AN ABSTRACT OF THE THESIS OF

JEROME STANLEY BLANK for the Ph. D. in Chemistry (Name) (Degree) (Major) Date thesis is presented _____August 12, 1964 Title __A STRUCTURE INVESTIGATION OF NITROGEN DIOXIDE: I. GEOMETRY AND AMPLITUDES OF VIBRATION II. QUADRATIC POTENTIAL CONSTANTS. Abstract approved ______(Major professor)

The molecular structure and root-mean-square amplitudes of vibration of gaseous nitrogen dioxide have been investigated by electron diffraction at a nozzle temperature of 380° K. The results are $r_{N-O} = 1.202\pm0.0013$ Å, $r_{O...O} = 2.213\pm0.0050$ Å, $<O-N-O = 134.02\pm0.65^{\circ}$, $l_{N-O} = 0.0382\pm0.0025$ Å and $l_{O...O} = 0.0470\pm0.0050$ Å. The interatomic distances given are r_a values from the third cycle of least-squares refinement of intensity curves and differ from the equilibrium values r_e by small amounts; the l_a values correspondingly differ from the l_e values. The estimated standard errors include standard deviations derived from least-squares, deviations of the individual photographic plates at a given camera distance, estimates of correlation among the data, uncertainty in the constants of the experiment, and uncertainty in the factors employed in the data reduction. These errors are clearly conservative estimates.

By combining the mean-square-amplitudes (described above) with the normal vibrational frequencies, a reasonable set of values have been obtained for the potential constants of the general quadratic function

$$2V = f_{r}[(\Delta r_{1})^{2} + (\Delta r_{2})^{2}] + 2f_{rr} (\Delta r_{1})(\Delta r_{2}) + f_{a}(r_{e}\Delta a)^{2} + 2f_{ra} (\Delta r_{1} + \Delta r_{2})(r_{e}\Delta a).$$

The values in millidynes/Å (with estimated standard errors) for the observed fundamental and harmonic frequencies, respectively, are $f_r = 10.77_1 \pm 0.90_3$ and $11.15_8 \pm 1.00_1$; $f_{rr} = 2.36_8 \pm 0.90_3$ and $2.25_1 \pm 1.00_1$; $f_a = 0.96_9 \pm 0.59_9$ and $1.09_4 \pm 0.67_7$; $f_{ra} = 0.52_0 \pm 0.32_8$ and $0.53_3 \pm 0.38_5$.

In addition to the potential constants described above, various combinations of frequencies and mean-square amplitudes were investigated using a least-squares procedure. These results are expressed in terms of symmetrized compliance constants based on valence force coordinates.

The agreement between the various sets of internal potential constants and compliance constants derived in this work with those of isotopic spectroscopy suggests very strongly that mean-square amplitudes from electron diffraction (at least for small molecules composed of similar atoms) are consistent with spectroscopy data (vibrational frequencies).

A STRUCTURE INVESTIGATION OF NITROGEN DIOXIDE I. GEOMETRY AND AMPLITUDES OF VIBRATION II. QUADRATIC POTENTIAL CONSTANTS

by

JEROME STANLEY BLANK

A THESIS

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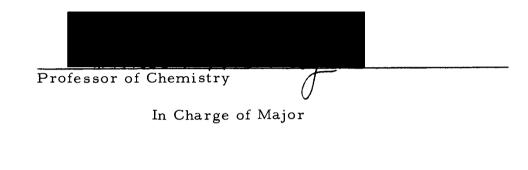
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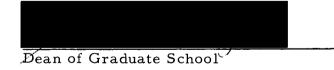
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A STRUCTURE INVESTIGATION OF NITROGEN DIOXIDE

INTRODUCTION

An understanding of the forces operating between atoms in a molecule is one of the principle objectives of vibrational spectroscopy. When applied to simple molecules this technique yields results (vibrational frequencies) which may be interpreted in terms of the values of potential constants defining a vibrational potential function; the values of the potential constants in principle permit one to make deductions concerning bond properties.

The main trouble encountered in the application of vibrational spectroscopy to the elucidation of vibrational potential functions lies not in the experiment itself, but in the physics of the problem. Even in the simpler harmonic cases the 3n-6 (or 3n-5) data (vibrational frequencies) for a single isotopic species generally number fewer than the parameters (potential constants) one would like to determine. The investigator must thus either content himself with an assumed abbreviated potential function, or he must study other isotopic species. The desirable latter alternative is not always possible for molecules due to experimental difficulties and interpretation problems.

Recent work (22, p. 594-598; 37, p. 643-652) indicates that another possible approach to this problem lies in combining the

vibrational amplitudes of electron diffraction with the frequencies of vibrational spectroscopy. The feasibility of this approach for simple molecules constitutes the purpose of this work; that is, this work is an attempt to ascertain the reliability and consistency of the observed vibrational amplitudes of electron diffraction, using the results (quadratic potential constants) of vibrational spectroscopy of isotopic species as the principal reliability criteria. The past thorough studies of nitrogen dioxide, together with the structural simplicity of the molecule from the electron diffraction point of view, make it especially useful as a test case. This structural simplicity involves the facts that (a) there are only two, wellresolved, interatomic distances in the molecule (N-O and O ··· O), and (b) the atomic number difference of the atoms is very small whick minimizes the complicating phase shift effect (13, p. 667-671). PART I

GEOMETRY AND AMPLITUDES OF VIBRATION

PREVIOUS STRUCTURAL INVESTIGATIONS OF NITROGEN DIOXIDE

Structural investigations of gaseous nitrogen dioxide by electron diffraction, ultraviolet, infrared and microwave spectroscopy have been carried out over a period in excess of thirty years (see bibliographies given in references cited $below^1$). Though some of the early investigations (15, p. 775-784; 31, p. 738-742) indicated a non-linear symmetric structure with a large bond angle, precise values of the equilibrium N-O distance, O-N-O angle, vibrational frequencies, and the quadratic potential constants have only recently been obtained (5 p. 1040-1043; 45, p. 1248-1251; l, p. 413-427). These recent investigations make nitrogen dioxide an especially favorable example for establishing the reliability of electron diffraction measurements in the determination of potential constants. In order to better acquaint the reader with the structural history of nitrogen dioxide, some of the results referred to above are summarized in Table 1.

¹Through 1945 (19, p. 284), 1948 (9, p. 207-210), 1956 (5, p. 1040-1043), 1958 (1, p. 413-427).

ELECTRON DIFFRACTION METHOD

List of Symbols (In order of appearance in Part I of text)

n	total number of atomic nuclei in the molecule.
λ	electron wavelength of the incident beam.
v	velocity of the incident beam electrons.
с	velocity of light in vacuum.
V	electron accelerating voltage.
θ	one-half the scattering angle.
S	electron diffraction variable. $s = 4\pi \lambda^{-1} \sin \theta$.
I(s)	number of electrons scattered per unit solid angle
	per unit time.
I _o	number of electrons crossing unit area per unit
	time in the incident beam.
m _e	electronic mass.
E	electronic charge.
h	planck's constant.
Z	atomic number.
F	atomic scattering factor for x-rays.
fi	atomic scattering factor for electrons.
	$f_{i} = (Z - F)_{i} / s^{2}$.

n_{ij}

the number of times the i, jth distance occurs in

the molecule.

r _{ij}	distance between ith and jth atoms in the mole-
	cule as measured by electron diffraction.
r_{ij}^i	instantaneous distance between ith and jth atoms
	in the molecule.
r^{e}_{ij}	equilibrium distance between ith and jth atoms in
	the molecule.
l_{ij}	root-mean-square vibrational amplitude cor-
	responding to the i, jth distance.
	$l_{ij} = \langle (r_{ij}^{i} - r_{ij}^{e})^{2} \rangle^{\frac{1}{2}}$.
S	incoherent scattering factor for x-rays tabulated
	by Bewilogua (4, p. 470-474) according to a
	theory of Heisenberg (18, p. 737-740).
η _i	phase coefficient for ith atom.
$\cos \eta_i - \eta_j $	phase shift for atomic pair i, j.
M(s)	function expressing the effect of molecular vibra-
	tions on the theoretically scattered electron
	intensity.
I _E (s)	modified molecular intensity function.
A _{ij}	variable coefficient of i, j distance normalized
	with respect to k, lth distance.
	$A_{ij} = (Z-F)_i(Z-F)_j Z_k Z_1 / (Z-F)_k (Z-F)_1.$

general distance parameter.

r

$$c' c' = n_{ij}A_{ij}/r_{ij}.$$

$$c'' c'' = \pi c'/2.$$

$$rD(r) generalized radial distribution function (Fourier sine transform of IE(s)).$$

$$rD'(r) experimental radial distribution function (includes the artificial temperature factor), where the improper integral in rD(r) has been replaced by a finite sum.
$$\Delta s increment in s.$$

$$rD'(r)_{Exp} same as rD'(r) save for the constant \Delta s interval which has been factored out.
$$rD'(r)_{Theor} theoretical radial distribution function corressponding to rD'(r)_{Exp}.$$

$$x_i general parameter.$$

$$f(x_1, x_2, \dots, x_m) general non-linear function.$$

$$n total number of observations.$$

$$m total number of parameters.$$

$$x_i^0 trial value of x_1.$$

$$f(x_1^0, x_2^0, \dots, x_m^0) trial value of f(x_1, x_2, \dots, x_m).$$

$$\Delta x_i correction to trial value $x_i^0.$

$$F_N matrix of function corresponding to adjusted values of parameters.$$

$$F_N = F.$$$$$$$$

 \mathbf{F}_{N}^{o} matrix of function corresponding to trial values

19	
	of parameters. $\mathbf{F}_{\mathbf{N}}^{\mathbf{O}} = \mathbf{F}^{\mathbf{O}}$.
[▲] Nm	matrix of derivatives. $A_{Nm} = A$.
₹ _m	matrix of corrections to trial values of para-
	meters. $\overline{\mathbf{X}}_{m} = \overline{\mathbf{X}}$.
₽ ^{Obs}	matrix of observed values of function. $\mathbb{F}_{N}^{Obs} = \mathbb{F}^{Obs}$.
V _N	matrix of residuals. $V_N = V = F_N - F_N^{Obs}$.
N	$\mathbb{N} = \mathbb{F}^{Obs} - \mathbb{F}^{O}.$
P	diagonal weight matrix.
ß	$\mathbb{B} = \mathbb{A} ! \mathbb{P} \mathbb{A}.$
¥	$\mathbf{Y} = \mathbf{A} \cdot \mathbf{P} \mathbf{N}.$
$\sigma(\mathbf{x}_i)$	standard error in x _i .
k'	amplitude scale factor with respect to the
	modified experimental intensity function.
b	arbitrary constant used in calculation of ${\mathbb P}.$
^{x}T	linear distance on the microdensitometer trace,
	measured from position of undiffracted beam.
x _p	linear distance on photographic plate, measured
	from position of undiffracted beam.
I _o (dens)	intensity of incident microdensitometer light
	beam.
I(dens)	intensity of transmitted microdensitometer light.
μ	light absorption coefficient.

- D photographic density.
- D' apparent photographic density determined from amplified trace.
- ΔD_1 amplification correction to D'.
- ΔD_2 scale correction to D'.
- h_k the kth camera distance (perpendicular distance from photographic plate to scattering point); k = a, b, and c denotes 478.00, 192.07 and 120.00 mm., respectively.
- δ blackness correction.
- γ proportionality constant related to the blackness correction.
- I (s) electron intensity incident on a flat photographic plate mounted perpendicular to the direction of the undiffracted electron beam.
 - t exposure time.
- E exposure.
- $I_{p}(s)$ $I_{p}(s)$ function from the ith plate at the kth camera distance.
- k I (s) composite I (s) function from the kth camera distance.

r_s radius on the sector measured from the undiffracted beam position. calibration (nearly constant except at small scattering angles).

 $a(r_s)$ angular opening of the sector.

- $g(\theta)$ sector function.
- I^k_t(s) total scattered intensity per unit solid angle corresponding to the kth camera distance.
- B^k_t(s) experimental background function corresponding to the kth camera distance.
- I^k_m(s) molecular intensity function corresponding to the kth camera distance.

composite molecular intensity function from the

three camera distances.

t(s) $t(s) = I_{p}^{a}(s) / [I_{p}^{a}(s) + I_{p}^{b}(s)]$ u(s) $u(s) = I^{b}(s) / [I_{p}^{a}(s) + I^{b}(s)]$

v(s) v(s) =
$$I_p^b(s) / [I_p^b(s) + I_p^c(s)]$$

$$w(s) = I_p^c(s) / [I_p^b(s) + I_p^c(s)]$$

$${}^{\mathrm{T}}_{\mathrm{E}^{(s)}\mathrm{Exp}}$$

w(s)

 $I_{m}^{T}(s)$

experimental modified molecular intensity function (composite) from the three camera

distances.

 $\begin{array}{c} {}^{T}_{E(s)}_{Theor} \\ {}^{k(i)}_{I}_{E(s)} \end{array}$

theoretical modified molecular intensity function. $I_{E}(s)$ function from the ith plate at the kth camera distance.

$I_{E}^{k}(s)$	composite $I_{E}^{}(s)$ function from the kth camera
	distance.
k''	amplitude scale factor with respect to experi-
	mental radial distribution functions
	$(rD'(r)_{Exp}).$
M	error matrix derived from least-squares refine-
	ment.
$\frac{1}{s}^2$	$\overline{\mathbf{s}}^2 = \mathbf{V} \cdot \mathbf{P} \mathbf{V} / (\mathbf{N} - \mathbf{m}).$
x	matrix of parameters actually adjusted by least-
	squares (includes interactomic distances
	and vibrational amplitudes).
U	matrix of parameters of interest (includes inter-
	atomic distances, bond angle and vibrational
	amplitudes).
D	matrix of coefficients transforming X to U.
	$\mathbf{U} = \mathbf{D} \mathbf{X}.$
a'	$a' = \partial (\langle O-N-O \rangle / \partial r_{N-O} = -r_{O} + O / r_{N-O}^2 \cos \theta$
	(<0-N-O/2).
b'	$b' = \partial (\langle O-N-O \rangle / \partial r_{O,O} = [r_{N-O} \cos \theta]$
	$((0-N-O/2)]^{-1}$.
σ_{i}^{LS}	same as $\sigma(\mathbf{x}_i)$

σ₂(x_j) standard error derived from variations in the most probable parameters as obtained from the individual photographic plates at a given camera distance.

a(i) x_i

xi^{b(i)}

x;

x_jb

 $\sigma_{2(x_i)}^{a(i)}$

 $\sigma_{2^{(x_i)}}^{b(i)}$

most probable parameters obtained from leastsquares analysis of the ith plate at 478.00 mm. most probable parameters obtained from leastsquares analysis of the ith plate at 192.07 mm. most probable parameters obtained from leastsquares analysis of the 478.00 mm composite. most probable parameters obtained from leastsquares analysis of the 192.07 mm composite. variation in the interatomic distances and vibrational amplitudes derived from the ith plate at the 478.00 mm camera distance.

variation in the interatomic distances and vibrational amplitudes derived from the ith plate at the 192.07 mm camera distance.

 $\sigma_2(<O-N-O)$ same as $\sigma_2(x_j)$ where the parameter is the bond angle.

 $\sigma_{T}(x_{i})$ overall standard error in the parameter x_{i} .

Scattering Theory

Since scattering theory applicable to gaseous electron diffraction has been presented by many authors (8, p. 231-239; 13, p. 667-671; 39, p. 19-199), there seems to be no need for more than a brief summary here.

In investigations of the structure of free molecules by gaseous electron diffraction, high velocity electrons¹ are used. The information obtained includes only the number (roughly) and magnitudes of interatomic distances, and their corresponding vibrational amplitudes.

Scattering theory for gaseous electron diffraction is developed by first considering the elastically scattered electrons, and then the aggregate effect of all the various kinds of inelastic scattering.

In the case of elastic scattering, a single atom is treated and then an array of atoms having fixed relative positions (a molecule). In this treatment, a single atom is represented by a small, spherically symmetrical region (a central force field) in which the potential energy of the scattered electrons is different from zero. The distribution of the scattered electrons is assumed to be observed at large

¹Operating voltages fall in the range of 30-50 kilovolts. For example, if λ is equal to 0.06458 A°, one finds by calculation that v/c and V are equal to 0.352 and 34.9 kilovolts, respectively.

distances from the atom, and an asymptotic solution is sought. An important approximation often utilized in this treatment is due to Born (39, p. 116-126), and amounts to an assumption that inside the atom the amplitude of the incident wave is much greater than that of the scattered wave. Further, it is assumed that no phase shift occurs in the scattering process. The solution for a molecule, obtained by summing the scattered waves due to the atoms, is averaged over all possible orientations in order to account for the random phase relations between the waves scattered by different molecules.

Unfortunately, in the case of inelastic scattering a reasonably rigorous theory is still lacking. Therefore, in lieu of treating the aggregate effect of the inelastic scattering by molecules, the atoms are treated separately and then summed over.

The result of these considerations for the intensity of scattering per unit solid angle is

$$I(s) = I_{0} (8\pi^{2}m_{e}\epsilon^{2}/h^{2})^{2} \left(\sum_{i, j} n_{ij}f_{i}f_{j}(sr_{ij})^{-1} \sin(sr_{ij}) \exp(-l_{ij}s^{2}/2) + \sum_{i} f_{i}^{2} + \sum_{i} S_{i}s^{-4}\right) = 1$$
(I, 1)

Equation (I, 1) is valid in the approximation of harmonic molecular vibrations. The first term on the right-hand side is the molecular structure sensitive part of the total scattered intensity. It can be

¹The effect of apparatus scattering (from aperatures, etc.) is not represented in this equation.

more generally written as

$$I_{0}(8\pi^{2}m_{e}\epsilon^{2}/h^{2})^{2}\sum_{i,j}^{n}n_{ij}f_{i}f_{j}\cos|\eta_{i}-\eta_{j}|M(s)(sr_{ij})^{-1}\sin(sr_{ij}), (I, 2)$$

where $\cos |\eta_i - \eta_j|$ denotes the phase shift (13, p. 667-671) which was assumed to be unity in the Born approximation, and M(s) is some function expressing the effect of a more general type of molecular vibration.

Principles of Structural Determination

Several methods are currently in use for elucidation of structural information from gaseous diffraction data. All of these begin, essentially, with the diffraction data in a form assumed to be described by an analytical function such as equation (I, 1) or (I, 2) or a convenient modification of them. The process by which the experimental data (the photographic blackening) is converted into the desired form is termed "data reduction" and will be described later in connection with the nitrogen dioxide work. The data in the chosen form may be called the "experimental intensity curve" or "function, " or the "radial distribution curve" or "function, " the latter being the Fourier sine transform of some experimental intensity curve. Each of these types of curves has advantages. Some investigators prefer to work almost entirely with radial distribution curves, fitting theoretical curves to the experimental one, often by least-squares techniques (7, p. 705-708); others use radial distribution curves in the early stages of an investigation, and refine the parameters by least-squares fitting based on intensity curves (17, p. 529-533; 24, p. 533-537). The latter approach was used in this thesis work. The radial distribution method was employed for the purpose of obtaining approximate values of the structural parameters, and these approximate values were then used as starting values in a least-squares refinement based on intensity curves.

The concluding portion of this section will be devoted to a brief discussion of the radial distribution method (44, p. 671-690) and of least-squares applied to electron diffraction intensity curves (17, p. 529-533; 24, p. 533-537).

Radial Distribution Method

It is convenient to use the following molecular intensity func-

$$I_{E}(s) = \sum_{i,j}^{n} n_{ij} r_{ij}^{-1} A_{ij}(s) \exp(-1\frac{2}{ij} s^{2}/2) \sin(sr_{ij}). \quad (I, 3)$$

Further, it is convenient for the initial discussion to treat the A_{ij} 's as constants.

In order to gain some insight as to the appearance of the distance spectrum for a molecule, it suffices to treat the contribution of a single¹ i, j pair to $I_E(s)$. Consider the integral

¹Analogous to considering a diatomic molecule.

$$\int_{0}^{\infty} [I_{E}(s)]_{ij} \sin (rs) ds = c' \int_{0}^{\infty} \exp (-l_{ij}^{2} s^{2}/s) \sin (r_{ij} s) x \sin (rs) ds . \qquad (I, 4)$$

Using the trigonometric identity

$$\sin x \sin y = 2^{-1} [\cos (x-y) - \cos (x+y)],$$
 (I, 5)

the right-hand side of equation (I, 4) can be written as

c'/2
$$\int_{0}^{\infty} \exp(-1_{ij} s^{2}/2) \cos[(r-r_{ij})s] ds$$

-c'/2 $\int_{0}^{\infty} \exp(-1_{ij} s^{2}/2) \cos[(r+r_{ij})s] ds$. (I, 6)

Evaluating (I, 6) by standard methods, it is found that

$$\int_{0}^{\infty} [I_{E}(s)]_{ij} \sin (rs) ds = [c''/l_{ij} (2\pi)^{l/2}] [exp(-(r-r_{ij})^{2}/2l_{ij}^{2}) - exp(-(r+r_{ij})^{2}/2l_{ij}^{2})]. \quad (I, 7)$$

It is clear that the second exponential term can be neglected with respect to the first one, so that

$$\int_{0}^{\infty} [I_{E}(s)]_{ij} \sin (rs) ds = [c''/l_{ij} (2\pi)^{l/2}] \\ x \exp [-(r-r_{ij})^{2}/2l_{ij}^{2}].$$
 (I, 8)

The right-hand side of equation (I, 8) is seen to be the normal Gaussian distribution. Each i, j pair in the molecule will make such a contribution and hence the curve representing the entire distance spectrum will be composed either of distinct Gaussian peaks (one for each i, j pair in the molecule), or when two or more r_{ij} 's are approximately equal in magnitude, of composites of Gaussian peaks.

Letting rD(r) represent the theoretical radial distribution function [in the literature, $\sigma(r)/r$ is often used to denote $4\pi rD(r)$], it is clear from the preceding that $I_{\rm E}(s)$ can be written as¹

$$I_{E}(s) = (2/\pi)^{1/2} \int_{0}^{\infty} r D(r) \sin(sr) dr$$
. (I, 9)

In the derivation of equation (I. 7), the A_{ij}'s were assumed to be independent of s. Since this is not usually the case, all but one of the peaks² in the theoretical radial distribution function will be slightly distorted from the ideal Gaussian form. Further distortion results from anharmonic instead of harmonic vibrations.

In practice, $I_E(s)$ as obtained experimentally is rarely available outside of the range $2 \le s \le 60$. The effect of not evaluating the integral in equation (I, 9) over the whole range in which the integrand is different from zero is the introduction of ripples (diffraction rings) in the experimental rD(r) curve, which, of course, contributes to skewing of the true peaks. For this reason, the factor $\exp(-as^2)$, often referred to as the artificial temperature factor, is usually introduced in the integrand to compensate for the finite upper limit, and the experimental radial distribution curve takes the form

 1 The constant (2/\pi) $^{1\!/_{2}}$ has been arbitrarily included for normalization purposes.

²The multiplication of $(Z-F)_i(Z-F)_j$ by $Z_kZ_1/(Z-F)_k(Z-F)_1$ exactly eliminates the dependence of A_{k1} on the parameter s.

$$s(max)$$

r D'(r) = $\sum_{s(min)}^{s(max)} I_E(s) \exp(-as^2) \sin(rs) \Delta s$, (I, 10)

where the integral has been replaced by a summation. The finite lower limit is often handled by the introduction of a theoretical intensity curve in the interval from zero to s(min). Further, since $I_E(s)$ is usually obtained experimentally at a constant Δs interval, Δs can be factored out of the summation and the equation actually used for evaluating rD'(r) is

$$r D'(r) = \sum_{s=0}^{s(max)} I_E(s) \exp(-as^2) \sin(rs)$$
. (I, 11)

The theoretical radial distribution curve corresponding to $r D'(r)_{Exp}$ can be calculated from the expression

$$r D'(r)_{Theor} = \sum_{i,j}^{r} n_{ij} Z_{i} Z_{j} (r_{ij})^{-1} (l_{ij}^{2} + 2a)^{-1/2} \times \exp \left[-(r - r_{ij})^{2} / 2(l_{ij}^{2} + 2a) \right]. \quad (I, 12)$$

Least-Squares Method

The problem of refinement by least-squares based on intensity curves is that of fitting a theoretical curve (which is a function of the molecular parameters) to an appropriate experimental curve. Since the adjustment is linear only for small ranges of parameter changes, it is necessary to have fairly good starting parameter values. As indicated earlier, such a starting model can be obtained from the r D'(r)_{Exp} curve.

The principles of least-squares curve-fitting in matrix form will be summarized in the following. Suppose $f(x_1, x_2, \dots, x_m)$ is a non-linear function representing a curve which consists of N experimental data. If approximate values for x_1, x_2, \dots, x_m are known, $f(x_1, x_2, \dots, x_m)$ may be expanded as

$$f(x_1, x_2, \cdots, x_m) = f(x_1^0, x_2^0, \cdots, x_m^0) + \sum_{i=1}^m \left(\frac{\partial f}{\partial x_i}\right)_0 \Delta x_i \quad (I, 13)$$

We have N such equations corresponding to the N observed points. If matrix notation is introduced,

$$\mathbb{F}_{N} = \mathbb{F}_{N}^{o} + \mathbb{A}_{Nm} \overline{\mathbb{X}}_{m}; \qquad (I, 13')$$

equation (I, 13') is usually referred to as the conditional equations. Since \mathbb{F}_N and \mathbb{F}_N^{Obs} differ by \mathbb{V}_N , equation (I, 13') gives (dropping subscripts)

$$\mathbb{F}^{Obs} + \mathbb{V} = \mathbb{F}^{\circ} + \mathbb{A} \,\overline{\mathbb{X}} \tag{I, 14}$$

$$\mathbf{V} = \mathbf{F}^{O} - \mathbf{F}^{Obs} + \mathbf{A} \, \overline{\mathbf{X}} \qquad (I, 15)$$

$$= -\mathbf{N} + \mathbf{A} \, \overline{\mathbf{X}}$$
 (I, 15')

The least-squares criterion may be expressed as

$$V' \mathbb{P} V \longrightarrow \text{minimum},$$
 (I, 16)

from which one finds

$$(\partial/\partial \mathbf{X}) (\mathbf{V}' \mathbf{P} \mathbf{V}) = \mathbf{A}' \mathbf{P} \mathbf{V} = 0 \qquad (\mathbf{I}, \mathbf{17})$$

Combination of equations (I, 15') and (I, 17) give the normal equations

21

$$\mathbb{B} \mathbb{X} = \mathbb{Y} \tag{I, 18}$$

where

$$\mathbb{B} = \mathbb{A} \cdot \mathbb{P} \mathbb{A} \tag{I, 19}$$

and

$$\mathbf{Y} = \mathbf{A} \cdot \mathbf{P} \mathbf{N} . \tag{I, 20}$$

The solutions are

$$\overline{\mathbf{X}} = \mathbf{B}^{-1} \mathbf{Y}, \qquad (\mathbf{I}, \mathbf{21})$$

and the standard errors are

$$\mathcal{O}(\mathbf{x}_{i}) = \left[\left(\mathbb{B}^{-1} \right)_{ii} \mathbb{V} \ \mathbb{P} \ \mathbb{V} / (\mathbb{N} - \mathbb{m}]^{\frac{1}{2}} \right]$$
(I, 22)

$$= \left[\left(\mathbb{B}^{-1} \right)_{ii} \left(\mathbb{N}' \mathbb{P} \mathbb{N} - \overline{X}' \mathbb{Y} \right) / \langle \mathbb{N} - \mathbb{m} \rangle \right]^{\frac{1}{2}}. \quad (I, 23)$$

In the case of electron diffraction, $f(x_1, x_2, \cdots, x_m)$ may be identified with an intensity function, say $I_E(s)$, the parameters of which are k' (scaling factor), some of the r_{ij} 's, and the l_{ij} 's. Therefore, the columns of the A matrix are $\partial I_E / \partial k'$, $\partial I_E / \partial r_{ij}$, \cdots , $\partial I_E / \partial r_{kl}$, $\partial I_E / \partial l_{ij}$, \cdots , $\partial I_E / \partial l_{kl}$, et cetera. The elements of the diagonal weight matrix, P, are often calculated using the analytical expression

$$(\mathbb{P})_{ii} = \text{const } s_i \exp(-bs_i^2),$$
 (I, 24)

which simply reflects general experience regarding the quality of the data.

DETERMINATION OF MOLECULAR STRUCTURE

Experimental

The electron diffraction photographs of gaseous nitrogen dioxide were taken with the Oslo sector apparatus (3, p. 232-238); the electron source being a hot cathode gun similar to that used in electron microscopes [see (14, p. 40-46; 20, p. 12-22) for discussions relating to the performance characteristics of such electron guns and the general problem of resolution in electron diffraction cameras, respectively].

The preparation of the nitrogen dioxide sample proceeded essentially as follows. Powdered $Pb(NO_3)_2$ was dried at temperatures ranging from 110° to 120° C. The powder was then transferred to a pyrex tube and slowly heated in the presence of a stream of O_2 . The reaction proceeds according to the equation

$$2Pb(NO_3)_2 \rightarrow 2PbO_{(s)} + 4NO_{2(g)} + O_{2(g)}$$
. (I, 25)

The water vapor liberated during the heating process was condensed with a cold trap (5° - 20° C). The nitrogen dioxide was passed over PbO_2 and Pb_2O_5 , and condensed in a dry ice bath. Finally, the nitrogen dioxide was purified by distillation.

Several photographic plates (Kodak B-40 lantern slide plates) were exposed at each of the three camera distances, 478.00, 192.07 and 120.00 mm, from which four plates per distance were subsequently selected for analysis (twelve plates in all); the exposure times ranged from about one-half minute to five minutes in duration.

The average nozzle temperature and electron wavelength for each of the runs were determined as 107° C and 0.06458 Å, respectively. The temperatures were read from a thermocouple placed in contact with the input gas nozzle a short distance from the tip. The wavelength associated with the electron beam was determined in separate experiments by diffraction from gold foil (8, p. 242).

The rotating sector, which must be used to even out the steeply falling background for photographic purposes, was spiral in shape (with a maximum radius of approximately 11 cm) such that its angular opening was proportional to the cube of the radius save for very small s values where the opening was larger in order to give a more uniform background. ¹ The mounting of the sector in the diffraction chamber was such that its rotational axis (perpendicular to the plane of the sector) coincided with the direction of the undiffracted electron beam; the distance between sector and photographic plate was approximately 16 mm. The sector described above acted effectively as an s³ screen (for the better part of the s range), which tended to offset the characteristic inverse square fall-off of intensity with distance from the

¹Such a sector is usually referred to as an "r³ sector."

scattering point, and therefore, to accentuate the oscillating features of the diffraction pattern. In other words, without a sector, the photographic plate would be over exposed at small s values and under exposed at large s values.

Data Reduction

Though it is usual to refer to the experimental diffraction curve as that which corresponds to a suitable molecular intensity function, it is only the information contained on the photographic plates which can be properly referred to as the experimental data. The microdensitometery of the plates and the various mathematical operations performed on the experimental data, eventually leading to the isolation of a suitable molecular intensity function, constitute the data reduction process.

Exposed photographic plates from gaseous electron diffraction show well-defined rings such that as the scattering angle increases, the blackening of the photographic emulsion appears to pass through successive maximum and minimum values. It has been pointed out (41, p. 868) that these maxima and minima are not real, but correspond to small fluctuations in the density superimposed on a monotonically falling background (see discussion of sector).

The photographic plates from the nitrogen dioxide experiments were traced with a Leeds and Northrup recording microdensitometer along a direction corresponding to a ring diameter, chosen to be as free as possible from photographic defects. During the tracing, the plates were oscillated about their centers in order to average out emulsion irregularities arising from graininess. This was accomplished by mounting a plate on an oscillating device which itself was mounted on the microdensitometer carriage. Since the diffraction pattern on the photographic plate was radially symmetric, the corresponding microdensitometer tracing consisted of two branches (left and right branch) separated by a narrow region corresponding to the position of the beam stop image which coincided with that of the undiffracted beam.

In practice, two traces corresponding to two different microdensitometer carriage speeds and amplifier gains¹ were actually made of a given plate. The slower carriage speed and higher amplifier gain had the advantage of spreading out and magnifying the individual undulations and hence facilitating the reading off of the photographic densities. The traces clearly showed the desired broad maxima and minima, which became progressively weaker as the scattering angle increased, and less easy to detect in the presence of the low level

¹In subsequent discussions, "unamplified" and "amplified" trace will refer to the tracings obtained with the faster carriage speed and lower amplifier gain, and the slower carriage speed and higher amplifier gain, respectively. In both of these cases, the chart speeds were the same and greater than the corresponding carriage speeds.

noise present in the traces. In addition to this noise, occasional spike-like absorption minima (equivalent to transmission maxima) occurred in the traces and were credited to dust on the surface of the photographic plate during the diffraction experiment and to emulsion defects.

The procedure employed in reading photographic densities from a trace involved the following steps.

First, a continuous smooth pencil line was drawn on each branch of a trace in an attempt to visually average out the effect of noise in the recorded signal. When the spikes described above were encountered, the line was drawn so as to correspond to the curvature of the trace on each side of the spike. A center line corresponding to zero scattering angle was then located on the amplified trace by averaging the center positions between corresponding maxima and minima on each of the two branches. The effective position of a given maximum or minimum was located by constructing tangents to the peak (one on the up side and one on the down side), and then locating the point of intersection of these two tangents. This tangent technique was also employed in locating the effective peak positions on the unamplified trace.

Second, an s scale, graduated in one-quarter s units, was

placed along the bottom of the amplified trace. ¹ Since the amplified trace was recorded at a chart speed greater than that of the corresponding carriage speed, it was necessary to relate distances on the amplified trace to those on the plate. This was done by simply tracing an accurately calibrated, etched glass scale under the same conditions used with the diffraction plates. The result (often called the "paper factor") was $x_T/x_P = 5.2350$. The value of the paper factor actually used in calculating the x_{T} 's was 5.2415, which was the value determined from the calibration trace in the Oslo laboratory before mailing to Oregon. The discrepancy between these two values was probably due to shrinkage of the chart paper caused by differences in humidity. This discrepancy was eventually taken account of by multiplying the final distance parameters of nitrogen dioxide by the factor 1.0012 = 5.2415/5.2350. A correction to the mean amplitudes is also required in principle, however it is so small in value that it was neglected.²

²For example the correction is about 2×10^{-6} Å for 1(N-O):

$$I \propto I_{o} \exp(-1^{2}s^{2}/2),$$

$$0 = -s^{2}dI - s1^{2}ds,$$

$$dI = -1^{2} (ds/s) = -(0.038)^{2}(1.2 \times 10^{-3}).$$

¹Since there were two branches per trace, each trace required two s scales using the previously determined center line as a common zero point relative to s. Obviously, the s scales differed in spacing and range for the different camera distances.

The third and final step of this procedure involved the actual reading of the photographic densities from the microdensitometer traces. Since the absorption of light by the photographic emulsion follows the exponential law

$$I(dens)/I_{o}(dens) = exp(-\mu D),$$
 (I, 26)

it was convenient to use a logarithmically scaled "T" square to read the photographic densities from the traces. The scale of the "T" square was in density units,

$$D = \log \left[I_0(dens) / I(dens) \right], \qquad (I, 27)$$

with the zero and infinity points at positions corresponding to the edges of the chart paper. It was necessary, of course, to scale the readings obtained from the amplified trace to the actual densities (D) as defined in equation (I, 26). Further, since the functional relationship of exposure (scattered electron intensity x time)¹ and density is known, a determination of the desired scattered electron intensity is possible. The scaling procedure was as follows. The only essential difference between the unamplified and amplified traces was that of amplifier gain. Clearly one correction to the apparent density (as read from the amplified trace) must consist of determining the increased amplification of the amplified trace in "T" square density units. This was accomplished by measuring the average difference

¹E = It is termed the reciprocity law.

in readings between corresponding maxima and minima on the unamplified and amplified traces, and then adding this term to the apparent density reading of the amplified trace. A second minor correction term was also necessary because of slight differences between the scale of the "T" square and the 0 to 100 percent transmission scale of the unamplified traces. This term was either subtracted or added to the apparent density described above, depending on whether the 100 percent transmission line of the "T" square fell above or below that of the unamplified trace.

An algebraic formulation of this procedure is as follows (see Figure 1 for the meaning of the various symbols). Let

 $D = \log \left[I_{o}^{\prime}(dens)/I^{\prime}(dens) \right] = \log \left[I_{o}^{\prime\prime}(dens)/I^{\prime\prime}(dens) \right]$ (I, 28)

and

$$D' = \log \left[I_{O}(dens)/I'(dens) \right], \qquad (I, 29)$$

then

$$\Delta D = D - D' = \log \left[I'_{O}(dens) / I'(dens) \right] - \log \left[I_{O}(dens) / I'(dens) \right] (I, 30)$$

or

$$\Delta D = \log \left[I_0'(dens)/I''(dens) \right] - \log \left[I_0(dens)/I'(dens) \right] . \quad (I, 30')$$

Rearrangement of equation (I, 30') yields

$$\Delta D = \log \left[I'(dens)/I''(dens) \right] - \log \left[I_0(dens)/I''_0(dens) \right], \quad (I, 31)$$

where

Letting $\Delta D_1 = \log [I'(dens)/I''(dens)]$ and $\Delta D_2 = \log [I_0(dens/I'_0(dens)])$, then

$$\Delta D = \Delta D_1 - \Delta D_2 \tag{I, 33}$$

or

$$D = D' + \Delta D_1 - \Delta D_2 , \qquad (I, 34)$$

 ΔD_1 and ΔD_2 may be identified with the first and second corrections, respectively, as discussed in the previous paragraph.

The recorded diffraction patterns covered the following scattering ranges:

$$h_a; 2.50 \le s \le 20.75$$

 $h_b; 10.25 \le s \le 42.00$
 $h_a; 18.50 \le s \le 49.75$.

Following the reading of the densities from the plates, as described above, the densities were corrected for non-linearity of photographic response according to the relation¹

$$I_{p} = \gamma(D + \delta)$$
 . (I, 35)

The values of δ actually used in this work (see Table 10) were obtained from the Oslo laboratory.² δ was taken as zero for D < 0.62,

^l The proportionality constant γ (in units of reciprocal time) was arbitrarily taken as unity.

²The Oslo calibration of photographic densities with electron intensities was based on a series of investigations extending over a period of some fourteen years, employing the procedure developed by Karle and Karle (27, p. 961).

for densities less than this value, the density-exposure curve was found to be linear. All twelve of the photographic plates used were sufficiently light in exposure that only data occurring in the following scattering ranges were actually blackness corrected: ¹

$$h_b; 10.25 \le s \le 18.00$$

 $h_c; 18.50 \le s \le 35.00$

The relevancy of this fact will be seen later in the discussion of uncertainties in the final mean square vibrational amplitudes.

As a check on the Oslo blackness correction, a blackness correction was constructed in this laboratory using two plates made at the 478 mm distance. As in the Oslo correction, the method of Karle and Karle (27, p. 961) was employed in this analysis. The applicability of this method rests on the validity of the reciprocity law

$$E = It$$
, (I, 36)

for fast electrons. From equation (I. 36), it is seen that it is possible to interpret the difference in two exposures as due to differences in electron intensity at constant time. This interpretation, combined with the assumption that D is proportional to I for $D \leq 0.25$ (for contrast lantern slide plates), constitute the basis of the method.

A comparison of the two corrections (Oregon and Oslo)

¹ The 478 mm plates did not require blackness correcting.

indicated that δ (Oregon) was somewhat greater than δ (Oslo) [for example, δ (Oregon) - δ (Oslo) \simeq 0.010 density units at D = 0.480]. This difference may or may not be significant; but because the two plates used in deriving the Oregon correction did not differ quite enough in density for optimal results, and because the blackness correction in any event was not great, it was decided to use the Oslo correction.

The $I_p(s)$ (or D) data (see Tables 2, 3, and 4) were plotted on large-scale graph paper in order to locate possible reading errors. A composite function for each of the camera distances was then obtained by summing the I_p data from each of the four plates at corresponding points of s:

$$I_{p}^{k}(s) = \sum_{i=1}^{4} I_{p}^{k(i)}(s)$$
 (I, 37)

This composite intensity function is related to the total scattered intensity per unit solid angle $[I_t^k(s)]$ by the equation $I_p^k(s) = I_t^k(s) g(\theta)$, (I, 38)

where $g(\theta)$ incorporates the effect of the sector and that of using a flat plate perpendicular to the undiffracted beam instead of a cylindrical film with an axis perpendicular to the undiffracted beam and a surface everywhere equidistant from the scattering point. Recalling the screening effect of the rotating sector, it is clear that one part of $g(\theta)$ will take the form $a(r_s) = \rho r_s^3$. The second factor of $g(\theta)$ is $\cos^3 2\theta$. Two powers of this factor are derived from the inverse fall-off of intensity with distance from the scattering point, and one power from the angle of inclination of the element of area on the flat plate with respect to the scattered electron rays striking it. Equation (I, 38) thus becomes

$$I_t^k(s) = I_p^k(s)/a (r_s) \cos^3 2\theta$$
. (I.39)

For the purpose of extracting the molecular sensitive part of the scattered intensity, it is convenient to multiply both sides of equation (I, 39) by s^4 , giving

$$s^{4}I_{t}^{k}(s) = s^{4}I_{p}^{k}(s)/a(r_{s})\cos^{3}2\theta.$$
 (I, 40)

For each camera distance, $s^4 I_t^k(s)$ curves were obtained by performing the multiplications indicated in equation (I, 40) and plotted on large-scale graph paper. Values of the calibration function $a(r_s)$ were obtained from the Oslo Laboratory.¹ It would now seem that the desired molecular intensity function $I_m^k(s)$ could be obtained by subtracting the last two terms in equation (I, 1) from $s^4 I_t^k(s)$; these two terms constitute the theoretical background and can be calculated. As has been pointed out, however, the theory of incoherent scattering is on poor ground and, even more important, there inevitably exists on any exposed plate a superposed experimental background derived

¹See Tables 11, 12, and 13 for $s^4/a(r_s) \cos^3 2\theta$ values actually used. These values correspond to a value of λ equal to 0.06449 Å; values calculated with $\lambda_{exp} = 0.06458$ would differ inconsequentially from these.

from apparatus scattering. In practice, therefore, since little is known about the apparatus background other than it is monatonically declining with increasing angle, one simply draws a background curve through the undulations of the experimental intensity and subtracts it. The result is the desired function,

$$I_{m}^{k}(s) = s^{4} I_{t}^{k}(s) - B_{t}^{k}(s).$$
 (I, 41)

The initial background often contains errors which manifest themselves by negative values of rD(r) calculated from $I_m(s)$, or small peaks in rD(r) at r < 1.00 Å. These errors are usually corrected by changing the background. Throughout this work, experimental background functions were used instead of theoretical functions.

Following subtraction of the background, the three $I_m^k(s)$ functions were placed on a common amplitude scale by comparing corresponding maxima and minima in the following overlap regions:

$$I_m^a(s) \text{ and } I_m^b(s); \quad 10.25 \le s \le 20.75$$

 $I_m^b(s) \text{ and } I_m^c(s); \quad 28.75 \le s \le 42.00$

A single composite function, $I_m^T(s)$, was then obtained by combining¹ $I_m^a(s)$, $I_m^b(s)$ and $I_m^c(s)$ now normalized as follows:

¹The data available from the $I_m^c(s)$ curve in the range 18.50 $\leq s \leq 28.75$, was not used in forming the composite curve $I_m^T(s)$.

2.50
$$\leq$$
 s \leq 10.00; $I_{m}^{T}(s) = I_{m}^{a}(s)$
10.25 \leq s \leq 20.75; $I_{m}^{T}(s) = t(s) I_{m}^{a}(s) + u(s) I_{m}^{b}(s)$
21.00 \leq s \leq 28.50; $I_{m}^{T}(s) = I_{m}^{b}(s)$
28.75 \leq s \leq 42.00; $I_{m}^{T}(s) = v(s) I_{m}^{b}(s) + w(s) I_{m}^{c}(s)$
42.25 \leq s \leq 49.75; $I_{m}^{T}(s) = I_{m}^{c}(s)$.

The weighting factors t(s), u(s), v(s) and w(s) were obtained from the $I_p^k(s)$ data. The overall range of the composite $I_m^T(s)$ was 2.50 $\leq s \leq 49.75$.

The composite curve $I_m^T(s)$ resulting from the procedures just described is in theory represented by the expression

$$sI_{m}^{T}(s) = k' \sum_{i,j}^{i} n_{ij}(Z-F)_{i}(Z-f)_{j} r_{ij}^{-1}$$

$$\cos | \Delta \eta_{ij} | \exp(-l_{ij}s^{2}/2) \sin(r_{ij}s), (I, 42)$$

which is, in fact, equation (I, 2) multiplied by s^5 . In order to replace the variable coefficients of $I_m^T(s)$ in equation (I, 42) by essentially constant coefficients, as is necessary for obtaining an easily interpreted radial distribution curve, the modified molecular intensity function $I_E^T(s)_{Exp}$ was calculated according to the equation

$$I_{E}^{T}(s)_{Exp} = sI_{m}^{T}(s) Z_{N}Z_{O}/(Z-F)_{N}(Z-F)_{O}$$
 (I, 43)

The values of $F_N(s)$ and $F_O(s)$ were obtained by combining those published by Hoerni and Ibers (21, p. 745) with those of Viervoll and Ögrim (43, p. 279). In the former case the $F_i(s)$'s were computed from Hartree-Fock radial wave functions, and in the latter an interpolation method was used to extend the calculations of James and Brindley (25, p. 81-111) to s equal to 30. Since the nitrogen dioxide data extended well-beyond s = 30, it was necessary to extrapolate the F_i curves to obtain values in this region. The values of $(Z-F/Z)_O$ and $(Z-F/Z)_N$ used are given in Table 14. Values of $I_E^T(s)_{Exp}$ are given in Table 5 and the curve is ploted in Figure 2.

Reference to equations (I, 42) and (I, 43) reveals that $I_E^T(s)_{Exp}$ for nitrogen dioxide corresponds to the theoretical scattering equation (if the relatively important cos $|\Delta\eta_i|$ term is ignored¹)

$$I_{E}^{T}(s)_{Theor} = k' [2Z_{N}Z_{O}r_{N-O}^{-1} \exp(-1_{N-O}s^{2}/2) \sin(sr_{N-O})$$
(I, 44)
+ $Z_{N}Z_{O}(Z-F)_{O}((Z-F)_{N}r_{O}...O)^{-1}\exp(-1_{O}...Os^{2}/2) \sin(sr_{O}...O)].$

The coefficient $Z_N Z_O (Z-F)_O / (Z-F)_N$ is essentially constant; Table 15 shows that it is approximately equal to Z_O^2 for $s \ge 7.00$. An $I_E^T(s)_{Theor}$ curve was calculated according to equation (I, 44) using the final refined parameter values (Table 22) and is shown in Figure 2 and tabulated in Table 5. The agreement between the experimental and theoretical curves is good.

In addition to the final composite intensity function $I_E^T(s)_{Exp}$, several other $I_E(s)_{Exp}$ curves were calculated which included (1) only data from plates taken at a single camera distance and (2) data

¹This term has an important effect on the Fourier transform only when the atomic number differences of the atoms in the molecule are large.

taken from single plates at a single camera distance. The purpose of these curves was to help with an understanding of the errors associated with the parameter values determined. The various curves and ranges of data they include are:

$$\begin{split} I_{E}^{a}(s); & 2.50 \leq s \leq 20.75 \\ I_{E}^{b}(s); & 10.25 \leq s \leq 42.00 \\ I_{E}^{c}(s); & 28.75 \leq s \leq 49.75 \text{ and } 18.50 \leq s \leq 49.75 \\ I_{E}^{a(1)}(s), & I_{E}^{a(2)}(s), & I_{E}^{a(3)}(s), & I_{E}^{a(4)}(s); & 2.50 \leq s \leq 20.75 \\ I_{E}^{b(1)}(s), & I_{E}^{b(2)}(s), & I_{E}^{b(3)}(s), & I_{E}^{b(4)}(s); & 10.25 \leq s \leq 42.00 . \end{split}$$

The curves described above are given in Tables 6, 7, and 8 and plotted¹ in Figure 3.

Radial Distribution Function and Preliminary Structure

The final radial distribution function $rD'(r)_{Exp}$ [see equation (I, 11)], from the modified experimental molecular intensity curve $I_{E}^{T}(s)_{Exp}$ ($\Delta s = 0.25$) was calculated according to the equation s=49.75

$$rD'(r)_{Exp} = \sum_{s=0} I_{E}^{T}(s)_{Exp} \exp(-0.001s^{2}) \sin(rs);$$
 (I,45)

the intensity data in the range $0 \le s \le 2.25$ was calculated from a theoretical curve according to equation (I, 44). The experimental radial distribution curve (values are given in Table 9 and the curve

 1 Only $I_{E}^{a}(s)$, $I_{E}^{b}(s)$ and $I_{E}^{c}(s)$ are plotted in this figure.

is shown in Figure 4) shows two strong peaks attributed to the N-O and $O \cdots O$ distances at about 1.2 and 2.2 Å, respectively. Careful analysis of these peaks gave the following preliminary values for the distance and amplitude parameters:

$$r(N-O) = 1.20_1 \text{ Å}, 1(N-O) = 0.038_5 \text{ Å}$$

 $r(O \cdots O) = 2.21_0 \text{ Å}, 1(O \cdots O) = 0.043_8 \text{ Å}$

For comparison, a theoretical radial distribution curve calculated using the final refined parameter values (Table 22) is shown in Figure 4 and tabulated in Table 9. The calculation was carried out according to the equation

$$rD'(r)_{Theor} = k'' \sum_{i,j}' n_{ij} Z_i Z_j r_{ij}^{-1} (1_{ij}^2 + .002)^{-\frac{1}{2}}$$
$$x \exp \left[-(r - r_{ij})^2 / (21_{ij}^2 + .004) \right], \qquad (I, 46)$$

where the scale factor k'' was determined from the peak heights in $rD'(r)_{Exp}$. The agreement between the experimental and theoretical curves is good.

Least-Squares Refinements

A large number of refinements, employing the Alwac III-E digital computer, were carried out according to the procedures

already described. The results of several 1 of these refinements are summarized in Tables 16 through 19. In each refinement the starting model was obtained from the $rD'(r)_{Exp}$ curve. The information to be deduced from these tables will be discussed in the following paragraphs.

Non-Systematic Errors

The error matrix, \mathbb{M} , derived from least-squares refinement is given by

$$\mathbb{M} = \overline{s}^2 \mathbb{D} \mathbb{B}^{-1} \mathbb{D}', \qquad (I, 47)$$

where the transformation matrix $\mathbb D$ is obtained from

$$\mathbf{U} = \mathbf{D} \times . \tag{I, 48}$$

In the nitrogen dioxide case, the only additional parameter of interest is the bond angle: equation (I, 48) thus becomes

$$\begin{array}{c} r(N-O) \\ r(O \cdot \cdot \cdot O) \\ <(O - N - O) \\ 1(N - O) \\ 1(O \cdot \cdot \cdot O) \end{array} = \mathbb{D} \begin{bmatrix} r(N-O) \\ r(O \cdot \cdot \cdot O) \\ 1(N - O) \\ 1(O \cdot \cdot \cdot O) \end{bmatrix} , \qquad (I, 48')$$

and \mathbb{D} is easily seen to be given by

¹Additional refinements were carried out investigating the effect on the parameter values of such things as the various background corrections, selection of suitable s ranges for separate composites, determination of the overlap ranges, et cetera.

$$\mathbb{D} = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ a' & b' & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} .$$
(I, 49)

Combining the parameter values given in the first column of Table 19 with the corresponding $\overline{s} \ ^2 \mathbb{B}^{-1}$ matrix, \mathbb{M} was evaluated ¹ and is shown in Table 20. The off-diagonal elements, $(\mathbb{M})_{ij}$, of this matrix are the average products of the errors \mathcal{O}_{i}^{LS} and \mathcal{O}_{j}^{LS} (often denoted² by $\rho_{ij}\mathcal{O}_{i}^{LS}\mathcal{O}_{j}^{LS}$); the square roots of the diagonal elements, $(\mathbb{M})_{ii}$, are the standard error (\mathcal{O}_{i}^{LS}) associated with each parameter.

Though the error matrix, M, provides a means of estimating the random errors arising from the discrepancy of the composite observations from the theoretical modified molecular intensity curve [equation (I, 44)], Morino³ has pointed out that another source of nonsystematic error arises from variations in the most probable parameters as obtained from the individual photographic plates for a given camera distance (see Table 17). For the parameters r(N-O),

¹From equations (I, 47) and (I, 49), the error, $(M)_{<O-N-O}$, is defined by

$$\overline{s}^{2}[(a')^{2}(\mathbb{B}^{-1})_{r_{N}-O, r_{N}-O} + 2a'b'(\mathbb{B}^{-1})_{r_{N}-O, r_{O}-..O} + (b')^{2}(\mathbb{B}^{-1})_{r_{O}-..O, r_{O}-..O}] . (I, 50)$$

 $\ensuremath{\bar{\rho}_{ij}}$ is usually referred to as the correlation coefficient.

³Morino, Yonezo. Private communication. Tokyo, Japan. University of Tokyo, 1964. $r(\odot\cdots O),\ l\,(N-O)$ and $l\,(\odot\cdots O),\ \sigma_2(x_j)^2$ was estimated as follows. Let

$$\mathcal{O}_{2}^{a(i)}(x_{j}) = x_{j}^{a} - x_{j}^{a(i)}$$
(I, 51)

and

$$\sigma_{2}^{b(i)}(x_{j}) = x_{j}^{b} - x_{j}^{b(i)}$$
 (I, 51')

The final values of $\sigma_2(x_j)$ were then calculated as

$$\sigma_{2}(\mathbf{x}_{j})^{2} = (1/8-1)(0.365 \sum_{i=1}^{4} [\sigma_{2}^{a(i)}(\mathbf{x}_{j})]^{2} + 0.635 \sum_{i=1}^{4} [\sigma_{2}^{b(i)}(\mathbf{x}_{j})]^{2}, \qquad (I, 52)$$

where the weights 0.365 and 0.635 were obtained by consideration of the total s ranges contributed by each of the two camera distances (478 and 192 mm) relative to $I_E^T(s)_{Exp}$. The additional information that might have been obtained by a similar analysis of the 120 mm plates did not seem justified. The corresponding standard deviation for the bond angle was estimated¹ as

$$\sigma_2((0-N-O)^2 = (a')^2 \sigma_2(r_{N-O})^2 + (b')^2 \sigma_2(r_{O-O})^2$$
. (I, 53)

Systematic Errors

Uncertainties arising from the measurement of camera

^lEquation (I, 53) neglects the negative cross term, 2a'b' $< \sigma_2(r_{N-O}) \sigma_2(r_{O,...O}) > [$ see equation (I, 50)].

distance, electron wavelength and the position coordinate (uncertainty Δx_T in the designation of the correct obscissa for a predetermined s scale) principally effect the size of the molecule and are negligible in their effect on the vibrational amplitudes. In terms of interatomic distances, the error associated with the first two of these parameters (h and λ) can be estimated as follows. Recalling that $s = 4\pi\lambda^{-1} \sin\theta$ where $\sin\theta = x_p/(h^2 + x_p^2)^{\frac{1}{2}}$,

$$-ds/s = [d\lambda/\lambda + hdh/(h^2 + x_p^2)] . \qquad (I, 54)$$

Since, for a given ring spacing

$$s \propto r_{ij}^{-1}$$
, (I, 55)

then

$$ds/s = -dr_{ij}/r_{ij}$$
, (I, 56)

and combining equations (I, 54) and (I, 56), we obtain

$$dr_{ij}/r_{ij} = [d\lambda /\lambda + hdh/(h^2 + x_p^2)].$$
 (I, 57)

Setting x_p equal to zero and noting that λ and h are independent parameters, the desired estimate is given by

$$dr'_{ij} = [(d\lambda /\lambda)^{2} + (dh/h)^{2}]^{\frac{1}{2}}r_{ij} . \qquad (I, 58)$$

Using the values $\lambda \pm d\lambda = 0.06458 \pm .00002$ Å and h \pm dh = 263.3 ± 0.1 mm (obtained by simple averaging of 478, 192, and 120 mm camera distances), equation (I, 58) gives a value of 0.0005 r_{ij} for

 $^{^{}l}d\lambda$ and dh were obtained from an examination of the variation of wavelength and camera distance over a period of several months.

 dr'_{ij} which agrees with the corresponding estimate given by Hedberg and Iwasaki (16, p. 592-593). In comparison, the error in the position coordinate can be neglected.

Uncertainties in the blackness correction and the atomic form factors affect largely the vibrational amplitudes. This error has been estimated as 0.021_{ij} (16, p. 593). Since this investigation sought to establish the reliability of these amplitudes, the significance of the earlier remarks pertaining to the fact that only a very small fraction of the densities used required a correction for blackness, should now be clear.

If the data on which the determinations are based are not all independent, the error estimates σ_{LS} are too small for all parameters. Very little is known about correlation among the data, but a rough, plausible guess might be that about one-half the observations are independent; this estimate would lead to standard errors σ_{LS} greater by about $2^{\frac{1}{2}}$ than those calculated.

No attempt was made to estimate the systematic errors arising from uncertainties in the sector correction¹ and in the experimental background, finite size of scattering region, deflection of the electrons resulting from interaction with the magnetic field of the earth which would give asymmetric rings, and the effect of

¹Recent work in this laboratory indicates that sensible errors from this source have very little effect on the final structure parameters.

anharmonicity.

Overall Standard Errors

The overall standard errors for the final structural parameters were estimated as follows:¹

1.
$$\sigma_{T}(r_{ij}) = [2 \sigma_{LS}(r_{ij})^{2} + \sigma_{2}(r_{ij})^{2} + (0.0005 r_{ij})^{2}]^{\frac{1}{2}}$$

2. $\sigma_{T}(
3. $\sigma_{T}(r_{ij}) = [2 \sigma_{LS}(r_{ij})^{2} + \sigma_{2}(r_{ij})^{2} + (0.02 r_{ij})^{2}]^{\frac{1}{2}}$.$

The complete error analysis is summarized in Table 21, it should be noted that if the random errors σ_{LS} and σ_2 were not assumed to be independent (that is, if the observations on several photographic plates did not belong to a single statistical population), it would seem appropriate to only include the larger of the two in evaluating σ_T . Further, it might very well be that σ_2 reflects the presence of hidden systematic errors in the individual observations. The results in Table 21 thus represent conservative estimates.

¹The factor two associated with the term 20^{2}_{LS} arises from considerations of data correlation discussed earlier. The value 1.0012 r_{ij} was used in evaluating the term (0.0005 r_{ij})².

Final Results

The final values¹ of the structural parameters (including estimated standard errors) are given in Table 22. These values were derived from those given in the first column in Table 19 and the r_{ij} parameters have been multiplied by 1.0012. The comparison of these results with the corresponding microwave work (5, p. 1040-1043) is pleasing. It should be noted that in neither case do the parameters represent true equilibrium values (2, p. 1219-1222; 23, p. 2961-2963; 29, 1945-1949; 37, p. 644-648; 38, p. 1108-1109), though the microwave parameters represent a closer approximation than those of electron diffraction.

¹The effect of weighing the observations which emphasized the intermediate and inner data (but not innermost) led to an increase in 1 N-O^{, r}O...O and 1O...O.

PART II

QUADRATIC POTENTIAL CONSTANTS

POTENTIAL CONSTANT INVESTIGATION

List of Symbols (In order of appearance in Part II of the text)¹

n	p.d.
^rl	internal bond stretching coordinate.
Δr ₂	same as ∆r _l .
Δα	internal valence angle bending coordinate.
Δr ₃	internal non-bonded stretching coordinate.
r ^e X-Y	equilibrium bond distance in non-linear XY_2 molecule.
< Y - X - Y	equilibrium valence angle in non-linear XY ₂ molecule.
$r^{e}_{Y \cdots Y}$	equilibrium non-bonded distance in non-linear XY_2
	molecule.
t	$t = r_{X-Y}^{e} \sin \left(\langle Y-X-Y \rangle / r_{Y}^{e} \right)$
u	$u = r_{X-Y}^{e} [1 - \cos((Y - X - Y))] / r_{Y \cdots Y}^{e}$
r _{ij}	p. d.
l_{ij}	p. d.
r_{ij}^{i}	p. d.
r^{e}_{ij}	p. d.
R	column matrix of internal coordinate set.
\$	column matrix of symmetry coordinate set.

¹p.d. will denote symbols previously defined.

Q column matrix of normal coordinate set.

 $\overline{\mathbf{V}}$ transformation matrix from **S** to **R**. **R** = $\overline{\mathbf{V}}$ **S**. L transformation matrix from Q to S, S = L Q, symmetrized G matrix. GS \mathbb{F}_{S} symmetrized F matrix. frequency of kth vibrational mode. v k eigenvalue matrix. $\lambda_{\mathbf{k}} = \mathbf{4}\pi^2 v_{\mathbf{k}}^2$. Δ V potential energy of vibration. Т kinetic energy of vibration. column matrix of Cartesian displacement coordinates. Х Ā transformation matrix from \mathbb{R} to \mathbf{X} . $\mathbf{X} = \mathbf{A}\mathbf{R}$. M diagonal matrix of the atomic masses. internal G matrix. $G_R = \overline{V} G_S \overline{V}'$. $\mathbf{G}_{\mathbf{R}}$ unit matrix. (\mathbb{E})_{ij} = δ_{ij} . E diagonal matrix of the mean-square amplitudes of Δ normal vibration. $\Delta = \langle Q Q' \rangle$. h p.d. k p. d. absolute temperature (° K). т the mean-square vibrational amplitude matrix in $\Sigma_{\rm R}$ internal coordinates,

 r^e same as r^e_{N-O} .

s ₁	$S_1 = (\Delta r_2 + \Delta r_2)/2^{\frac{1}{2}}.$
s ₂	$S_2 = r^e \Delta a$.
s ₃	$S_3 = (\Delta r_1 - \Delta r_2)/2^{\frac{1}{2}}.$
Δr	$\Delta \mathbf{r} = \Delta \mathbf{r}_1 \text{or} \Delta \mathbf{r}_2.$
a	equilibrium O-N-O angle.
F ₁₁	$\mathbf{F}_{11} = \mathbf{f}_{\mathbf{r}} + \mathbf{f}_{\mathbf{rr}} .$
F ₁₂	$F_{12} = 2^{\frac{1}{2}} f_{ro.}$
F ₂₂	$F_{22} = f_a$.
F 33	$F_{33} = f_{r} - f_{rr}$.
μ	$\mu_i = m_i^{-1}$ where m_i is the mass of the ith atom.
G ₁₁	$G_{11} = 2\mu_N \cos^2(\alpha/2) + \mu_O$.
G ₁₂	$G_{12} = -2^{3/2} \mu_N \sin(\alpha/2) \cos(\alpha/2).$
G ₂₂	$G_{22} = 2 [2\mu_N \sin^2(\alpha/2) + \mu_O].$
G ₃₃	$G_{33} = G_{22}/2.$
β	$\beta = F_{11}F_{22} - F_{12}^2.$
Ÿ	$\overline{\gamma} = G_{11}G_{22} - G_{12}^2$
С	$\mathbf{C} = \mathbf{F}^{-1}.$
K	$\mathbb{K} = \mathbf{G}^{-1}.$
φ	$\phi = \lambda^{-1}.$
C _S	$\mathbb{C}_{S} = \mathbb{F}_{S}^{-1}.$
c ₁₁	$C_{11} = F_{22}/\beta.$
C ₁₂	$C_{12} = -F_{22}/\beta.$
C ₂₂	$C_{22} = F_{11}/\beta.$

$$C_{33} \qquad C_{33} = F_{33}^{-1}.$$

v observed fundamental frequency of the ith vibrational mode.

 ω_i harmonic frequency of the ith vibrational mode.

POt diagonal weight matrix used in least-squares determination of symmetrized compliance constants.

f_i ith internal potential constant.

 $\sigma(f_i)$ estimated error in f_i due to uncertainties in

1
N-O and 1 O···O'

 $\sigma_{T}(1_{ij}) \qquad p.d.$ $\sigma_{LS}(1_{ij}) \qquad p.d.$

Molecular Potential Functions

In the harmonic approximation, a non-linear polyatomic molecule can be viewed as an aggregation of 3n-6 (3n-5 for a linear molecule) independent simple harmonic oscillators. As internal coordinates one normally selects either "valence" or "central force" coordinates [various choices are possible (46, p. 223)]. The former set consists of bond distance and bond angle displacements from equilibrium and the latter solely of internuclear distance displacements. For example, for a non-linear XY₂ molecule the valence force coordinates would be the two equivalent X-Y stretches and the Y-X-Y angle distortion, which may be denoted by Δr_1 , Δr_2 and Δa^1 , respectively; the corresponding central force coordinates would then be Δr_1 and Δr_2 and the Y···Y distance displacement Δr_3 . By geometric means, it is easily shown that (assuming small displacements)

 $\Delta r_3 = (\Delta r_1 + \Delta r_2) \sin (\langle Y - X - Y/2 \rangle + r_{X-Y}^e \Delta \alpha \cos (\langle Y - X - Y/2 \rangle).$ (II, 1)

With the coordinates defined above one may consider many vibrational models. Some of the more common are the simple central force, simple valence force, generalized central force, generalized valence force, and the Urey-Bradley force field which may be

 $[^]l$ For dimensional reasons it is often convenient to replace the internal bending coordinate Δa by r^e_{X-Y} Δa .

abbreviated by SCF, SVF, GCF, GVF, and UBF, respectively. For a bent XY_2 molecule the vibrational potentials corresponding to these models have the forms (in the harmonic approximation)

SCF; 2V =
$$A_r [(\Delta r_1)^2 + (\Delta r_2)^2] + A_{r'} (\Delta r_3)^2$$
, (II, 2)

SVF;
$$2V = B_r [(\Delta r_1)^2 + (\Delta r_2)^2] + B_a (r_{X-Y}^e \Delta a)^2$$
, (II, 3)
GCF; $2V = D_r [(\Delta r_1)^2 + (\Delta r_2)^2] + D_{r'} (\Delta r_3)^2$

+
$$2D_{rr} (\Delta r_1 \Delta r_2) + 2D_{rr'} (\Delta r_1 + \Delta r_2) \Delta r_3$$
, (II, 4)
GVF; $2V = H_r [(\Delta r_1)^2 + (\Delta r_2)^2] + H_a (r_{X-Y}^e \Delta a)^2$

$$+ 2H_{rr} (\Delta r_{1} \Delta r_{2}) + 2H_{ra} (\Delta r_{1} + \Delta r_{2}) r_{X-Y}^{e} \Delta a, (II, 5)$$

$$UBF; 2V = (K + t^{2}F' + u^{2}F) [(\Delta r_{1})^{2} + (\Delta r_{2})^{2}] + (H - u^{2}F' + t^{2}F) (r_{X-Y}^{e} \Delta c)^{2}$$

$$+ 2(-t^{2}F' + u^{2}F) \Delta r_{1} \Delta r_{2} + 2tu (F' + F) (\Delta r_{1} + \Delta r_{2}) r_{X-Y}^{e} \Delta c. (II, 6)$$

In equation (II, 6), K and H denote the stretching and bending potential constants and F and F', the repulsive potential constants between non-bonded atoms. F' is often approximated as -(1/10)F, which follows from taking the potential energy proportional to $(r_{Y + \cdots + Y}^{e})^{-9}$. Furthermore, the potential constants defined in equations (II, 4), (II, 5) and (II, 6) can be simply related. Equating corresponding coefficients in equations (II, 5) and (II, 6),

$$H_{r} = K + t^{2}F' + u^{2}F,$$

$$H_{a} = H - u^{2}F' + t^{2}F,$$

$$H_{rr} = -t^{2}F' + u^{2}F,$$

$$H_{ra} = tu (F' + F).$$
(II, 7)

Since the potential and kinetic energy expressions must be invariant with respect to the coordinate system, one has

method is not always easy or satisfactory.

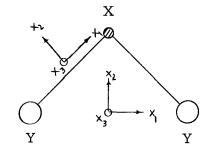
Potential and Compliance Constants of Nitrogen Dioxide from Mean-Square Amplitudes and Vibrational Frequencies

The early work of James (26, p. 737-754) established the connection between molecular vibration and the intensity of scattering from molecules. Although this work was specifically concerned with x-ray scattering, the results are also applicable to electrons, and have been successfully applied to the interpretation of electron diffraction patterns for many years. Recently, a good deal of attention has been devoted to exploring the connection between amplitudes of vibration, frequencies of vibration, and force constants [see (10, p. 1-200; 11, p. 1121-1122; 22, p. 594-598; 33, p. 395; 34, p. 726-733; 35, p. 1927-1933; 36, p. 737-747; 37, p. 643-652) and bibliographies therein cited]; the work by James provides the theoretical backbone for the interpretation of the diffraction results. It is the intention here to present only an outline of those ideas and equations needed to relate potential constants to mean amplitudes and normal frequencies of vibration.

Morino and Hirota (36, p. 737-747) distinguish three types of generalized vibrational amplitudes with respect to a specific atom pair (i, j) in a molecule. Let the coordinates x_1 , x_2 and x_3 denote the Cartesian axes parallel and perpendicular, respectively, to r_{ij} ; then Δx_1 , Δx_2 and Δx_3 will denote the net displacement coordinates of the i, j atomic pair along each of these axial directions. The various amplitudes are then defined as follows:

<
$$\Delta x_1^2$$
 >; the mean-square parallel amplitude,
< Δx_2^2 >, < Δx_3^2 >; the mean-square perpendicular amplitudes,
< $\Delta x_1 \Delta x_2$ >, < $\Delta x_2 \Delta x_3$ >, < $\Delta x_2 \Delta x_1$ >; the mean cross products.

It has been shown (36, p. 743) that symmetry considerations allow one to conclude that for a non-linear XY_2 molecule the only non-zero amplitudes for the atomic pair Y-X are $\langle \Delta x_1^2 \rangle$ and $\langle \Delta x_1 \Delta x_2 \rangle$, and for Y...Y, $\langle \Delta x_1^2 \rangle$; the diagram shows the orientation of coordinates.



Now, in the usual definition (10, p. 1) of the mean amplitude of vibration for an atom pair i, j one has

$$l_{ij} = \langle (r_{ij}^{i} - r_{ij}^{e})^{2} \rangle^{\frac{1}{2}}$$
 (II, 10)

As a first approximation 1. is equivalent to the square root of the mean-square parallel amplitude discussed earlier. That is,

$$r_{ij}^{i} - r_{ij}^{e} = \sum_{k=1}^{3} (\partial r_{ij}^{i} / \partial x_{k})_{e} \Delta x_{k} + higher order terms = \sum_{k=1}^{3} (x_{k} / r_{ij}^{e}) \Delta x_{k}$$

+ higher order terms; neglecting the higher order terms, squaring and averaging gives equation (II, 10). The various relationships defining the basic framework of the potential constant calculation may be summarized as follows.

Let the column matrices \mathbb{R} , \mathbb{S} , and \mathbb{Q} represent respectively sets of internal coordinates, symmetry coordinates, and the normal coordinates. The relations between these sets of coordinates are

$$\mathbf{R} = \mathbf{\overline{V}} \mathbf{S} \tag{II, 11}$$

and

$$\mathbf{S} = \mathbf{L} \mathbf{Q} . \tag{II, 12}$$

The matrix
$$\mathbf{L}$$
 is determined by the equations (47, p. 1047-1052; 48, p. 76-84)

$$\mathbf{G}_{\mathbf{S}} \mathbf{F}_{\mathbf{S}} \mathbf{L} = \mathbf{L} \boldsymbol{\Lambda} , \qquad (\mathbf{II}, 13)$$

$$\mathbf{L}'\mathbf{F}_{\mathbf{S}}\mathbf{L} = \boldsymbol{\Lambda} , \qquad (\mathbf{II}, 14)$$

and

$$\mathbf{L} \ \mathbf{L}' = \mathbf{G}_{\mathbf{S}} . \tag{II, 15}$$

The matrix \mathbb{F}_{S} , of course, is defined in terms of the potential energy

$$2V = \mathbf{S'F_SS}. \tag{II, 16}$$

The matrix G_S is connected to the kinetic energy, as may be seen by the following equations:

$$\mathbf{X} = \tilde{\mathbf{A}} \mathbf{R}, \qquad (\mathbf{II}, 17)$$

$$2T = \dot{X} \cdot \vec{M} \dot{X}$$

$$= \vec{R} \cdot \vec{A} \cdot \vec{M} \vec{A} \vec{R}$$

$$= \dot{R} \cdot \vec{G}_{R}^{-1} \vec{R}$$

$$= \dot{S} \cdot \vec{\nabla} \cdot \vec{G}_{R}^{-1} \vec{\nabla} \dot{S}$$

$$= \dot{S} \cdot \vec{G}_{S}^{-1} \dot{S}. \qquad (II, 18)$$

The matrix Λ is a diagonal matrix the elements of which are given by

$$\lambda_{k} = 4\pi^{2} \nu_{k}^{2}; \qquad (II, 19)$$

they are related to the G and F matrices by the secular equations (47, p. 1047-1052)

$$\mathbf{G}_{\mathbf{S}} \mathbf{F}_{\mathbf{S}} - \lambda \mathbf{E} = 0 \tag{II, 20}$$

and

$$\mathbf{G}_{\mathbf{R}} \mathbf{F}_{\mathbf{R}} - \lambda \mathbf{E} = 0.$$
 (II, 21)

The mean square amplitudes of a normal vibration defined by the diagonal matrix

$$\langle \mathbf{Q} \mathbf{Q}' \rangle = \langle \mathbf{Q}^2 \rangle^1 = \Delta$$
 (II, 22)

and in the harmonic approximation are given by (6, p. 309; 26,

p. 737-754)

<
$$Q_k^2 > = h/8\pi^2 v_k \operatorname{coth}(hv_k/2kT)$$
. (II, 23)

The mean square vibrational matrix in internal coordinates ($\Sigma_{
m R}$)

(34, p. 726-727) is given by

 $^{^{\}rm l}$ < Q Q $^{\rm \prime}$ > is diagonal due to the non-mixing character of the normal coordinates.

$$\Sigma_{\mathbf{R}} = \langle \mathbf{R} \mathbf{R}' \rangle = \langle \mathbf{\bar{V}} \mathbf{L} \mathbf{Q} \mathbf{Q}' \mathbf{L}' \mathbf{\bar{V}}' \rangle$$

$$= \mathbf{\bar{V}} \mathbf{L} \langle \mathbf{Q} \mathbf{Q}' \rangle \mathbf{L}' \mathbf{\bar{V}}' = \mathbf{\bar{V}} \mathbf{L} \boldsymbol{\Delta} \mathbf{L}' \mathbf{\bar{V}}'.$$
(II, 24)

The solution to the vibrational problem is contained in equations (II, 13) and (II, 24). The V and G matrices can be written down by inspection, and by eliminating the L matrix elements from these two equations [with the aid of the normalization conditions expressed in equations (II, 14) and (II, 15)] one obtains expressions for the potential constants in terms of the measured mean-square vibrational amplitudes and vibrational frequencies.

For nitrogen dioxide the general quadratic potential function in terms of the internal valence force coordinates, Δr_1 , Δr_2 , and $r^e \Delta a$ is [see equation (II, 5)]

$$2V = f_{r} \left[\left(\Delta r_{1} \right)^{2} + \left(\Delta r_{2} \right)^{2} \right] + 2f_{rr} \left(\Delta r_{1} \Delta r_{2} \right) + f_{a} \left(r^{e} \Delta a \right)^{2}$$
$$+ 2f_{ra} \left(\Delta r_{1} + \Delta r_{2} \right) r^{e} \Delta a . \qquad (II, 25)$$

The molecular point group of nitrogen dioxide is C_{2v} . The symmetry species (49, p. 146-162) as obtained by standard procedures are

$$\Gamma (NO_2) = \Gamma (r) + \Gamma (a)$$

= (A₁ + B₁) + A₁
= 2A₁ + B₁, (II, 26)

where A_1 and B_1 denote symmetric and antisymmetric modes, respectively. The selection rules thus predict two infrared and Raman active A_1 modes (symmetric stretch and bend, respectively) and one active B_1 mode (antisymmetric stretch) for nitrogen dioxide. Representing the column matrices $\,\mathbb{R}\,$ and $\,\mathbb{S}\,$ as

$$\mathbb{R} = \{ \Delta r_1, r^e \Delta a, \Delta r_2 \}$$
(II, 27)

and

$$\mathbf{S} = \{ S_1, S_2, S_3 \},$$
 (II, 28)

the transformation matrix \overline{V} can be obtained as follows. Let the subscripts 1 and 2 denote the totally symmetric N-O stretch and <O-N-O bend, respectively, and the subscript 3, the antisymmetric N-O stretch. Then the symmetry coordinates are given by (42, p. 902)

$$S_1 = S_r^{(A_1)} = 2^{-\frac{1}{2}} (\Delta r_1 + \Delta r_2)$$
, (II, 29)

$$S_2 = S_a^{(A_1)} = r^e \Delta a$$
 (II, 30)

and

$$S_3 = S_r^{(B_1)} = 2^{-\frac{1}{2}} (\Delta r_1 - \Delta r_2).$$
 (II, 31)

The orthogonality of $\overline{\mathbf{V}}$ is easily demonstrated in this case. Since an orthogonal transformation leaves the sum of squares of both sets of coordinates invariant, the following relationship should and does exist:

$$(\Delta r_1)^2 + (\Delta r_2)^2 + (r^e \Delta a)^2 = S_1^2 + S_2^2 + S_3^2$$
. (II, 32)

Hence, $\overline{\mathbb{V}}^{-1} = \overline{\mathbb{V}}'$ and we have

$$\bar{\mathbb{V}} = \begin{bmatrix} 2^{-\frac{1}{2}} & 0 & 2^{-\frac{1}{2}} \\ & 1 & 0 \\ & & -2^{-\frac{1}{2}} \end{bmatrix} .$$
(II, 33)

One may now write the column matrix Q as

$$Q = \{ Q_1, Q_2, Q_3 \} = \{ Q_r^{(A_1)}, Q_a^{(A_1)}, Q_r^{(B_1)} \}, \quad (II, 34)$$

the transformation matrix \mathbb{L} [see equation (II, 12)] as

$$\mathbf{L} = \begin{bmatrix} \mathbf{L}_{11} & \mathbf{L}_{12} & 0 \\ \mathbf{L}_{21} & \mathbf{L}_{22} & 0 \\ 0 & 0 & \mathbf{L}_{33} \end{bmatrix}, \quad (\mathbf{II}, 35)$$

and the mean-square normal coordinate matrix, Δ [see equation (II, 22)], as

$$\boldsymbol{\Delta} = \begin{bmatrix} \boldsymbol{\Delta}_1 & \boldsymbol{0} & \boldsymbol{0} \\ & \boldsymbol{\Delta}_2 & \boldsymbol{0} \\ & & \boldsymbol{\Delta}_3 \end{bmatrix} .$$
 (II, 36)

From the expression for $\Sigma_{\rm R}$ [equation (II, 24)] we can relate the mean-square vibrational amplitudes $l_{\rm N-O}^2$ and $l_{O\cdots O}^2$ to the elements of the $\bar{\bf V}$, ${\bf L}$ and Δ matrices as follows. Using the first expression in equation (II, 24)

$$< \mathbb{R} \mathbb{R}^{\prime} > = \begin{bmatrix} 1_{N-O}^{2} & r^{e} < \Delta r \Delta a > & < \Delta r_{1} \Delta r_{2} > \\ & (r^{e})^{2} < \Delta a^{2} > & r^{e} < \Delta r \Delta a > \\ & & 1_{N-O}^{2} \end{bmatrix}, \qquad (II, 37)$$

from which

$$\begin{bmatrix} \bar{z}^{1}(\Delta_{1}L_{11}^{2}+\Delta_{2}L_{12}^{2}+\Delta_{3}L_{33}^{2}), \bar{z}^{\frac{1}{2}}(\Delta_{1}L_{11}L_{12}^{2}+\Delta_{2}L_{12}L_{22}), \bar{z}^{-1}(\Delta_{1}L_{11}^{2}+\Delta_{2}L_{12}^{2}-\Delta_{3}L_{33}^{2}) \\ \Delta_{1}L_{21}^{2}+\Delta_{2}L_{22}^{2}, \bar{z}^{\frac{1}{2}}(\Delta_{1}L_{11}L_{12}^{2}+\Delta_{2}L_{12}L_{22}) \\ \bar{z}^{1}(\Delta_{1}L_{11}^{2}+\Delta_{2}L_{12}^{2}+\Delta_{3}L_{33}^{2}) \end{bmatrix}$$
(II, 38)

60

If one squares both sides of equation (II, 1) and takes the time average

$$I_{O \cdots O}^{2} = \langle \Delta r_{3}^{2} \rangle = 2(I_{N-O}^{2} + \langle \Delta r_{1} \Delta r_{2} \rangle) \sin^{2} (\alpha/2) + (r^{e})^{2} \langle \Delta \alpha^{2} \rangle \cos^{2} (\alpha/2) + 2r^{e} \langle \Delta r \Delta \alpha \rangle \sin \alpha$$
 (II, 39)

Combining equations (II, 37), (II, 38) and (II, 39), one obtains

$$l_{N-O}^{2} = 2^{-1} \left(\Delta_{1} L_{11}^{2} + \Delta_{2} L_{22}^{2} + \Delta_{3} L_{33}^{2} \right)$$
(II, 40)

and

$$I_{O...O}^{2} = 2(\Delta_{1}L_{11}^{2} + \Delta_{2}L_{12}^{2}) \sin^{2}(\alpha/2) + (\Delta_{1}L_{21}^{2} + \Delta_{2}L_{22}^{2})\cos^{2}(\alpha/2) + 2^{\frac{1}{2}}(\Delta_{1}L_{11}L_{21} + \Delta_{2}L_{12}L_{22}) \sin \alpha . \quad (II, 41)$$

The \mathbb{F}_{S} and \mathbb{G}_{S} matrices may be written down immediately (42, p. 902)

$$\mathbb{F}_{S} = \begin{bmatrix} f_{r} + f_{rr} & 2^{\frac{1}{2}} f_{ra} & 0 \\ & f_{a} & 0 \\ & & f_{r} - f_{rr} \end{bmatrix} = \begin{bmatrix} F_{11} & F_{12} & 0 \\ & F_{22} & \\ & & F_{33} \end{bmatrix}$$
(II, 42)

and

$$\mathbb{G}_{S} = \begin{bmatrix} 2\mu_{N}\cos^{2}(\alpha/2) + \mu_{O}, -2^{3/2}\mu_{N}\sin(\alpha/2)\cos(\alpha/2), & 0\\ & 2(2\mu_{N}\sin^{2}(\alpha/2) + \mu_{O})\\ & & 2\mu_{N}\sin^{2}(\alpha/2) + \mu_{O} \end{bmatrix}$$

$$= \begin{bmatrix} G_{11} & G_{12} & 0 \\ & G_{22} & 0 \\ & & & G_{33} \end{bmatrix} .$$
 (II, 43)

Solving equation (II, 14) for \mathbb{F}_{S}^{-1} , one obtains

$$\mathbb{F}_{S}^{-1} = \mathbb{L} \wedge^{-1} \mathbb{L}'. \qquad (II, 44)$$

Since

$$\mathbb{F}_{S}^{-1} = \begin{bmatrix} F_{22}/\beta & -F_{12}/\beta & 0 \\ & F_{11}/\beta & 0 \\ & & F_{33} \end{bmatrix}$$
(II, 45)

and

$$\Lambda^{-1} = \begin{bmatrix} 1/\lambda_1 & 0 & 0 \\ & 1/\lambda_2 & 0 \\ & & 1/\lambda_3 \end{bmatrix},$$
 (II, 46)

one obtains with equations (II, 35) and (II, 43),

$$\begin{bmatrix} G_{11} & G_{12} & 0 \\ G_{22} & 0 \\ & G_{33} \end{bmatrix} = \begin{bmatrix} L_{11}^2 + L_{12}^2 & L_{11}L_{21} + L_{12}L_{22} & 0 \\ & L_{21}^2 + L_{22}^2 & 0 \\ & & L_{33}^2 \end{bmatrix}$$
(II, 47)

and

$$\begin{bmatrix} F_{22}/\beta & -F_{12}/\beta & 0 \\ & F_{11}/\beta & 0 \\ & & F_{33}^{-1} \end{bmatrix}$$

$$= \begin{bmatrix} L_{11}^{2}\tilde{\lambda}_{1}^{1} + L_{12}^{2}\tilde{\lambda}_{2}^{1}, & L_{11}L_{21}\tilde{\lambda}_{1}^{1} + L_{12}L_{22}\tilde{\lambda}_{2}^{1}, & 0 \\ & & L_{21}^{2}\tilde{\lambda}_{1}^{1} + L_{22}^{2}\tilde{\lambda}_{2}^{-1}, & 0 \\ & & & L_{33}^{2}\tilde{\lambda}_{3}^{-1} \end{bmatrix} .$$
(II, 48)

The solution of equation (II, 20) can be written down by inspection (30, p. 3) giving

$$\lambda_1 + \lambda_2 = G_{11}F_{11} + G_{22}F_{22} + 2G_{12}F_{22}$$
, (II, 49)

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$$\lambda_1 \lambda_2 = \beta (G_{11} G_{22} - G_{12}^2) = \beta \overline{\gamma},$$
 (II, 50)

and

$$\lambda_3 = G_{33}F_{33}$$
. (II, 51)

Combining equations (II, 47) and (II, 48), one obtains

$$L_{11}^{2} = [\lambda_{1}/\beta(\lambda_{1}-\lambda_{2})] (-\lambda_{2}F_{22} + \beta G_{11}), \qquad (II, 52)$$

$$L_{22}^{2} = [\lambda_{2}/\beta(\lambda_{1}-\lambda_{2})] (\lambda_{1}F_{11} - \beta G_{22}), \qquad (II, 53)$$

$$L_{33}^2 = G_{33} = \lambda_3 / F_{33} , \qquad (II, 54)$$

$$L_{12}^{2} = [\lambda_{2} / \beta(\lambda_{1} - \lambda_{2})] (\lambda_{1} F_{22} - \beta G_{11}), \qquad (II, 55)$$

$$L_{21}^{2} = [\lambda_{1}/\beta(\lambda_{1}-\lambda_{2})] (-\lambda_{2}F_{11} + \beta G_{22}), \qquad (II, 56)$$

$$L_{11}L_{21} = [\lambda_1/\beta(\lambda_1 - \lambda_2)] (\lambda_2F_{12} + \beta G_{12}), \quad (II, 57)$$

$$L_{12}L_{22} = [-\lambda_2/\beta(\lambda_1 - \lambda_2)] (\lambda_1 F_{12} + \beta G_{12}).$$
 (II, 58)

Finally, by condensing the various relationships one has

$$I_{N-O}^{2} = A_{1}F_{22} + A_{2}(F_{11}F_{22} - F_{12}^{2}) + A_{3}$$
, (II, 59)

$${}^{2}_{O \cdots O} = {}^{A}_{4} {}^{F}_{22} + {}^{A}_{5} {}^{F}_{11} + {}^{A}_{6} {}^{F}_{12} + {}^{A}_{7}$$
, (II, 60)

$$A_8 = A_9 F_{22} + A_{10} F_{11} + A_{11} F_{12} , \qquad (II, 61)$$

and

$$F_{33} = \lambda_3 / G_{33} , \qquad (II, 62)$$

where

$$A_{1} = \overline{c}f/2g, A_{2} = G_{11}\overline{b}\overline{c}/2dg, A_{3} = G_{33}e/2, A_{4} = 2\overline{i} \sin^{2}(a/2),$$

$$A_{5} = \overline{i} \cos^{2}(a/2), A_{6} = -2^{3/2}\overline{i} \sin(a/2) \cos(a/2),$$

$$A_{7} = (\overline{b}/g)[2G_{11}\sin^{2}a/2 + (G_{22}\cos a/2 + 2^{3/2}G_{12}\sin a/2)\cos a/2],$$

$$A_{8} = \overline{h}, A_{9} = G_{22}, A_{10} = G_{11}, A_{11} = 2G_{12} \qquad (II, 63)$$

with

$$\overline{\mathbf{b}} = \Delta_1 \lambda_1 - \Delta_2 \lambda_2, \ \overline{\mathbf{c}} = \overline{\gamma}, \ \mathbf{d} = \lambda_1 \lambda_2, \ \mathbf{e} = \Delta_3, \ \mathbf{f} = \Delta_2 - \Delta_2,$$
$$\mathbf{g} = \lambda_1 - \lambda_2, \ \overline{\mathbf{h}} = \lambda_1 + \lambda_2, \ \overline{\mathbf{i}} = \overline{\mathbf{c}} \mathbf{f}/\mathbf{g} = 2\mathbf{A}_1.$$
(II, 64)

Since equation (II, 59) is quadratic in F_{12} , two sets of solutions are possible. The most physically reasonable is selected.

During the course of this work J. C. Decius (12, p. 241-248) introduced the notion of a compliance matrix. With this approach the secular equation takes the form

$$\mathbb{C} \mathbb{K} - \Phi \mathbb{E} = 0, \qquad (II, 65)$$

where $\mathbb{K} = \mathbb{G}^{-1}$, $\mathbb{C} = \mathbb{F}^{-1}$, and $\phi = \lambda^{-1}$. Since this paper describes the determination of compliance constants from normal frequencies and mean-square amplitudes (or centrifugal distortion data), treating among other molecules, nitrogen dioxide as an example, ¹ no attempt will be made here to duplicate this development. Since the compliance constants to be reported in this thesis correspond to the inverse of the \mathbb{F}_{S} matrix defined in equation (II, 45), the symmetrized compliance matrix \mathbb{C}_{S} (defined in terms of valence force symmetry coordinates) will take the form

 $[^]l$ The values of l^2_{N-O} and $l^2_{O\cdots O}$ used by Professor Decius correspond to preliminary values obtained during the course of this thesis work.

$$\mathbb{C}_{S} = \begin{bmatrix} C_{11} & C_{12} & 0 \\ & C_{22} & 0 \\ & & C_{33} \end{bmatrix} = \begin{bmatrix} F_{22}/\beta & -F_{12}/\beta & 0 \\ & F_{11}/\beta & 0 \\ & & & F_{33}^{-1} \end{bmatrix}.$$
(II, 66)

The compliance matrix of nitrogen dioxide reported by Decius is defined in terms of central force coordinates, it differs numerically from \mathbb{C}_{S} of equation (II, 66).

Computation of Potential and Compliance Constants

The numerical solutions of equations (II, 59) - (II, 61) were obtained by the use of the university Alwac III-E digital computer. Since the computer program is rather specialized (non-linear XY₂ molecules), it will not be reproduced here though a brief description will be given. The vibrational frequencies (1, p. 413-427) used are given¹ in Table 24. The computer output gave elliptical contours (22, p. 596-598) corresponding to the observed values of I_{N-O} and $I_{O...O}$, respectively, such that on each of the two contours (corresponding to I_{N-O} and $I_{O...O}$), all real combinations of the symmetrized potential constants F_{11} , F_{22} and F_{12} were represented. Systematic investigation of the output contours identified their approximate intersections (ideally, there are two of them); these

¹Separate calculations were made using first the v_i 's and then the ω_i 's.

intersections were subsequently calculated exactly. Since the intersections represented two combinations of symmetrized potential constants compatible with both electron diffraction and spectroscopic data, they are the solutions of equations (II, 59) - (II, 61). Figure 5 is a plot of these contours. Finally, these solutions were transformed to the corresponding ones in terms of the internal potential constants f_r , f_{rr} , f_a and f_{ra} [see equation (II, 42)].

In addition to the potential constants obtained by the method described above, various combinations of frequencies (see Table 30a) and vibrational amplitudes were investigated using a newly devised least-squares program of R. Ottinger.¹ The elements of the diagonal weight matrix used were given by

$$(\mathbb{P}_{Ot})_{v_{i}} = 1 \text{ and } (\mathbb{P}_{Ot})_{l_{ij}}^{2} = 2500.$$
 (II, 67)

These results are expressed in terms of the symmetrized compliance constants defined in equation (II, 66).

Errors in the Internal Potential Constants Derived from the Intersections of Elliptical Contours

A complete error analysis should include uncertainties arising from the determination of the vibrational amplitudes, normal frequencies, interatomic distances, physical constants and the errors

¹Ottinger, Robert. Private communication. Corvallis, Oregon. Oregon State University, 1964.

arising from the method of calculation employed. The effect in the potential constants arising from the uncertainties in the vibrational amplitudes were estimated as follows. Let f_i denote one of the internal potential constants f_r , f_{rr} , f_a , and f_{ra} , then

 $f_i = f_i (r_{N-O}, r_{O-O}, l_{N-O}, l_{O-O}, \nu_1, \nu_2, \nu_3). \quad (II, 68)$ Further, let $\mathcal{O}(f_i)$ be defined as

$$2\mathfrak{Q}_{f_{i}} = f_{i}[r_{N-O}, r_{O} \cdots O, l_{N-O} + m \sigma_{T}(l_{N-O}), l_{O} \cdots O + n \sigma_{T}(l_{O} \cdots O), \nu_{1}, \nu_{2}, \nu_{3}]$$

- $f_{i}(r_{N-O}, r_{O}, \dots O, l_{N-O}, l_{O} \cdots O, \nu_{1}, \nu_{2}, \nu_{3}).$ (II, 69)

It is clear that $\sigma(f_i)$ (as a very rough approximation) will reflect the uncertainty in f_i arising from those in the vibrational amplitudes. The values of the coefficients m and n were obtained from the error matrix given in Table 24. The correlation between l_{N-O} and $l_{O \cdots O}$ is positive indicating that the error which increases one mean amplitude also increases the other, hence, m and n should have the same algebraic signs. Arbitrarily, m was taken as two, and n as one-half. The results are given in Tables ¹ 26a and 26b.

No attempt was made to estimate the errors arising from the determination of normal frequencies, internuclear distances, and physical constants. From the form of equations (II-59) to (II-64), it was felt that these errors would be negligible by comparison to those

¹Similar estimates were obtained for the set of potential constants derived from the ω_i 's instead of the ν_i 's. The effect of $\sigma_{LS}(l_{ij})$ in place of $\sigma_{T}(l_{ij})$ was also investigated.

of the vibrational amplitudes.

Errors in the Symmetrized Compliance Constants Obtained from Least-Squares Fitting

The only errors estimated here were the standard errors obtained from least-squares fitting (Table 30a). The significance of these errors is mainly that of indicating the compatibility of the vibrational amplitudes and the normal frequencies with respect to the compliance constants.

Final Results

The constants used in the various calculations are given in Tables 23-25. The final results are given in Tables 27-30b. Comparison of the internal potential constants determined in this work with those obtained by isotopic spectroscopy (1, p. 413-427) shows the agreement to be good (Table 27). The comparison of the observed and calculated frequencies (derived from the final internal potential constants), as given in Table 29, is pleasing, especially so in the case of the ω_i 's. The comparison of the observed vibrational amplitudes from this work with those calculated by Cyvin (10, p. 117) from potential constants derived from isotopic spectroscopy, is given in Table 29. Again the agreement¹ is good. The numerous compliance constant results given in Tables 30a and 30b are discussed in the next section.

¹Though the observed amplitudes and calculated ones correspond to two different temperatures (380° and 298°K, respectively), the temperature effect in this case is surely very small since the vibrational frequencies are high.

SUMMARY

Part I

The molecular geometry of nitrogen dioxide was determined. The parameter values of r_{N-O} , r_{O-O} , and <O-N-O agree well with the corresponding microwave results (5, p. 1040-1043). Conservative estimates of standard errors lead to probable accuracies of 0. 1, 0. 2, and 0. 5 percent for r_{N-O} , r_{O-O} , and <O-N-O, respectively. Corresponding conservative estimates for the rootmean-square amplitudes of vibration lead to seven percent for l_{N-O} and 11 percent for l_{O-O} .

Part II

The two sets of internal quadratic potential constants determined from $\{1_{N-O}, 1_{O}, \dots, 0, r_{N-O}, r_{O}, \dots, 0, \nu_1, \nu_2, \nu_3\}$ and from $\{1_{N-O}, 1_{O}, \dots, 0, r_{N-O}, r_{O}, \dots, 0, \omega_1, \omega_2, \omega_3\}$ agree well with those obtained from isotopic spectroscopy. The comparison of calculated and observed frequencies indicated that there is probably very little anharmonicity in the O···O motion. Further, the observed vibrational amplitudes agree well with those calculated by Cyvin.

The numerous least-squares fitting for symmetrized compliance constants indicated that (1) the results are essentially insensitive to the bond angle¹ parameter used within reasonable limits, (2) the off-diagonal compliance constants are quite sensitive to input data combinations, where the diagonal elements are not. The agreement between the various sets of compliance constants and internal potential constants suggest very strongly that vibrational amplitudes from electron diffraction (at least for small polyatomics composed of similar atoms) are compatible with spectroscopy data (vibrational frequencies) with respect to either potential or compliance constant determinations. This statement is further reinforced by the various comparisons of observed and calculated frequencies.

In conclusion, the reliability and consistency of the vibrational amplitudes from electron diffraction for potential or compliance constant determinations can be regarded as favorable, at least for small polyatomic molecules composed of similar atoms.

¹As determined from r_{N-O} and $r_{O} \cdot \cdot \cdot O'$

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APPENDICES

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APPENDIX I

TABLES

r _{N-O} , Å	<0-N-0, deg.	Comments
1.21 <u>+</u> .02	130 +2	electron diffraction (31). ^(a)
1.20 + .02	132 +3	electron diffraction (9). ^(a)
1.21	141	Spurr (50, p. 27) reanalyzed the electron diffraction data of Maxwell and Mosley (31).
1.28	15 4	partial analysis of ultraviolet spectrum (15).
1.188 <u>+</u> .00 4	13 4 . 07 <u>+</u> . 25	infrared (32).
1.189 <u>+</u> .003	133.95 <u>+</u> .10	calculated (45) from rotational data of Keller and Nielsen (28) and Moore (32).
1.186 <u>+</u> .003	133.53 <u>+</u> ,15	electron diffraction. (b), 1
1.197	13 4 . 25	microwave (5).

Table 1. Previous structure investigations of nitrogen dioxide.

(a) Visual method (8, p. 250-254; 41, p. 867-881).

(b) Sector-microphotometer method (27).

¹Severinsson, Robert. Private communication. Oslo, Norway. Universitetets Kjemisk Institutt, 1955.

Table 2. Electron intensity incident on the photographic plate: h = 478.00 mm.

	$I_p^{a(1)}$		$I_p^{a(2)}$]	a(3) p	$I_p^{a(4)}$		
S	L	R	L	R	L	R	L	R	
8.50	0.3350	0.3780	0.2850	0.2880	0.3920	0.3800	0.3140	0.3270	
8.75	0.3280	0.3720	0.2790	0.2830	0.3850	0.3730	0.3090	0.3220	
9.00	0.3230	0.3690	0.2770	0.2760	0.3810	0.3670	0.3030	0.3200	
9.25	0.3190	0.3660	0.2740	0.2730	0.3770	0.3620	0.3010	0.3180	
9.50	0.3160	0.3650	0.2710	0.2690	0.3740	0.3580	0.2970	0.3160	
9•75	0.3130	0.3630	0.2680	0.2660	0.3730	0.3530	0.2940	0.3130	
10.00	0.3110	0.3600	0.2670	0.2640	0.3720	0.3510	0.2920	0.3110	
10.25	0.3080	0.3590	0.2660	0.2620	0.3720	0.3500	0.2910	0.3100	
10.50	0.3070	0.3630	0.2680	0.2620	0.3720	0.3510	0.2920	0.3110	
10.75	0.3110	0.3670	0.2690	0.2650	0.3770	0.3530	0.2930	0.3130	
11.00	0.3130	0.3710	0.2720	0.2680	0.3800	0.3580	0.2980	0.3150	
11.25	0.3170	0.3760	0.2750	0.2710	0.3850	0.3610	0.3000	0.3190	
11.50	0.3160	0.3800	0.2760	0.2720	0.3880	0.3620	0.3010	0.3220	
11.75	0.3150	0.3810	0.2770	0.2720	0.3900	0.3630	0.3000	0.3210	
12.00	0.3110	0.3800	0.2740	0.2700	0.3850	0.3590	0.2960	0.3180	
12.25	0.3040	0.3750	0.2670	0.2630	0.3790	0.3520	0.2890	0.3120	
12.50	0.2950	0.3660	0.2600	0.2560	0.3680	0.3420	0.2800	0.3040	
12.75	0.2860	0.3570	0.2520	0.2470	0.3570	0.3310	0.2700	0.2940	
13.00	0.2750	0.3480	0.2420	0.2360	0.3450	0.3190	0.2580	0.2840	
13.25	0.2660	0.3380	0.2350	0.2290	0.3340	0.3080	0.2500	0.2750	
13.50	0.2610	0.3330	0.2300	0.2220	0.3270	0.2990	0.2430	0.2700	
13.75	0.2560	0.3290	0.2290	0.2170	0.3230	0.2940	0.2400	0.2640	
14.00	0.2530	0.3270	0.2270	0.2150	0.3220	0.2900	0.2370	0.2630	
14.25	0.2520	0.3270	0.2270	0.2130	0.3200	0.2880	0.2370	0.2630	

Table 2 (continued).

Table 2 (continued).

<u></u> , <u></u> , <u></u> , <u></u> , <u></u> ,	$I_p^{a(1)}$		$I_p^{a(2)}$		$I_p^{a(3)}$		Ip ^{a(4)}	
S	L	R	L	R	L	R	L	R
20.50 20.75	0.2280 0.2310	0.3300 0.3310	0.2240 0.2240	0.1950 0.1960	0.3030 0.3050	0.2600 0.2620	0.2120 0.2120	0.2560 0.2570

Table 2 (continued).

L Left branch

,

R Right branch

	T	o(1) o	I ^b	(2)	I ^b	(3)	Ip ^{b(}	(4)
S	L	R	L	R	L	R	<u>L</u>	R
10.25 10.50 10.75 11.00 11.25 11.50 11.75 12.00 12.25 12.50 12.75 13.00 13.25	0.9401 0.9200 0.8998 0.8868 0.8739 0.8621 0.8402 0.8177 0.7839 0.7409 0.7409 0.7080 0.6384	1.0580 1.0389 1.0188 1.0076 0.9890 0.9707 0.9522 0.9222 0.8809 0.8402 0.8050 0.7560 0.7184	1.0959 1.0658 1.0514 1.0311 1.0150 1.0027 0.9780 0.9538 0.9118 0.8796 0.8360 0.7904 0.7518	1.2336 1.2009 1.1853 1.1660 1.1481 1.1320 1.1050 1.0682 1.0274 0.9780 0.9294 0.8820 0.8244	0.9249 0.9031 0.8870 0.8740 0.8636 0.8520 0.8335 0.8083 0.7780 0.7398 0.7050 0.6728 0.6383	1.0681 1.0325 1.0111 0.9951 0.9830 0.9708 0.9461 0.9103 0.8750 0.8311 0.7939 0.7482 0.7133	0.9356 0.9103 0.8902 0.8786 0.8670 0.8485 0.8322 0.8097 0.7859 0.7441 0.7110 0.6760 0.6443	1.0879 1.0619 1.0429 1.0338 1.0211 1.0050 0.9803 0.9500 0.9091 0.8659 0.8211 0.7759 0.7377
13.50 13.75 14.00 14.25 14.50 14.75 15.00 15.25 15.50 15.75 16.00	0.6090 0.5900 0.5760 0.5670 0.5560 0.5510 0.5460 0.5420 0.5360 0.5320	0.6977 0.6770 0.6575 0.6494 0.6433 0.6363 0.6312 0.6231 0.6170 0.6100 0.6060	0.7259 0.7008 0.6905 0.6780 0.6728 0.6677 0.6626 0.6565 0.6504 0.6443 0.6413	0.7960 0.7739 0.7550 0.7462 0.7354 0.7290 0.7290 0.7207 0.7143 0.7090 0.7009 0.6935	0.6110 0.5920 0.5790 0.5720 0.5660 0.5630 0.5590 0.5550 0.5490 0.5470 0.5420	0.6873 0.6668 0.6514 0.6413 0.6373 0.6302 0.6251 0.6221 0.6160 0.6070 0.6040	0.6150 0.5920 0.5790 0.5740 0.5670 0.5560 0.5510 0.5510 0.5450 0.5410 0.5350	0.7163 0.6903 0.6790 0.6698 0.6616 0.6544 0.6494 0.6433 0.6352 0.6292 0.6231

Table 3. Electron intensity incident on the photographic plate: h = 192.07 mm.

Table 3 (continued).

	I ^k	o(1)	1 ^{b(2)}			I ^{b(3)}		(4)
S	L	R	L	R	L	R	L	R
1 - A				_		·····	·····	· · ·
22.25	0.4200	0.4640	0.5070	0.5350	0.4340	0.4690	0.4260	0.4780
22.50	0.4170	0.4600	0.5030	0.5300	0.4310	0.4650	0.4250	0.4730
22.75	0.4140	0.4560	0.4990	0.5240	0.4280	0.4610	0.4230	0.4690
23.00	0.4110	0.4510	0.4930	0.5200	0.4250	0.4560	0.4200	0.4640
23.25	0.4 0 60	0.4460	0.4870	0.5130	0.4210	0.4510	0.4140	0.4590
23.50	0.4000	0.4380	0.4820	0.5040	0.4150	0.4460	0.4090	0.4490
23.75	0.3940	0.4310	0.4740	0.4950	0.4110	0.4380	0.4040	0.4430
24.00	0.3890	0.4240	0.4670	0.4880	0.4040	0.4310	0.3980	0.4360
24.25	0.3810	0.4170	0.4600	0.4820	0.3980	0.4260	0.3920	0.4300
24.50	0.3780	0.4120	0.4560	0.4770	0.3930	0.4200	0.3890	0.4240
24.75	0.3750	0.4100	0.4520	0.4710	0.3910	0.4160	0.3850	0.4210
25.00	0.3730	0.4060	0.4500	0.4680	0.3900	0.4130	0.3840	0.4180
25.25	0.3710	0.4060	0.4490	0.4670	0.3880	0.4120	0.3810	0.4160
25.50	0.3710	0.4060	0.4510	0.4670	0.3890	0.4120	0.3820	0.4170
25.75	0.3720	0.4070	0.4540	0.4690	0.3890	0.4140	0.3820	0.4180
26.00	0.3730	0.4080	0.4550	0.4680	0.3900	0.4140	0.3830	0.4190
26.25	0.3720	0.4080	0.4560	0.4680	0.3890	0.4140	0.3810	0.4190
26.50	0.3730	0.4080	0.4580	0.4660	0.3890	0.4150	0.3810	0.4180
26.75	0.3710	0.4080	0.4560	0.4660	0.3880	0.4150	0.3800	0.4170
27.00	0.3700	0.4070	0.4540	0.4640	0.3860	0.4130	0.3780	0.4150
27.25	0.3670	0.4030	0.4530	0.4610	0.3830	0.4110	0.3760	0.4120
27.50	0.3650	0.3990	0.4500	0.4580	0.3790	0.4090	0.3740	0.4090
27.75	0.3610	0.3960	0.4470	0.4540	0.3770	0.4060	0.3710	0.4060
28.00	0.3590	0 .3 950	0.4450	0.4500	0,3740	0.4030	0.3700	0,4030

Table 3 (continued).

<u></u>	Ip(1)		$I_{p}^{b(1)} \qquad I_{p}^{b(2)}$		lp	(3)	Ip ^{b(4)}	
S	L	R	L	R	L	R	L	R
28.25 28.50 28.75 29.00 29.25 29.50 29.75 30.00 30.25 30.50 30.75 31.00 31.25 31.50	0.3560 0.3540 0.3510 0.3480 0.3450 0.3410 0.3380 0.3360 0.3360 0.3310 0.3310 0.3310 0.3310 0.3310 0.3310	0.3920 0.3870 0.3840 0.3800 0.3760 0.3720 0.3680 0.3650 0.3600 0.3600 0.3590 0.3600 0.3590	0.4420 0.4380 0.4360 0.4320 0.4270 0.4240 0.4200 0.4170 0.4150 0.4150 0.4160 0.4160 0.4170	0.4470 0.4420 0.4390 0.4340 0.4300 0.4250 0.4210 0.4170 0.4140 0.4130 0.4120 0.4120 0.4120 0.4130	0.3710 0.3680 0.3650 0.3630 0.3600 0.3570 0.3530 0.3500 0.3460 0.3440 0.3420 0.3420 0.3420 0.3410	0.4010 0.3970 0.3940 0.3920 0.3880 0.3850 0.3810 0.3790 0.3770 0.3750 0.3750 0.3750 0.3750 0.3750	0.3670 0.3630 0.3590 0.3560 0.3530 0.3490 0.3430 0.3430 0.3430 0.3400 0.3380 0.3380 0.3380 0.3380 0.3370 0.3370	0.4000 0.3950 0.3920 0.3890 0.3840 0.3800 0.3780 0.3750 0.3720 0.3710 0.3690 0.3690 0.3680 0.3680
31.75 32.00 32.25 32.50 32.75 33.00 33.25 33.50 33.75 34.00	0.3300 0.3290 0.3280 0.3260 0.3250 0.3230 0.3210 0.3180 0.3160	0.3600 0.3600 0.3580 0.3550 0.3550 0.3510 0.3500 0.3480 0.3450 0.3420	0.4170 0.4160 0.4150 0.4140 0.4120 0.4090 0.4070 0.4040 0.4040 0.4000 0.3990	0.4120 0.4120 0.4100 0.4080 0.4060 0.4030 0.4010 0.3980 0.3950 0.3920	0.3420 0.3410 0.3410 0.3400 0.3370 0.3350 0.3320 0.3280 0.3280 0.3240	0.3760 0.3750 0.3730 0.3720 0.3710 0.3690 0.3660 0.3640 0.3640 0.3610	0.3380 0.3370 0.3380 0.3360 0.3340 0.3320 0.3290 0.3260 0.3240 0.3220	0.3690 0.3680 0.3650 0.3630 0.3610 0.3580 0.3560 0.3550 0.3500 0.3480

Table 3 (continued).

		$I_p^{b(1)}$		1 ^{b(2)}		I ^{b(3)}		$I_p^{b(4)}$	
S	L	R	L	R	L	R	L .	R	
34.25	0.3150	0.3410	0 .3 950	0.3900	0.3230	0.3590	0.3200	0.3450	
34.50	0.3140	0.3370	0.3940	0.3870	0.3210	0.3570	0.3200	0.3430	
34.75	0.3120	0.3340	0.3920	0.3850	0.3190	0.3550	0.3180	0.3390	
35.00	0.3110	0.3330	0.3900	0.3820	0.3180	0.3540	0.3160	0.3370	
35.25	0.3100	0.3300	0 .3 890	0.3810	0.3170	0.3510	0.3140	0.3350	
35.50	0.3080	0.3290	0.3870	0.3770	0.3140	0.3500	0.3120	0.3330	
35.75	0.3060	0.3280	0 .3 850	0.3760	0.3130	0 .3 480	0.3110	0.3310	
36.00	0.3050	0.3270	0.3830	0.3740	0 .31 10	0.3470	0.3100	0.3300	
36.25	0.3040	0.3270	0.3820	0.3730	0.3110	0.3470	0.3090	0.3280	
36.50	0.3040	0.3260	0.3830	0.3720	0.3100	0.3470	0,3090	0.3270	
36.75	0.3040	0.3260	0.3830	0.3720	0.3090	0.3470	0.3090	0.3270	
37.00	0.3030	0.3260	0.3820	0.3720	0.3090	0.3480	0.3080	0.3270	
37.25	0.3020	0.3250	0.3820	0.3720	0.3080	0.3480	0.3080	0.3280	
37.50	0.3020	0.3240	0.3800	0.3710	0.3090	0.3470	0.3070	0.3260	
37.75	0.3010	0.3230	0.3790	0 .3 690	0.3080	0.3470	0.3070	0.3250	
38.00	0.3000	0.3220	0.3780	0.3670	0.3070	0.3460	0.3050	0.3240	
38.25	0.2990	0.3200	0.3770	0.3640	0.3060	0.3440	0.3040	0.3230	
38.50	0.2970	0.3180	0.3740	0.3620	0.3040	0.3430	0.3020	0.3210	
38.75	0.2950	0.3160	0.3720	0.3610	0.3010	0.3410	0.3000	0.3200	
39.00	0.2940	0.3140	0.3700	0.3590	0.3000	0.3400	0.2990	0.3190	
39.25	0.2920	0.3120	0.3670	0.3570	0.2990	0.3380	0.2970	0.3170	
39.50	0.2910	0.3100	0.3660	0.3550	0.2980	0.3370	0.2960	0.3150	
39.75	0.2900	0.3080	0.3650	0.3540	0.2960	0.3360	0.2950	0.3140	
+0.00	0.2900	0.3070	0.3640	0.3520	0.2950	0.3340	0.2940	0.3130	

Table 3 (continued).

	$I_p^{b(1)}$		Ip ^{b(2)}		Ip ^{b(3)}		$I_p^{b(4)}$	
<u> </u>	L	R	L	R	L	R	F	R
40.25 40.50 40.75 41.00 41.25 41.50 41.75 42.00	0.2890 0.2880 0.2870 0.2860 0.2850 0.2850 0.2850 0.2840	0.3070 0.3060 0.3040 0.3030 0.3020 0.3020 0.3010 0.3010	0.3630 0.3620 0.3620 0.3620 0.3610 0.3610 0.3600 0.3590	0.3500 0.3490 0.3470 0.3460 0.3450 0.3450 0.3440 0.3430	0.2940 0.2920 0.2910 0.2890 0.2890 0.2880 0.2880 0.2880 0.2870	0.3330 0.3330 0.3330 0.3330 0.3310 0.3310 0.3310 0.3310	0.2930 0.2930 0.2930 0.2920 0.2910 0.2890 0.2890 0.2880	0.3120 0.3110 0.3110 0.3110 0.3100 0.3090 0.3090 0.3090

Table 3 (continued).

L Left branch

R Right branch

- 	I ^{c(1)}		Ip	(2)		I _p ^{c(3)}		(4)
S	L	R	L	R	L	R	L	R
s 18.50 18.75 19.00 19.25 19.50 19.75 20.00 20.25 20.50 20.75 21.00 21.25 21.50 21.75 22.00 22.25	L 1.0997 1.0695 1.0249 0.9926 0.9681 0.9498 0.9474 0.9377 0.9245 0.9125 0.9054 0.8960 0.8854 0.8737 0.8622 0.8541	R 1.2665 1.2320 1.1837 1.1495 1.1265 1.1090 1.0957 1.0891 1.0852 1.0721 1.0630 1.0527 1.0337 1.0262 1.0098 0.9975	L 0.8618 0.8308 0.8102 0.7865 0.7709 0.7600 0.7502 0.7458 0.7426 0.7373 0.7297 0.7244 0.7171 0.7098 0.7025 0.6942	0.9983 0.9628 0.9265 0.8991 0.8861 0.8745 0.8641 0.8572 0.8526 0.8468 0.8399 0.8330 0.8239 0.8114 0.8012	L 0.8293 0.8009 0.7729 0.7466 0.7348 0.7241 0.7199 0.7136 0.7085 0.7033 0.6981 0.6908 0.6845 0.6763 0.6701 0.6630	0.9454 0.9106 0.8788 0.8522 0.8362 0.8247 0.8190 0.8156 0.8099 0.8065 0.7964 0.7930 0.7806 0.7717 0.7630	L 0.8108 0.7860 0.7617 0.7250 0.7135 0.7041 0.7020 0.6926 0.6916 0.6843 0.6812 0.6812 0.6709 0.6617 0.6556 0.6454	0.9092 0.8856 0.8394 0.8188 0.8097 0.7995 0.7995 0.7905 0.7905 0.7826 0.7748 0.7671 0.7584 0.7697 0.7389
22.25 22.50 22.75 23.00 23.25 23.50 23.75 24.00 24.25	0.8541 0.8484 0.8334 0.8220 0.8050 0.7914 0.7735 0.7604 0.7440	0.9975 0.9815 0.9693 0.9547 0.9414 0.9197 0.8971 0.8772 0.8576	0.6942 0.6848 0.6745 0.6612 0.6500 0.6389 0.6257 0.6166 0.6046	0.7910 0.7787 0.7676 0.7611 0.7458 0.7297 0.7139 0.6973 0.6848	0.6630 0.6517 0.6426 0.6366 0.6265 0.6163 0.5973 0.5883 0.5763	0.7532 0.7455 0.7380 0.7295 0.7136 0.7001 0.6908 0.6763 0.6609	0.6454 0.6384 0.6273 0.6222 0.6121 0.5961 0.5871 0.5731 0.5621	0.7303 0.7187 0.7093 0.6989 0.6833 0.6740 0.6597 0.6485 0.6303

Table 4. Electron intensity incident on the photographic plate: h = 120.00 mm.

	I	c(1)	I_p	(2)	I _p	(3)	I _p	(4)
s	L	R	L	R	L	R	L	R
24.50 24.75 25.00 25.25 25.50 25.75 26.00 26.25 26.50 26.75 27.00 27.25 27.50 27.50 27.75 28.00 28.25 28.50 28.50 28.75 29.00	0.7280 0.7185 0.7070 0.7029 0.6987 0.6977 0.6946 0.6935 0.6914 0.6862 0.6810 0.6707 0.6656 0.6533 0.6453 0.6382 0.6382 0.6301 0.6230 0.6179	0.8392 0.8266 0.8186 0.8152 0.8118 0.8084 0.8061 0.8050 0.8027 0.7936 0.7936 0.7936 0.7768 0.7768 0.7713 0.7614 0.7560 0.7473 0.7397 0.7333 0.7226	0.5966 0.5866 0.5836 0.5806 0.5776 0.5776 0.5776 0.5756 0.5726 0.5706 0.5706 0.5596 0.5596 0.5596 0.5526 0.5466 0.5416 0.5346 0.5296 0.5236 0.5186	0.6714 0.6632 0.6561 0.6500 0.6500 0.6429 0.6409 0.6399 0.6328 0.6328 0.6328 0.6328 0.6196 0.6136 0.6086 0.6046 0.5946 0.5896 0.5846 0.5796	0.5683 0.5623 0.5563 0.5543 0.5523 0.5503 0.5513 0.5503 0.5463 0.5463 0.5413 0.5293 0.5263 0.5193 0.5143 0.5143 0.5143 0.5143 0.5083 0.5013 0.4963 0.4903	0.6477 0.6386 0.6335 0.6265 0.6245 0.6234 0.6224 0.6214 0.6163 0.6113 0.6063 0.5983 0.5983 0.5923 0.5803 0.5803 0.5723 0.5613 0.5523	0.5551 0.5451 0.5391 0.5341 0.5321 0.5331 0.5331 0.5271 0.5261 0.5201 0.5131 0.5081 0.5081 0.5031 0.4981 0.4911 0.4861 0.4821 0.4761	R 0.6212 0.6131 0.6071 0.6031 0.6011 0.5971 0.5951 0.5911 0.5861 0.5821 0.5711 0.5671 0.5621 0.5581 0.5581 0.5581 0.5531 0.55401 0.5401 0.5351
29.25 29.50 29.75	0.6099 0.6059 0.5969	0.7174 0.7091 0.70 1 8	0.5136 0.5096 0.5036	0.5716 0.5656 0.5606	0.4843 0.4783 0.4733	0.5483 0.5433 0.5363	0.4701 0.4671 0.4571	0.5301 0.5221 0.5171
30.00 30.25	0.5909 0.5859	0.6945 0.6883	0.4996 0.4966	0.5516 0.5506	0.4703 0.4673	0.5313 0.5283	0.4531 0.4471	0.5121 0.5081

Table 4 (continued)

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····	I	c(1)	I _p	(2)	I ^{c(}	3)	I ^C	(4)
S	L	R	L	R	L	R	L	R
30.50 30.75 31.00 31.25 31.50 31.75 32.00 32.25 32.50 32.75 33.00 33.25 33.50 33.75 34.00 34.25 34.50 34.50 34.75 35.00 35.25 35.50	0.5809 0.5776 0.5779 0.5759 0.5719 0.5699 0.5619 0.5599 0.5549 0.5549 0.5489 0.5489 0.5449 0.5449 0.5449 0.5449 0.5449 0.5449 0.5449 0.5449 0.5419 0.5279 0.5229 0.5179 0.5109 0.5079	0.6831 0.6779 0.6758 0.6789 0.6789 0.6789 0.6748 0.6717 0.6655 0.6655 0.6605 0.6605 0.6544 0.6503 0.6422 0.6382 0.6382 0.6281 0.6250 0.6220 0.6159 0.6119	0.4946 0.4926 0.4916 0.4906 0.4906 0.4896 0.4876 0.4856 0.4856 0.4756 0.4756 0.4756 0.4756 0.4756 0.4756 0.4566 0.4516 0.4526 0.4516 0.4516 0.4486 0.4406	0.5466 0.5446 0.5426 0.5426 0.5396 0.5396 0.5396 0.5356 0.5336 0.5336 0.5336 0.5336 0.5336 0.5276 0.5226 0.5186 0.5156 0.5126 0.5126 0.5096 0.5026 0.5026 0.4996 0.4976 0.4936	0.4663 0.4623 0.4623 0.4613 0.4593 0.4593 0.4573 0.4573 0.4553 0.4553 0.4493 0.4493 0.4493 0.4493 0.4393 0.4393 0.4313 0.4283 0.4273 0.4223 0.4193 0.4163 0.4143	0.5223 0.5213 0.5203 0.5183 0.5173 0.5163 0.5113 0.5113 0.5063 0.5013 0.4943 0.4903 0.4903 0.4813 0.4723 0.463 0.463 0.463 0.4613 0.4583	0.4471 0.4451 0.4431 0.4431 0.4421 0.4391 0.4391 0.4381 0.4351 0.4321 0.4321 0.4301 0.4221 0.4211 0.4211 0.4121 0.4091 0.4091 0.4001 0.3991 0.3951	0.5041 0.5021 0.5011 0.5001 0.4981 0.4961 0.4961 0.4901 0.4851 0.4851 0.4851 0.4751 0.4751 0.4661 0.4631 0.4591 0.4511 0.4451
35.75 36.00 36.25	0.5049 0.5019 0.4999	0.6079 0.6049 0.6029	0.4396 0.4376 0.4366	0.4916 0.4906 0.4886	0.4123 0.4113 0.4103	0.4553 0.4543 0.4533	0.3931 0.3911 0.3901	0.4411 0.4401 0.4371

Table 4 (continued).

	I ^{c(}	(1)	I ^{c(}	2)	I ^{c(}	3)	I ^{c(}	(4)
S	L	R	L	R	L	R	L	R
36.50	0.4999	0.6009	0.4356	0.4896	0.4093	0.4533	0.3901	0.4381
36.75	0.4989	0.5999	0.4346	0.4886	0.4073	0.4513	0.3891	0.4361
37.00	0.4969	0.5979	0.4336	0.4876	0.4083	0.4503	0.3891	0.4351
37.25	0.4949	0.5959	0.4316	0.4876	0.4063	0.4483	0.3861	0.4321
37.50	0.4919	0.5939	0.4306	0.4846	0.4043	0.4463	0.3851	0.4331
37.75	0.4899	0.5909	0.4276	0.4836	0.4013	0.4463	0.3821	0.4301
38.00	0.4859	0.5879	0.4246	0.4806	0.3993	0.4423	0.3801	0.4281
38.25	0.4809	0.5839	0.4216	0.4786	0.3973	0.4403	0.3781	0.4251
38.50	0.4769	0.5799	0.4196	0.4756	0.3943	0.4373	0.3751	0.4231
38.75	0.4739	0.5759	0.4166	0.4736	0.3913	0.4343	0.3721	0.4211
39.00	0.4709	0.5729	0.4136	0.4706	0.3893	0.4323	0.3701	0.4181
39.25	0.4669	0.5669	0.4116	0.4666	0.3873	0.4293	0.3671	0.4161
39.50	0.4649	0.5639	0.4076	0.4646	0.3843	0.4263	0.3641	0.4141
39.75	0.4619	0.5619	0.4066	0.4616	0.3813	0.4243	0.3621	0.4121
40.00	0.4589	0.5599	0.4036	0.4597	0.3793	0.4223	0.3601	0.4101
40.25	0.4569	0.5579	0.4026	0.4586	0.3773	0.4203	0.3571	0.4091
40.50	0.4549	0.5559	0.3996	0.4566	0.3763	0.4203	0.3541	0.4071
40.75	0.4519	0.5549	0.3976	0.4546	0.3743	0.4173	0.3531	0.4051
41.00	0.4489	0.5539	0.3966	0.4536	0.3733	0.4153	0.3511	0.4041
41.25	0.4479	0.5479	0.3956	0.4526	0.3713	0.4143	0.3501	0.4031
41.50	0.4449	0.5469	0.3936	0.4516	0.3683	0.4143	0.3491	0.4021
41.75	0.4429	0.5439	0.3926	0.4516	0.3673	0.4143	0.3471	0.4021
42.00	0.4409	0.5429	0.3916	0.4496	0.3663	0.4133	0.3451	0.4011
42.25	0.4409	0.5429	0.3896	0.4496	0.3643	0.4113	0.3441	0.4001

Table 4 (continued).

	I ^c p	(1)	I ^{c(}	2)	I ^{c(}	3)	I ^{c(}	4)
S	L	R	L	R	L	R	L	R
42.50 42.75 43.00 43.25 43.50 43.75 44.00 44.25 44.50 44.75 45.00 45.25 45.50 45.75 46.00 46.25 46.50 46.25 46.50 46.75 47.00 47.25 47.50 47.50 48.00 48.25	0.4409 0.4379 0.4359 0.4339 0.4309 0.4269 0.4239 0.4199 0.4179 0.4179 0.4179 0.4179 0.4179 0.4059 0.4059 0.4059 0.4059 0.4059 0.4059 0.4059 0.4059 0.4059 0.4059 0.3969 0.3969 0.3959 0.3959 0.3929 0.3909	0.5429 0.5429 0.5429 0.5399 0.5399 0.5329 0.5269 0.5269 0.5269 0.5229 0.5229 0.5229 0.5229 0.5229 0.5129 0.5159 0.5159 0.5159 0.5159 0.5159 0.5159 0.5159 0.5119 0.5119 0.5119 0.5119	0.3896 0.3876 0.3866 0.3816 0.3806 0.3776 0.3756 0.3746 0.3716 0.3716 0.376 0.3746 0.3716 0.3686 0.3666 0.3656 0.3656 0.3616 0.3596 0.3586 0.3566 0.3566 0.3526	0.4496 0.4486 0.4456 0.4456 0.4446 0.4416 0.4406 0.4396 0.4376 0.4376 0.4336 0.4336 0.4336 0.4336 0.4336 0.4336 0.4296 0.4296 0.426 0.4246 0.4246 0.4246 0.4226 0.4226 0.4216	0.3633 0.3623 0.3613 0.3583 0.3563 0.35533 0.3513 0.3493 0.3493 0.3443 0.3433 0.3413 0.3403 0.3383 0.3373 0.3363 0.3323 0.3283 0.3283 0.3283 0.3283 0.3283 0.3283 0.3283 0.3283 0.3283 0.3283 0.3263 0.3253	0.4113 0.4093 0.4093 0.4083 0.4063 0.4053 0.4023 0.4023 0.4023 0.4023 0.4023 0.4023 0.3993 0.3993 0.3963 0.3933 0.3903 0.3883 0.3883 0.3883 0.3883 0.3883 0.3883 0.3883 0.3883 0.3883 0.3863 0.38	0.3421 0.3411 0.3401 0.3381 0.3371 0.3351 0.3321 0.321 0.321 0.3271 0.3251 0.3251 0.3241 0.3221 0.3221 0.3201 0.3221 0.3201 0.3181 0.3171 0.3161 0.3151 0.3141 0.3121 0.3101	0.4001 0.3971 0.3971 0.3971 0.3951 0.3931 0.3921 0.3911 0.3891 0.3871 0.3871 0.3851 0.3821 0.3821 0.3821 0.3821 0.3811 0.3801 0.3771 0.3771 0.3771 0.3761

Table 4 (continued)

	I ^C p	(1)	I	c(2)	Ip	(3)	I _F	(4)
S	P	R	L	R	L	R	L	R
48.50 48.75 49.00 49.25 49.50 49.75	0.3889 0.3879 0.3849 0.3819 0.3809 0.3789	0.5099 0.5089 0.5069 0.5059 0.5049 0.5019	0.3516 0.3506 0.3496 0.3486 0.3466 0.3446	0.4206 0.4196 0.4196 0.4196 0.4176 0.4166	0.3243 0.3233 0.3203 0.3193 0.3183 0.3163	0.3853 0.3843 0.3833 0.3823 0.3823 0.3813	0.3081 0.3071 0.3051 0.3051 0.3031 0.3011	0.3761 0.3751 0.3741 0.3751 0.3751 0.3741 0.3731

Table 4 (continued).

L Left branch

R Right branch

S	$I_{E}^{T}(s)_{Exp}$	$I_{E}^{T}(s)_{Theor}$	S	${}^{\mathrm{T}}_{\mathrm{E}}(\mathrm{s})_{\mathrm{Exp}}$	${}^{\mathrm{T}}_{\mathrm{E}}$ (s) $_{\mathrm{Theor}}$
s 0.00 0.25 0.75 1.00 1.25 1.75 2.25 2.50 5.75 0.25 0.25 0.25 0.25 0.25 0.25 0.25 0.2	-41.0 -179.0 -316.0 -369.0 -448.0 -493.0 -530.0 -556.0 -528.0 -528.0 -528.0 -528.0 -127.0 93.0 326.0 527.0 654.0 702.0 635.0 -316.0 -355.0 -317.0 -212.0 -316.0 -355.0 -212.0 -221.0	0.0 240.7 441.2 593.0 645.9 622.0 530.0 394.2 242.2 97.3 -25.0 -121.8 -199.9 -269.2 -337.9 -408.7 -473.8 -515.8 -513.6 -450.2 -317.8 -515.8 -513.6 -450.2 -317.8 -513.6 -450.2 -317.8 -52.9 508.0 309.8 95.4 -100.4 -251.3 -347.7 -392.2 -399.5 -387.4 -370.0 -353.5 -334.0 -298.8 -233.1	s 10.50 10.75 11.00 11.25 11.50 12.50 12.50 12.50 13.00 13.50 13.75 14.02 14.50 15.50 15.75 16.05 17.00 17.50 17.50 17.50 18.25 19.00 19.50 19.50 19.50 20.25 20.50 20.50 20.50	$\begin{array}{c} -151.0 \\ -8.0 \\ 154.0 \\ 316.0 \\ 454.0 \\ 547.0 \\ 557.0 \\ 447.0 \\ 293.0 \\ 110.0 \\ -145.0 \\ -352.0 \\ -501.0 \\ -590.0 \\ -590.0 \\ -599.0 \\ -599.0 \\ -599.0 \\ -599.0 \\ -291.0 \\ -291.0 \\ -291.0 \\ -291.0 \\ -291.0 \\ -291.0 \\ -291.0 \\ -291.0 \\ -514.0 \\ 45.0 \\ 118.0 \\ 220.0 \\ 327.0 \\ 402.0 \\ 445.0 \\ 476.0 \\ 373.0 \\ 269.0 \\ 89.0 \\ -124.0 \\ -303.0 \\ -455.0 \\ -514.0 \\ -514.0 \\ -514.0 \\ -514.0 \\ -459.0 \\ -367.0 \\ -244.0 \\ -116.0 \\ 5.0 \\ \end{array}$	-126.5 21.6 198.6 380.1 534.4 630.4 645.3 571.4 418.0 210.1 -16.9 -226.4 -387.6 -482.1 -507.5 -474.2 -401.9 -312.3 -222.8 -142.7 -72.0 -3.4 72.2 160.8 260.9 362.1 446.5 492.8 483.3 408.8 273.2 93.0 -105.0 -289.3 -430.8 509.5 -517.7 -461.8 -358.3 -230.0 -99.6 15.3

Table 5. Experimental and theoretical $I_E^T(s)$ curves.

Table 5 (continued).

S	$I_{E}^{T}(s)_{Exp}$	I _E (s) _{Theor}	S	$I_{E}^{T}(s)_{Exp}$	I _E (s) _{Theor}
42.00	-47.0	2.0	46.00	-75.0	-102.8
42.25 42.50	21.0 83.0	52.0 99.5	46.25 46.50	-78.0 -69.0	-85.4 -64.4
42.75 43.00	131.0 188.0	138.1 162.0	46.75	-66.0 1.0	-40.9 -15.5
43.25 43.50	188.0 139.0	167.4 153.3	47.25 47.50	27.0 21.0	11.1 38.1
43.75 44.00 44.25	64.0 7.0	121.9 78.1	47.75 48.00	77.0 81.0	63.7 85.6
44.25 44.50 44.75	18.0 -18.0	28.4 -20.5 -62.5	48.25 48.50	117.0 104.0	101.0 107.2
45.00	-107.0 -74.0 -66.0	-93.8 -112.4	48.75 49.00 49.25	118.0 77.0 112.0	102.7 87.0 61.7
45.50 45.75	-85.0 -79.0	-112.4 -118.8 -114.7	49.50	64.0 7.0	29.7
	-13.0	~↓↓~~● (11.52	1.0	-5.0

Table 5 (continued).

		<u></u>			
S	$I_{E}^{a}(s)_{Exp}$	$I_E^{a(1)}(s)_{Exp}$	$I_E^{a(2)}(s)_{Exp}$	$I_E^{a(3)}(s)_{Exp}$	$I_{E}^{a(4)}(s)_{Exp}$
2.50	-41.0	-11.2	-1 7 . 5	-7 7.7	-15.5
2.75	-179.0	-100.0	-91.1	-170.0	-96.0
3.00	-316.0	-188.0	-164.0	-257.0	-1 72.0
3.25	-369.0	-217.0	-1 93.0	-287.0	-205.0
3.50	-448.0	-266.0	-235.0	-323.0	-242.0
3.75	-493.0	-296.0	-258.0	-354.0	-269.0
4.00	-530.0	-317.0	-280.0	-376.0	-291.0
4.25	-556.0	-327.0	-292.0	-390.0	-3 05.0
4.50	-528.0	-305.0	-275.0	-368.0	-294.0
4.75	-450.0	-262.0	-237.0	-321.0	-246.0
5.00	-317.0	-174.0	-167.0	-232.0	-168.0
5.25	-127.0	-56.3	- 67.4	-118.0	-65.1
5.50	93.0	80.3	56.4	21.9	60.6
5.75	326.0	213.0	178.0	173.0	189.0
6.00	527.0	329.0	284.0	312.0	302.0
6.25	654.0	402.0	354.0	392.0	379.0
6.50	703.0	428.0	383.0	427.0	402.0
6.75	647.0	402.0	359.0	386.0	367.0
7.00	543.0	334.0	309.0	325.0	309.0
7.25	337.0	211.0	199.0	210.0	192.0
7.50	121.0	91.7	74•9	70.0	68.8
7.75	-58.0	-15.2	-21.3	-58.0	-22.7
8.00	-212.0	-110.0	-99.0	-164.0	-110.0
8.25	-316.0	-175.0	-157.0	-226.0	-176.0
8,50	-355.0	-198.0	-187.0	-249.0	-198.0
8.75	-374.0	-216.0	-195.0	-264.0	-206.0
9.00	-368.0	-212.0	-194.0	-260.0	-207.0 -190.0
9.25	-354.0	-205.0	-185.0	-257.0	-1 87 . 0
9.50	-346.0	-207.0	-183.0	-253.0 -238.0	-181.0
9.75	-327.0	-181. 0 -16 4.0	-177.0 -152.0	-205.0	-159.0
10.00	-288.0	-142.0	-123.0	-161.0	-126.0
10.25	-235.0 -133.0	-80.5	-65.5	-103.0	-66.1
10.50	-8.0	6.7	-6.4	-16.5	-7.9
10.75 11.00	1 52.0	88.8	79.9	86.4	87.5
11.25	333.0	202.0	170.0	198.0	185.0
	461.0	266.0	234.0	279.0	266.0
11.50	557.0	312.0	285.0	356.0	306.0
11.75 12.00	573.0	327.0	300.0	349.0	314.0
12.00	486.0	281.0	226.0	304.0	269.0
12.50	323.0	214.0	167.0	190.0	183.0
12.75	131.0	70.6	69.3	63.2	71.4
*-•17	•••0	1010	- / • •	<u> </u>	

Table 6. Experimental $I_E^a(s)$ and $I_E^{a(i)}(s)$ curves (h = 478.00 mm).

Table 6 (continued).

S	$I_{E}^{a}(s)_{Exp}$	$I_E^{a(1)}(s)_{Exp}$	$I_E^{a(2)}(s)_{Exp}$	$I_E^{a(3)}(s)_{Exp}$	$I_E^{a(4)}(s)_{Exp}$
13.00	-124.0	-69.2	-77.8	-96.8	-75.5 -182.0
13.25	-333.0	-196.0	-169.0	-242.0	
13.50	-485.0	-263.0	-258.0	-351.0	-263.0
13.75	-585.0	-328.0	-299.0	-406.0 -416.0	-322.0 -334.0
14.00	-607.0	-351.0	-321.0	-	
14.25	-576.0	-327.0	-314.0	-407.0	-300.0
14.50	-495.0	-291.0	-277.0	-326.0	-273.0
14.75	-390.0	-231.0	-224.0	-261.0	-214.0
15.00	-292.0	-179.0	-181.0	-195.0	-141.0
15.25	-225.0	-145.0	-153.0	-151.0	-100.0
15.50	-148.0	-82.7	-110.0	-107.0	-71.4
15.75	-57.0	-34.2	-56.1	-45.6	-26.5
16.00	43.0	19.5	19.7	13.2	17.0
16.25	118.0	76.8	59·4	62.0	61.1
16.50	236.0	133.0	97.8	139.0	127.0
1 6 . 75	363.0	196.0	180.0	224.0	200.0
17.00	438.0	234.0	241.0	286.0	221.0
17.25	474.0	274.0	256.0	279.0	244.0
17.50	494.0	260.0	261.0	305.0	272.0
17.75	436.0	229.0	207.0	296.0	239.0
18.00	304.0	1 67.0	149.0	199.0	158.0
18.25	113.0	62.1	62.8	67.1	48.2
18.50	-101.0	-54.1	-67.4	-79.7	-46.0
18.75	-293.0	-140.0	-154.0	-198.0	-203.0
19.00	-441.0	-258.0	-231.0	-307.0	-232.0
1 9.25	-528.0	-303.0	-268.0	-372.0	-281.0
19.50	-535.0	-325.0	-268.0	-375.0	-279.0
19.75	-514.0	-309.0	-242.0	-371.0	-290.0
20.00	-395.0	-255.0	-191.0	-303.0	-201.0
20.25	-290.0	-197.0	-154.0	-233.0	-146.0
20.50	-163.0	-138.0	-82.7	-153.0	-85.3
20.75	-24.0	-45.7	-31.3	-41.7	-31.3

		~			
S	$I_{E}^{b}(s)_{Exp}$	$I_{\rm E}^{b(1)}$ (s) $_{\rm Exp}$	$I_{E}^{b(2)}$ (s) $_{Exp}$	$I_{E}^{b(3)}$ (s) $_{Exp}$	$I_{E}^{b(4)}$ (s) E_{xp}
10.25	-226	-658	- 768	-520	-560
10,50	- 168	-390	-586	-395	-390
10.75	- 7	-10	0	5	-7
11.00	155	439	426	405	474
11.25	300	768	834	818	869
11.50	451	1122	1308	1236	1174
11.75	543	1364	1533	1436	1405 1428
12.00	552 1/22	1403 1038	1572 1189	1371 1106	1438 1192
12.25	433 262	564	823	627	699
12.50 12.75	89 89	219	254	215	228
13.00	-1 66	-455	-457	-396	-3 89
13.25	-370	-909	-1190	-858	-831
13.50	-508	-1237	-1528	-1263	-1175
13.75	-592	-1404	-1735	-1455	-1482
14.00	-594	-1490	-1 681	-1484	-1424
14.25	- 537	-1354	- 1544	-1376	-1234
1 4.50	-450	-1149	-1313	-1142	-1065
14.75	-405	-1016	-1130	-1013	-983
15.00	-291	-753	-854	-749	-690 -484
15.25	-207	-594	-615	-492	
15.50	-134	-390 -221	- 370 -154	-343 -146	-352 -113
15.75 16.00	-50 46	-221 55	142	1 18	-115
16.25	1 18	197	326	308	277
16.50	204	396	564	490	501
16.75	290	602	872	656	712
17.00	385	852	1110	880	9 1 6
17.25	432	955	1253	969	1054
17.50	468	1066	1356	1039	1146
17.75	343	804	940 (a)	729	881 51-0
18.00	234	479	698	495	542 151
18.25	65 -1 48	60 -348	301 -338	31 -500	-394
18.50 18.75	-313	-340 -733	-820	-873	-809
19.00	-463	-1109	-1276	-1267	-1078
19.25		-1188	-1450	-1320	-1208
19.50	-503	-1191	-1421	-1289	-1253
19.75	-430	-937	-1256	-1204	-1 042
20.00	-339	-770	-1023	- 952	-813
20.25	-198	-477	-602	-613	-462
20.50	-69	-166	-215	-315	-147

Table 7. Experimental $I_E^b(s)$ and $I_E^{b(i)}(s)$ curves (h = 192.07 mm).

Table 7 (continued).

.

S	$I_{E}^{b}(s)_{Exp}$	$I_{E}^{b(1)}(s)_{Exp}$	$I_{E}^{b(2)}$ (s) $_{Exp}$	$I_{E}^{b(3)}(s)_{Exp}$	${ m I}_{ m E}^{ m b(4)}$ (s) ${ m Exp}$
			.		
20.75	40	68	156	- 94	81
21.00	123	304	357	152	268
21.25	182	389 521	481 643	376	431 618
21.50 21.75	251 271	534 597	754	581 564	665
22.00	293	654	746	730	657
22.25	351	752	983	823	845
22.50	332	714	907	762	851
22.75 23.00	332 293	731 658	841 72 1	768 680	918 855
23.00	243	555	545	610	718
23.50	118	212	223	379	342
23.75	-9	-89	-208	115	142
24.00	-128	-332	-513	-233	-140
24.25	-276 270	-796	-860 -1066	-514	-453 -669
24.50 24.75	-370 -403	-974 -959	-1250	-839 -884	-009 -743
25.00	-416	-1039	-1270	-885	-721
25.25	-365	- 864	-1 065	-775	-684
25.50	-231	-594	- 674	-468	-308
25.75 26.00	-81 38	-244 94	-150 115	-132 146	-4 347
26.00	140	335	491	372	545
26.50	229	605	725	629	726
26.75	304	773	918	973	908
27.00	337	939	1009	886 0ali	975
27.25 27.50	300 264	766 655	1016 942	804 684	916 882
27.75	236	5 3 0	853	656	834
28.00	226	615	790	551	878
28.25	204	549	750	523	821
28.50	126	414	530	369	582 1.28
28.75 29.00	91 23	319 118	536 236	270 2 3 0	438 311
29.25	-65	-66	-46	32	72
29.50	-161	-321	-285	-113	-186
29.75	-236	-527	-531	-391	-256
30.00	-298	-641 -861	-745	-516 676	-420 -560
30.25 30.50	-360 -328	-829	-803 -670	-676 -649	-500 -510
30.75	-262	-584	-403	-626	-396
31.00	-175	-500	-92	-416	-166

				····	
S	$I_{E}^{b}(s)_{Exp} I_{E}^{b}$	¹⁾ (s) _{Exp}	$I_{\rm E}^{b(2)}$ (s) $_{\rm Exp}$	$I_{E}^{b(3)}$ (s) $_{Exp}$	$I_{E}^{b(4)}(s)_{Exp}$
31.25	-80	- 125	205	-253	-42
31.50	25	38	601	-28	202
	155	306	823	361	620
31.75	222	518	1011	435	723
32.00		567	1082	+35 554	
32.25	256			610	851
32.50	261	549	1091		775
32.75	259	581	1095	561	754
33.00	210	441	899	494	624
33.25	194	494	922	308	541
33.50	133	446	754	96	344
33.75	58	168	431	137	168
34.00	0	- 34	336	-70	65
34.25	-56	-16	45	- 152	-157
34.50	- 94	-222	-59	-288	-101
34.75	-173	-441	-170	- 425	- 379
35.00	-182	-368	-338	-372	- 467
35.25	-202	-470	-244	- 484	- 556
35.50	- 245	-472	-482	- 587	-620
35.75	-262	-527	-520	-663	-663
36.00	-244	-438	-577	-681	- 558
36.25	- 225	-350	-562	-526	-642
36.50	-166	-227	-318	-419	-515
36.75	-41	82	60	-212	-190
37.00	42	242	266	136	-24
37.25	121	275	543	251	295
37.50	143	404	527	465	238
37.75	141	372	431	520	298
38.00	138	401	401	545	223
38.25	109	339	262	<u>44</u> 8	242
38.50	29	128	-20	333	28
38.75	-26	-25	-33	25	<u>-</u> 45
39.00	-45	-86	-182	38	-28
39.25	-128	-293	-456	- 84	-229
39.50	- 161	-407	-540	-133	-376
39.75	-213		-569	-324	- 456
	-202	-398	-585	-411	-437
40.00	-202 -209	-390	-909 -674	-411 -442	-481
40.25				-442 -416	
40.50	-182	-241	-583		-330
40.75	-165	-376	-568	-337	-142
41.00	-162	-389	-436	-373	-66
41.25	-127	-332	-210	-332	-35
41.50	-98	-110	83	-241	-198

S	$I_{E}^{b}(s)_{Exp}$	$I_{E}^{b(1)}$ (s) $_{Exp}$	$I_{E}^{b(2)}(s)_{Exp}$	$I_{E}^{b(3)}$ (s) $_{Exp}$	$I_{\rm E}^{b(4)}$ (s) $_{\rm Exp}$
41.75	-38	30	-35	13	48
42.00	-26	97	-70	78	89

Table 7 (continued).

S	$I_{\rm E}^{\rm c}(s)_{\rm Exp}$	S	$I_{E}^{c}(s)_{Exp}$	S	$I_{E}^{c}(s)_{Exp}$
18.50	1 34.0	29.00	12.0	39.50	-150.0
18.75	-23.0	29.25	-59.0	39.75	-172.0
19.00	-207.0	29.50	-137.0	40.00	-1 95 . 0
19.25	-351.0	29.75	-236.0	40.25	-193.0
19.50	-361.0	30.00	-294.0	40.50	-176.0
19.75	-336.0	30.25	-306.0	40.75	-189.0
20.00	-228.0	30.50	-311.0	41.00	-164.0
20.25	-123.0	30.75	-282.0	41.25	-153.0
20.50	-55.0	31.00	-181.0	41.50	-113.0
20.75	50.0	31.25	-61.0	41.75	-81.0
21.00	142.0	31.50	24.0	42.00	-54.0
21.25	225.0	31.75	145.0	42.25	21.0
21.50	236.0	32.00	227.0	42.50	83.0
21.75	281.0	32.25	254.0	42.75	131.0
22.00	331.0	32.50	270.0	43.00	188.0 188.0
22.25	401.0	32.75	289.0	43.25	139.0
22.50	359.0	33.00	243.0	43.50 43.75	64.0
22.75	327.0	33.25	141.0 110.0	43.19	7.0
23.00	356.0	33.50	24.0	44.25	18.0
23.25	272.0 160.0	33•75 34•00	-24.0	44.50	-18.0
23.50 23.75	9.0	34.25	-100.0	44.75	-107.0
24.00	-95.0	34.50	-111.0	45.00	-74.0
24.25	-260.0	34.75	-168.0	45.25	-66.0
24.50	-412.0	35.00	-220.0	45.50	-85.0
24.75	-444.0	35.25	-280.0	45.75	-79.0
25.00	-415.0	35.50	-292.0	46.00	-75.0
25.25	-370.0	35.75	-305.0	46.25	-78.0
25.50	-276.0	36.00	-263.0	46.50	-69.0
25.75	-1 35.0	36.25	-245.0	46.75	-66.0
26.00	10.0	36.50	-97.0	47.00	1.0
26.25	166.0	36.75	-7.0	47.25	27.0 21.0
26.50	267.0	37.00	99.0	47.50	77.0
26.75	327.0	37.25	117.0 152.0	47.75 48.00	80.0
27.00	309.0	37.50	149.0	48.25	117.0
27.25	235.0 240.0	37•75 38.00	149.0	48.50	104.0
27.50	182.0	38.25	111.0	48.75	118.0
27.75 28.00	183.0	38.50	87.0	49.00	77.0
28.25	119.0	38.75	47.0	49.25	112.0
28.50	92.0	39.00	2.0	49.50	64.0
28.75	78.0	39.25	-85.0	49.75	-7.0
	,			- • •	

Table 8. Experimental $I_E^c(s)$ curve (h = 120.00 mm).

r	rD'(r) Exp	rD'(r) Theor	r	rD'(r) _{Exp}	rD'(r) _{Theor}
$\begin{array}{c} 0.00\\ 0.04\\ 0.08\\ 0.12\\ 0.16\\ 0.20\\ 0.24\\ 0.28\\ 0.32\\ 0.36\\ 0.44\\ 0.52\\ 0.56\\ 0.64\\ 0.55\\ 0.60\\ 0.68\\ 0.72\\ 0.76\\ 0.80\\ 0.96\\ 1.00\\ 1.24\\ 1.28\\ 1.32\\ 1.36\\ 1.40\\ 1.24\\ 1.28\\ 1.32\\ 1.36\\ 1.40\\ 1.44\\ 1.52\\ 1.56\\ 1.60\\ \end{array}$	$\begin{array}{c} 0.0\\ -9.9\\ -13.1\\ -13.7\\ -16.7\\ -15.6\\ -2.1\\ 12.8\\ 13.8\\ 5.5\\ -0.1\\ -3.9\\ -10.1\\ -3.9\\ -10.1\\ -3.9\\ -10.1\\ -3.9\\ -10.1\\ -3.9\\ -10.1\\ -3.9\\ -0.1\\ -3.9\\ -0.1\\ -3.9\\ -0.1\\ -3.9\\ -0.1\\ -3.9\\ -10.1\\$	$\begin{array}{c} 0.0\\ 0.0\\ 0.0\\ 0.0\\ 0.0\\ 0.0\\ 0.0\\ 0.0$	1.68 1.72 1.76 1.80 1.84 1.96 2.04 2.16 2.04 2.22 2.22 2.22 2.22 2.22 2.22 2.22	$\begin{array}{c} 0.4\\ 2.5\\ 3.2\\ 2.0\\ 0.4\\ -0.9\\ -1.4\\ -2.1\\ -3.3\\ -2.5\\ 4.5\\ 20.9\\ 44.1\\ 60.3\\ 54.5\\ 20.9\\ 44.1\\ 60.3\\ 54.5\\ 30.9\\ 9.2\\ -3.8\\ -5.4\\ $	$\begin{array}{c} 0.0\\ 0.0\\ 0.0\\ 0.0\\ 0.0\\ 0.0\\ 0.0\\ 0.0$
1.64	-0.5	0.0	3. 32	0.7	0.0

Table 9. Experimental and theoretical rD'(r) curves.

r	rD'(r) _{Exp}	rD'(r) _{Theor}	r	rD'(r) _{Exp}	rD'(r) _{Theo} r
3.36	-0,3	0.0	4.20	-1.1	0.0
3.40	-0.1	0.0	4.24	-0.3	0.0
3.44	0.0	0.0	4.28	-0.3	0.0
3.48	-0.1	0.0	4.32	-1.3	0.0
3.52	0.1	0.0	4.36	-1.6	0.0
3.56	1.1	0.0	4.40	-0.9	0.0
3.60	2.0	0.0	4.44	-0.1	0.0
3.64	1.7	0.0	4.48	0.1	0.0
3.68	0.5	0.0	4.52	0.1	0.0
3.72	-0.1	0.0	4.56	-0.1	0.0
3.76	-0.1	0.0	4.60	-0.7	0.0
3.80	-0,1	0.0	4.64	-1.1	0.0
3.84	0.1	0.0	4.68	-0.7	0.0
3.88	0.3	0.0	4.72	-0.5	0.0
3.92	0.9	0.0	4.76	-0.9	0.0
3.96	1.3	0.0	4.80	-1.1	0.0
4.00	0.8	0.0	4.84	-0.7	0.0
4.04	-0.2	0.0	4.88	-0.4	0.0
4.08	-0.7	0.0	4.92	-0.1	0.0
4.12	-0.8	0.0	4.96	-0.4	0.0
4.16	-1.2	0.0	5.00	0.0	0.0

Table 9 (continued).

D	δ	D	δ	D	δ
_					0-06
0.6200	.0001	1.0400	.0624	1.4600	.2726
0.6300	.0002	1.0500	.0658	1.4700	.2790
0.6400	.0003	1.0600	.0693	1.4800	.2854
0.6500	.0004	1.0700	.0728	1.4900	.2919 .2984
0.6600	.0006	1.0800	.0764	1.5000	
0.6700	.0008	1.0900	.0800 .0838	1.5100 1.5200	.3050 .3117
0.6800	.0011	1.1000	.0030	1.5300	.3185
0.6900	.0015 .0019	1.1100 1.1200	.0921	1.5400	.3253
0.7000 0.7100	.0019	1.1300	.0964	1.5500	.3321
0.7200	.0025	1.1400	.1007	1.5600	.3390
0.7300	.0021	1.1500	.1051	1.5700	.3460
0.7400	.0041	1.1600	.1095	1.5800	.3531
0.7500	.0050	1.1700	.1141	1.5900	.3602
0,7600	.0059	1.1800	.1187	1.6000	.3674
0.7700	.0069	1.1900	.1235	1.6100	.3747
0.7800	.0081	1.2000	.1283	1.6200	.3821
0.7900	.0094	1.2100	.1331	1.6300	.3895
0.8000	.0107	1.2200	.1380	1.6400	.3969
0.8100	.0121	1.2300	.1429	1.6500	.4043
0.8200	.0135	1.2400	.1479	1.6600	.4119
0.8300	.0150	1.2500	.1529	1.6700	.4195
0.8400	.0165	1.2600	.1580	1.6800	.4272
0.8500	.0180	1.2700	.1632	1.6900	.4350
0.8600	.0196	1.2800	.1684	1.7000	.4428
0.8700	.0213	1.2900	.1737	1.7100	.4506
0.8800	.0231	1.3000	.1790	1.7200	.4584
0.8900	.0250	1.3100	.1844	1.7300	.4663
0.9000	.0270	1.3200	.1898	1.7400	.4743
0.9100	.0290	1.3300	. 1953	1.7500	.4825
0.9200	.0311	1.3400	.2008	1.7600	.4907
0.9300	.0333	1.3500	.2064	1.7700	.4989
0.9400	.0355	1.3600	.2121	1.7800	.5072 .5156
0.9500	.0377	1.3700	.2179	1.7900 1.8000	.5241
0.9600	.0400 .0424	1.3800	,2237 2206	1.8100	.5326
0.9700 0.9800	.0424 .0450	1.3900 1.4000	.2296 .2356	1.8200	.5411
•	.0450 .0476	1.4100	.2390	1.8300	• 5497
0.9900 1.0000	.0478	1.4200	.2410	1.8400	.5584
1.0100	.0502	1.4300	.2539	1.8500	.5671
1.0200	.0561	1.4400	.2601	1.8600	.5758
1.0300	.0592	1.4500	.2663	1.8700	.5846
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Table 10. Blackness correction table (Oslo).

Table 11. Sector function: h = 478.00 mm.

Table 12. Sector function: h = 192.07 mm.

S	g(θ)	S	g(θ)	S	g(θ)
10.25	4744	21.00	13295	31.75	20707
10.50	4963	21.25	13444	32.00	20878
10.75	5226	21.50	13633	32.25	21063
11.00	5472	21.75	13792	32.50	21227
11.25	5705	22.00	13951	32.75	21412 [.]
11.50	5943	22.25	14159	33.00	21588
11.75	6184	22.50	14311	33.25	21788
12.00	6414	22.75	14488	33.50	21977
12.25	6613	23.00	14649	33.75	22144
1 2.50	6830	23.25	14836	34.00	22311
12.75	7049	23.50	14998	34.25	22466
13.00	7253	23.75	15169	34.50	22633
13.25	7494	24.00	1 5349	34.75	22803
13.50	7690	24.25	15503	35.00	22985
13.75	7907	24.50	15649	35.25	23168
14.00	8128	24.75	15822	35.50	23366
14.25	8338	25.00	15978	35.75	23538
14.50	8553	25.25	16161	36.00	23736
14.75	8725	25.50	16345	36.25	23899
15.00	8945	25.75	16521	36.50	24073
15.25	9147	26.00	16688	36.75	24288
15.50	9346	26.25	16876	37.00	24479
15.75	9559 0771	26.50	17033	37.25	24657
16.00	9774	26.75	17211	37.50	24836
16.25	9963	27.00	17391 17541	37.75	24990
16.50 16.75	10159 1 0340	27.25 27.50	1 7541 1 7702	38.00 38.25	25171 25353
17.00	10540 10539	27.75	17882	38.50	25524
17.25	10734	28.00	18055	38.75	25720
17.50	10944	28.25	18238	39.00	25907
17.75	11090	28.50	18422	39.25	26092
18.00	11268	28.75	18606	39.50	26267
18.25	11448	29.00	18769	39.75	26428
18,50	11602	29.25	18946	40.00	26631
18.75	11776	29.50	19121	40.25	26808
19.00	11951	29.75	19298	40.50	27014
19,25	12128	30.00	19464	40.75	27194
19.50	12311	30.25	19643	41.00	27373
19.75	12489	30.50	19822	41.25	27585
20.00	12645	30.75	20001	41.50	27767
20.25	12808	31.00	20170	41.75	27966
20.50	12980	31.25	20353	42.00	28137
20.75	13145	31.50	20524	42.25	28337
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S	g(θ)	S	g(θ)	S	g(θ)
18.50	44984	29.00	89385	39.50	126704
18.75	46111	29.25	90250	39.75	127612
19.00	47308	29.50	91049	40.00	128522
19.25	48480	29.75	9 1 957	40.25	129375
19.50	49689	30.00	92871	40.50 40.75	130380 131286
19.75 20.00	50 8 08 5 1 998	30.25 30.50	9 3 737 94562	40.75 41.00	132194
20.00	53038	30.90	954 3 8	41.00	133150
20.50	5 3 964	31.00	96363	41.50	134196
20.75	55087	31.25	97249	41.75	135065
21.00	56213	31.50	98140	42.00	136023
21.25	57256	31.75	99123	42.25	137077
21.50	58283	32.00	100025	42.50	137871
21.75	59381	32.25	100939	42.75	138930
22.00	60556	32.50	101779	43.00	139951
22.25	61812	32.75	102752	43.25	140935
22.50	62690	33.00	103611	43.50	141920
22.75	63681	33.25	104484	43.75	142755
23.00	64851	33.50	105296	44.00	143598
23.25	659 33 66980	33•75 34•00	10 6 155 107103	44.25 44.50	144655 145482
23.50 23.75	68026	34.00	107847	44.50 44.75	146438
24.00	69156	34.50	108679	45.00	147483
24.25	70184	34.75	109494	45.25	148531
24.50	71014	35.00	110323	45.50	149597
24.75	72130	35.25	111301	45.75	150588
25.00	73264	35.50	112228	46.00	151565
25.25	74217	35.75	113072	46.25	152484
25.50	75144	36.00	113967	46.50	153506
25.75	76249	36.25	114755	46.75	154397
26.00	77312	36.50	115777	47.00	155428 156426
26.25	78417 70406	36.75 37.00	116808	47.25 47.50	157441
26.50 26.75	79496 8056 3	37.25	117793 118657	47.75	158385
27.00	8 1 470	37.50	119533	48.00	159352
27.25	82428	37.75	120376	48.25	160427
27.50	83397	38.00	121433	48.50	161414
27.75	84349	38.25	122314	48.75	162419
28.00	85348	38.50	123299	49.00	163453
28.25	86349	38.75	124223	49.25	164487
28.50	87397	39.00	125060	49.50	165380
28.75	88448	39.25	125894	49.75	166405

Table 13. Sector function: h = 120.00 mm.

s	[(Z-F)/Z] _N	[(Z-F)/Z] _O	S	[(Z-F)/Z] _N	$\left[(Z-F)/Z\right]_{O}$
0.00	0.0000	0.0000	10.50	0.7985	0.8090
0.25	0.0093	0.0072	10.75	0.8013	0.8113
0.50	0.0240	0.0180	11.00	0.8039	0.8135
0.75	0.0460	0.0380	11.25	0.8064	0.8160
1.00	0.0770	0.0619	11.50	0.8090	0.8180
1.25	0.1140	0.0928	11.75	0.8117	0.8210
1.50	0.1595	0.1293	12.00	0.8140	0.8233
1.75	0.2031	0.1680	12.25	0.8166	0.8259
2.00	0.2495	0.2090	12.50	0.8193	0.8282
2.25	0.2959	0.2513	12.75	0.8217	0.8300
2.50	0.3421	0.2940	13.00	0.8242	0.8321
2.75	0.3880	0.3350	13.25	0.8267	0.8340
3.00	0.4300	0.3770	13,50	0.8287	0.8360
3.25	0.4694	0.4160	13.75	0.8314	0.8380
3.50	0.5030	0.4520	14.00	0.8335	0.8399
3.75	0.5340	0.4860	14.25	0.8360	0.8418
4.00	0.5650	0.5180	14.50	0.8385	0.8437
4.25	0.5928	0.5470	14.75	0.8410	0.8456
4.50	0.6160	0.5740	15.00	0.8435	0.8472
4.75	0.6373	0.5990	15.25	0.8462	0.8494
5.00	0.6550	0.6225	15.50	0.8484	0.8513
5.25	0.6719	0.6428	15.75	0.8510	0.8535
5.50	0.6875	0.6618	16.00	0.8535	0.8553
5.75	0.7003	0.6768	16.25	0.8559	0.8572
6.00	0.7110	0.6930	16.50	0.8580	0.8590
6.25	0.7220	0.7070	16.75	0.8600	0.8606
6.50	0.7310	0.7185	17.00	0.8620	0.8623
6.75	0.7387	0.7290	17.25	0.8645	0.8645
7.00	0.7447	0.7390	17.50	0.8665	0.8662
7.25	0.7509	0.7480	17.75	0.8690	0.8681
7.50	0.7560	0.7560	18.00	0.8715	0.8699
7.75	0.7613	0.7640	18.25	0.8738	0.8718
8.00	0.7660	0.7701	18.50	0.8760	0.8736
8.25	0.7700	0.7770	18.75	0.8785	0.8752
8.50	0.7740	0.7822	19.00	0.8810	0.8772
8.75	0.7780	0.7860	19.25	0.8830	0.8788
9.00	0.7820 0.7850	0.7900 0.7040	19.50	0.8855 0.8875	0.8806
9.25	0.7877	0.7940	19.75	0.8895	0,8823 0.8841
9•50 9•75	0.7900	0.7973 0.8003	20.00 20.25	0.8917	0.8860
10.00	0.7930	0.8039	20.29	0.8935	0.8878
10.25	0.7958	0.8060	20.90	0.8955	0.8895
10.27	0.1900	0.0000	20.12	0.0977	0.0099

Table 14. $[(Z-F/Z]_N \text{ and } [(Z-F)/Z]_O \text{ table.}$

Table 14 (continued).

s	$\left[\left(Z-F\right)/Z\right]_{N}$	$\left[(Z-F)/Z\right]_{O}$	S	[(Z-F)/Z] _N	[(Z-F)/Z] _O
21.00	0.8977	0.8907	31.50	0.9555	0.9473
	0.9000	0.8921	31.75	0.9560	0.9480
21.25		0.8940	32.00	0.9567	0.9490
21.50	0.9020	0.8955	32.25	0.9575	0.9498
21.75	0.9040	0.8970	32.50	0.9582	0.9503
22.00	0.9062		32.75	0.9592	0.9513
22.25	0.9080	0.8984		0,9600	0.9520
22.50	0.9102	0.9000	33.00	0.9606	0.9528
22.75	0.9120	0.9015	33.25	0.9614	0.9537
23.00	0.9140	0.9030	33.50	0.9620	0.9542
23.25	0.9157	0.9044	33.75	0.9624	0,9550
23.50	0.9168	0.9060	34.00	0.9632	0.9560
23.75	0.9185	0.9075	34.25	0.9639	0.9564
24.00	0.9202	0.9089	34.50	0.9039	0.9570
24.25	0.9220	0.9103	34.75	0.9642	0.9576
24.50	0.9237	0.9120	35.00	0.9647	0.9510
24.75	0.9252	0.9137	35.25	0.9655	0.9580
25.00	0.9268	0.9150	35.50	0.9660	0.9584
25.25	0.9281	0.9169	35.75	0.9663	0.9594
25.50	0.9297	0.9182	36.00	0.9670	0.9600
25.75	0.9316	0.9199	36.25	0.9675	0.9603
26.00	0.9325	0.9210	36.50	0.9680	0.9613
26.25	0.9338	0.9222	36.75	0.9684	0.9617
26,50	0.9347	0.9238	37.00	0.9691	0.9621
26.75	0.9360	0.9250	37.25	0.9699	0.9625
27.00	0.9374	0.9261	37.50	0.9702	0.9633
27.25	0.9382	0.9279	37.75	0.9708	0.9637
27.50	0 .93 95	0.9292	38.00	0.9714	0.9639
27.75	0.9403	0.9303	38.25	0.9720	0.9642
28.00	0.9418	0.9320	38.50	0.9723	0.9646
28.25	0.9425	0.9334	38.75	0.9727	0.9653
28.50	0.9438	0.9342	39.00	0.9735	0.9657
28.75	0.9445	0.9358	3 9 . 25	0.9739	0.9661
29.00	0.9457	0.9367	3 9.50	0.9741	0.9663
29.25	0.9468	0.9378	39.75	0.9743	0.9668
29.50	0.9480	0.9387	40.00	0.9748	0.9675
29.75	0.9491	0.9399	40.25	0.9754	0.9678
30.00	0.9500	0.9410	40.50	0.9758	0.9681
30.25	0.9516	0.9423	40.75	0.9760	0.9685
30.50	0.9522	0.9435	41.00		0.9687
30.75	0.9532	0.9442	41.25	0.9765	0.9693
31.00	0.9540	0.9450	41.50	0.9771	0.9696
31.25	0.9545	0.9462	41.75	0.9776	0.9700
J/		-			

Table 14 (continued).

S	$\left[\left(Z-F\right)/Z\right]_{N}$	$\left[(Z-F)/Z\right]_{O}$	S	$\left[\left(Z-F\right)/Z\right]_{N}$	$\left[(Z - F)/Z \right]_{C}$
42.00	0.9779	0.9702	46.00	0.9816	0.9745 0.9748
42.25 42.50 42.75	0.9780 0.9783 0.9785	0.9703 0.9705 0.9707	46.25 46.50 46.75	0.9818 0.9820 0.9821	0.9753 0.9756
43.00	0.9790 0.9790 0.9795	0.9712 0.9719	47.00 47.25	0.9823 0.9824	0.9758 0.9760
43.50 43.75	0.9798 0.9800	0.9721	47.50 47.75	0.9826 0.9831	0.9761 0.9763
44.00 44.25	0.9802 0.9804	0.9726 0.97 3 0	48.00 48.25	0.9835 0.9836	0.9765 0.9765
44.50 44.75	0.9805 0.9807	0.9733 0.9735	48.50 48.75	0.9839 0.9840	0.9768 0.9772
45.00 45.25	0.9810 0.9810 0.9812	0.9736 0.9740 0.9741	49.00 49.25 49.50	0.9841 0.9843 0.9845	0.9775 0.9778 0.9780
45.50 45.75	0.9814	0.9741	49.90	0.9846	0.9781

S	А ₀ 0	S	A _O o	S	А ₀ о
0.25	49.5	10.75	64.8	21.25	63.4
	48.0	11.00	64.8	21.50	63.4
0.50		11.00	64.8	21.75	63.4
0.75	52.9		64.7	22.00	63.3
1.00	51.4	11.50	64 . 7	22.00	63.3
.25	52.1	11.75			63.3
1.50	51.9	12.00	64.7	22,50	63.3
.75	52.9	12.25	64.7	22.75	63.5
2.00	53.6	12.50	64.7	23.00	63.2
2.25	54.4	12.75	64.6	23.25	63.2
2.50	55.0	13.00	64.6	23.50	63.2
2.75	55.3	13.25	64.6	23.75	63.2
3.00	56.1	13.50	64.6	24.00	63.2
3.25	56.7	13.75	64.5	24.25	63.2
3.50	57.5	14.00	64.5	24.50	63.2
3.75	58.2	14.25	64.4	24.75	63.2
+.00	58.7	14.50	64.4	25.00	63.2
₊. 25	59.1	14.75	64.3	25.25	63.2
⊧.50	59.6	15.00	64.3	25,50	63.2
+.75	60.2	15.25	64.3	25.75	63.2
5.00	60.8	15.50	64.2	26.00	63.2
5.25	61.2	15.75	64.2	26.25	63.2
5.50	61.6	16.00	64.1	26.50	63.3
5.75	61.8	16.25	64.1	26.75	63.2
5.00	62.4	16.50	64.1	27.00	63.2
5.25	62.7	16.75	64.1	27.25	63.3
5.50	62.9	17.00	64.0	27.50	63.3
5.75	63.2	17.25	64.0	27.75	63.3
7.00	63.5	17.50	64.0	28.00	63.3
. 25	63.8	1 7 . 75	63.9	28.25	63.4
7.50	64.0	18.00	63.9	28.50	63.3
'• 75	64.3	18.25	63.9	28.75	63.4
3.00	64.3	18.50	63.8	29.00	63.4
.25	64.6	18.75	63.8	29.25	63.4
• 50	64.7	19.00	63.7	29.50	63.4
3.75	64.6	19.25	63.7	29.75	63.4
.00	64.6	19.50	63.6	30.00	63.4
.25	64.7	19.75	63.6	30.25	63.4
9.50	64.8	20.00	63.6	30,50	63.4
9.75	64.8	20.25	63.6	30.75	63.4
.00	64.9	20,50	63.6	31.00	63,4
0.25	64.8	20.75	63.6	31.25	63.4
D.50	64.8	21.00	63.5	31.50	63.4

Table 15. $Z_N Z_O (Z-F)_O / (Z-F)_N$ table.

Table 15 (continued)

 $A_{O \cdots O} = Z_N Z_O (Z - F)_O / (Z - F)_N.$

	Ï	$\frac{1}{E}$; 2.50 \leq s	< 20.75		ь І _Е ; 10	. 25 < s < ·	\leq 42.00 $I_{\rm F}^{\rm c}$; 28.75 \leq s $<$ 4			49.75 C_{F} ;18.50 < s < 49.75	
	∆\$				∆s				<u>Δs</u>		
	. 25	.50	.75	1.00	.25	. 50	. 75	. 25	.50	. 75	. 25
^r N-O' ^A	1.200	1.200	1.200	1.200	1.202	1,202	1,202	1.200	1.200	1.200	1.200
$\sigma_{LS}(r_{N-O}), \tilde{A}$	<u>+</u> .0015	<u>+</u> .0023	<u>+</u> .0028	<u>+</u> .0034	<u>+</u> .0009	<u>+</u> .0013	<u>+</u> .0016	<u>+</u> .0008	<u>+</u> .0013	<u>+</u> .0017	<u>+</u> .0010
r _O O, ^A	2.207	2,207	2,206	2.210	2,211	2,211	2,211	2.212	2,213	2.216	2.207
$\sigma_{LS}(r_{O}\cdots O), A$	<u>+</u> .0058	<u>+</u> .0087	<u>+</u> .0111	<u>+</u> .0139	<u>+</u> .0036	<u>+</u> .0053	<u>+</u> .0068	<u>+</u> .0044	<u>+</u> .0067	<u>+</u> .0080	<u>+</u> .0043
l _{N-O} , Å	.0336	.0347	.0309	.0334	.0368	.0362	,0363	.0378	.0367	.0373	. 0334
$\sigma_{LS}(1_{N-O}), \tilde{A}$	<u>+</u> .0044	<u>+</u> .0064	<u>+</u> .0087	<u>+</u> .0100	<u>+</u> .0014	<u>+</u> .0021	<u>+</u> .0026	<u>+</u> .0020	<u>+</u> .0032	<u>+</u> .0040	<u>+</u> .0017
¹ 00, ⁰ A	.0504	.0511	.0526	.0547	.0444	.0447	.0449	.0464	.0447	.0443	.0420
$(\tilde{l}_{LS}(1_{0\cdots 0}), \tilde{A})$	<u>+</u> .0077	<u>+</u> .0116	<u>+</u> .0141	<u>+</u> .0167	<u>+</u> .0033	<u>+</u> . 0049	<u>+</u> .0062	<u>+</u> . 0032	<u>+</u> .0051	<u>+</u> . 0063	<u>+</u> .0036
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Table 16. Results of least-squares refinements (a): comparison of separate composites for different Δs intervals.

(a) $(P)_{ii} = 1$, $A_{N-O} = 2Z_N Z_O$, and $A_{O-O} = Z_O^2$ were used in all refinements.

	2.50 < s < 20.75, Δ s = .25					$10.50 \le s \le 20.75, \Delta s = .25$			10.25 $\leq s \leq$ 42.00, $\Delta s = .25$					
	a I _E	a(1) I E	a(2) I E	a(3) I _E	a(4) I _E	I E	a(1) I E	$I_{E}^{a(2)}$ $I_{E}^{a(3)}$	a(4) I _E	ь I _E	b(1) I _E	^{b(2)} Е	ь(3) І _Е	^{b(4)} ^I E
^г N-О, А	1.200	1.199	1. 199	1. 200	1. 201	1.200	1. 199	1.199	1.201	1.202	1.202	1.203	1.201	1.201
$\sigma_{LS(r_{N-O}), A}$	<u>+</u> . 0015	<u>+</u> .0016	<u>+</u> . 0018	<u>+</u> . 0022	<u>+</u> . 0015	<u>+</u> . 0018	<u>+</u> . 0019	<u>+</u> . 0023	<u>+</u> . 0019	<u>+</u> . 0009	<u>+</u> . 0010	<u>+</u> .0012	<u>+</u> . 0010	<u>+</u> .0014
^r 0· • • 0' ^A	2.207	2,203	2.212	2.202	2,207	2,208	2.202	2.216	2.208	2.211	2.213	2.213	2,207	2.212
$\sigma_{LS(r_{O}\dots O)}, A$	<u>+</u> . 0056	<u>+</u> . 0068	<u>+</u> . 0073	<u>+</u> . 0085	<u>+</u> . 0055	<u>+</u> . 0071	<u>+</u> . 0086	<u>+</u> . 0099	<u>+</u> .0071	<u>+</u> . 0036	<u>+</u> . 0041	<u>+</u> . 0051	<u>+</u> . 0041	<u>+</u> . 0055
^l N-O', ^Å	.0036	.0354	. 0369	. 0293	.0381	. 0201	.0126	. 0221	. 0260	. 0367	. 0382	. 0365	.0385	.0400
$\sigma_{LS(1_{N-O}), A}^{o}$	<u>+</u> .0042	<u>+</u> .0044	<u>+</u> . 0047	<u>+</u> . 0072	<u>+</u> . 0038	<u>+</u> . 0137	<u>+</u> . 0228	<u>+</u> . 0163	<u>+</u> . 0109	<u>+</u> . 0014	<u>+</u> . 0015	<u>+</u> . 0019	<u>+</u> . 0016	<u>+</u> . 0020
¹ 00, [°] A	.0504	.0617	.0589	. 0507	.0511	.0422	.0516	.0495	.0426	.0441	.0457	. 0446	. 0448	. 0466
$\sigma_{LS}(1_0,\ldots,0), A$	<u>+</u> . 0075	<u>+</u> . 0077	<u>+</u> . 0086	<u>+</u> .0113	<u>+</u> .0072	<u>+</u> .0115	<u>+</u> . 0111	<u>+</u> . 0138	<u>+</u> .0114	<u>+</u> . 0033	<u>+</u> . 0037	<u>+</u> . 0046	<u>+</u> . 0038	<u>+</u> . 00 4 9

Table 17. Results of least-squares refinements (a): comparison of individual photographic plates with their composites.

(a) $(\mathbb{P})_{ii} = 1$, $A_{N-O} = 2Z_NZ_O$, and $A_{O\cdots O} = Z_NZ_O (Z-F)_O / (Z-F)_N$ were used in all refinements.

	$I_{E}^{a}; 2.50 \le s \le 20.75, \Delta s = .25$		$I_E^b; 10.25 \le s \le 4$	2.00, ∆s=.25	I_{E}^{c} ;28.75 < s < 49.75, $\Delta_{s} = .25$	$\frac{I^{T}; 2.50 < s < 49.75}{E} \Delta s = .25$	
	c ^(b)	ر(د)	С	v	C	· V	
r _{N-O} , A	1.200	1.200	1.202	1.202	1,200	1.201	
$\sigma_{\rm LS}(r_{\rm N-O}), {\rm A}$	<u>+</u> .0015	<u>+</u> .0015	<u>+</u> .0009	<u>+</u> . 0009	<u>+</u> .0008	<u>+</u> .0007	
r ₀ 0, Å	2.207	2.207	2.211	2.211	2.212	2.210	
$\sigma_{\rm LS}(r_{\rm O\cdots O}), {\rm A}$	<u>+</u> .0058	<u>+</u> .0056	<u>+</u> .0036	<u>+</u> .0036	<u>+</u> .0044	+ .0030	
I _{N-O} , Å	. 0036	. 0336	. 0368	. 0367	. 0378	. 0382	
$0_{LS}(1_{N-O}), \tilde{A}$	<u>+</u> ,0044	<u>+</u> ,0042	<u>+</u> .0014	<u>+</u> .0014	<u>+</u> .0020	<u>+</u> .0080	
¹ 00, [°] A	. 0504	.0504	. 0444	.0441	. 0464	. 0470	
$O_{LS}(1_0,\ldots,0), \stackrel{\circ}{A}$	<u>+</u> .0077	<u>+</u> .0075	<u>+</u> .0033	<u>+</u> .0033	<u>+</u> .0032	<u>+</u> .0025	

Table 18. Results of least-squares refinements^(a): comparison of different composites.

(a) $(P)_{ii} = 1$ was used in all refinements.

(b) $A_{N-O} = 2Z_N Z_O$ and $A_{O\cdots O} = Z_O^2$ (c) $A_{N-O} = 2Z_N Z_O$ and $A_{O\cdots O} = Z_N Z_O (Z-F)_O / (Z-F)_N$.

Table 19. Results of least-squares refinements:^(a) effect of variable weight matrix in analysis of $I_{E}^{T}(s)$.

		$I_{E}^{T}(s)$; 2.50 $\leq s \leq 49.75$, Δs	= . 25					
	(P) _{ii}							
	1	const $s_i \exp(0016 s_i^2)$	const $s_i \exp(002 s_i^2)$					
r _{N-O} , Å	1.2009	1.2010	1.2012					
σ _{LS} (r _{N-O}), Å	<u>+</u> . 0007	<u>+</u> .0007	<u>+</u> .0007					
r _O O, Å	2.2102	2.2096	2.2095					
$\sigma_{LS}(r_{O} \cdots O), \mathring{A}$	<u>+</u> .0030	<u>+</u> .0027	<u>+</u> .0028					
¹ N-O, Å	. 03815	. 03753	. 037 4 7					
σ _{LS} (1 _{N-O}), Å	<u>+</u> .00079	<u>+</u> .00098	<u>+</u> .00108					
^l o···o' ^Å	. 0 4 698	. 0 4 701	. 04714					
$\sigma_{LS}(1_{O} \cdots O), \overset{\circ}{A}$	<u>+</u> .00253	<u>+</u> .00263	<u>+</u> .00282					

 $(a)_{A_{N-O}} = 2 Z_N Z_O \text{ and } A_{O, \dots O}(s) = Z_N Z_O (Z-F)_O / (Z-F)_N \text{ were used in all refinements.}$

Table 20. Error matrix $(x10^6)$ obtained from third cycle of leastsquares refinement^(a) of $I_E^T(s)$: 2.50 $\leq s \leq 49.75$ and $\Delta s = 0.25$.

r _{N-O} (b)	r 0· · · 0	<0-N-0 ^(c)	1 _{N-O}	¹ 0· · · 0
. 4736	0002	-106.4285	0052	0097
	8.7908	1072.76	.0107	1374
		154815.8	2.4791	-14.5843
			. 6223	. 2792
				6.4444

(a) (P)_{ii} = 1, $A_{N-O} = 2 Z_N Z_O$ and $A_{O \cdots O}(s) = Z_N Z_O (Z-F)_O / (Z-F)_N$. (b) Distance and amplitude quantities in $(Å)^2$. (c) Angle quantities in $(deg)^2$.

	r _{N-O}	^r O· · · O	<0-N-0	¹ N-O	^l o···o
1) (.0005 $r_{ij}^2 \ge 10^6$. 361	1. 224			
2) (.02 l_{ij}) ² x 10 ⁶				. 5 82	. 883
3) $\sigma_{LS}^2 \times 10^6$	<u>+</u> .474	<u>+</u> 8. 791	<u>+</u> 15 48 16	<u>+</u> . 622	<u>+</u> 6. 44 4
4) $0^2_2 \times 10^6$	<u>+</u> . 443	<u>+</u> 5.867	<u>+</u> 109700	<u>+</u> 4. 22	<u>+</u> 11. 34
5) $0^2_{LS}/0^2_2$	1.07	1,50	1,41	. 15	. 57
6)	<u>+</u> . 0013	<u>+</u> .0050	<u>+</u> . 65	<u>+</u> .0025	<u>+</u> .0050
7) $(0_{\rm T}^2 - 2 0_{\rm LS}^2)^{\frac{1}{2}}$	<u>+</u> .0009	<u>+</u> .0027	<u>+</u> . 33	<u>+</u> .0022	<u>+</u> .0035
8) $({}^{0}_{T}^{2} - {}^{0}_{2}^{2})^{\frac{1}{2}}$	<u>+</u> .0011	<u>+</u> . 0043	<u>+</u> . 56	<u>+</u> .0014	<u>+</u> .0037

Table 21. Error analysis of structure parameters.

(1) - (4) Distance and amplitude quantities in $(\text{\AA})^2$; angle quantities in $(\text{deg})^2$.

(6) - (8) Distance and amplitude quantities in A; angle quantities in deg.

	r _{N-O} , Å	r ₀ ,Å	<0-N-0, deg	l _{N-O} , Å	l ₀ ₀, Å
This work	1.202 <u>+</u> .0013	2.213 <u>+</u> .0050	134. 02 <u>+</u> . 65	. 0382 <u>+</u> . 0025	. 0470 <u>+</u> . 0050
Microwave (5)	1,197	(2.207) ^(a)	134 . 25		

Table 22. Final results of structure analysis.

(a) Calculated from the relation $r_{O'' O} = 2 r_{N-O} \sin (< O-N-O/2)$.

	N ¹	4 ₀₂	N	⁵ 0 ₂
	I(a)	_{II} (ь)	III ^(a)	IV ^(b)
G ₁₁ , Å/md sec ²	. 08407	. 08429	. 08264	. 08284
G ₁₂	07232	07261	06751	06778
G ₂₂	. 36741	. 36699	. 351298	. 35090
G ₃₃	. 18371	. 18349	. 17565	. 17545

Table 23. Numerical evaluation of G_{S} (x 10⁻²⁸/6.02472) for N¹⁴O₂ and N¹⁵O₂.

(a) < O-N-O = 134, 25 deg (5) was used.

(b) < O-N-O = 134.02 deg (this work) was used.

Table 24. Vibrational frequencies (in cm⁻¹) of $N^{14}O_2$ and $N^{15}O_2$ (1, p. 413-427).

	N ¹⁴ O ₂	ν ¹⁵ 0 ₂
v 1	1319, 7	1306.5
v 2	749.8	740.15
v 3	1617.75	1580.32
ω 1	1357.8	1342. 5
^ω 2	756.8	747.1
ω3	1665.5	1628.0

	I ^(a)	п(р)
λ_{1} , sec ⁻²	6. 179 4 5	6.54141
^λ 2	1.99 4 76	2.03218
λ ₃	9.28587	9. 84213
$^{\Delta}_{l}$, md Å sec ²	2 . 1 4 9796	2.08568
Δ2	4 . 197205	4. 14563
Δ ₃	1.73773	1.68668

Table 25. Numerical evaluation of Λ (x $10^{-28})$ and Δ (x $10^{31})$ for $N^{14}O_2.$

(a) v_i 's (observed fundamental frequencies) were used.

(b) ω_i 's (harmonic frequencies) were used.

<u></u>	I(a)	II(p)	III(c)	IV ^(d)	V(e)
fr	10.771	8 .966	10. 162	11.158	9.156
fa	. 969	2, 167	1.27 4	1. 09 4	2 . 44 7
f _{rr}	2.368	. 563	1.758	2.251	. 2 4 9
fra	. 520	1.176	. 566	. 533	1.303

Table 26a.Error analysis of internal potential constants (in md/Å)obtained from intersections of elliptical contours.

(a) $< 0-N-O = 134.02 \text{ deg}, 1_{N-O} = .03815 \text{ Å}, 1_{O} = .04698 \text{ Å}, T = 380.16^{\circ} \text{ K}, v_{1} = 1319.7, v_{2} = 749.8 \text{ and } v_{3} = 1617.75 \text{ cm}^{-1}$ were used in this calculation.

(b) Same as (a) save for amplitudes: $1_{N-O} + 2\sigma_T(1_{N-O}) = .04309 \text{ Å}$ and $1_{O} \cdots O + \sigma_T (1_{O} \cdots O)/2 = .04949 \text{ Å}.$

(c) Same as (a) save for amplitudes: $l_{N-O} + 2\sigma_{LS}(l_{N-O}) = .03973 \text{ Å}$ and $l_{O} \cdots O + \sigma_{LS}(l_{O} \cdots O)/2 = .04825 \text{ Å}.$

(d) Same as (a) save for frequencies: $\omega_1 = 1357.8$, $\omega_2 = 756.8$ and $\omega_3 = 1665.5$ cm⁻¹.

(e) < 0-N-O = 134.02 deg, $1_{N-O} + 2\sigma_T (1_{N-O}) = .04309 \text{ Å}$, $1_{O} \cdots O + \sigma_T (1_{O} \cdots O)/2 = .04949 \text{ Å}$, T = 380.16° K, $\omega_1 = 1357.8$, $\omega_2 = 756.8 \text{ and } \omega_3 = 1665.5 \text{ cm}^{-1}$.

	I ^(a)	п(р)	III ^(c)
$\sigma(f_r)$	<u>+</u> . 903	<u>+.</u> 305	<u>+</u> 1.001
$\sigma(f_a)$	<u>+</u> . 599	<u>+</u> . 153	<u>+</u> .677
$\sigma_{(f_{rr})}$	<u>+</u> , 903	<u>+</u> . 305	<u>+</u> 1.001
$\sigma_{(f_{ra})}$	<u>+</u> . 328	<u>+</u> . 023	<u>+</u> .385

Table 26b. Errors in internal potential constants (in md/Å) derived from uncertainties in l_{N-O} and $l_{O} \cdots O'$

(a) Effect of ^σ_T(l_{ij})'s on internal potential constants derived from ^ν_i's and l_{ij}'s.
 (b) Effect of ^σ_{LS}(l_{ij})'s on internal potential constants derived from ^ν_i's and l_{ij}'s.
 (c) Effect of ^σ_T(l_{ij})'s on internal potential constants derived from <sub>ω_i's and l_{ij}'s.
</sub>

Table 27. Final results of internal potential constants (GVF) for nitrogen dioxide (in md/Å).

	I(a)	П(р)	III ^(c)	IV ^(d)
f _r	10.77 ₁ <u>+</u> .90 ₃	10. 4 06 <u>+</u> . 025	11.15 ₈ <u>+</u> 1.00 ₁	10.927 <u>+</u> .065
fa	.96 <u>9+</u> .59 ₉	1.0968 <u>+</u> .0009	1.09 <u>4</u> +.67 ₇	1. 125 <u>+</u> . 003
frr	2.36 ₈ <u>+</u> .90 ₃	2.024 <u>+</u> .025	2.25 ₁ <u>+</u> 1.00 ₁	2.038 <u>+</u> .065
^f ra	. ⁵² 0 ⁺ . ³² 8	.535 <u>+</u> .005	. ⁵³ 3 <u>+</u> . ³⁸ 5	. 390 <u>+</u> . 020

(a)<0-N-O = 134.02 deg, $l_{N-O} = .03815$ Å, $l_{O} = .04698$ Å, T = 380.16° K, $v_1 = 1319.7$, $v_2 = 749.8$ and $v_3 = 1617.75$ cm⁻¹ were used in this calculation (present work).

(b)<0-N-O = 134.25 deg, $v_1 = 1319.7$, $v_2 = 749.8$, $v_3 = 1617.75$, $v_1^* = 1306.5$, $v_2^* = 740.15$ and $v_3^* = 1580.32$ cm⁻¹ were used in this calculation (1, p. 413-427).

(c)Same as (a) save for frequencies: $\omega_1 = 1357.8$, $\omega_2 = 756.8$ and $\omega_3 = 1665.5$ cm⁻¹ (present work).

(d) Same as (b) save for frequencies: $\omega_1 = 1357.8$, $\omega_2 = 756.8$, $\omega_3 = 1665.5$, $\omega_1^* = 1342.5$, $\omega_2^* = 747.1$ and $\omega_3^* = 1628.0$ cm⁻¹ (1, p. 413-427).

*These frequencies correspond to $N^{15}O_2$.

	Calculated ^(a)	(b) Observed	Difference (Percent)
v 1	1342.6	1319.7	-1.7
v 2	707.2	749.8	+5.7
^v 3	1618.1	1617.75	⁰ 2
ω ₁	1360. 7	1357.8	2
^ω 2	750.8	756.8	+ .8
^ω 3	1665.9	1665.5	0 ₂

Table 28. Comparison of the calculated and observed frequencies (in cm⁻¹) of $N^{14}O_2$.

(a) Calculated from internal potential constants tabulated in columns I and III in Table 27 (this work).

(b)_{Arakawa and Nielsen (1, p. 413-427).}

Table 29.	Comparison of the calculated and observed root-mean-
	Comparison of the calculated and observed root-mean-square amplitudes (in Å) of $N^{14}O_2$.

	Calculated ^(a)	Observed ^(b)
at 298° K		
^l N-O	. 0382	
¹ 0· · · 0	. 0469	
at 380° K		
l _{N-O}		. 0 3 82 <u>+</u> . 0025
¹ 0· · · 0		. 0 4 70 <u>+</u> . 0050

⁽a)Cyvin (10, p. 117).

(b)This work.

	(a)	(b) II	(c)	IV ^(d)	v(e) V	VI ^(f)	VII ^(g)	VIII ^(h)
с ₁₁	. 0835 <u>+</u> . 0003	.0836 <u>+</u> .0003	. 0792 <u>+</u> . 0002	. 0793 <u>+</u> . 0002	.0822 <u>+</u> .0002	.0779 <u>+</u> .0001	. 0829 <u>+</u> . 0005	. 0787 <u>+</u> . 0004
C ₁₂	0411 <u>+</u> . 0025	0423 <u>+</u> .0025	0354 <u>+</u> .0015	0365 <u>+</u> .0016	0676 <u>+</u> .0112	0542 <u>+</u> . 0016	0507 <u>+</u> .0069	0427 <u>+</u> .0044
с ₂₂	.9253 <u>+</u> .0053	.9252 <u>+</u> .0053	.9009 <u>+</u> .0033	.9007 <u>+</u> .0033	.9750 <u>+</u> .0197	.9374 <u>+</u> .0030	.9424 <u>+</u> .0134	.9137 <u>+</u> .0089
с ₃₃	.1193 <u>+</u> .0001	. 1192 <u>+</u> . 0001	. 1125 <u>+</u> . 0001	. 1124 <u>+</u> . 0001	. 1190 <u>+</u> . 0005	. 1123 <u>+</u> , 0001	. 1192 <u>+</u> . 0004	. 1124 <u>+</u> . 0002

Table 30a. Symmetrized compliance constants (in Å/md) obtained from least-squares refinements.

(a) Input data: $\langle O-N-O = 134.25 \text{ deg}, \nu_1 = 1319.7, \nu_2 = 749.8, \nu_3 = 1617.75, \nu_1 = 1306.5, \nu_2 = 740.15, \text{ and } \nu_3 = 1580.32 \text{ cm}^{-1}.$

(b) Input data: same as (a) save for < O-N-O = 134.02 deg.

(c) Input data: $< O-N-O = 132.25 \text{ deg}, \ \omega_1 = 1357.8, \ \omega_2 = 756.8, \ \omega_3 = 1665.5, \ \omega_1 = 1342.5, \ \omega_2 = 747.1, \text{ and } \ \omega_3 = 1628.0 \text{ cm}^{-1}.$

- (d) Input data: same as (c) save for <O-N-O = 134.02 deg.
- (e) Input data: $< 0-N-O = 134.02 \text{ deg}, T = 380.16^{\circ} \text{ K}, 1_{N-O}^{2} = (.03815)^{2} \text{ A}^{2}, 1_{O\cdots O}^{2} = (.04698)^{2} \text{ A}^{2}, v_{1} = 1319.7, v_{2} = 749.8 \text{ and} v_{3} = 1617.75 \text{ cm}^{-1}.$
- (f) Input data: same as (e) save for frequencies; $\omega_1 = 1357.8$, $\omega_2 = 756.8$ and $\omega_3 = 1665.5$ cm⁻¹.
- (g) Input data: same as (e) plus $v *_1 = 1306.5$, $v *_2 = 740.15$ and $v *_3 = 1580.32$ cm⁻¹.
- (h) Input data: same as (f) plus $\omega *_1 = 1342.5$, $\omega *_2 = 747.1$ and $\omega *_3 = 1628.0$ cm⁻¹.

	Observed	bserved <u>Calculated</u>							
		I ^(a)	II(p)	III ^(c)	IV(d)	v ^(e)	VI ^(f)	VII ^(g)	VIII ^(h)
	1319.7	1320.1	1320.1			1319.7		1319.7	
	749.8	749.8	749.8			749.8		750.1	~ = ~
	1617.75	1616,92	1616,90			1617.87		1616.97	
	1306.5	1306.1	1306.1	 -		an an 14		1306.6	
	740.15	740,13	740,13					739,90	
	1580.32	1581.06	1581.07					1581.14	
	1357.8			1357.7	1357.4		1357.8		1357.1
	756.8			756.8	756.8		756.8		756.9.
	1665.5			1665.2	1665.2		1665.5		1665.2
	1342.5			1342.8	1342.8				1343.2
	747.1			747.1	747.1				746.9
	1628.0			1628.3	1628.3				1628.3
K	(i)				- <u></u>				
С	.001455 ⁽ⁱ⁾					.001506 ₄	.001462 ₇	.001508 ₉	.001465 ₄
•0	.002207 ^(j)					.002206 ₇	.002206 ₈	.002286 ₀	. 002264 ₈

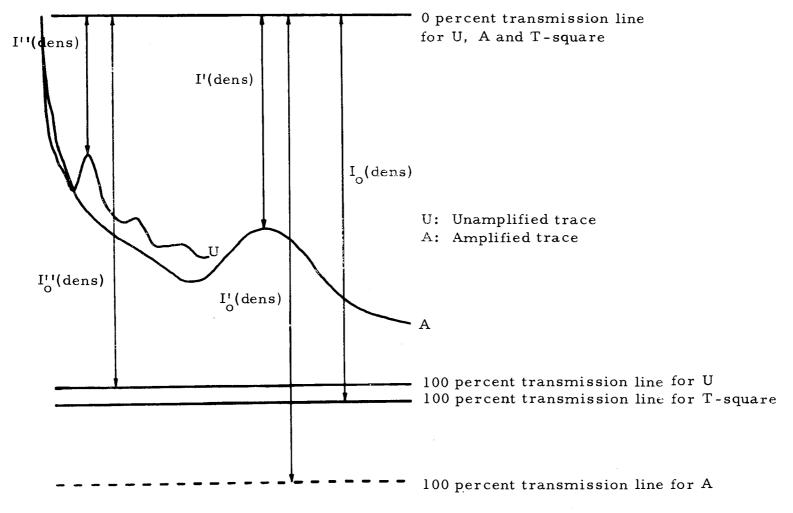
Table 30b. Comparison of the observed and calculated frequencies (in cm⁻¹) and mean-square amplitudes (in $\overset{\circ}{A}^2$) for nitrogen dioxide.

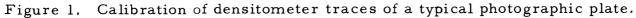
(a) - (h) Same as Table 30a. (i) $(.0381_5)^2 = .001455$ (j) $(.0469_8)^2 = .002207$

* These frequencies correspond to $N^{15}O_2$.

APPENDIX II

FIGURES





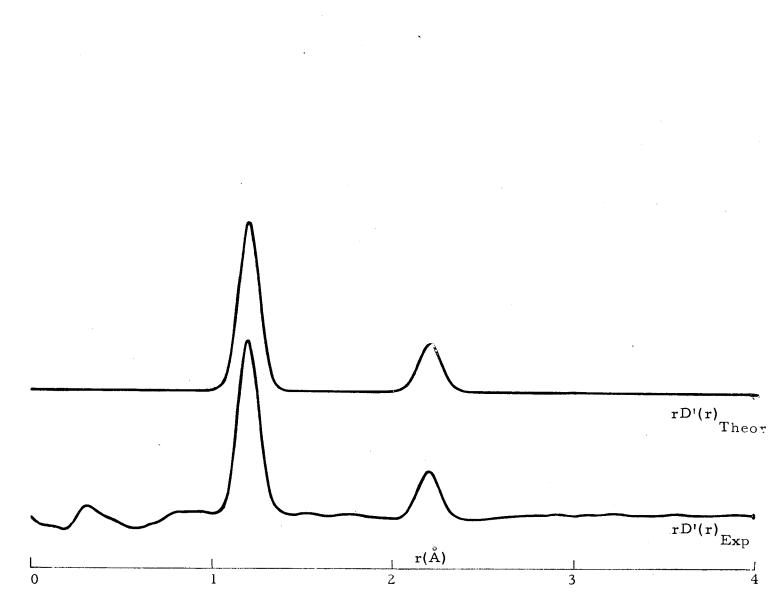


Figure 2. Experimental and theoretical radial distribution curves for nitrogen dioxide,

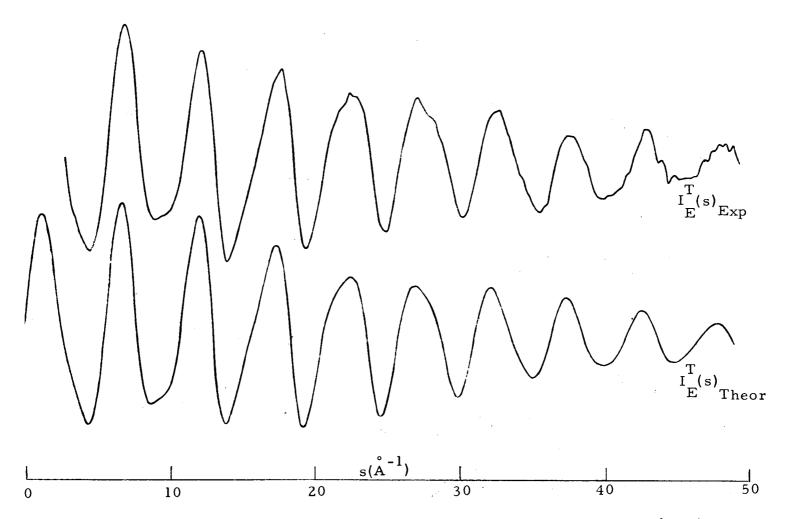


Figure 3. Experimental and theoretical modified molecular intensity curves for nitrogen dioxide.

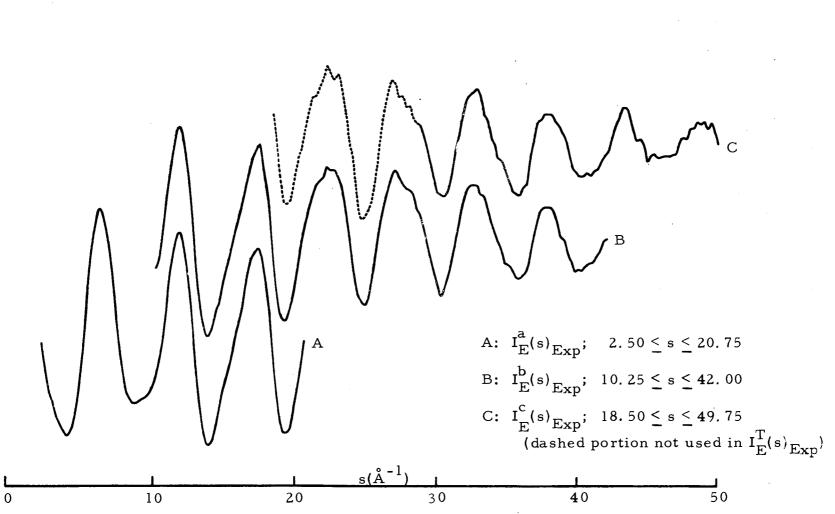


Figure 4. Experimental modified molecular intensity curves from separate camera distances for nitrogen dioxide.

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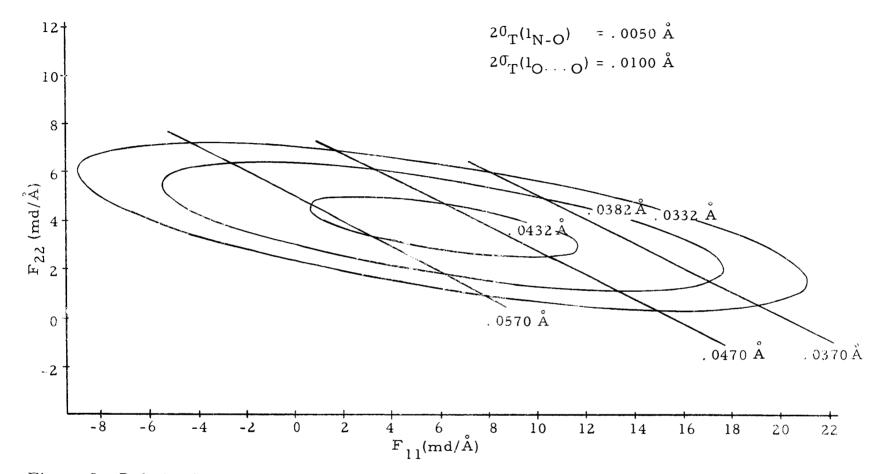


Figure 5. Relation between root-mean-square amplitudes and symmetrized potential constants for nitrogen dioxide.