# Irrigation Efficiency, Consumptive Use, Certain Soil Characteristics <br> of the <br> North Unit, Deschutes Irrigation Project, Oregon 

J. A. CURRIE
J. W. WOLFE
L. R. SWARNER


This is a final report of an investigation made under a cooperative agreement between the Oregon Agricultural Experiment Station and the United States Bureau of Reclamation.

IRRIGATION EFFFICIENCY, CONSUMPTIVE USE, AND CERTIAIN SOIL CHARACIERISTICS OF THE NORTH UNIT OF THE DESCHUIES IRRIGATION PROJECT, OREGON
J. A. Currie, J. W. Wolfe, and L. R. Swarner*

## Summary

A field study was made on the North Unit of the Deschutes Irrigation Project near Madras, Oregon to determine disposition of irrigation water delivered to farms. Total seasonal application, surface runoff, application efficiency, and consumptive use are reported for 22 farm fields. Farm efficiencies were obtained for six farms.

A supplementary study compared the border method of irrigation with the corrugation method. Another study correlated consumptive use with pan evaporation. In addition, measurement of certain physical properties of soil were made on several sites of major soil types.

## Introduction

Complete control and regulation of water at all times is essential for good crop production under successful irrigation. Such control and regulation should assure an adequate supply of avallable molsture in the soll throughout the growing season. Too much water may reduce yields or destroy crops. Even though the crop is not damaged, over-irrigation causes unnecessary loss of plant nutrients by leaching and contributes greatly to drainage problems of an irrigated area.

Most efficient utilization of irrigation water under acceptable methods of application, cultural practices, and land preparation requires considerable information. Relationships among soil moisture-holding capacities, intake rates, length of runs, and width of corrugation spacings must be developed by actual experimentation or trial on the land.

To determine and demonstrate irrigation principles and practices leading to more efficient and economic utilization of irrigation water in irrigated areas of central Oregon, a cooperative memorandum of agreement was drawn up between the Bureau of Reclamation and Oregon State College. This cooperative work began in July, 1950, and continued throughout the 1951, 1.952, and 1953 irrigation seasons. Although the information developed was applicable to the entire central Oregon area as well as to other irrigated areas in the Northwest, most irrigation trials were conducted at locations on the North Unit of the Deschutes Project as shown on the map on the following page.

This is a summary report of the results of irrigation studies carried out over the 3-year period.

[^0]

## DESCRIPTION OF THE AREA

The Central Oregon area is comprised of Crook, Deschutes, and Jefferson Counties. The first irrigation projects in the area were developed in Crook and Deschutes Counties about 1910. The first water was delivered to the North Unit of the Deschutes Project in Jefferson County in 1946. Water was available for the entire North Unit in 1949 for the first time.

Much of the area is a semiarid intermountain plain, sloping from elevations of around 3600 feet in the South to about 2300 feet in the North. The growing season is approximately 130 days in length. The whole area is underlain by lava formations.

In general soils are of shallow depth and may contain considerable quantities of pumice. Soils, especially on the North Unit of the Deschutes Project, are underlain by a gray conglomeratic-like caliche hardpan of variable thickness, which grades into semi-cemented basalt fragments, then into basalt rock. Internal drainage in the soils is impeded and in many cases entirely stopped by this hardpan.

Predominate crops of the Central Oregon area are potatoes and clover seed, but grains and alfalfa for hay occupy considerable acreages. Many farmers have small livestock enterprises, especially in older irrigated areas.

Table 1. Irrigated Acreages on Various Tributaries of and on the Deschutes River in the Central Oregon Experimental Area.

| Stream or River | Acreage |
| :--- | ---: |
| Crooked River | 55,492 |
| Deschutes River | 111,658 |
| Paulina Creek | 503 |
| Squaw Creek | 14,680 |
| Lake Creek | 394 |
| Trout Creek | 4,507 |
| Willow Creek | 230 |
|  |  |
|  | Total |

## Soil Type Acreages Under Irrigation

Table 2 shows irrigated acreage of each soil type by slopes and the percentage each soil type is of the total irrigated acreage. The main types in descending order are Madras loam, Madras sandy loam, Metolius sandy loam, Agency loam, Era sandy loam, Agency sandy loam, and Lamonta loam. This breakdown is only for the North Unit of the Deschutes Project. Adequate information was not available for calculations in Deschutes County.

## Soil Characteristics

Moisture equivalent, 15 -atmosphere percentage and volume welght soil characteristics were determined for the predominant soil types. The characteristics are listed in detail in Appendix Table l. Volume weights for the

|  | Sold Typencreag North |  | Proiect |  | Slope |  |  | Percent |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Number | Soil Series and Type | Group* | A-0 to 3\% | B-4 to $7 \%$ | $\mathrm{C}-8$ to $12 \%$ | D-13 to 20\% | Total | of total |
| 39 | Madras Loam | 1 | 12,110.6 | 2,426.7 | 170.1 |  | 14,707.4 | 29.4 |
| 28 | ${ }^{\prime \prime}$ | 6 | 1,334.9 | 105.0 |  |  | 1,439.9 | 2.9 |
| 40 | Sandy Loam | 1 | 8,398.2 | 1,398.2 | 44.9 | 11.4 | 9,853.3 | 19.7 |
| 27 | " " " | 6 | 1,592.0 | 1,045.3 | 297.2 | 14.0 | 2,948.5 | 5.9 |
| 10 | * | 6 | 15.5 | 74.1 | 11.4 | 4.3 | 105.3 | 0.2 |
| 12 | " | 6 | 74.5 | 22.1 |  |  | 96.6 | 0.2 |
| 68 | " Stony | 1 | 59.2 | 95.9 | 11.0 | 7.3 | 173.4 | 0.4 |
| 13 | " Stony Sandy Loam | 6 | 123.2 | 56.5 | 13.0 |  | 192.7 | 0.4 |
| 42 | Metolius Sandy Loam | 2 | 5,610.3 | 511.9 | 8.6 |  | 6,130.8 | 12.3 |
| 60 | " t 4 | 2 | 865.3 | 85.4 |  |  | 950.7 | 1.9 |
| 62 | " $\quad$ " | 2 | 58.6 |  |  |  | 58.6 | 0.1 |
| 92 | " Loamy Sand | 2 |  | 9.5 |  |  | 9.5 | -- |
| 36 | Agency Loam | 3 | 3,928.9 | 220.4 |  |  | 4,151.1 | 8.3 |
| 35 | " Sandy Loam | 3 | 2,654.4 | 44.9 |  |  | 2,699.3 | 5.4 |
| 37 | * Gravelly Loam | 3 | 82.0 | 197.1 | 31.0 | 7.0 | 317.1 | 0.6 |
| 63 | * Stony Loam | 3 | 154.1 | 33.2 |  |  | 187.3 | 0.4 |
| 43 | Era Sandy Loam | 4 | 1,968.8 | 1,077.1 | 107.2 |  | 3,153.1 | 6.3 |
| 30 | Lamonta Loam | 5 | 844.6 | 1,257.5 | 73.8 | 10.0 | 2,185.9 | 4.4 |
| 84 | " " | 5 |  |  | 20.5 |  | 20.5 | -- |
| 33 | * Stony Loam | 5 | 81.6 | 56.0 | 23.4 |  | 161.0 | 0.3 |
| 34 | " Sandy Clay Loam | 5 | 55.9 | 59.3 | 3.0 |  | 118.2 | 0.2 |
| 31 | " $\quad$ : $*$ " | 5 | 6.0 | 1.0 |  |  | 7.0 | -- |
| 75 | Redmond Sandy Loam | 7 | 55.6 | 26.7 |  |  | 82.3 | 0.1 |
| 75 d | " " " | 7 | 60.6 |  |  |  | 60.6 | 0.1 |
| 3 | Deschutes Sandy Loam | 4 | 39.0 | 11.6 |  |  | 50.6 | 0.1 |
| L3 | * Loamy Sand | 4 | 7.4 |  |  |  | 7.4 | -- |
| 26 | " " | 6 | 82.8 |  |  |  | 82.8 | 0.1 |
| 5 | " Stony Sandy Loam | 4 | 5.0 |  |  |  | 5.0 | - |
| 51 | Cdin Clay Loam | 8 | 17.0 |  |  |  | 17.0 | -- |

8. Poorly drained, light textured surface soil with heavy textured subsoil over basalt or mixed consolidated materials.
most part are uniform and vary little from the standard 1.3 used for average arable soils. Moisture equivalents varied somewhat, with differences mainly between surface soil and clayey subsoils. Little difference is noted between loams and sandy loams. Surface depth molsture equivalents ranged from 16 to $27 \%$ with an average somewhere near $24 \%$ and clayey subsoils gave some values as high as $40 \%$. Values for the 15 -atmosphere determination varied in the same relative magnitudes as the moisture equivalents. An average value would probably be about $12 \%$ with subsoils somewhat higher. In general soils sampled in Deschutes County were not as heavy in the subsoil area. Surface values for both determinations were secured throughout the profile.

## Weather Records

The Madras weather station is located in a depression or drainage channel approximately 200 feet lower in elevation than the surrounding farm area. Many people thought the weather records were not representative of the farming area. However, records from the Metolius station four miles southwest of Madras and from the airport station two miles north do not seem to indicate any great climatic variations. A study being conducted by the Weather Bureau may at a later time show some significant variation.

Wind and evaporation measurements were made at the airport station in 1952 and 1953. No attempt was made to average the values.

Average rainfall for the Mry through September growing season is 2.70 inches. Average monthly temperature varies from a low of 52 degrees in May to a high of 66 degrees in July. Wind movement is greatest in spring and lowest in October. Evaporation is greatest in July when nearly 10 inches evaporates. Table 3 gives monthly totals or averages. Daily fluctuations are plotted in Figures 2 and 3.

Table 3. Temperature, Wind, Rain, and Evaporation for 1952-1953, measured at Madras and at Madras Airport.

|  | Maäras Average |  | Madras Airport |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | 1952 |  | 1953 |  |
|  |  |  | Wind |  | Wind |  |
|  | Temp. | Rain | Miles | Evap. | Miles | Evap. |
|  | degrees | inches | per month | inches | per month | Inches |
| January | 29.7 | 1.09 |  |  |  |  |
| February | 34.6 | 0.69 |  |  |  |  |
| March | 40.9 | 0.64 |  |  |  |  |
| April | 46.2 | 0.63 | 2432 | 5.81 | 1990 | 3.82 |
| May | 52.6 | 0.86 | 2128 | 7.13 | 2278 | 5.45 |
| June | 59.5 | 0.70 | 2019 | 6.69 | 1851 | 6.12 |
| July | 66.5 | 0.20 | 1832 | 9.87 | 1937 | 10.51 |
| August | 64.2 | 0.28 | 1713 | 8.14 | 1623 | 7.81 |
| September | 56.8 | 0.66 | 1565 | 6.14 | 1531 | 6.25 |
| October | 48.0 | 0.65 | 1146 | 3.48 | 1280 | $2.5{ }^{\circ}$ |
| November | 38.2 | 1.30 |  |  |  |  |
| December | 31.5 | 1.10 |  |  |  |  |



Wind Velocity Miles per day

Rainfall
Inches T -

# Terms and Formulas Used <br> 1. Field water application efficiency (percent): <br> Water stored in the soil during irrigation, as determined from soil moisture samples plus that moisture calculated as used during irrigation <br> x 100 <br> Water delivered to the field. <br> 2. Farm water application efficiency (percent): 

Water stored in soil during irrigation, as determined from soil moisture samples plus that noisture calculated as used during irrigation $\times 100$

Water delivered to the farm.
3. Consumptive use:

Consumptive use is the quantity of water, in inches per acre, absorbed by the crop and transpired or used directly in the building of plant tissue, together with that evaporated from the soll surface.

Conversion of percent moisture to inches of water:
Percent moisture $x$ volume weight $x$ inches of soil sampled $=$ inches of water in the depth of soil sampled.

## Procedures

## Sampling of Soils and Determination of Soil Moisture Percentages

Soil moisture samples were obtained with a l-inch King tube. Samples were taken at three depths, 0 to 6 inches, 6 to 12 inches, and 12 inches to hardpan. At least two cores were composited to make a sample. Samples obtained before and after the irrigation season were taken from random locations over the whole field being sampled. During the irrigation season samples were taken before and after each irrigation. At each irrigation the portion of field being irrigated in one "set" of water was divided arbitrarily into an upper, middle, and lower third and separate composite samples were taken from each portion. Data obtained were averaged for each sampling depth. On exceptionally long or short runs, fields were divided into quarters or halved as sampling areas for each set of water. Samples were dried at least 24 hours in a forced draft "Precision" Thelco Oven at 105 degrees Centigrade.

Total consumptive use consists of three separately determined values. First is the quantity determined from soil moisture sampling after one irrigation and before the next. Second is the quantity calculated for the period during irrigation, from the daily use determination after irrigation. Third is the moisture added as rain during the periods between irrigations. Any rain which fell during an irrigation is omitted.

Insofar as possible the before-irrigation samples were obtained immediately prior to the time water was placed on a particular "set" in the field. The after-irrigation samples were taken as soon as the soil had drained so it could be walked upon. The moisture content of the soil at the time the field could be walked upon without miring down is, in this report, considered the field capacity. On most fields, during the hot days of summer, field capacity was reached in about 24 hours after irrigation was completed. During cooler weather, early and late in the irrigation season, up to 96 hours were required for field capacity to be reached.

## Water Measurements

Water flow measurements were made by means of weirs and water stage recorders. Cipolletti weirs were used to measure farm delivery flow. Field and set runoff measurements were obtained with portable "V"-notch ( 90 degree) rectangular, and trapezoidal (Cipolletti) weirs. Application heads at the farm turnout were found to be nearly constant. Because of that and the small number of instruments available, stage recorders with few exceptions were used primarily in measurement of runoff flow. Where possible, weirs were set in runoff ditches and left for the season. Semi-permanent supports for water stage recorders were set up at these runoff weirs. However, the instruments themselves were not left permanently in one location, but were moved from place to place as needed.

Nine water stage recorders were used. Five were Stevens type E, using 48 -hour charts. One was a Stevens type $L$ with an 8 -day chart. The remaining three instruments were Freiz type F W with 24 -hour, 4 -day, and 8-day chart time intervals. All instruments performed satisfactorily, but the Stevens type $E$ was found to be superior for the completely portable water measurement set-up.

Flows over the various weirs were so variable that it was necessary to integrate all of the recorder charts by finding the average head for short periods of time. Planimeter integration of the recorder charts from the Cipolletti and rectangular weirs was used in 1951.

Some difficulty was encountered in measuring runoff water. All ditches had sufficient head for proper operation of weirs. Only rarely did weedclogged ditches cause submerged weir conditions and then only until the weeds were removed. Co-efficients determined by Clemens Herschel, as described in the Bureau of Reclamation "Manual for Measurement of Irrigation Water," were used to integrate the recorder charts for any submerged weir conditions.

## Moisture Equivalent and 15-Atmosphere Percentage

Samples for moisture equivalent and 15-atmosphere percentage determinations were taken from 0 to 6,6 to 12, and 12-inch to hardpan depths. Sampling locations were selected at random in various fields or plots. A 3 -inch orchard auger was used to secure samples. Material from two borings 10 to 12 feet apart was composited to make one sample. Samples were airdried, bagged, and sent to the Soils Department of Oregon State College where determinations were made. The 15 -atmosphere percentage was determined by Richard's pressure plate apparatus.

## Volume Weight

The modified Pomona sampler, obtained from the Utah Scientific Research Foundation, was employed to obtain samples for volune weight determinations. Cores secured with the Pomona sampler were 2 inches in diameter and $11 / 2$ Inches long. Sampiting was done in the same random locations selected for moisture equivalent and 15 -atmosphere percentage sampling. At least two locations in each field were selected. The soll profile was sampled at 3 -inch depth intervals at each sampling location. Samples were oven-dried at 105 degrees Centigrade. Results of the 3-inch depth determinations for each farm were averaged to give 0 to 6,6 to 12 , and 12 -inch to hardpan depths. Average volume weights were used in converting soil moisture percentages to inches depth of water. Cores taken were carefully checked for rocks. None were found which would alter the results--even in the second decimal place.

Crop Yields
Crop yields were obtained on the whole field basis. All hay harvested from fields in these studies was baled, and a bale weight average for the field was secured by weighing a sample number of bales at each cutting of hay. Grain was handled in bulk and total weight at time of marketing or bin measurements were secured. Each 2.19 acre plot in the irrigation method comparison study was treated as a separate field and harvested with a self-propelled combine. The portion of the field not included in the plots was harvested first. All adjustments to the combine were made in the portion of the field not occupied by plots. Seed from each plot was bagged, weighed, and cleaned separately at the seed cleaning plant. Before entering the first plot and at completion of harvest on each plot, the combine was cleaned as thoroughly as possible.

## Selection of Farms for Study

Farms were selected on the basis of soil uniformity and water measurement facilities. Considerable time was spent on farms selected from soil map studies to further confirm soil consistency. The farm layout and irrigation procedure were carefully checked to make, sure various water measurements would be possible. Portable and semi-permanent weirs and stage recorders were established within the farmer's system. The farmer's permission for and acceptance of the structures and many soll samplings were carefully determined. Close cooperation was necessary throughout the entire season between farmer and technician.

## Results and Discussion

A summary of data from twenty-two fields is presented in Table 4. The figures in this table are seasonal totals or averages, and are taken from the more complete presentation in Appendix Table 2.

Total application ranged from 20 inches to 174 inches, whereas consumptive use ranged from 14 to a maximum of 34 inches. The water applied in excess of the consumptive use requirement left the field as deep percolation or as surface runoff. Considering the mean of the figures for all fields, only $39 \%$ of the water applied was stored for consumptive use, $46 \%$ was lost as surface runoff, and the remainder was presumed lost to deep percolation.

Seasonal consumptive use was highest for pasture and lowest for potatoes and wheat. Alfalfa and clover consumptive use were close enough to that for pasture that differences could have been due to error.

Peak consumptive use rates show a wide variation, indicating a possible fallure of the sample values to represent the average field conditions. The high value for potatoes could be questioned on the basis that the sampling error would be spread over fewer days, thus raising the per day error. On the other hand, high consumptive use is known to be associated with frequent irrigations. The peak rate for pasture could be questioned because of the large difference between the two measurements. It could also be questioned whether or not the peak rate of alsike clover would consistently be so much lower than ladino and kenland. The mean peak use rates for ladino clover and for wheat are considered good estimates for the corresponding mean length of use period because of the greater number of flelds measured. None of the data have been subjected to statistical analysis.

Overall farm irrigation efficiencies were obtained on six farms with the following results: Harris, $35.2 \%$; Short-Johnson, $39.8 \%$; Brewer, $49 \%$; Drazil-Griffin, 41\%; Kizer, $37.6 \%$; Greenwood, $38 \%$. The average of these six is $40 \%$. Only the last four of these six are represented in the field summary in Table 4. The average of these four farm efficiencies is $41.4 \%$. This compares with the $39 \%$ average of the respective field efficiencies. It is believed that the apparent difference in these values can be attributed to the re-use of waste water by applying the runoff from one field onto another field on the same farm.

Appendix Table 2 contains the principal results of this investigation, not all of which have been thoroughly discussed.

## Supplementary Studies

## Comparison of Border Strip and Corrugation Methods of Irrigation

It is a common practice of farmers on the North Unit to irrigate fields by means of corrugations. Even large relatively flat fields are irrigated without the aid of border strips to confine heads of water to relatively narrow strips. Often the corrugations become filled with sediment, or, especiaily in clover fields, obstructed by plant leaves or other plant debris, causing the streams of water to leave the corrugations and resulting in wild flooding. In efforts to moisten the whole soil surface and to irrigate all

Table 4, Disposition of Water Applied to 22 Fields Seasonal Totals or Averages

| Crop | Seasonal Application | Runoff | Application Efficiency | Seasonal Consumptive $\qquad$ |  | ```Length of period of peak use``` |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Inches | \% | \% | Inches | Inches/day | Days |
| Ladino | 74 | 51 | 36 | 32.3 | 0.40 | 8 |
|  | 66 | 51 | 34 | 26A | 0.31 | 22 |
|  | 53 | 53 | 50 | 29.8 | 0.33 | 10 |
|  | 47 | 51 | 45 | 26.8 | 0.27 | 9 |
|  | 104 | 51 | 24 | 22.7 | 0.32 | $\frac{13}{12}$ |
| Mean | 68.8 | 51.4 | 37.8 | 27.6 | 0.326 | 12.4 |
| Wheat | 36 | 50 | 28 | 14.0 | 0.22 | 21 |
|  | 24 | 40 | 45 | 17.8 | 0.24 | 19 |
|  | 28 | 41 | 47 | 17.4 | 0.32 | 17 |
|  | 40 | 49 | 48 | 26.7 | 0.30 | 15 |
|  | 26 | 24 | 45 | 18.3 | 0.26 | 15 |
|  | 26 | 42 | 35 | 16.6 | 0.17 | 30 |
|  | 20 | 32 | 62 | 17.1 | 0.35 | 14 |
| Mean | 28.6 | 39.7 | 44.3 | 18.3 | 0.266 | 18.7 |
| Alfalfa | 151 | 73 | 13 | 25.1 | 0.38 | 7 |
|  | 40 | 31 | 50 | 26.2 | 0.22 | 38 |
| Mean | 95.5 | 52.0 | 31.5 | 25.7 | 0.30 | 22.5 |
| Kenland | 51 | 38 | 46 | 28.0 | 0.29 | 10 |
| Pasture | 174 | 48 | 22 | 34.1 | 0.56 | 5 |
|  | 43 | 38 | 41 | 26.3 | 0.18 | 15 |
| Mean | 108.5 | 43.0 | 31.5 | 30.2 | 0.37 | 10 |
| Potatoes | 63 | 71 | 20 | 17.1 | 0.47 | 3 |
|  | 35 | 55 | 44. | 17.3 | 0.50 | 3 |
|  | 43 | 42 | 40 | 18.1 | 0.40 | 17 |
| Mean | 47.0 | 56.0 | 34.7 | 17.50 | 0.457 | 7.7 |
| Alsike | 27 | 45 | 48 | 20.2 | 0.19 | 11 |
|  | 49 | 33 | 42 | 24.8 | 0.24 | 18 |
| Mean | 38 | 39 | 45 | 22.50 | 0.215 | 14.5 |
| Grand Mean | 55 | 46 | 39 | 22.9 |  |  |

portions of their fields under these conditions, farmers may allow water to flow for periods as long as 48 hours with much subsequent runoff, or they may greatly increase the size of stream on a small area to "force" water over obstructions, resulting also in much runoff.

In irrigating by the border strip method, water is confined to a relatively narrow portion of a field and not allowed to flood land outside the area intended to be irrigated. Large streams of water are used so that the entire strip is flooded and moisture in infiltrated over the entire soil surface. When confined in this manner, the stream of water will usually flow over and wet a given area of land in less time than is required when attempts are made to irrigate through filled or obstructed corrugations. The border strip method usually calls for more frequent changes of sets than the corrugation method. The number of irrigations is also sometimes increased by use of border strips if infiltration is slow. For these reasons some increase in labor is required-an argument against the border strip method in the opinions of North Unit operators.

To study the relative efficiencies of the two methods, comparison of the border strip and corrugation methods was continued on the same field of the Chester Luelling farm in 1951, 1952, and 1953. The plots were selected at random across the portion of the field available for studies.

Border strips were laid out after a rough topographic survey had been made to determine slope, direction of flow, and width of each border strip. Factors entering into choice of border strip spacings were: amount of side fall, size of stream of water available, size of stream that could be applied without causing excessive erosion. Borders or dikes were prepared by the farmer who also performed all tillage operations.

The corrugations were irrigated in the manner determined best for this field. Runoff was kept to a minimum and inspection of runoff stage recorder charts indicated that runoff at each irrigation was just at the peak, or had not reached the peak when irrigation was stopped on the corrugations. In irrigating border strips one second foot of water was considered the proper head to get the best distribution in 30 -foot strips. This head was allowed to run until it was estimated that the advance would irrigate the remaining portion of the strip. Corrugation spacing was 24 inches.

## Results

Irrigation efficiency on the border strip method was higher than on the corrugation method throughout the three-year study. The values for each are 60 , 88 , and $94 \%$ on the border strips and 47,55 , and $73 \%$ on the corrugations. Runoff percentage varied from 6 to $13 \%$ of the total application on the strips and 23 to $31 \%$ on the corrugations. The 1953 results are shown in detail in Appendix Table 2.

Results indicate that under certain conditions a change in irrigation method could save water.

Pan Evaporation vs. Consumptive Use
Measurements of evaporation of water from small pans or other devices is being used in some places as an estimate of consumptive use of crops. If
a high correlation is obtained between these two factors, measurement of evaporation can be used to predict when and how much to irrigate. The consumptive use data from this project has been correlated with evaporation from standard class A weather bureau pan at the Madras 2 N station. The results appear in Figures 4 through 11.

Each point on each one of these graphs represents a consumptive use measurement between two irrigations. Usually the points which represent high values of evaporation and consumptive use were measured either early or late in the season. Because the irrigation intervals during most of the season were of approximately equal length there are many points clustered in a small area on most of the graphs.

Some of the graphs show a fairly large group of points at some distance from the line of regression. Whenever these groupings could be identified with rainfall characteristics, the identification has been shown on the graphs. Because some of the fields measured were located several miles from the weather station it is believed that some of the rains recorded at the weather station would not have been recorded at the field in the same amount. Had the rain been measured at each field it is believed that higher correlation coefficients would have been obtained on most of the regression lines.

Correlation coefficients ranged from 0.9650 to 0.5934 . They were computed for the following crops, listed in order of decreasing correlation coefficients: alfalfa, pasture, alsike clover, kenland clover, ladino clover, wheat, and potatoes. Each of the perennial crops showed a higher correlation coefficient than any of the annual crops.

The results of this study appear promising, especially for alfalfa, pasture, and alsike clover. On alfalfa, for instance, the regression line indicates that when three inches of water have been evaporated from the pan, the consumptive use has been almost two inches. If the crop is growing on a soil which will permit the removal of 2 inches of water without reducing yield, irrigation can be applied at this time. Assuming an irrigation efficiency of $50 \%$, a 4 -inch application of water would be sufficient. These results appear to warrant further investigation.
Fan Evaporation vs. Consumptive Use of Alfalfa




Pan Eveporation vs. Consumptive Use of Kenland Clover Each point represents a period between irrigations.




Pan Evaporation vs. Consumptive Use of Potatoes Each point represents a period between irrigations.



$+1+1 \rightarrow=$
H
$H$


\#
16







Appendix Table 1. Soil Characteristics.

| Soil | Farm | Location | Depth <br> Inches | Moisture Equivalent $\qquad$ | Wilting <br> Point <br> 15-atm\% | Volume Weight |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Madras | Ellis | S.E. 4 | 0-6 | 22.72 | 10.76 | 1.39 |
| Loam | Kiser | N.W. 4 | 6-12 | 26.17 | 13.85 | 1.15 |
|  |  | and | 12-23 | 34.39 | 20.37 | 1.32 |
|  |  | S. W. 4 | 0-6 | 21.40 | 10.04 | 1.27 |
|  |  | N.E. 4 | 6-12 | 22.35 | 11.51 | 1.23 |
|  |  | Sec. 8 | 12-23 | 29.83 | 17.74 | 1.22 |
|  |  | T.10S |  |  |  |  |
|  |  | R.14E | 0-6 | 21.14 | 11.13 | 1.30 |
|  |  |  | 6-12 | 25.66 | 14.18 | 1.26 |
|  |  |  | 12-25 | 29.21 | 16.56 | 1.27 |
|  |  |  | Q-6 | 21.62 | 10.51 | 1.39 |
|  |  |  | 6-12 | 23.27 | 11.90 | 1.37 |
|  |  |  | 12-24 | 27.58 | 14.90 | 1.31 |
|  |  |  | 0-6 | 21.82 | 11.98 | 1.27 |
|  |  |  | 6-12 | 24.91 | 13.94 | 1.20 |
|  |  |  | 12-21 | 33.60 | 19.20 | 1.44 |
|  |  |  |  |  | 10.56 |  |
|  |  |  | 6-12 | 23.53 | 11.04 | 1.36 |
|  |  |  | 12-29 | 24.70 | 12.77 | 1.32 |
| Madras | Chester | S.W. 4 | 0-6 | 18.07 | 8.10 | 1.24 |
| Loam | Luelling | N.W. 4 | 6-12 | 18.43 | 8.37 | 1.27 |
|  |  | $\begin{aligned} & \text { Sec. } 27 \\ & \text { T. } 9 \mathrm{~S} \end{aligned}$ | 12-27 | 16.50 | 7.57 | 1.37 |
|  |  | R.13E | 0-6 | 23.70 | 9.46 | 1.21 |
|  |  |  | 6-12 | 22.69 | 9.85 | 1.26 |
|  |  |  | 12-23 | 21.88 | 9.77 | 1.31 |
|  |  |  | 0-6 | 20.33 | 10.0 | 1.29 |
|  |  |  | 6-12 | 21.64 | 9.5 | 1.23 |
|  |  |  | 12-21 | 23.58 | 10.8 | 1.17 |
|  |  |  | 0-6 | 21.10 | 10.2 | 1.30 |
|  |  |  | 6-12 | 22.08 | 10.0 | 1.24 |
|  |  |  | 12-21 | 25.31 | 12.6 | 1.16 |
|  |  |  |  |  | 10.0 |  |
|  |  |  | 6-12 | 20.74 | 10.8 | 1.16 |
|  |  |  | 12-2.4 | 27.10 | 16.4 | 1.20 |
|  | Lydy | S.E. 4 NE4 | First f | . 30.25 | 11.30 | 1.37 |
|  |  | Sec 28 | Second | +22.74 | 12.01 | 1.44 |
|  |  | T9S <br> R13E | Hardpan | 21.85 | 13.33 |  |


| Soil | Farm | Location | Depth Inches | Moisture Equivalent \% | Wilting <br> Point <br> 15 Atm\% | Volume Weight |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Madras | Harris | NEL ${ }^{\text {NEL }} 4$ | First ft. | 24.42 | 13.28 | 1.40 |
| Loam |  | Sec 15 | Second ft | 26.01 | 15.09 | 1.33 |
|  |  | T 10 S | First ft. | 23.63 | 13.12 | 1.31 |
|  |  | R 13E | Second ft | 22.18 | 11.01 | 1.39 |
|  |  |  | Hardpan | 23.65 | 11.75 | - |
|  |  |  | $0-6$ | 23.08 | 10.2 | 1.42 |
|  |  |  | 6-9 | 25.99 | 12.3 | 1.24 |
|  |  |  | 9-17 | 27.33 | 14.2 | 1.24 |
|  |  |  | 17-20 | 26.84 | 13.2 | 1.29 |
|  |  |  | 0-6 | 22.71 | 10.6 | 1.51 |
|  |  |  | 6-11 | 24.58 | 11.5 | 1.37 |
|  |  |  | 11-23 | 26.04 | 12.4 | 1.39 |
|  |  |  | 0-6 | 22.89 | 11.6 | 1.35 |
|  |  |  | 6-12 | 23.16 | 11.2 | 1.51 |
|  |  |  | 12-16 | 23.14 | 10.6 | 1.50 |
|  |  |  | 16-30 | 23.01 | 11.0 | 1.54 |
|  | LeachCorwin | $\mathrm{SE}_{4} \mathrm{SE}_{4}$ | First ft | 18.60 | 10.81 | 1.29 |
|  |  | Sec 9 | Second ft | 20.99 | 13.68 | 1.37 |
|  |  | T 12 S | First ft | 19.83 | 10.94 | 1.28 |
|  |  | R 13E | Second ft | 21.65 | 11.53 | 1.33 |
|  |  |  | First ft | 21.67 | 12.37 | 1.37 |
|  |  |  | Second ft | 23.18 | 14.32 | 1.23 |
|  |  |  | Hardpan | 29.23 |  |  |
|  | Clowers | $\mathrm{NE}_{4} \mathrm{NE}_{4}$ | First ft | 23.41 | 11.82 | 1.29 |
|  |  | Sec 28 | Second ft | 27.37 | 13.36 | 1.30 |
|  |  | T9S | Hardpan | 29.78 | 16.55 |  |
|  |  |  | First ft | 25.00 | 11.54 | 1.41 |
|  |  |  | Second ft | 27.07 | 13.59 | 1.41 |
|  |  |  | Hardpan | 23.43 | 11.08 |  |
| Madras | $\begin{aligned} & \text { Dean } \\ & \text { King } \end{aligned}$ | S.W. 4 | 0-6 | 22.39 | 10.68 | 1.34 |
|  |  | Sec. 10 | 6-12 | 26.18 | 14.29 | 1.36 |
|  |  | $\begin{aligned} & \text { T.11S } \\ & \text { R.13E } \end{aligned}$ | 12-21 | 36.35 | 21.51 | 1.36 |
|  |  |  |  | 21.70 | 11.38 | 1.28 |
|  |  |  | 6-12 | 29.57 | 16.81 | 1.20 |
|  |  |  | 12-24 | 32.64 | 19.97 | 1.23 |
|  |  |  |  |  |  |  |
|  |  |  | 6-12 | 26.42 | 14.02 | 1.19 |
|  |  |  | 12-23 | 28.50 | 16.53 | 1.26 |
|  |  |  | 0-6 | 23.12 | 11.08 | 1.23 |
|  |  |  | 6-12 | 25.05 | 13.65 | 1.25 |
|  |  |  | 12-18 | 28.27 | 16.03 | 1.20 |


| Soil | Farm | Location | Depth <br> Inchas | Moisture Equivalent \% | Wilting Point $15 \mathrm{Atm} \%$ | Volume Weight |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Madras | Jim | SW4 SE4 | 0-6 | 25.26 | 11.86 | 1.47 |
| Sandy | Brooks | Sec. 15 | 6-12 | 25.00 | 11.66 | 1.35 |
| Loam |  | T 10 S | 12-17 | 26.85 | 16.02 | 1.34 |
|  |  | R 13 E | 17-20 | 29.09 | 17.80 | 1.35 |
|  |  |  | 0-6 | 25.52 | 12.17 | 1.41 |
|  |  |  | 6-12 | 27.60 | 14.80 | 1.40 |
|  |  |  | 12-18 | 27.86 | 15.86 | 1.41 |
|  |  |  | 18-22 | 31.88 | 20.21 | - |
|  |  |  | 22-26 | 36.47 | 25.21 | - |
|  | Duling | $\mathrm{SE}_{4}$ NW4 | $0-8$ | 25.87 | 13.49 | 1.22 |
|  |  | Sec. 17 | 8-16 | 39.03 | 25.92 | 1.17 |
|  |  | T 12 S | 16-22 | 38.99 | 26.36 | - |
|  |  | R14E | 0-8 | 26.52 | 13.14 | 1.23 |
|  |  |  | 8-16 | 44.53 | 32.62 | 1.17 |
|  |  |  | 16-22 | 43.85 | 33.66 | - |
|  |  |  | Hardpan | 35.96 | 23.20 | - |
|  | Short- <br> Johnson | W2 NW4 | 0-6 | 22.73 | 11.6 | 1.43 |
|  |  | Sec. 17 | 6-12 | 25.55 | 13.6 | 1.14 |
|  |  | T 12 S | 12-24 | 26.11 | 14.5 | 1.14 |
|  |  | R13 E | 0-6 | 22.87 | 12.2 | 1.43 |
|  |  |  | 6-15 | 24.35 | 12.8 | 1.26 |
|  |  |  | 15-24 | 26.30 | 13.7 | 1.38 |
|  |  |  | 0-6 | 21.06 | 11.3 | 1.39 |
|  |  |  | 6-14 | 24.40 | 12.6 | 1.32 |
|  |  |  | 14-22 | 25.39 | 13.1 | 1.28 |
|  |  |  | 0-6 | 22.45 | 11.2 | 1.45 |
|  |  |  | 6-12 | 24.73 | 12.5 | 1.35 |
|  |  |  | 12-20 | 24.95 | 19.7 | 1.28 |
|  |  |  |  | 29.17 | 10.7 | 1.29 |
|  |  |  | 6-11 | 23.37 | 11.3 | 1.45 |
|  |  |  | 11-16 | 23.98 | 18.6 | 1.44 |
|  |  |  | 16-20 | 28.56 | 22.9 | 1.24 |
|  |  |  | 0-6 | 24.76 | 11.6 | 1.37 |
|  |  |  | 6-9 | 30.60 | 16.0 | 1.29 |
|  |  |  | 9-25 | 30.57 | 16.0 | 1.16 |
| 42 A <br> Metolius <br> Sandy <br> Loam | Barber |  | First ft |  | 13.13 | 1.44 |
|  |  | $\text { Sec. } 18$ | Second ft | 30.25 | 17.00 | 1.36 |
|  |  | T 12 S | First ft | 25.76 | 13.39 | 1.55 |
|  |  | R 13 E | Second ft | 30.85 | 18.14 | 1.35 |
|  | LuteBarber |  |  |  | 10.5 | 1.30 |
|  |  | Sec。18 | 6-12 | 23.26 | 11.2 | 1.30 |
|  |  | T 12 S | 12-21 | 25.83 | 12.0 | 1.28 |
|  |  | R 13 E | 0-6 | 23.42 | 11.2 | 1.40 |
|  |  |  | 6-13 | 22.87 | 11.1 | 1.38 |
|  |  |  | 13-29 | 25.00 | 11.7 | 1.25 |
| $60 \mathrm{~A}$ | Coad |  |  |  |  |  |
| Metolius |  | Sec. 21 | Upper 4 f | t 19.16 | 9.10 | 1.33 1.33 |
| Sandy |  | T 13 S |  |  |  |  |


| Soil | Farm | Location | Depth <br> Inches | Moisture Equivalent \% | Wilting Point 15 Atm 5 | Volume Weight |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Metolius | William | N.E. 4 | 0-6 | 27.48 | 11.22 | 1.09 |
| Sandy | E. Wood | S.W. 4 | 6-12 | 26.40 | 10.90 | 1.12 |
| Loam |  | Sec. 3 | 12-48 | 22.88 | 9.47 | 1.04 |
|  |  | T.12.S |  |  |  |  |
|  |  | R.13E |  |  |  |  |
|  | Frank Crocker | S.E. 4 | 0-6 | 26.98 | 13.12 | 1.18 |
|  |  | N.W. 4 | 6-12 | 25.31 | 12.14 | 1.24 |
|  |  | Sec. 10 | 12-46 | 24.40 | 11.36 | 1.17 |
|  |  | $\begin{aligned} & \mathrm{T} .12 \mathrm{~S} \\ & \mathrm{R} .13 \mathrm{E} \end{aligned}$ |  |  |  |  |
| Metolius <br> Sandy <br> Loam | Jerry Drazil | Lot 4 Sec 18 T12S R13E | 0-6 | 19.39 | 8.34 | 1.29 |
|  |  |  | 6-12 | 18.84 | 9.15 | 1.38 |
|  |  |  | 12-32 | 20.77 | 8.82 | 1.45 |
|  |  |  | 0-6 | 21.39 | 9.38 | 1.20 |
|  |  |  | 6-12 | 20.75 | 9.40 | 1.26 |
|  |  |  | 12-32 | 24.62 | 11.72 | 1.35 |
|  |  |  | 0-6 | 19.08 | 9.29 | 1.24 |
|  |  |  | 6-12 | 20.28 | 10.80 | 1.32 |
|  |  |  | 12-34 | 22.41 | 9.59 | 1.43 |
| Agency Sandy Loam | Greenwood \& Sons | Lots 1 \& 2 <br> Sec. 3 <br> T12S R13E | 0-6 | 18.76 | 9.37 | 1.40 |
|  |  |  | 6-12 | 23.74 | 12.32 | 1.35 |
|  |  |  | 12-22 | 30.51 | 16.90 | 1.22 |
|  |  |  | 0-6 | 19.06 | 9.40 | 1.47 |
|  |  |  | 6-12 | 25.69 | 13.55 | 1.26 |
|  |  |  | 12-20 | 29.38 | 16.01 | 1.34 |
|  |  |  | 0-6 | 19.99 | 9.24 | 1.29 |
|  |  |  | 6-12 | 26.12 | 13.72 | 1.30 |
|  |  |  | 12-28 | 35.62 | 20.86 | 1.27 |
|  |  |  | 0-6 | 21.49 | 10.32 | 1.42 |
|  |  |  | 6-12 | 21.76 | 10.94 | 1.41 |
|  |  |  | 12-24 | 22.72 | 11.41 | 1.52 |
|  |  |  | 0-6 | 20.51 | 9.79 | 1.37 |
|  |  |  | 6-12 | 22.94 | 11.17 | 1.34 |
|  |  |  | 12-26 | 26.20 | 13.03 | 1.34 |
|  |  |  | 0-6 | 18.08 | 8.57 | 1.53 |
|  |  |  | 6-12 | 18.97 | 9.12 | 1.31 |
|  |  |  | 12-24 | 27.27 | 14.21 | 1.42 |
|  |  |  | 0-6 | 21.02 | 14.57 | 1.37 |
|  |  |  | 6-12 | 23.08 | 17.68 | 1.41 |
|  |  |  | 12-30 | 24.89 | 19.24 | 1.21 |


| Soil | Farm | Location | Depth <br> Inches | Moisture Equivalent \% | Wilting <br> Point <br> 15Atm\% | Volume Weight |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Agency | buling- | SE4 SW4 | 0-6 | 23.69 | 11.93 | 1.36 |
| Sandy | Barber | Sec. 8 | 6-12 | 25.63 | 13.48 | 1.30 |
| Loar |  | T 12 S | 12-24 | 25.09 | 13.04 | 1.27 |
|  |  | R 13 EA | Above Hardpan 26.01 |  | 13.52 | - |
|  |  |  | Hardpan | 32.23 | 19.00 | - |
|  |  |  | 0-6 | 24.38 | 11.81 | 1.31 |
|  |  |  | 6-12 | 26.06 | 13.08 | 1.40 |
|  |  |  | 12-18 | 28.57 | 13.46 | 1.40 |
|  |  |  | 18-20 | 28.37 | 15.10 | - |
| Agency | A. | N.E. 4 | 0-6 | 17.03 | 8.1 .6 | 1.37 |
| Sandy | Remsey | N.E. 4 | 6-12 | 17.86 | 8.2 .4 | 1.44 |
| Loem |  | Sec. ${ }^{\text {P }}$ | 12-30 | 18.32 | 8.25 | 1.42 |
|  |  | T. $10 . \mathrm{S}$ |  |  |  |  |
|  |  | R. 135 |  |  |  |  |
|  | L. R. Bailey | S.W. 4 | 0-6 | 21.00 | 10.58 | 1.36 |
|  |  | S.W. 4 | 6-12 | 23.46 | 11.82 | 1.20 |
|  |  | Sec. 36 | 12-18 | 26.10 | 14.41 | 1.34 |
|  |  | T.9.S |  |  |  |  |
|  |  | R. 13 E |  |  |  |  |
|  | George Clowers | S. F. 4 | 0-6 | 20.90 | 9.94 | 1.09 |
|  |  | N. F. 4 | 6-12 | 21.68 | 10.22 | 1.12 |
|  |  | Sec. 2 | 12-22 | 19.07 | 8.70 | 1.04 |
|  |  | T.10.S |  |  |  |  |
|  |  | E.J.3E |  |  |  |  |
| Agency | Floyd | N $\frac{1}{2}$ SW4 | 0-6 | 26.79 | 9.56 | 1.36 |
| Loam | Brewer | Sec 15 | 6-12 | 31.50 | 11.11 | 1.33 |
|  |  | T12S R13E | E $12-24$ | 33.36 | 13.08 | 1.36 |
|  |  |  | $0-6$ | 25.18 | 12.60 | 1.42 |
|  |  |  | 6-12 | 27.11 | 13.21 | 1.39 |
|  |  |  | 12-24 | 27.22 | 15.46 | 1.31 |
|  |  |  | $0-6$ | 24.98 | 14.03 | 1.50 |
|  |  |  | 6-12 | 24.69 | 13.37 | 1.31 |
|  |  |  | 12-26 | 27.31 | 14.74 | 1.28 |
|  |  |  | 0-6 | 21.09 | 11.04 | 1.34 |
|  |  |  | 6-12 | 20.24 | 10.69 | 1.33 |
|  |  |  | 12-30 | 20.59 | 10.40 | 1.36 |
| Agency <br> Loam | Guy | S.W. 4 | 0-6 | 23.38 | 12.36 |  |
|  | Corwin | Now. 4 | 12-34 | 24.02 |  | 1.24 |
|  |  | Sec. 1.5 T .12 S |  | 25.17 | 12.42 | 1.23 |
|  |  | R. 13 E |  |  |  |  |
|  | W. V. Merchant | N.W. 4 | 0-6 | 22.70 | 11.34 | 1.47 |
|  |  | S.W. 4 | 6-12 | 23.53 | 11.47 | 1.34 |
|  |  | Sec. 15 T .12 S | 12-27 | 35.70 | 21.80 | 1.36 |
|  |  | R.13E |  |  |  |  |


| Soil | Farm | Location | Depth <br> Inches | Moisture Equivalent \% | Wilting Point 15 Atm | Volume Weight |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Agency | Gibson- | SW4 NW4 | 0-14 | 25.73 | 13.44 | 1.42 |
| Loam | Corwin | Sec. 15 | 14-26 | 30.07 | 17.43 | 1.39 |
|  |  | T 12 S | 0-18 | 23.32 | 11.81 | 1.30 |
|  |  | R 13 E | 18-36 | 22.97 | 10.08 | 1.24 |
|  |  |  | Hardpan 26-32 | 33.45 | 18.38 |  |
| Agency | Short | W2 W44 | 0-6 | 23.86 | 12.2 |  |
| Gravely | Johnson | Sec 17 | 6-12 | 27.36 | 14.6 |  |
| Loam |  | T12S | 12-20 | 26.70 | 14.0 |  |
|  |  | R13E | 0-6 | 23.96 | 12.1 |  |
|  |  |  | 6-12 | 28.51 | 14.7 |  |
|  |  |  | 12-23 | 28.01 | 15.9 |  |
| Lamonta <br> Loam | H. P . Woodworth | N.W. 4 | 0-6 | 17.01 | 9.80 | 1.25 |
|  |  | S.W. 4 | 6-12 | 16.76 | 9.68 | 1.20 |
|  |  | Sec. 14 | 12-36 | 14.04 | 7.75 | 1.18 |
|  |  | T. 12 S |  |  |  |  |
|  |  | Ro13E |  |  |  |  |
| Lamonta <br> Lorm | Grover <br> Douglas | N. E. 4 | 0-6 | 16.00 | 8.32 | 1.39 |
|  |  | N.W. 4 | 6-12 | 17.48 | 7.88 | 1.32 |
|  |  | Sec. 27 | 12-36 | 21.42 | 9.82 | 1.28 |
|  |  | T. 12 S |  |  |  |  |
|  |  | R.13E | 0-6 | 23.08 | 11.88 | 1.38 |
|  |  |  | 6-12 | 24.00 | 12.75 | 1.20 |
|  |  |  | 12-35 | 36.70 | 20.97 | 1.20 |
|  | A. B. Cook | S.W. 4 | 0-6 | 25.12 | 14.22 | 1.43 |
|  |  | N. $\mathrm{E}^{2} 4$ | 6-12 | 28.88 | 16.04 | 1.33 |
|  |  | Sec. 22 | 12-18 | 41.08 | 26.85 | 1.16 |
|  |  | T. 12 S |  |  |  |  |
|  |  | R.13E |  |  |  |  |
| Era | Fred | S.W. 4 | 0-6 | 20.53 | 10.48 | 1.39 |
| Sendy | Silver | S.W. 4 | 6-12 | 24.93 | 13.10 | 1.25 |
| Loam |  | Sec. 4 | 12-20 | 37.04 | 24.47 | 1.28 |
|  |  | T. 12 S |  |  |  |  |
|  |  | R. 13 E |  |  |  |  |
|  |  |  | 0-6 | 23.08 | 11.88 | 1.33 |
|  |  |  | 6-12 | 24.00 | 12.75 | 1.25 |
|  |  |  | 12-35 | 36.70 | 20.92 | 1.38 |


| Soil | Ferm | Location | Depth <br> Inches | Moisture <br> Equivelent 2 | Wilting <br> Point <br> 15 Atm | Volume Weight |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Redmond | Florian | E2 NW2 | 0-6 | 23.74 | 10.29 | 1.24 |
| Sandy | Meng | Sec 4 | 6-12 | 31.18 | 17.57 | 1.23 |
| Loam (deep | phase) | TIIS R14E | 12-60+ | 34.14 | 17.54 | 1.18 |
|  |  |  | 0-6 | 22.14 | 9.64 | 1.05 |
|  |  |  | 6-12 | 33.02 | 17.49 | 1.18 |
|  |  |  | 12-60+ | 40.66 | 20.93 | 1.08 |
| Deschutes | Williem | SW4 SW4 | 0-6 | 19.57 | 9.31 | 1.13 |
| Sandy | Greene | Sec 33 | 6-12 | 26.97 | 11.31 | 1.02 |
| Loam |  | TIOS R14E | 12-48 | 27.48 | 12.1 .4 | 1.11 |
|  |  |  | 0-6 | 23.54 | 10.28 | 1.17 |
|  |  |  | 6-12 | 27.95 | 11.68 | 1.22 |
|  |  |  | 12-48 | 27.93 | 11.68 | 1.15 |
| Deschutes | Redmond | SW4 SEL4 | 0-6 | 18.69 | 7.25 | 1.22 |
| Sandy | Fairgrounds | s Sec 16 | 0-6 | 17.70 | 7.29 | 1.27 |
| Loam |  | T15S R13E | 12-30 | 16.85 | 6.99 | 1.24 |
| Deschutes | Hostetler | NE4 NE4 | 0-6 | 17.02 | 6.09 | 1.26 |
| Sandy |  | Sec. 31 | 6-12 | 15.48 | 5.48 | 1.32 |
| Loam |  | T15S R13E | 12-26 | 16.37 | 6.23 | 1.39 |
| Leschutes | Cole | $\mathrm{NE}_{4} \mathrm{NE}_{4}$ | 0-6 | 16.69 | 6.50 | 1.16 |
| Loamy |  | Sec. 6 | 6-12 | 15.66 | 6.66 | 1.36 |
| Sand |  | T2SS RIIE | 12-24 | 15.99 | 6.57 | 1.43 |
| Deschutes | Griswold | SW4 SW4 | 0-6 | 11.23 | 4.40 | 1.53 |
| Coarse Sandy |  | See 5 | 6-12 | 11.37 | 4.80 | 1.41 |
| Loam |  | T15S RIIE | 12-42 | 11.53 | 4.82 | 1.48 |
| Deschutes | Unknown | NE/ $\mathrm{NE}_{4}$ | 0-6 | 15.25 | 5.41 | 1.13 |
| Loamy |  | Sec 28 | 6-12 | 15.16 | 5.87 | 1.31 |
| Sand |  | T16S RI2E | 12-22 | 14.88 | 6.47 | 1.32 |
| Redmond | Unknown | $\mathrm{SE}_{4} \mathrm{SE}_{4}$ | 0-6 | 20.58 | 8.75 | 1.18 |
| Sandy |  | Sec 13 | 6-12 | 20.22 | 8.62 | 1.23 |
| Loam |  | T14S R13E | 12-36 | 19.78 | 8.33 | 1.33 |
| Un- <br> classed | Clifford |  | 0-18 | 18.02 | 10.3 |  |
|  | Dickson |  | 18-24 | 18.18 | 9.7 |  |
|  | Powell |  | 0-18 | 17.99 | 10.0 |  |
|  | Butte |  | 18-24 | 18.10 | 9.5 |  |
|  |  |  | 0-7 | 20.28 | 10.2 |  |
|  |  |  | 7-27 | 36.86 | 21.1 |  |
|  |  |  | 27-36 | 20.26* | 10.9 |  |
|  |  |  | 27-37 | 32.89\# | 20.8 |  |
| Un-classed | Lewie |  | 0-13 | 17.19 | 9.5 |  |
|  | Stahancyk |  | 13-20 | 24.92 | 12.8 |  |
|  | Prineville |  | 20-0 | 18.30 | 10.5 |  |

Appendix Table 2. Summar, of Disposition of Water Applied to Fields

The following explanation of the columns of this Table may be helpful. The left margin contains the yield, the average land slope, and the length of the irrigation run in addition to field identification. When column 1 has two dates, they bracket the time that water was on the field. When there is only one date, no irrigation occurred. The source of the water in column 3 was surface runoff from another field on the same farm. Column 4 is the sum of columns plus the estimalver column 4. Column 9 is column 7 divided by column 4. Column 11 was computed from the start of one irrigation to the start of the next, and column 12 is the average daily use for this period.

Consumptive Use

| Since | Per Day |
| :--- | :--- |
| Last | Irrigation |
| Inches |  | Rain Retween Inches Percent Inches

Irrigation Inches




| Field "B" | 4/26-5/1 | . 2 | 0 | 8.72 | 2.47 | 28.3 | 1.68 | 4.57 | 19.3 |  | 1.68* |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Ladino | 5/17-22 | . 2 | 0 | 6.14 | 2.33 | 37.9 | 2.24 | 1.57 | 36.5 | . 6 | 1.89 | . 09 |
| Kiser | 5/28-6/1 | 0 | 0 | 5.65 | 3.86 | 68.3 | . 93 | . 86 | 16.5 | 0 | 1.76 | . 16 |
| Farm | 6/22-26 | 0 | 0 | 7.74 | 4.77 | 61.6 | 4.08 | -1.11 | 52.7 | 1.5 | 3.84 | . 16 |
| 1952 | $7 / 14-18$ | 0 | 0 | 8.58 | 3.50 | 40.8 | 4.13 | . .95 | 48.1 | 1.3 | 6.82 | . 31 |
| $58 \mathrm{lbs} / \mathrm{ac}$ | 7/30-8/1 | 0 | 0 | 10.68 | 5.91 | 55.3 | 1.90 | 2.87 | 17.8 | - 0 | 3.68 | . 23 |
|  | 8/9-18 | 0 | 0 | 6.32 | 4.08 | 64.6 | 2.61 | -. 37 | 41.3 | 0 | 2.52 | . 28 |
| 2.1\% slope | 10/2-6 | 0 | 0 | 12.45 | 6.29 | 50.5 | 5.30 | . 86 | 42.6 | . 7 | 2.30 | . 10 |
| $370^{\prime}$ run | 11/3 |  |  |  |  | 50.5 | 5. |  |  | $\bigcirc$ | 1.86 | . .06 |
| Total | $r$ Average | . 4 | 0 | 66.28 | 33.21 | 50.91A | 22.87 | 10.20 | 34.35A | 4.1 | 26.4 | .17A |

*Consumptive use before first irrigation was estimated as equal to the soil moisture added at the first irrigation.

Summary of Disposition of Water Applied to Fields

| Field "C" | 4/18-23 | 0 | 5.83 | 5.83 | 2.53 | 43.4 | 1.20 | 2.10 | 20.6 |  | 1.20* |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Ladino | 5/6-10 | . 1 | 2.69 | 2.79 | 1.53 | 54.8 | 1.57 | -. 31 | 56.3 | . 2 | 1.62 | . 09 |
| Kiser | 5/22-26 | 0 | 3.43 | 3.43 | 1.85 | 53.9 | 2.63 | -1.05 | 76.7 | . 6 | 2.88 | . 18 |
| Farm | 6/6-10 | 0 | 4.13 | 4.13 | 1.53 | 37.0 | 2.68 | -. 08 | 64.9 | . 4 | $3 \cdot 36$ | . 24 |
| 1952 | 7/9-11 | 0 | 8.77 | 8.77 | 4.18 | 47.7 | 3.10 | 1.49 | 35.3 | 2.4 | 5.27 | . 19 |
| 123 lbs/ac | 7/18-21 | 0 | 4.00 | 4.00 | 2.61 | 65.2 | 2.97 | -1.58 | 74.2 | 0 | 2.88 | . 32 |
|  | 7/28-31 | 0 | 10.79 | 11.18 | 6.44 | 57.6 | 2.76 | 1.98 | 24.7 | 0 | 3.30 | . 33 |
| 2.1\% slope | 9/22-27 | 0 | 5.77 | 12.70 | 7.84 | 61.7 | 5.67 | -. 81 | 44.6 | - 7 | 5.40 | . 10 |
| 610.1 run | 11/3 |  |  |  |  |  |  |  |  | 0 | 2.87 | . 07 |
| Total | or Average | . 1 | 45.41 | 52.83 | 28.51 | 52.65 A | 22.58 | 1.74 | 49.66A | 4.3 | 29.8 | .19A |
| Field "D" | 4/16-22 | 0 | 4.05 | 6.28 | 2.92 | 46.5 | 2.82 | .54 | 44.9 | 0 | 1.72 | . 11 |
| Ladino | 5/9-14 | . 5 | 3.04 | 5.96 | 2.14 | 35.9 | 1.99 | 1.83 | 33.4 | . 3 | 2.07 | . 09 |
| Kiser | 5/22-27 | 0 | 4.51 | 4.85 | 2.44 | 50.3 | 1.36 | 1.05 | 28.0 | . 1 | 2.34 | . 18 |
| Farm | 6/13-17 | . 4 | 6.24 | 6.83 | 3.13 | 45.8 | 2.36 | 1.34 | 34.6 | 0 | 1.89 | . 09 |
| 1952 | 7/10-13 | 0 | 4.77 | 5.18 | 2.32 | 44.8 | 1.99 | . 87 | 38.4 | 1.6 | 4.86 | . 18 |
| 123 1bs/ac | 7/19-23 | 0 | 4.06 | 4.54 | 2.63 | 57.9 | 3.30 | -1.39 | 72.7 | 0 | 2.43 | . 27 |
| 123 1bs/a | 7/30-8/2 | 0 | 4.62 | 5.35 | 3.62 | 67.7 | 2.30 | -. 57 | 43.0 | 0 | 3.41 | . 31 |
|  | 9/24-10/2 | 0 | 6.47 | 8.23 | 4.62 | 56.1 | 5.56 | -1.95 | 67.6 | - 7 | 5.40 | $.10$ |
| $620^{\prime} \text { run }$ | $11 / 3$ |  |  |  |  |  |  |  |  | 0 | $2 \cdot 73$ | . 07 |
| Total | or Average | . 9 | 37.76 | 47.22 | 23.82 | 50.62A | 21.68 | 1.72 | 45.32 A | 2.7 | 26.8 | .16A. |
| Field "E" | 4/25-5/1 | . 2 | 14.70 | 14.90 | 5.91 | 39.7 | 2.31 | 6.68 | 15.5 | 0 | 0.4 | . 02 |
| Ladino | 5/10-13 | 0 | 14.97 | 14.97 | 8.69 | 58.0 | 1.05 | 5.23 | 7.0 | . 1 | 1.35 | . 09 |
| Kiser | 5/29-6/3 | 0 | 14.80 | 14.80 | 9.14 | 61.8 | 3.29 | 2.37 | 22.2 | . 1 | 2.28 | . 12 |
| Farm | 6/26-7/2 | 1.2 | 5.09 | 6.29 | 1.56 | 24.8 | 3.55 | 1.17 | 55.6 | 1.5 | 4.59 | . 17 |
|  | 7/9-11 | 0 | 12.22 | 12.22 | 4.32 | 35.4 | 3.86 | 4.04 | 31.6 | 0 | 4.16 | . 32 |
| 5.4\% slope | 7/22-26 | 0 | 20.73 | 20.73 | 11.15 | 53.8 | 2.09 | 7.49 | 10.1 | 0 | 3.38 | . 26 |
| $270^{\prime}$ run | 10/4-11 | 0 | 0 | 19.77 | 10.27 | 51.9 | 5.60 | 3.90 | 28.3 | - 7 | 5.04 | . 07 |
|  | 11/4 | 0 |  |  |  |  |  |  |  |  | 1.50 | . 05 |
| Total | or Average | 1.4 | 82.51 | 103.68 | 51.04 | 46.49A | 21.76 | 30.88 | 24.47 A | 2.4 | 22.7 | .14 A |

[^1]Sumnary of Disposition of Water foplied to Fields

|  |
| :---: |
| $\dot{\sim} \dot{\sim} \dot{\sim}$ |
|  |  |
|  |  |

$090 \infty$ O

$28.0 \quad .15 \mathrm{~A}$
世
$\stackrel{4}{1}$
$!$
꼬옹


| Sumary of Disposition of Water Applied to Fields |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Field "I" | 4/18-22 | 0 | 7.97 | 7.97 | 2.42 | 30.4 | 2.54 | 3.01 | 31.9 | . 2 | 1.24 | . 07 |
| Pasture | 5/2-7 | 0 | 11.12 | 11.12 | 5.24 | 47.1 | 1.70 | 4.18 | 15.3 | . 2 | 2.38 | . 17 |
| Kiser | 5/15-18 | 0 | 6.74 | 6.74 | 4.55 | 67.5 | . 85 | 1.34 | 12.6 | . 6 | 1.95 | . 15 |
| Ferm | 5/26-29 | 0 | 8.35 | 8.35 | 4.41 | 52.8 | 1.38 | 2.56 | 16.5 | . 1 | 1.21 | .11 |
| 1952 | 6/2-4 | 0 | 5.65 | 5.65 | 1. 32 | 23.4 | 1.34 | 2.99 | 23.7 | - | 1.44 | . 24 |
|  | 7/7-10 | 0 | 4.96 | 4.96 | 2.16 | 43.5 | 2.74 | . 06 | 55.2 | 2.8 | 5.60 | . 16 |
| 9.3\% slope | 7/15-18 | 0 | 10.58 | 10.58 | 4.52 | 42.7 | 1.82 | 4.24 | 17.2 | 0 | 2.24 | . 28 |
| 150' run | 7/24-27 | 0 | 17.10 | 17.10 | 12.13 | 70.9 | 1.69 | 3.28 | 9.9 | 0 | 1.08 | . 12 |
|  | 8/3-6 | 0 | $\stackrel{0}{0}$ | 9.65 | 5.00 | 51.8 | 2.61 | 2.04 | 27.0 | 0 | 1.53 | . 17 |
|  | 8/8-12 | 0 | 20.74 | 20.74 | 11.93 | 57.5 | 2.44 | 6.37 | 11.8 | 0 | 2.80 | . 56 |
|  | 8/18-26 | 0 | 9.78 | 9.78 | 3.75 | 38.3 | 4.34 | 1.69 | 44.4 | . 1 | 1.60 | . 16 |
|  | 9/3-12 | 0 | 34.70 | 34.70 | 13.63 | 39.3 | 3.50 | 17.57 | 10.1 | 0 | 5.25 | . 35 |
|  | 10/3-9 | . 7 | 0 | 26.38 | 13.94 | 52.8 | 2.73 | 9.71 | 10.3 | 0 | 4.20 | . 14 |
|  | 11/4 |  |  |  |  |  |  |  |  | 0 | 1.55 | . 05 |
| Total or Average |  | . 7 | 137.69 | 173.72 | 85.00 | 47.54A 29.68 |  | 59.04 | 21.99A | 4.0 | 34.1 | -20A |
| Field "C" <br> Potatoes <br> King Farm <br> 1952 <br> $16 \mathrm{~T} / \mathrm{ac}$ | $6 / 10-13$$6 / 26-7 / 2$ | . 4 | 0 | 6.21 | . 85 | 13.7 |  |  | 36.9 | . 4 | 0.4 | . 07 |
|  |  | 1.2 | 0 | 5.59 | 1.68 | 30.1 | 2.04 | 1.87 | 36.5 | .40 | 1.44 | . 09 |
|  | 7/6-8 $7 / 11-15$ | 0 | 0 | 3.99 | 2.95 | 73.982.4 | 1.06 | -. 02 | 26.6 |  | 2.30 | . 23 |
|  |  | 0 | 0 | 2.45 | 2.02 |  | . 29 | . 14 | 11.8 | 0 | 2.30 | . 46 |
|  | $7 / 11-15$ $7 / 16-18$ | 0 | 0 | 2.732.26 | $\begin{aligned} & 1.82 \\ & 1.86 \end{aligned}$ | 66.7 | .05-.88 | $\begin{array}{r} .86 \\ .48 \end{array}$ | 1.8 | 0 | $\begin{gathered} 0 \\ .40 \end{gathered}$ | 0.10 |
|  | $7 / 16-18$ $7 / 20-21$ | 0 | 0 |  |  | 82.3 |  |  | 38.9 | 0 |  |  |
| $0.6 \%$ slope $660^{\prime}$ run | 7/23-26 | 0 | 0 | $\begin{aligned} & 3.33 \\ & 4.00 \end{aligned}$ | 2.46 | 73.9 | . .04 | . 83 | 1.218.5 | 0 | 1.41 | . 47 |
|  | $7 / 27-29$$7 / 31-8 / 5$ | 0 | 0 |  | $\begin{aligned} & 3.04 \\ & 3.88 \end{aligned}$ | 76.0 | . 74 | $\begin{aligned} & .22 \\ & .39 \end{aligned}$ |  | 00 | 0 | 0 |
|  |  | 0 | 0 | 4.31 |  | 90.0 | $\begin{aligned} & .04 \\ & .48 \end{aligned}$ |  | $\begin{array}{r} 0.9 \\ 12.0 \end{array}$ |  | 1.36 | $\begin{aligned} & .34 \\ & .08 \end{aligned}$ |
|  | $7 / 31-8 / 5$ $8 / 7-9$ | 0.3 | 0 | 3.99 | 2.92 | 73.2 |  | $\begin{array}{r} .39 \\ .59 \end{array}$ |  | 0 | . 48 |  |
|  | $8 / 12-14$$8 / 15-17$ |  | 0 | 4.40 | 3.36 | 76.4 | 1.20 | $-.16$ | $\begin{aligned} & 12.0 \\ & 27.3 \end{aligned}$ | 0 | . 40 | . 08 |
|  |  | 0 | 0 | 2.38 | 2.22 | 93.3 | . 95 | -. 79 | 39.9 | 0 | 1.32 | . 44 |
|  | 8/18-20 | 0 | 0 | 4.16 | 3.25 | 78.1 | . 50 | . 41 | 12.0 | 0 | 1.08 | . 36 |
|  |  | 0 | 0 | 4.08 | 2.90 | 71.1 | . 62 | . 56 | 15.2 | 0 | . 50 | . 10 |
|  | 8/28-31 | 0 | 0 | $\begin{aligned} & 4.60 \\ & 4.16 \end{aligned}$ | $\begin{aligned} & 3.42 \\ & 3.24 \end{aligned}$ | $\begin{array}{r} 74.3 \\ 77.9 \end{array}$ | $\begin{array}{r} 1.73 \\ .38 \end{array}$ | $\begin{array}{r} -.55 \\ .54 \end{array}$ | $\begin{array}{r} 37.6 \\ 9.1 \end{array}$ | 00.4 | $\begin{array}{r} .60 \\ 2.20 \\ .91 \end{array}$ | $\begin{aligned} & .12 \\ & .44 \\ & .07 \end{aligned}$ |
|  | $9 / 2-4$ $9 / 15$ | 0 | 0 |  |  |  |  |  |  |  |  |  |
| Total or Average |  | 1.9 | 0 | 62.64 | 41.87 | 70.83 A 13.29 |  | 7.48 | 20.39A | 1.2 | 17.1 | . 20 |

Summary of Disposition of Water Applied to Fields

Surmary of Disposition of Water Applied to Fields


Sumary of Disposition of Water Applied to Fields

Summary of Disposition of Water Applied to Fields

Summary of Disposition of Water Applied to Fields

Summary of Disposition of Water Applied to Fields



[^0]:    *Formerly Research Assistant, Oregon Agricultural Experiment Station, Associate Agricultural Engineer, Oregon Agricultural Experiment Station, and Agricultural Engineer, Region 1, U. S. Bureau of Reclamation, respectively.

[^1]:    *Consumptive use before first irrigation was estimated as equal to the soil moisture added at the first irrigation.

