| 0.8300 | . 0150 | 1.2500 | . 1529 | 1.6700 | . 4195 |
| 0.8400 | . 0165 | 1.2600 | . 1580 | 1.6800 | . 4272 |
| 0.8500 | . 0180 | 1.2700 | . 1632 | 1.6900 | . 4350 |
| 0.8600 | . 0196 | 1.2800 | . 1684 | 1.7000 | . 4428 |
| 0.8700 | . 0213 | 1.2900 | . 1737 | 1.7100 | . 4506 |
| 0.8800 | . 0231 | 1.3000 | . 1790 | 1.7200 | . 4584 |
| 0.8900 | . 0250 | 1.3100 | . 1844 | 1.7300 | . 4663 |
| 0.9000 | . 0270 | 1.3200 | . 1898 | 1.7400 | . 4743 |
| 0.9100 | . 0290 | 1.3300 | . 1953 | 1.7500 | . 4825 |
| 0.9200 | . 0311 | 1.3400 | . 2008 | 1.7600 | . 4907 |
| 0.9300 | . 0333 | 1.3500 | . 2064 | 1.7700 | . 4989 |
| 0.9400 | . 0355 | 1.3600 | . 2121 | 1.7800 | . 5072 |
| 0.9500 | . 0377 | 1.3700 | . 2179 | 1.7900 | . 5156 |
| 0.9600 | . 0400 | 1.3800 | . 2237 | 1.8000 | . 5241 |
| 0.9700 | . 0424 | 1.3900 | . 2296 | 1.8100 | . 5326 |
| 0.9800 | . 0450 | 1.4000 | . 2356 | 1.8200 | . 5411 |
| 0.9900 | . 0476 | 1.4100 | . 2416 | 1.8300 | . 5497 |
| 1.0000 | . 0502 | 1.4200 | . 2477 | 1.8400 | . 5584 |
| 1.0100 | . 0531 | 1.4300 | . 2539 | 1.8500 | . 5671 |
| 1.0200 | . 0561 | 1.4400 | . 2601 | 1.8600 | . 5758 |
| 1.0300 | . 0592 | 1.4500 | . 2663 | 1.8700 | . 5846 |

Table 1l. Sector function: $\mathrm{h}=478.00 \mathrm{~mm}$.

| s | $g(\theta)$ | s | $g(\theta)$ | s | $g(\theta)$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 2.50 | 41.29 | 8.75 | 303.62 | 15.00 | 525.21 |
| 2.75 | 50.85 | 9.00 | 312.73 | 15.25 | 533.16 |
| 3.00 | 59.21 | 9.25 | 321. 54 | 15.50 | 542.39 |
| 3.25 | 70.07 | 9.50 | 329.92 | 15.75 | 551.28 |
| 3.50 | 80.39 | 9.75 | 338.62 | 16.00 | 559.79 |
| 3.75 | 92.39 | 10.00 | 347.69 | 16.25 | 568.32 |
| 4.00 | 105.28 | 10.25 | 356.92 | 16.50 | 577.43 |
| 4.25 | 118.36 | 10.50 | 366.17 | 16.75 | 586.77 |
| 4.50 | 131.65 | 10.75 | 374.45 | 17.00 | 595.34 |
| 4.75 | 143.71 | 11.00 | 383.48 | 17.25 | 604.12 |
| 5.00 | 155.41 | 11.25 | 392.81 | 17.50 | 613.11 |
| 5.25 | 166.97 | 11.50 | 401.63 | 17.75 | 622.13 |
| 5.50 | 177.75 | 11.75 | 410.18 | 18.00 | 631.28 |
| 5.75 | 189.01 | 12.00 | 419.30 | 18.25 | 639.79 |
| 6.00 | 200.41 | 12.25 | 428.16 | 18.50 | 648.87 |
| 6.25 | 211.24 | 12.50 | 436.88 | 18.75 | 657.32 |
| 6.50 | 222.19 | 12.75 | 446.07 | 19.00 | 665.99 |
| 6.75 | 231.41 | 13.00 | 454.82 | 19.25 | 674.68 |
| 7.00 | 240.85 | 13.25 | 464.05 | 19.50 | 683.83 |
| 7.25 | 250.28 | 13.50 | 472.51 | 19.75 | 693.47 |
| 7.50 | 259.05 | 13.75 | 480.47 | 20.00 | 702.22 |
| 7.75 | 268.22 | 34.00 | 489.25 | 20.25 | 710.98 |
| 8.00 | 277.15 | 14.25 | 498.55 | 20.50 | 719.86 |
| 8.25 | 285.40 | 14.50 | 507.03 | 20.75 | 729.50 |
| 8.50 | 294.55 | 24.75 | 516.71 | 21.00 | 739.07 |

Table 12. Sector function: $\mathrm{h}=192.07 \mathrm{~mm}$.

| s | $\mathrm{g}(\theta)$ | s | $\mathrm{g}(\theta)$ | s | $\mathrm{s}(\theta)$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |
| 10.25 | 4744 | 21.00 | 13295 | 31.75 | 20707 |
| 10.50 | 4963 | 21.25 | 13444 | 32.00 | 20878 |
| 10.75 | 5226 | 21.50 | 13633 | 32.25 | 21063 |
| 11.00 | 5472 | 21.75 | 13792 | 32.50 | 21227 |
| 11.25 | 5705 | 22.00 | 13951 | 32.75 | 21412 |
| 11.50 | 5943 | 22.25 | 14159 | 33.00 | 21588 |
| 11.75 | 6184 | 22.50 | 14311 | 33.25 | 21788 |
| 12.00 | 6414 | 22.75 | 14488 | 33.50 | 21977 |
| 12.25 | 6613 | 23.00 | 14649 | 33.75 | 22144 |
| 12.50 | 6830 | 23.25 | 14836 | 34.00 | 22311 |
| 12.75 | 7049 | 23.50 | 14998 | 34.25 | 22466 |
| 13.00 | 7253 | 23.75 | 15169 | 34.50 | 22633 |
| 13.25 | 7494 | 24.00 | 15349 | 34.75 | 22803 |
| 13.50 | 7690 | 24.25 | 15503 | 35.00 | 22985 |
| 13.75 | 7907 | 24.50 | 15649 | 35.25 | 23168 |
| 14.00 | 8128 | 24.75 | 15822 | 35.50 | 23366 |
| 14.25 | 8338 | 25.00 | 15978 | 35.75 | 23538 |
| 14.50 | 8553 | 25.25 | 16161 | 36.00 | 23736 |
| 14.75 | 8725 | 25.50 | 16345 | 36.25 | 23899 |
| 15.00 | 8945 | 25.75 | 16521 | 36.50 | 24073 |
| 15.25 | 9147 | 26.00 | 16688 | 36.75 | 24288 |
| 15.50 | 9346 | 26.25 | 16876 | 37.00 | 24479 |
| 15.75 | 9559 | 26.50 | 17033 | 37.25 | 24657 |
| 16.00 | 9774 | 26.75 | 17211 | 37.50 | 24836 |
| 16.25 | 9963 | 27.00 | 17391 | 37.75 | 24990 |
| 16.50 | 10159 | 27.25 | 17541 | 38.00 | 25171 |
| 16.75 | 10340 | 27.50 | 17702 | 38.25 | 25353 |
| 17.00 | 10539 | 27.75 | 17882 | 38.50 | 25524 |
| 17.25 | 10734 | 28.00 | 18055 | 38.75 | 25720 |
| 17.50 | 10944 | 28.25 | 18238 | 39.00 | 25907 |
| 17.75 | 11090 | 28.50 | 18422 | 39.25 | 26092 |
| 18.00 | 11268 | 28.75 | 18606 | 39.50 | 26267 |
| 18.25 | 11448 | 29.00 | 18769 | 39.75 | 26428 |
| 18.50 | 11602 | 29.25 | 18946 | 40.00 | 26631 |
| 18.75 | 11776 | 29.50 | 19121 | 40.25 | 26808 |
| 19.00 | 11951 | 29.75 | 19298 | 40.50 | 27014 |
| 19.25 | 12128 | 30.00 | 19464 | 40.75 | 27194 |
| 19.50 | 12311 | 30.25 | 19643 | 41.00 | 27373 |
| 19.75 | 12489 | 30.50 | 19822 | 41.25 | 27585 |
| 20.00 | 12645 | 30.75 | 20001 | 41.50 | 27767 |
| 20.25 | 12808 | 31.00 | 20170 | 41.75 | 27966 |
| 20.50 | 12980 | 31.25 | 20353 | 42.00 | 28137 |
| 20.75 | 13145 | 31.50 | 20524 | 42.25 | 28337 |
|  |  |  |  |  |  |
|  |  |  |  |  |  |
|  |  |  |  |  |  |

Table 13. Sector function: $h=120.00 \mathrm{~mm}$.

| s | $\mathrm{g}(\theta)$ | s | $\mathrm{g}(\theta)$ | s | $\mathrm{g}(\theta)$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |
| 18.50 | 44984 | 29.00 | 89385 | 39.50 | 126704 |
| 18.75 | 46111 | 29.25 | 90250 | 39.75 | 127612 |
| 19.00 | 47308 | 29.50 | 91049 | 40.00 | 128522 |
| 19.25 | 48480 | 29.75 | 91957 | 40.25 | 129375 |
| 19.50 | 49689 | 30.00 | 92871 | 40.50 | 130380 |
| 19.75 | 50808 | 30.25 | 93737 | 40.75 | 131286 |
| 20.00 | 51998 | 30.50 | 94562 | 41.00 | 132194 |
| 20.25 | 53038 | 30.75 | 95438 | 41.25 | 133150 |
| 20.50 | 53964 | 31.00 | 96363 | 41.50 | 134196 |
| 20.75 | 55087 | 31.25 | 97249 | 41.75 | 135065 |
| 21.00 | 56213 | 31.50 | 98140 | 42.00 | 136023 |
| 21.25 | 57256 | 31.75 | 99123 | 42.25 | 137077 |
| 21.50 | 58283 | 32.00 | 100025 | 42.50 | 137871 |
| 21.75 | 59381 | 32.25 | 100939 | 42.75 | 138930 |
| 22.00 | 60556 | 32.50 | 101779 | 43.00 | 139951 |
| 22.25 | 61812 | 32.75 | 102752 | 43.25 | 140935 |
| 22.50 | 62630 | 33.00 | 103611 | 43.50 | 141920 |
| 22.75 | 63681 | 33.25 | 104484 | 43.75 | 142755 |
| 23.00 | 64851 | 33.50 | 105296 | 44.00 | 143598 |
| 23.25 | 65933 | 33.75 | 106155 | 44.25 | 144655 |
| 23.50 | 66980 | 34.00 | 107103 | 44.50 | 145482 |
| 23.75 | 68026 | 34.25 | 107847 | 44.75 | 146438 |
| 24.00 | 69156 | 34.50 | 108679 | 45.00 | 147483 |
| 24.25 | 70184 | 34.75 | 109494 | 45.25 | 148531 |
| 24.50 | 71014 | 35.00 | 110323 | 45.50 | 149597 |
| 24.75 | 72130 | 35.25 | 111301 | 45.75 | 150588 |
| 25.00 | 73264 | 35.50 | 112228 | 46.00 | 151565 |
| 25.25 | 74217 | 35.75 | 113072 | 46.25 | 152484 |
| 25.50 | 75144 | 36.00 | 113967 | 46.50 | 153506 |
| 25.75 | 76249 | 36.25 | 114755 | 46.75 | 154397 |
| 26.00 | 77312 | 36.50 | 115777 | 47.00 | 155428 |
| 26.25 | 78417 | 36.75 | 116808 | 47.25 | 156426 |
| 26.50 | 79496 | 37.00 | 117793 | 47.50 | 157441 |
| 26.75 | 80563 | 37.25 | 118657 | 47.75 | 158385 |
| 27.00 | 81470 | 37.50 | 119533 | 48.00 | 159352 |
| 27.25 | 82428 | 37.75 | 120376 | 48.25 | 160427 |
| 27.50 | 83397 | 38.00 | 121433 | 48.50 | 161414 |
| 27.75 | 84349 | 38.25 | 122314 | 48.75 | 162419 |
| 28.00 | 85348 | 38.50 | 123299 | 49.00 | 163453 |
| 28.25 | 86349 | 38.75 | 124223 | 49.25 | 164487 |
| 28.50 | 87397 | 39.00 | 125060 | 49.50 | 165380 |
| 28.75 | 88448 | 39.25 | 125894 | 49.75 | 166405 |
|  |  |  |  |  |  |
|  |  |  |  |  |  |
|  |  |  |  |  |  |
|  |  |  |  |  |  |

Table 14. $\left[(Z-F / Z]_{N}\right.$ and $[(Z-F) / Z]_{\mathrm{C}}$ table.

| s | $[(Z-F) / Z]_{N}[(Z-F) / Z]_{O}$ |  | s | $[(Z-F) / Z]_{N}[(Z-F) / Z]_{0}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 0.00 | 0.0000 | 0.0000 | 10.50 | 0.7985 | 0.8090 |
| 0.25 | 0.0093 | 0.0072 | 10.75 | 0.8013 | 0.8113 |
| 0.50 | 0.0240 | 0.0180 | 11.00 | 0.8039 | 0.8135 |
| 0.75 | 0.0460 | 0.0380 | 11.25 | 0.8064 | 0.8160 |
| 1.00 | 0.0770 | 0.0619 | 11.50 | 0.8090 | 0.8180 |
| 1.25 | 0.1140 | 0.0928 | 11.75 | 0.8117 | 0.8210 |
| 1.50 | 0.1595 | 0.1293 | 12.00 | 0.8140 | 0.8233 |
| 1.75 | 0.2031 | 0.1680 | 12.25 | 0.8166 | 0.8259 |
| 2.00 | 0.2495 | 0.2090 | 12.50 | 0.8193 | 0.8282 |
| 2.25 | 0.2959 | 0.2513 | 12.75 | 0.8217 | 0.8300 |
| 2.50 | 0.3421 | 0.2940 | 13.00 | 0.8242 | 0.8321 |
| 2.75 | 0.3880 | 0.3350 | 13.25 | 0.8267 | 0.8340 |
| 3.00 | 0.4300 | 0.3770 | 13.50 | 0.8287 | 0.8360 |
| 3.25 | 0.4694 | 0.4160 | 13.75 | 0.8314 | 0.8380 |
| 3.50 | 0.5030 | 0.4520 | 14.00 | 0.8335 | 0.8399 |
| 3.75 | 0.5340 | 0.4860 | 14.25 | 0.8360 | 0.8418 |
| 4.00 | 0.5650 | 0.5180 | 14.50 | 0.8385 | 0.8437 |
| 4.25 | 0.5928 | 0.5470 | 14.75 | 0.8410 | 0.8456 |
| 4.50 | 0.6160 | 0.5740 | 15.00 | 0.8435 | 0.8472 |
| 4.75 | 0.6373 | 0.5990 | 15.25 | 0.8462 | 0.8494 |
| 5.00 | 0.6550 | 0.6225 | 15.50 | 0.8484 | 0.8513 |
| 5.25 | 0.6719 | 0.6428 | 15.75 | 0.8510 | 0.8535 |
| 5.50 | 0.6875 | 0.6618 | 16.00 | 0.8535 | 0.8553 |
| 5.75 | 0.7003 | 0.6768 | 16.25 | 0.8559 | 0.8572 |
| 6.00 | 0.7110 | 0.6930 | 16.50 | 0.8580 | 0.8590 |
| 6.25 | 0.7220 | 0.7070 | 16.75 | 0.8600 | 0.8606 |
| 6.50 | 0.7310 | 0.7185 | 17.00 | 0.8620 | 0.8623 |
| 6.75 | 0.7387 | 0.7290 | 17.25 | 0.8645 | 0.8645 |
| 7.00 | 0.7447 | 0.7390 | 17.50 | 0.8665 | 0.8662 |
| 7.25 | 0.7509 | 0.7480 | 17.75 | 0.8690 | 0.8681 |
| 7.50 | 0.7560 | 0.7560 | 18.00 | 0.8715 | 0.8699 |
| 7.75 | 0.7613 | 0.7640 | 18.25 | 0.8738 | 0.8718 |
| 8.00 | 0.7660 | 0.7701 | 18.50 | 0.8760 | 0.8736 |
| 8.25 | 0.7700 | 0.7770 | 18.75 | 0.8785 | 0.8752 |
| 8.50 | 0.7740 | 0.7822 | 19.00 | 0.8810 | 0.8772 |
| 8.75 | 0.7780 | 0.7860 | 19.25 | 0.8830 | 0.8788 |
| 9.00 | 0.7820 | 0.7900 | 19.50 | 0.8855 | 0.8806 |
| 9.25 | 0.7850 | 0.7940 | 19.75 | 0.8875 | 0,8823 |
| 9.50 | 0.7877 | 0.7973 | 20.00 | 0.8895 | 0.8841 |
| 9.75 | 0.7900 | 0.8003 | 20.25 | 0.8917 | 0.8860 |
| 10.00 | 0.7930 | 0.8039 | 20.50 | 0.8935 | 0.8878 |
| 10.25 | 0.7958 | 0.8060 | 20.75 | 0.8955 | 0.8895 |

Table 14 (continued).

| s | $[(Z-F) / Z]_{N}[(Z-F) / Z]_{O}$ |  | $[(Z-F) / Z]_{N}[(Z-F) / Z]_{O}$ |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 21.00 | 0.8977 | 0.8907 | 31.50 | 0.9555 | 0.9473 |
| 21.25 | 0.9000 | 0.8921 | 31.75 | 0.9560 | 0.9480 |
| 21.50 | 0.9020 | 0.8940 | 32.00 | 0.9567 | 0.9490 |
| 21.75 | 0.9040 | 0.8955 | 32.25 | 0.9575 | 0.9498 |
| 22.00 | 0.9062 | 0.8970 | 32.50 | 0.9582 | 0.9503 |
| 22.25 | 0.9080 | 0.8984 | 32.75 | 0.9592 | 0.9513 |
| 22.50 | 0.9102 | 0.9000 | 33.00 | 0.9600 | 0.9520 |
| 22.75 | 0.9120 | 0.9015 | 33.25 | 0.9606 | 0.9528 |
| 23.00 | 0.9140 | 0.9030 | 33.50 | 0.9614 | 0.9537 |
| 23.25 | 0.9157 | 0.9044 | 33.75 | 0.9620 | 0.9542 |
| 23.50 | 0.9168 | 0.9060 | 34.00 | 0.9624 | 0.9550 |
| 23.75 | 0.9185 | 0.9075 | 34.25 | 0.9632 | 0.9560 |
| 24.00 | 0.9202 | 0.9089 | 34.50 | 0.9639 | 0.9564 |
| 24.25 | 0.9220 | 0.9103 | 34.75 | 0.9642 | 0.9570 |
| 24.50 | 0.9237 | 0.9120 | 35.00 | 0.9647 | 0.9576 |
| 24.75 | 0.9252 | 0.9137 | 35.25 | 0.9655 | 0.9580 |
| 25.00 | 0.9268 | 0.9150 | 35.50 | 0.9660 | 0.9584 |
| 25.25 | 0.9281 | 0.9169 | 35.75 | 0.9663 | 0.9594 |
| 25.50 | 0.9297 | 0.9182 | 36.00 | 0.9670 | 0.9600 |
| 25.75 | 0.9316 | 0.9199 | 36.25 | 0.9675 | 0.9603 |
| 26.00 | 0.9325 | 0.9210 | 36.50 | 0.9680 | 0.9613 |
| 26.25 | 0.9338 | 0.9222 | 36.75 | 0.9684 | 0.9617 |
| 26.50 | 0.9347 | 0.9238 | 37.00 | 0.9691 | 0.9621 |
| 26.75 | 0.9360 | 0.9250 | 37.25 | 0.9699 | 0.9625 |
| 27.00 | 0.9374 | 0.9261 | 37.50 | 0.9702 | 0.9633 |
| 27.25 | 0.9382 | 0.9279 | 37.75 | 0.9708 | 0.9637 |
| 27.50 | 0.9395 | 0.9292 | 38.00 | 0.9714 | 0.9639 |
| 27.75 | 0.9403 | 0.9303 | 38.25 | 0.9720 | 0.9642 |
| 28.00 | 0.9418 | 0.9320 | 38.50 | 0.9723 | 0.9646 |
| 28.25 | 0.9425 | 0.9334 | 38.75 | 0.9727 | 0.9653 |
| 28.50 | 0.9438 | 0.9342 | 39.00 | 0.9735 | 0.9657 |
| 28.75 | 0.9445 | 0.9358 | 39.25 | 0.9739 | 0.9661 |
| 29.00 | 0.9457 | 0.9367 | 39.50 | 0.9741 | 0.9663 |
| 29.25 | 0.9468 | 0.9378 | 39.75 | 0.9743 | 0.9668 |
| 29.50 | 0.9480 | 0.9387 | 40.00 | 0.9748 | 0.9675 |
| 29.75 | 0.9491 | 0.9399 | 40.25 | 0.9754 | 0.9678 |
| 30.00 | 0.9500 | 0.9410 | 40.50 | 0.9758 | 0.9681 |
| 30.25 | 0.9516 | 0.9423 | 40.75 | 0.9760 | 0.9685 |
| 30.50 | 0.9522 | 0.9435 | 41.00 | 0.9762 | 0.9687 |
| 30.75 | 0.9532 | 0.9442 | 41.25 | 0.9765 | 0.9693 |
| 31.00 | 0.9540 | 0.9450 | 41.50 | 0.9771 | 0.9696 |
| 31.25 | 0.9545 | 0.9462 | 41.75 | 0.9776 | 0.9700 |

Table 14 (continued).

| $s$ |  | $[(Z-F) / Z]_{N}[(Z-F) / Z]_{O}$ | $s$ |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $[(Z-F) / Z]_{N}[(Z-F) / Z]_{O}$ |  |  |  |
| 42.00 | 0.9779 | 0.9702 | 46.00 | 0.9816 | 0.9745 |
| 42.25 | 0.9780 | 0.9703 | 46.25 | 0.9818 | 0.9748 |
| 42.50 | 0.9783 | 0.9705 | 46.50 | 0.9820 | 0.9753 |
| 42.75 | 0.9785 | 0.9707 | 46.75 | 0.9821 | 0.9756 |
| 43.00 | 0.9790 | 0.9712 | 47.00 | 0.9823 | 0.9758 |
| 43.25 | 0.9795 | 0.9719 | 47.25 | 0.9824 | 0.9760 |
| 43.50 | 0.9798 | 0.9721 | 47.50 | 0.9826 | 0.9761 |
| 43.75 | 0.9800 | 0.9722 | 47.75 | 0.9831 | 0.9763 |
| 44.00 | 0.9802 | 0.9726 | 48.00 | 0.9835 | 0.9765 |
| 44.25 | 0.9804 | 0.9730 | 48.25 | 0.9836 | 0.9765 |
| 44.50 | 0.9805 | 0.9733 | 48.50 | 0.9839 | 0.9768 |
| 44.75 | 0.9807 | 0.9735 | 48.75 | 0.9840 | 0.9772 |
| 45.00 | 0.9810 | 0.9736 | 49.00 | 0.9841 | 0.9775 |
| 45.25 | 0.9810 | 0.9740 | 49.25 | 0.9843 | 0.9778 |
| 45.50 | 0.9812 | 0.9741 | 49.50 | 0.9845 | 0.9780 |
| 45.75 | 0.9814 | 0.9742 | 49.75 | 0.9846 | 0.9781 |
|  |  |  |  |  |  |

Table 15. $\mathrm{Z}_{\mathrm{N}} \mathrm{Z}_{\mathrm{O}}^{(\mathrm{Z}-\mathrm{F})_{\mathrm{O}} /(\mathrm{Z}-\mathrm{F})_{\mathrm{N}}}$ table.

|  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\mathrm{A}_{\mathrm{O}} \ldots \mathrm{O}$ | s | $\mathrm{A}_{\mathrm{O}} \ldots \mathrm{O}$ | s | $\mathrm{A}_{\mathrm{O}} \ldots \mathrm{O}$ |
|  |  |  |  |  |  |
| 0.25 | 49.5 | 10.75 | 64.8 | 21.25 | 63.4 |
| 0.50 | 48.0 | 11.00 | 64.8 | 21.50 | 63.4 |
| 0.75 | 52.9 | 11.25 | 64.8 | 21.75 | 63.4 |
| 1.00 | 51.4 | 11.50 | 64.7 | 22.00 | 63.3 |
| 1.25 | 52.1 | 11.75 | 64.7 | 22.25 | 63.3 |
| 1.50 | 51.9 | 12.00 | 64.7 | 22.50 | 63.3 |
| 1.75 | 52.9 | 12.25 | 64.7 | 22.75 | 63.3 |
| 2.00 | 53.6 | 12.50 | 64.7 | 23.00 | 63.2 |
| 2.25 | 54.4 | 12.75 | 64.6 | 23.25 | 63.2 |
| 2.50 | 55.0 | 13.00 | 64.6 | 23.50 | 63.2 |
| 2.75 | 55.3 | 13.25 | 64.6 | 23.75 | 63.2 |
| 3.00 | 56.1 | 13.50 | 64.6 | 24.00 | 63.2 |
| 3.25 | 56.7 | 13.75 | 64.5 | 24.25 | 63.2 |
| 3.50 | 57.5 | 14.00 | 64.5 | 24.50 | 63.2 |
| 3.75 | 58.2 | 14.25 | 64.4 | 24.75 | 63.2 |
| 4.00 | 58.7 | 14.50 | 64.4 | 25.00 | 63.2 |
| 4.25 | 59.1 | 14.75 | 64.3 | 25.25 | 63.2 |
| 4.50 | 59.6 | 15.00 | 64.3 | 25.50 | 63.2 |
| 4.75 | 60.2 | 15.25 | 64.3 | 25.75 | 63.2 |
| 5.00 | 60.8 | 15.50 | 64.2 | 26.00 | 63.2 |
| 5.25 | 61.2 | 15.75 | 64.2 | 26.25 | 63.2 |
| 5.50 | 61.6 | 16.00 | 64.1 | 26.50 | 63.3 |
| 5.75 | 61.8 | 16.25 | 64.1 | 26.75 | 63.2 |
| 6.00 | 62.4 | 16.50 | 64.1 | 27.00 | 63.2 |
| 6.25 | 62.7 | 16.75 | 64.1 | 27.25 | 63.3 |
| 6.50 | 62.9 | 17.00 | 64.0 | 27.50 | 63.3 |
| 6.75 | 63.2 | 17.25 | 64.0 | 27.75 | 63.3 |
| 7.00 | 63.5 | 17.50 | 64.0 | 28.00 | 63.3 |
| 7.25 | 63.8 | 17.75 | 63.9 | 28.25 | 63.4 |
| 7.50 | 64.0 | 18.00 | 63.9 | 28.50 | 63.3 |
| 7.75 | 64.3 | 18.25 | 63.9 | 28.75 | 63.4 |
| 8.00 | 64.3 | 18.50 | 63.8 | 29.00 | 63.4 |
| 8.25 | 64.6 | 18.75 | 63.8 | 29.25 | 63.4 |
| 8.50 | 64.7 | 19.00 | 63.7 | 29.50 | 63.4 |
| 8.75 | 64.6 | 19.25 | 63.7 | 29.75 | 63.4 |
| 9.00 | 64.6 | 19.50 | 63.6 | 30.00 | 63.4 |
| 9.25 | 64.7 | 19.75 | 63.6 | 30.25 | 63.4 |
| 9.50 | 64.8 | 20.00 | 63.6 | 30.50 | 63.4 |
| 9.75 | 64.8 | 20.25 | 63.6 | 30.75 | 63.4 |
| 10.00 | 64.9 | 20.50 | 63.6 | 31.00 | 63.4 |
| 10.25 | 64.8 | 20.75 | 63.6 | 31.25 | 63.4 |
| 10.50 | 64.8 | 21.00 | 63.5 | 31.50 | 63.4 |
|  |  |  |  |  |  |

Table 15 (continued)

| s | $\mathrm{A}_{\mathrm{O}} \ldots \mathrm{O}$ | s | $\mathrm{A}_{\mathrm{O}} \ldots \mathrm{O}$ | s | $\mathrm{A}_{\mathrm{O}} \cdots \mathrm{O}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |
| 31.75 | 63.5 | 37.75 | 63.5 | 43.75 | 63.5 |
| 32.00 | 63.5 | 38.00 | 63.5 | 44.00 | 63.5 |
| 32.25 | 63.5 | 38.25 | 63.5 | 44.25 | 63.5 |
| 32.50 | 63.5 | 38.50 | 63.5 | 44.50 | 63.5 |
| 32.75 | 63.5 | 38.75 | 63.5 | 44.75 | 63.5 |
| 33.00 | 63.5 | 39.00 | 63.5 | 45.00 | 63.5 |
| 33.25 | 63.5 | 39.25 | 63.5 | 45.25 | 63.5 |
| 33.50 | 63.5 | 39.50 | 63.5 | 45.50 | 63.5 |
| 33.75 | 63.5 | 39.75 | 63.5 | 45.75 | 63.5 |
| 34.00 | 63.5 | 40.00 | 63.5 | 46.00 | 63.5 |
| 34.25 | 63.5 | 40.25 | 63.5 | 46.25 | 63.5 |
| 34.50 | 63.5 | 40.50 | 63.5 | 46.50 | 63.6 |
| 34.75 | 63.5 | 40.75 | 63.5 | 46.75 | 63.6 |
| 35.00 | 63.5 | 41.00 | 63.5 | 47.00 | 63.6 |
| 35.25 | 63.5 | 41.25 | 63.5 | 47.25 | 63.6 |
| 35.50 | 63.5 | 41.50 | 63.5 | 47.50 | 63.6 |
| 35.75 | 63.5 | 41.75 | 63.5 | 47.75 | 63.6 |
| 36.00 | 63.5 | 42.00 | 63.5 | 48.00 | 63.5 |
| 36.25 | 63.5 | 42.25 | 63.5 | 48.25 | 63.5 |
| 36.50 | 63.6 | 42.50 | 63.5 | 48.50 | 63.5 |
| 36.75 | 63.6 | 42.75 | 63.5 | 48.75 | 63.6 |
| 37.00 | 63.5 | 43.00 | 63.5 | 49.00 | 63.6 |
| 37.25 | 63.5 | 43.25 | 63.5 | 49.25 | 63.6 |
| 37.50 | 63.5 | 43.50 | 63.5 | 49.50 | 63.6 |
|  |  |  |  | 49.75 | 63.6 |

$A_{O} \cdots O_{N}=Z_{N} Z_{O}(Z-F)_{O} /(Z-F)_{N}$.

Table 16. Results of least-squares refinements ${ }^{(a)}$ : comparison of separate composites for different $\Delta s$ intervals.

|  | ${ }^{\mathrm{I}} \mathrm{I}_{\mathrm{E}} ; 2.50 \leq s \leq 20.75$ |  |  |  | $\mathrm{I}_{\mathrm{E}}^{\mathrm{b}} ; 10.25 \leq s \leq 42.00$ |  |  | $\mathrm{I}_{\mathrm{E}}^{\mathrm{c}} ; 28.75 \leq s \leq 49.75$ |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\Delta s$ |  |  |  |  | $\Delta$ s |  |  | $\Delta$ s |  |  |
|  | . 25 | . 50 | 75 | 1.00 | 25 | . 50 | . 75 | 25 | . 50 | 75 | 25 |
| ${ }^{\mathrm{r}} \mathrm{N}-\mathrm{O}^{\prime}{ }^{\circ}$ | 1.200 | 1.200 | 1.200 | 1. 200 | 1. 202 | 1. 202 | 1.202 | 1. 200 | 1.200 | 1. 200 | 1. 200 |
| $\sigma_{L S}\left(\mathrm{r}_{\mathrm{N}-\mathrm{O}}\right), \stackrel{\circ}{\text { A }}$ | $\pm .0015$ | $\pm .0023$ | $\pm .0028$ | $\pm .0034$ | $\pm .0009$ | $\pm .0013$ | $\pm .0016$ | $\pm .0008$ | $\pm .0013$ | $\pm .0017$ | $\pm .0010$ |
| $r_{O} \ldots 0^{\circ}{ }^{\circ}$ | 2.207 | 2.207 | 2.206 | 2.210 | 2.211 | 2.211 | 2.211 | 2.212 | 2.213 | 2.216 | 2. 207 |
| $\sigma_{L S}(\mathrm{r} O \cdots)^{\prime}, \stackrel{\circ}{\text { a }}$ | $\pm .0058$ | $\pm .0087$ | $\pm .0111$ | $\pm .0139$ | $\pm .0036$ | $\pm .0053$ | $\pm .0068$ | $\pm .0044$ | $\pm .0067$ | $\pm .0080$ | $\pm .0043$ |
| $\mathrm{l}_{\mathrm{N}-\mathrm{O}}$, ${ }_{\text {A }}$ | . 0336 | . 0347 | . 0309 | . 0334 | . 0368 | . 0362 | . 0363 | . 0378 | . 0367 | . 0373 | . 0334 |
| $\sigma_{L S}\left(1_{N-O}\right), \stackrel{\circ}{\text { a }}$ | $\pm .0044$ | $\pm . .0064$ | $\pm .0087$ | $\pm .0100$ | $\pm .0014$ | $\pm .0021$ | $\pm .0026$ | $\pm .0020$ | $\pm .0032$ | $\pm .0040$ | $\pm .0017$ |
| ${ }^{1} \mathrm{O} \cdot \mathrm{O} \mathrm{O}^{\text {, }} \stackrel{\text { A }}{ }$ | . 0504 | . 0511 | . 0526 | . 0547 | . 0444 | . 0447 | . 0449 | . 0464 | . 0447 | . 0443 | . 0420 |
| $\left.\sigma_{L S}(1) \ldots\right)^{\prime}, \stackrel{\circ}{\text { a }}$ | $\pm .0077$ | $\pm .0116$ | $\pm .0141$ | $\pm .0167$ | $\pm .0033$ | $\pm .0049$ | $\pm .0062$ | $\pm .0032$ | $\pm .0051$ | $\pm .0063$ | $\pm .0036$ |

${ }^{(a)}\left(\mathrm{P}_{\mathrm{ii}}=1, \mathrm{~A}_{\mathrm{N}-\mathrm{O}}=2 Z_{\mathrm{N}} Z_{\mathrm{O}}\right.$, and $\mathrm{A}_{\mathrm{O}} \ldots \mathrm{O}=\mathrm{Z}_{\mathrm{O}}^{2}$ were used in all refinements.

Table 17. Results of least-squares refinements ${ }^{(a)}$ : comparison of individual photographic plates with their composites.

|  | $2.50 \leq s \leq 20.75, \Delta s=.25$ |  |  |  |  | $10.50<s<20.75, \Delta s=.25$ |  |  |  | $10.25 \leq s \leq 42.00, \Delta s=.25$ |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\mathrm{I}_{\mathrm{E}}{ }^{\text {a }}$ | $\mathrm{I}_{\mathrm{E}}{ }^{\text {(1) }}$ | $\mathrm{I}_{\mathrm{E}}{ }^{(2)}$ | $\mathrm{I}_{\mathrm{E}}{ }^{\text {(3) }}$ | $\mathrm{I}_{\mathrm{E}}{ }^{\text {(4) }}$ | $I_{E}^{\text {a }}$ | $\mathrm{I}_{\mathrm{E}}{ }^{\text {a(1) }}$ | $\begin{array}{cc} \mathrm{I}^{\mathrm{a}(2)} & \mathrm{I}_{\mathrm{E}}{ }^{2(3)} \\ \hline \end{array}$ | $\mathrm{I}_{\mathrm{E}}^{\text {a(4) }}$ | $\mathrm{I}_{\mathrm{E}}^{\mathrm{b}}$ | $I_{E}^{b(1)}$ | $I_{E}^{b(2)}$ | $I_{E}^{b(3)}$ | $\mathrm{I}_{\mathrm{E}}^{\mathrm{b}}{ }^{(4)}$ |
| ${ }^{\mathrm{r}} \mathrm{N}-\mathrm{O},{ }^{\text {A }}$ | 1. 200 | 1. 199 | 1. 199 | 1. 200 | 1.201 | 1. 200 | 1. 199 | 1.199 --- | 1.201 | 1. 202 | 1. 202 | 1. 203 | 1.201 | 1.201 |
| $\sigma_{L S}\left(\mathrm{r}_{\mathrm{N}-\mathrm{O}}\right), \AA^{\circ}$ | $\pm .0015$ | $\pm .0016$ | $\pm .0018$ | $\pm .0022$ | $\pm .0015$ | $\pm .0018$ | $\pm .0019$ | $\pm .0023--$ | $\pm .0019$ | $\pm .0009$ | $\pm .0010$ | $\pm .0012$ | $\pm .0010$ | $\pm .0014$ |
| ${ }^{\mathrm{r}} \mathrm{O} \ldots \mathrm{O}^{\prime}{ }^{\circ}{ }^{\mathrm{A}}$ | 2.207 | 2.203 | 2.212 | 2.202 | 2.207 | 2.208 | 2.202 | 2.216 --- | 2. 208 | 2.211 | 2.213 | 2.213 | 2.207 | 2.212 |
| $\sigma_{L S}(\mathrm{r} 0 \ldots \mathrm{O}), \stackrel{\circ}{ }{ }^{\circ}$ | $\pm .0056$ | $\pm .0068$ | $\pm .0073$ | $\pm .0085$ | $\pm .0055$ | $\pm .0071$ | $\pm .0086$ | 土. 0099 --- | $\pm .0071$ | $\pm .0036$ | $\pm .0041$ | $\pm .0051$ | $\pm .0041$ | $\pm .0055$ |
| ${ }^{1} \mathrm{~N}-\mathrm{O},{ }^{\text {A }}$ | . 0036 | . 0354 | . 0369 | . 0293 | . 0381 | . 0201 | . 0126 | . 0221 --- | . 0260 | . 0367 | . 0382 | . 0365 | . 0385 | . 0400 |
| $\sigma_{L S}\left(1{ }^{1}-\mathrm{O}\right),{ }_{\text {A }}$ | $\pm .0042$ | $\pm .0044$ | $\pm .0047$ | $\pm .0072$ | $\pm .0038$ | $\pm .0137$ | $\pm .0228$ | 士. 0163 --- | $\pm .0109$ | $\pm .0014$ | $\pm .0015$ | $\pm .0019$ | $\pm .0016$ | $\pm .0020$ |
| ${ }^{1} 0 . .0$, ${ }^{\text {A }}$ | . 0504 | . 0617 | . 0589 | . 0507 | . 0511 | . 0422 | . 0516 | . 0495 --- | . 0426 | . 0441 | . 0457 | . 0446 | . 0448 | . 0466 |
| $\sigma_{L S}\left(1{ }_{O} \ldots O^{\prime},{ }^{\circ}\right.$ | $\pm .0075$ | $\pm .0077$ | $\pm .0086$ | $\pm .0113$ | $\pm .0072$ | $\pm .0115$ | $\pm .0111$ | $\pm .0138-\mathrm{-}$ | $\pm .0114$ | $\pm .0033$ | $\pm .0037$ | $\pm .0046$ | $\pm .0038$ | $\pm .0049$ |

${ }^{(a)}{ }_{(\mathbb{P})_{i i}}=1, A_{N-O}=2 Z_{N} Z_{O}$, and $A_{O} \ldots \mathrm{O}=Z_{N} Z_{O}(Z-F)_{\mathrm{O}} /(Z-F)_{N}$ were used in all refinements.

Table 18. Results of least-squares refinements ${ }^{(a)}$ : comparison of different composites.

|  | $\mathrm{I}_{\mathrm{E}}^{\mathrm{a}} ; 2.50 \leq s \leq 20.75, \Delta s=.25$ |  | $\mathrm{I}_{\mathrm{E}}^{\mathrm{b}}$ 10.25 | $\Delta s=.25$ | $\mathrm{I}_{\mathrm{E}}^{\mathrm{C}} ; 28.75<s<49.75$, $\Delta_{s}=.25$ | $\begin{gathered} \mathrm{I}_{\mathrm{E}}^{\mathrm{T} ; 2.50<s<49.75} \quad \Delta s=.25 \\ \mathrm{~s}^{s} \equiv .2 \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $c^{(b)}$ | $V$ (c) | C | V | C | V |
| ${ }_{\mathrm{r}}^{\mathrm{N}-\mathrm{O}}, \stackrel{\circ}{\mathrm{~A}}$ | 1. 200 | 1. 200 | 1. 202 | 1. 202 | 1. 200 | 1. 201 |
| $\sigma_{L S}\left(\mathrm{r}_{\mathrm{N}-\mathrm{O}}\right),{ }^{\circ}$ | $\pm .0015$ | $\pm .0015$ | $\pm .0009$ | $\pm .0009$ | $\pm .0008$ | $\pm .0007$ |
| ${ }^{\mathrm{r}} \mathrm{O}_{\mathrm{O}} \mathrm{O}, \stackrel{\circ}{\mathrm{~A}}$ | 2. 207 | 2. 207 | 2.211 | 2.211 | 2.212 | 2.210 |
| $\sigma_{L S}\left(\mathrm{r}_{\mathrm{O}} \ldots \mathrm{O}\right),{ }^{\text {A }}$ | $\pm .0058$ | $\pm .0056$ | $\pm .0036$ | $\pm .0036$ | $\pm .0044$ | $\pm .0030$ |
| $\mathrm{l}_{\mathrm{N}-\mathrm{O}},{ }^{\text {a }}$ | . 0036 | . 0336 | . 0368 | . 0367 | . 0378 | . 0382 |
| $\sigma_{\text {LS }}\left(1_{N-O}\right), ~ \stackrel{\circ}{\text { a }}$ | $\pm .0044$ | $\pm .0042$ | $\pm .0014$ | $\pm .0014$ | $\pm .0020$ | $\pm .0080$ |
| ${ }^{1} 0 \ldots 0,{ }^{\circ}$ | . 0504 | . 0504 | . 0444 | . 0441 | . 0464 | . 0470 |
| $\sigma_{L S}(10 \ldots 0), \AA^{\circ}$ | $\pm .0077$ | $\pm .0075$ | $\pm .0033$ | $\pm .0033$ | $\pm .0032$ | $\pm .0025$ |

(a) $(\mathbb{P})_{i i}=1$ was used in all refinements.
(b) $A_{N-O}=2 Z_{N} Z_{O}$ and $A_{O} \cdots O=Z_{O}^{2}$
(c) $\mathrm{A}_{\mathrm{N}-\mathrm{O}}=2 Z_{\mathrm{N}} \mathrm{Z}_{\mathrm{O}}$ and $\mathrm{A}_{\mathrm{O}} \cdots \mathrm{O}=\mathrm{Z}_{\mathrm{N}} \mathrm{Z}_{\mathrm{O}}(\mathrm{Z}-\mathrm{F})_{\mathrm{O}} /(\mathrm{Z}-\mathrm{F})_{\mathrm{N}}$.

Table 19. Results of least-squares refinements:(a) effect of variable weight matrix in analysis of $\mathrm{I}_{\mathrm{E}}^{\mathrm{T}}(\mathrm{s})$.

|  | $\mathrm{I}_{\mathrm{E}}^{\mathrm{T}}(\mathrm{s}) ; 2.50 \leq \mathrm{s} \leq 49.75, \Delta \mathrm{~s}=.25$ |  |  |
| :---: | :---: | :---: | :---: |
|  | $(\mathbb{P})_{\text {ii }}$ |  |  |
|  | 1 | const $\mathrm{s}_{\mathrm{i}} \exp \left(-.0016 \mathrm{~s}_{\mathrm{i}}^{2}\right)$ | const $\mathrm{s}_{\mathrm{i}} \exp \left(-.002 \mathrm{~s}_{\mathrm{i}}^{2}\right)$ |
| $\mathrm{r}_{\mathrm{N}-\mathrm{O}}, \AA$ | 1. 2009 | 1. 2010 | 1. 2012 |
| $\sigma_{\text {LS }}\left(\mathrm{r}_{\mathrm{N}, \mathrm{O}}\right), \AA^{\text {A }}$ | $\pm .0007$ | $\pm .0007$ | $\pm .0007$ |
| $\mathrm{r}_{\mathrm{O}} \ldots \mathrm{O},{ }^{\text {A }}$ | 2. 2102 | 2. 2096 | 2. 2095 |
| $\sigma_{\text {LS }}(\mathrm{r} \mathrm{O} \ldots \mathrm{O}), \AA$ | $\pm .0030$ | $\pm .0027$ | $\pm .0028$ |
| $\mathrm{l}_{\mathrm{N}-\mathrm{O}}, \stackrel{\AA}{\text { A }}$ | . 03815 | . 03753 | 03747 |
| $\sigma_{\text {LS }}\left(1_{N-O}\right), \stackrel{\AA}{A}$ | $\pm .00079$ | $\pm .00098$ | $\pm .00108$ |
| ${ }^{1} \mathrm{O} . . \mathrm{O}^{\prime}{ }^{\text {A }}$ | . 04698 | . 04701 | . 04714 |
| $\sigma_{L S}{ }^{(1)} \mathrm{O} \cdot \mathrm{O}^{\text {) }}$, ${ }^{\AA}$ | $\pm .00253$ | $\pm .00263$ | $\pm .00282$ |

Table 20. Error matrix ( $\times 10^{6}$ ) obtained from third cycle of leastsquares refinement ${ }^{(a)}$ of $\mathrm{I}_{\mathrm{E}}^{\mathrm{T}}(\mathrm{s}): 2.50 \leq \mathrm{s} \leq 49.75$ and $\Delta s=0.25$.

| $\mathrm{r}_{\mathrm{N}-\mathrm{O}}{ }^{(\mathrm{b})}$ | $\mathrm{r}_{\mathrm{O}} \cdots \mathrm{O}$ | $<\mathrm{O}-\mathrm{N}-\mathrm{O}^{(\mathrm{c})}$ | $\mathrm{l}_{\mathrm{N}-\mathrm{O}}$ | $\mathrm{l}_{\mathrm{O}} \cdots \mathrm{O}$ |
| :--- | :---: | :---: | :---: | :---: |
| .4736 | -.0002 | -106.4285 | -.0052 | -.0097 |
|  | 8.7908 | 1072.76 | .0107 | -.1374 |
|  |  | 154815.8 | 2.4791 | -14.5843 |
|  |  | .6223 | .2792 |  |
|  |  |  | 6.4444 |  |


${ }^{(b)}$ Distance and amplitude quantities in $(\AA)^{2}$.
${ }^{(c)}$ Angle quantities in $(\mathrm{deg})^{2}$.

Table 21. Error analysis of structure parameters.

|  | ${ }^{\text {r }} \mathrm{N}-\mathrm{O}$ | ${ }^{\text {r }} \mathrm{O} \cdot \cdots \mathrm{O}$ | $<\mathrm{O}-\mathrm{N}-\mathrm{O}$ | ${ }^{\mathrm{N}-\mathrm{O}}$ | ${ }^{1} \mathrm{O} \cdot . \mathrm{O}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1) $\left(.0005 \mathrm{r}_{\mathrm{ij}}\right)^{2} \times 10^{6}$ | . 361 | 1. 224 | --- | --- | --- |
| 2) $\left(.021_{i j}\right)^{2} \times 10^{6}$ | --- | --- | --- | . 582 | . 883 |
| 3) $\sigma_{L S}^{2} \times 10^{6}$ | $\pm .474$ | +8. 791 | $\pm 154816$ | $\pm .622$ | $\pm 6.444$ |
| 4) $\sigma_{2}^{2} \times 10^{6}$ | $\pm .443$ | $\pm 5.867$ | $\pm 109700$ | $\pm 4.22$ | $\pm 11.34$ |
| 5) $\sigma_{L S}^{2} / \sigma_{2}^{2}$ | 1.07 | 1.50 | 1.41 | . 15 | . 57 |
| 6) $\sigma_{T}$ | $\pm .0013$ | $\pm .0050$ | $\pm .65$ | $\pm .0025$ | $\pm .0050$ |
| 7) $\left(\sigma_{T}^{2}-2 \sigma_{L S}^{2}\right)^{\frac{1}{2}}$ | $\pm .0009$ | $\pm .0027$ | $\pm .33$ | $\pm .0022$ | $\pm .0035$ |
| 8) $\left(\sigma_{T}^{2}-\sigma_{2}^{2}\right)^{\frac{1}{2}}$ | $\pm .0011$ | $\pm .0043$ | $\pm .56$ | $\pm .0014$ | $\pm .0037$ |

(1) - (4) Distance and amplitude quantities in $\left(\begin{array}{l}\mathrm{A}\end{array}\right)^{2}$; angle quantities in (deg) ${ }^{2}$.
(6) - (8) Distance and amplitude quantities in $A$; angle quantities in deg.

Table 22. Final results of structure analysis.

|  | $\mathrm{r}_{\mathrm{N}-\mathrm{O}}, \AA$ | $\mathrm{r}_{\mathrm{O}} \cdots \mathrm{O}, \AA$ | $<\mathrm{O}-\mathrm{N}-\mathrm{O}, \mathrm{deg}$ | $1_{\mathrm{N}-\mathrm{O},}, \AA$ | $\mathrm{l}_{\mathrm{O}} \cdots \mathrm{O}, \AA$ |
| :--- | :--- | :--- | :--- | :--- | :--- |
| This work | $1.202 \pm .0013$ | $2.213 \pm .0050$ | $134.02 \pm .65$ | $.0382 \pm .0025$ | $.0470 \pm .0050$ |
| Microwave (5) | 1.197 | $(2.207)^{(a)}$ | 134.25 | $\ldots$ | $\ldots$ |

(a)

Calculated from the relation $\mathrm{r}_{\mathrm{O}} \cdots \mathrm{O}=2 \mathrm{r}_{\mathrm{N}-\mathrm{O}} \sin (<\mathrm{O}-\mathrm{N}-\mathrm{O} / 2)$.

Table 23. Numerical evaluation of $G_{S}\left(\times 10^{-28} / 6.02472\right)$ for $N^{14} O_{2}$ and $\mathrm{N}^{15} \mathrm{O}_{2}$.

|  | $\mathrm{N}^{14} \mathrm{O}_{2}$ |  | $\mathrm{~N}^{15} \mathrm{O}_{2}$ |  |
| :--- | :---: | :---: | :---: | :---: |
|  | $\mathrm{I}^{(\mathrm{a})}$ | $\mathrm{II}^{(\mathrm{b})}$ | $\mathrm{III}^{(\mathrm{a})}$ | $\mathrm{IV}^{(\mathrm{b})}$ |
| $\mathrm{G}_{11}, \stackrel{\circ}{\mathrm{~A} / \mathrm{md} \mathrm{sec}^{2}}$ | .08407 | .08429 | .08264 | .08284 |
| $\mathrm{G}_{12}$ | -.07232 | -.07261 | -.06751 | -.06778 |
| $\mathrm{G}_{22}$ | .36741 | .36699 | .351298 | .35090 |
| $\mathrm{G}_{33}$ | .18371 | .18349 | .17565 | .17545 |

(a) $<\mathrm{O}-\mathrm{N}-\mathrm{O}=134.25 \mathrm{deg}(5)$ was used.
(b) $<\mathrm{O}-\mathrm{N}-\mathrm{O}=134.02 \mathrm{deg}$ (this work) was used.

Table 24. Vibrational frequencies (in $\mathrm{cm}^{-1}$ ) of $\mathrm{N}^{14} \mathrm{O}_{2}$ and $\mathrm{N}^{15} \mathrm{O}_{2}$ (1, p. 413-427).

|  | $\mathrm{N}^{14} \mathrm{O}_{2}$ | $\mathrm{~N}^{15} \mathrm{O}_{2}$ |
| :---: | :---: | :---: |
| $v_{1}$ | 1319.7 | 1306.5 |
| $v_{2}$ | 749.8 | 740.15 |
| $v_{3}$ | 1617.75 | 1580.32 |
| $\omega_{1}$ | 1357.8 | 1342.5 |
| $\omega_{2}$ | 756.8 | 747.1 |
| $\omega_{3}$ | 1665.5 | 1628.0 |

Table 25. Numerical evaluation of $\Lambda\left(\times 10^{-28}\right)$ and $\Delta\left(\times 10^{31}\right)$ for $\mathrm{N}^{14} \mathrm{O}_{2}$.

|  | $I^{(a)}$ | II $^{(\mathrm{b})}$ |
| :--- | :---: | :---: |
| $\lambda_{1}, \mathrm{sec}^{-2}$ | 6.17945 | 6.54141 |
| $\lambda_{2}$ | 1.99476 | 2.03218 |
| $\lambda_{3}$ | 9.28587 | 9.84213 |
| $\Delta_{1}, \mathrm{md} \mathrm{A} \mathrm{sec}^{2}$ | 2.149796 | 2.08568 |
| $\Delta_{2}$ | 4.197205 | 4.14563 |
| $\Delta_{3}$ | 1.73773 | 1.68668 |

${ }^{(a)} \nu_{i}$ 's (observed fundamental frequencies) were used.
(b) $\omega_{i}$ 's (harmonic frequencies) were used.

Table 26a. Error analysis of internal potential constants (in md/A) obtained from intersections of elliptical contours.

|  | $I^{(a)}$ | $I^{(b)}$ | $I I I^{(c)}$ | $I^{(d)}$ | $V^{(e)}$ |
| :--- | ---: | ---: | ---: | ---: | ---: |
| $\mathrm{f}_{\mathrm{r}}$ | 10.771 | 8.966 | 10.162 | 11.158 | 9.156 |
| $\mathrm{f}_{\mathrm{a}}$ | .969 | 2.167 | 1.274 | 1.094 | 2.447 |
| $\mathrm{f}_{\mathrm{rr}}$ | 2.368 | .563 | 1.758 | 2.251 | .249 |
| $\mathrm{f}_{\mathrm{ra}}$ | .520 | 1.176 | .566 | .533 | 1.303 |

(a)
$<\mathrm{O}-\mathrm{N}-\mathrm{O}=134.02 \mathrm{deg}, \mathrm{l}_{\mathrm{N}_{-} \mathrm{O}}=.03815 \AA, 1_{\mathrm{O}} \ldots \mathrm{O}=.04698 \AA$, $\mathrm{T}=380.16^{\circ} \mathrm{K}, v_{1}=1319.7, v_{2}=749.8$ and $v_{3}=1617.75 \mathrm{~cm}^{-1}$ were used in this calculation.
(b) Same as (a) save for amplitudes: $1_{N-O}+2 \sigma_{T}\left(l_{N-O}\right)=.04309 \AA$ and $\left.l_{\mathrm{O}} \ldots \mathrm{O}^{+\sigma} \mathrm{T}^{\left(l_{\mathrm{O}} \ldots \mathrm{O}\right.}\right)^{\prime 2}=.04949 \AA$.
${ }^{(c)}$ Same as (a) save for amplitudes: $1_{N-O_{0}}+2 \sigma_{L S}\left(1_{\mathrm{N}-\mathrm{O}}\right)=.03973 \AA$ and $1_{O} \ldots O^{+\sigma_{L S}}{ }^{\left(l_{O} \ldots O\right) / 2=.04825 \AA}$.
${ }^{(d)}$ Same as (a) save for frequencies: $\omega_{1}=1357.8, \omega_{2}=756.8$ and $\omega_{3}=1665.5 \mathrm{~cm}^{-1}$.
$(\mathrm{e})_{<\mathrm{O}-\mathrm{N}-\mathrm{O}}=134.02 \mathrm{deg}, \mathrm{l}_{\mathrm{N}_{-} \mathrm{O}}+2 \sigma_{\mathrm{T}}\left(\mathrm{l}_{\mathrm{N}-\mathrm{O}}\right)=.04309 \AA, \mathrm{l}_{\mathrm{O}} \ldots \mathrm{O}$ $+\sigma_{\mathrm{T}}\left(\mathrm{l}_{\mathrm{O}} \ldots \mathrm{O}\right) / 2=.04949 \AA, \mathrm{~T}=380.16^{\circ} \mathrm{K}, \omega_{\mathrm{l}}=1357.8$, $\omega_{2}=756.8$ and $\omega_{3}=1665.5 \mathrm{~cm}^{-1}$.

Table 26b. Errors in internal potential constants (in md/ $\AA$ ) derived from uncertainties in $1_{N-O}$ and $l_{O} \cdots O^{\circ}$

|  | $\mathrm{I}^{(\mathrm{a})}$ | $\mathrm{II}^{(\mathrm{b})}$ | $\mathrm{III}^{(\mathrm{c})}$ |
| :--- | :--- | :--- | :--- |
| $\sigma\left(\mathrm{f}_{\mathrm{r}}\right)$ | $\pm .903$ | $\pm .305$ | $\pm 1.001$ |
| $\sigma\left(\mathrm{f}_{\mathrm{a}}\right)$ | $\pm .599$ | $\pm .153$ | $\pm .677$ |
| $\sigma\left(\mathrm{f}_{\mathrm{rr}}\right)$ | $\pm .903$ | $\pm .305$ | $\pm 1.001$ |
| $\sigma\left(\mathrm{f}_{\mathrm{ra}}\right)$ | $\pm .328$ | $\pm .023$ | $\pm .385$ |

${ }^{(a)}$ Effect of $\sigma_{\mathrm{T}}\left(l_{\mathrm{ij}}\right)^{\prime}$ 's on internal potential constants derived from $v_{i}$ 's and $l_{i j}$ 's.
(b)

Effect of $\sigma{ }_{L S}\left(l_{i j}\right)$ 's on internal potential constants derived from $v_{i}{ }^{\prime} s$ and $l_{i j}{ }^{1}{ }^{\prime} s$.
(c)

Effect of $\sigma_{T}\left(1_{i j}\right)^{\prime}$ s on internal potential constants derived from $\omega_{i}{ }^{\prime} s$ and $1_{i j}{ }^{\prime} s$.

Table 27. Final results of internal potential constants (GVF) for nitrogen dioxide (in md/A).

|  | $I^{(a)}$ | $\mathrm{II}^{(\mathrm{b})}$ | III ${ }^{(c)}$ | IV ${ }^{(d)}$ |
| :---: | :---: | :---: | :---: | :---: |
| $\mathrm{f}_{\mathrm{r}}$ | $10.771 \pm .90_{3}$ | $10.406 \pm .025$ | $11.158+1.00{ }_{1}$ | 10.927 $\pm .065$ |
| $\mathrm{f}_{\mathrm{a}}$ | . $969 \pm .599$ | $1.0968 \pm .0009$ | $1.094 \pm .67_{7}$ | 1. $125 \pm .003$ |
| $\mathrm{f}_{\mathrm{r} \mathrm{r}}$ | $2.368{ }_{8}+90_{3}$ | $2.024 \pm .025$ | $2.25{ }_{1}+1.00{ }_{1}$ | $2.038 \pm .065$ |
| $\mathrm{f}_{\mathrm{ra}}$ | $.520 \pm .328$ | . $535 \pm .005$ | $.53{ }_{3} \pm .38{ }_{5}$ | . $390 \pm .020$ |

$(\mathrm{a})_{<\mathrm{O}}-\mathrm{N}-\mathrm{O}=134.02 \mathrm{deg}, \mathrm{l}_{\mathrm{N}-\mathrm{O}}=.03815 \mathrm{~A}, 1_{\mathrm{O}} \cdots \mathrm{O}=.04698 \AA$, $\mathrm{T}=380.16^{\circ} \mathrm{K}, v_{1}=1319.7, v_{2}=749.8$ and $v_{3}=1617.75 \mathrm{~cm}^{-1}$ were used in this calculation (present work).
(b) $<\mathrm{O}-\mathrm{N}-\mathrm{O}=134.25 \mathrm{deg}, v_{1}=1319.7, v_{2}=749.8, v_{3}=1617.75$, $v_{1}^{*}=1306.5, v_{2}^{*}=740.15$ and $v_{3}^{*}=1580.32 \mathrm{~cm}^{-1}$ were used in this calculation (1, p. 413-427).
${ }^{(c)}{ }_{\text {Same as }}(\mathrm{a})$ save for frequencies: $\omega_{1}=1357.8, \omega_{2}=756.8$ and $\omega_{3}=1665.5 \mathrm{~cm}^{-1}$ (present work).
(d)

Same as (b) save for frequencies: $\omega_{1}=1357.8, \omega_{2}=756.8$, $\omega_{3}=1665.5, \omega_{1}^{*}=1342.5, \omega_{2}^{*}=747.1$ and $\omega_{3}^{*}=1628.0 \mathrm{~cm}^{-1}$ (1, p. 413-427).
$*$ These frequencies correspond to $\mathrm{N}^{15} \mathrm{O}_{2}$.

Table 28. Comparison of the calculated and observed frequencies (in $\mathrm{cm}^{-1}$ ) of $\mathrm{N}^{14} \mathrm{O}_{2}$.

|  | Calculated $^{(\mathrm{a})}$ | Observed $^{(\mathrm{b})}$ | Difference (Percent) |
| :--- | :---: | :---: | :---: |
| $\nu_{1}$ | 1342.6 | 1319.7 | -1.7 |
| $\nu_{2}$ | 707.2 | 749.8 | +5.7 |
| $\nu_{3}$ | 1618.1 | 1617.75 | $-.0_{2}$ |
| $\omega_{1}$ | 1360.7 | 1357.8 | -.2 |
| $\omega_{2}$ | 750.8 | 756.8 | +.8 |
| $\omega_{3}$ | 1665.9 | 1665.5 | $-.0_{2}$ |

${ }^{(a)}$ Calculated from internal potential constants tabulated in columns I and III in Table 27 (this work).
(b) Arakawa and Nielsen (1, p. 413-427).

Table 29. Comparison of the calculated and observed root-meansquare amplitudes (in $\AA$ ) of $N^{14} \mathrm{O}_{2}$.

|  | Calculated ${ }^{(a)}$ | Observed ${ }^{(b)}$ |
| :---: | :---: | :---: |
| at $298{ }^{\circ} \mathrm{K}$ |  |  |
| $1_{\mathrm{N}-\mathrm{O}}$ | . 0382 | --- |
| ${ }^{1} \mathrm{O} \cdot . \mathrm{O}$ | . 0469 | --- |
| at $380^{\circ} \mathrm{K}$ |  |  |
| ${ }^{1} \mathrm{~N}-\mathrm{O}$ | --- | . $0382 \pm .0025$ |
| ${ }^{1} \mathrm{O} \cdot \mathrm{O}$ | --- | . $0470 \pm .0050$ |

(a)Cyvin (10, p. 117).
(b) This work.

Table 30a. Symmetrized compliance constants (in $\AA / \mathrm{md}$ ) obtained from least-squares refinements.

|  | $1^{(a)}$ | II $^{\text {(b) }}$ | $\mathrm{III}^{(\mathrm{c})}$ | IV ${ }^{(d)}$ | $v^{(e)}$ | $\mathrm{VI}^{(f)}$ | $\mathrm{VII}^{(\mathrm{g})}$ | VIII ${ }^{(\mathrm{h})}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $C_{11}$ | $.0835 \pm .0003$ | . $0836 \pm .0003$ | $.0792 \pm .0002$ | $.0793 \pm .0002$ | $.0822 \pm .0002$ | $.0779 \pm .0001$ | $.0829 \pm .0005$ | $.0787 \pm .0004$ |
| $\mathrm{C}_{12}$ | $-.0411 \pm .0025$ | $-.0423 \pm .0025$ | $-.0354 \pm .0015$ | $-.0365 \pm .0016$ | $-.0676 \pm .0112$ | $-.0542 \pm .0016$ | $-.0507 \pm .0069$ | $-.0427 \pm .0044$ |
| $C_{22}$ | . $9253 \pm .0053$ | $.9252 \pm .0053$ | $.9009 \pm .0033$ | $.9007 \pm .0033$ | $.9750 \pm .0197$ | $.9374 \pm .0030$ | $.9424 \pm .0134$ | $.9137 \pm .0089$ |
| $\mathrm{C}_{33}$ | $.1193 \pm .0001$ | $.1192 \pm .0001$ | $.1125 \pm .0001$ | $.1124 \pm .0001$ | $.1190 \pm .0005$ | $.1123 \pm .0001$ | $.1192 \pm .0004$ | $.1124 \pm .0002$ |

(a) Input data: $<\mathrm{O}-\mathrm{N}-\mathrm{O}=134.25 \mathrm{deg}, v_{1}=1319.7, v_{2}=749.8, \quad v_{3}=1617.75, v *_{1}=1306.5, v *_{2}=740.15$, and $v *_{3}=1580.32 \mathrm{~cm}^{-1}$.
(b) Input data: same as (a) save for $<\mathrm{O}-\mathrm{N}-\mathrm{O}=134.02$ deg.
(c) Input data: $<O-N-O=132.25 \mathrm{deg}, \omega_{1}=1357.8, \omega_{2}=756.8, \omega_{3}=1665.5, \omega *_{1}=1342.5, \omega *_{2}=747.1$, and $\omega *_{3}=1628.0 \mathrm{~cm}^{-1}$.
(d) Input data: same as (c) save for $\angle \mathrm{O}-\mathrm{N}-\mathrm{O}=134.02$ deg.
(e) Input data: $<\underset{\nu}{ } \mathrm{O}-\mathrm{N}-\mathrm{O}=134.02 \mathrm{deg}, \mathrm{T}=380.16^{\circ} \mathrm{K}, \mathrm{l}_{\mathrm{N}-\mathrm{O}}^{2}=(.03815)^{2} \AA^{2}, 1_{O}^{2} \ldots \mathrm{O}=(.04698)^{2} \AA^{2}, \nu_{1}=1319.7, \nu_{2}=749.8$ and $v_{3}=1617.75 \mathrm{~cm}^{-1}$.
(f) Input data: same as (e) save for frequencies; $\omega_{1}=1357.8, \omega_{2}=756.8$ and $\omega_{3}=1665.5 \mathrm{~cm}^{-1}$.
(g) Input data: same as (e) plus $v *_{1}=1306.5, \quad v *_{2}=740.15$ and $v *_{3}=1580.32 \mathrm{~cm}^{-1}$.
(h) Input data: same as (f) plus $\omega *_{1}=1342.5, \omega *_{2}=747.1$ and $\omega *_{3}=1528.0 \mathrm{~cm}^{-1}$.

Table 30b. Comparison of the observed and calculated frequencies (in $\mathrm{cm}^{-1}$ ) and mean-square amplitudes (in $\AA^{2}$ ) for nitrogen dioxide.

|  | Observed | Calculated |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $1^{\text {(a) }}$ | $\mathrm{HI}^{(\mathrm{b})}$ | $\mathrm{III}^{(\mathrm{c})}$ | IV ${ }^{\text {(d) }}$ | $\mathrm{V}^{(\mathrm{e})}$ | $\mathrm{VI}^{(f)}$ | $\mathrm{VII}^{(8)}$ | $\mathrm{VIII}^{(\mathrm{h})}$ |
| $\nu_{1}$ | 1319.7 | 1320.1 | 1320.1 | --- | --- | 1319.7 | --- | 1319.7 | --- |
| $v_{2}$ | 749.8 | 749.8 | 749.8 | --- | --- | 749.8 | --- | 750.1 | --- |
| $\nu_{3}$ | 1617.75 | 1616.92 | 1616.90 | --- | --- | 1617.87 | --- | 1616.97 | --- |
| $\nu^{*}{ }_{1}$ | 1306.5 | 1306.1 | 1306.1 | --- | --- | --- | --- | 1306.6 | --- |
| ${ }^{2} *_{2}$ | 740.15 | 740.13 | 740.13 | --- | --- | --- | --- | 739.90 | --- |
| $\nu^{*}{ }_{3}$ | 1580. 32 | 1581.06 | 1581.07 | --- | ---- | --- | --- | 1581.14 | --- |
| $\omega_{1}$ | 1357.8 | --- | --- | 1357.7 | 1357.4 | --- | 1357.8 | --- | 1357.1 |
| $\omega_{2}$ | 756.8 | --- | --- | 756.8 | 756.8 | --- | 756.8 | --- | ${ }^{756.9} 7$ |
| $\omega_{3}$ | 1665.5 | --- | --- | 1665.2 | 1665.2 | --- | 1665.5 | --- | 1665.2 |
| $\omega{ }_{1}$ | 1342.5 | --- | --- | 1342.8 | 1342.8 | --- | --- | --- | 1343.2 |
| $\omega{ }_{2}$ | 747.1 | --- | --- | 747.1 | 747.1 | --- | --- | --- | 746.9 |
| $\omega{ }^{*} 3$ | 1628.0 | --- | --- | 1628.3 | 1628.3 | --- | --- | --- | 1628.3 |
| $\begin{gathered} \text { at } 380^{\circ} \mathrm{K} \\ 1^{2} \mathrm{~N}-\mathrm{O} \end{gathered}$ | $.001455^{(\mathrm{i})}$ | --- | --- | --- | --- | . $.0015064_{4}$ | .0014627 | . 0015089 | .0014654 |
| $1^{2} 0 \cdots 0$ | $.002207^{(1)}$ | --- | --- | --- | --- | $.002206_{7}$ | $.002206_{8}$ | .$^{.002286} 9$ | .0022648 |

(a) $-(\mathrm{h})$ Same as Table 30a.
(i)
$\left(.0381_{5}\right)^{2}=.001455$
(i)

* These frequencies correspond to $\mathrm{N}^{15} \mathrm{O}_{2}$.

APPENDIX II

FIGURES


Figure 1. Calibration of densitometer traces of a typical photographic plate.


Figure 2. Experimental and theoretical radial distribution curves for nitrogen dioxide.


Figure 3. Experimental and theoretical modified molecular intensity curves for nitrogen dioxide.


Figure 4. Experimental modified molecular intensity curves from separate camera distances for nitrogen dioxide.


Figure 5. Relation between root-mean-square amplitudes and symmetrized potential constants for nitrogen dioxide.


[^0]:    ${ }^{1}$ Through 1945 (19, p. 284), 1948 (9, p. 207-210), 1956 (5, p. 1040-1043), 1958 (1, p. 413-427).

[^1]:    ${ }^{1}$ The effect of apparatus scattering (from aperatures, etc.) is not represented in this equation.

[^2]:    ${ }^{1}$ Analogous to considering a diatomic molecule.

[^3]:    ${ }^{1}$ The constant $(2 / \pi)^{1 / 2}$ has been arbitrarily included for normalization purposes.
     exactly eliminates the dependence of $A_{k l}$ on the parameter $s$.

[^4]:    ${ }^{1}$ In subsequent discussions, "unamplified" and 'amplified" trace will refer to the tracings obtained with the faster carriage speed and lower amplifier gain, and the slower carriage speed and higher amplifier gain, respectively. In both of these cases, the chart speeds were the same and greater than the corresponding carriage speeds.

[^5]:    ${ }^{1}$ This term has an important effect on the Fourier transform only when the atomic number differences of the atoms in the molecule are large.

[^6]:    ${ }^{1}{ }_{\text {Only }} \mathrm{I}_{\mathrm{E}}^{\mathrm{a}}(\mathrm{s}), \mathrm{I}_{\mathrm{E}}^{\mathrm{b}}(\mathrm{s})$ and $\mathrm{I}_{\mathrm{E}}^{\mathrm{c}}(\mathrm{s})$ are plotted in this figure.

[^7]:    ${ }^{1}$ Equation (I, 53) neglects the negative cross term, $2 a^{\prime} b^{\prime}<\sigma_{2}\left(x_{N \ldots \mathrm{O}}\right) \sigma_{2}\left(\mathrm{r}_{\mathrm{O}} \ldots \mathrm{O}\right)>[$ see equation $(\mathrm{I}, 50)]$.

[^8]:    ${ }^{1} d \lambda$ and $d h$ were obtained from an examination of the variation of wavelength and camera distance over a period of several months.

[^9]:    ${ }^{1}$ Recent work in this laboratory indicates that sensible errors from this source have very little effect on the final structure parameters.

[^10]:    ${ }^{1}$ The effect of weighing the observations which emphasized the intermediate and inner data (but not innermost) led to an increase in $1_{\mathrm{N}-\mathrm{O}} \mathrm{r}^{\mathrm{r}} \mathrm{O} \ldots \mathrm{O}$ and $\mathrm{l}_{\mathrm{O}} \mathrm{O} . \mathrm{O}$.

[^11]:    ${ }^{l}$ For dimensional reasons it is often convenient to replace the internal bending coordinate $\Delta a$ by $r_{X-Y}^{e} \Delta a$.

[^12]:    ${ }^{1}$ The values of $1_{N-O}^{2}$ and $1_{O}^{2} \ldots$ o used by Professor Decius correspond to preliminary values obtained during the course of this thesis work.

[^13]:    ${ }^{l}$ Separate calculations were made using first the $v_{i}$ 's and then the $\omega_{i}{ }^{\prime} s$.

[^14]:    ${ }^{1}$ Similar estimates were obtained for the set of potential constants derived from the $\omega_{i}$ 's instead of the $v_{i}{ }^{\prime} s$. The effect of $\sigma_{L S}\left(l_{i j}\right)$ in place of $\sigma_{T}\left(1_{\mathrm{ij}}\right)$ was also investigated.

[^15]:    1
    As determined from $\mathrm{r}_{\mathrm{N}}-\mathrm{O}$ and $\mathrm{r}_{\mathrm{O}} \cdots \mathrm{O}^{\circ}$

