

DURABILITY OF GLUED WOOD TO METAL JOINTS

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DURABILITY OF GLUED WOOD TO METAL JOINTS¹

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This study on the durability of glued wood-to-metal joints subjected to various exposure conditions was conducted at the request of the Army-Navy-Civil Committee on Aircraft Design Criteria. The purpose of the study was to gain information on the comparative durability properties of wood-to-metal joints made with different commercial adhesives, so that they might be more widely and safely used in aircraft construction. Exposure conditions were selected to measure resistance of painted and unpainted aluminum-to-wood and steel-to-wood joints to water, high humidities, high and low temperatures, aircraft fluids, and weather.

Type of Specimen

The type of specimen used for this study consisted of a 1- by 2-inch piece of 0.037-inch (20 gauge) cold-rolled steel or 0.032-inch aluminum-clad aluminum alloy lap-jointed 1/2-inch with a 1-1/4- by 2-inch piece of three-ply, 3/16-inch yellow birch plywood (fig. 1). With one of the adhesives (glue C of table 1), some specimens were prepared by direct bonding of the metal and birch, and other specimens with a 1/28-inch shim of walnut veneer in the lap area between the metal and the birch plywood. In one-half of the specimens, the metal portion was protected with paint.

Glues and Gluing Processes

Six commercial gluing processes formulated for use in bonding wood to metal were included in this study. With two of these gluing processes, a woodworking resorcinol resin was used as a secondary glue. These gluing processes are designated by numbers and the glues by letters as given in table 1.

¹This is one of a series of progress reports prepared by the Forest Products Laboratory relating to the use of wood in aircraft. Results here reported are preliminary and may be revised as additional data become available.

The processes by which the glues were employed differed according to the manufacturer's instructions. Glues A, C, and F were used by themselves in direct bonding. Glues D and E were used together in direct bonding. Glue G was used as the secondary glue with glue B and, in process 6, as a secondary glue for bonding the birch to the walnut shim.

Test Procedures

Preparation of Metal for Gluing

Gluing Process 1.--One- by 2-inch pieces of steel and aluminum-clad aluminum alloy were placed in a jig and 9/64-inch locating holes drilled into them (fig. 2). Burrs formed in drilling were ground off.

The steel pieces were degreased by immersion for 4 to 6 minutes in a hot (160° to 180° F.) trisodium phosphate solution prepared by saturating warm water with trisodium phosphate and adding 0.5 gram of wetting agent per 100 cubic centimeters of solution. The solution was rinsed from the pieces with cold tap water and then with hot distilled water.

After degreasing, the steel pieces were etched for about 5 minutes in an acid solution of the following composition:

Parts by volume

Concentrated hydrochloric acid	50
30 percent hydrogen peroxide	2
Formalin	10
Distilled water	45

If 5 minutes' immersion was not sufficient time to remove all evidence of rust or mill scale, the etching treatment was continued as long as necessary. Immediately after etching, the metal pieces were rinsed in flowing tap water, immersed in hot distilled water, dipped in acetone, and air dried.

The small aluminum pieces were wiped with a cloth wet with acetone to remove the identification lettering. They were then degreased by immersing in a hot (160° to 180° F.) bath of the following composition:

Sodium metasilicate	3.6 ounces
Wetting agent	.4 ounce
Distilled water	1.0 gallon

The pieces were immersed until the film of wash tap water showed no "break" as it drained. The period of immersion ranged from 7 to 12 minutes. After degreasing, the pieces were rinsed successively in cold tap water, hot distilled water, and acetone, and finally air dried.

Gluing process 2.--For gluing with this process, 8- by 8-inch metal squares were degreased and etched preparatory to application of glue and cutting into 1- by 2-inch pieces.

The steel squares were degreased and etched in the same manner as described for the small steel pieces under Gluing Process 1.

The aluminum squares were wiped with an acetone-soaked cloth to remove the identification lettering, degreased in sodium metasilicate solution in the same manner as described under Gluing Process 1, then immersed for about 20 minutes at 140° to 150° F. in an acid bath of the following composition:

<u>Parts by weight</u>	
Sodium dichromate	1
Concentrated sulphuric acid	10
Distilled water	30

After etching, the pieces were rinsed in tap water, immersed in hot distilled water, dipped in acetone, then air dried.

Gluing Process 3.--Steel sheets, 8 by 8 inches in size, were degreased and etched in accordance with the recommendations by the manufacturer of glue C (Process 3). The degreasing was done by immersion for 5 to 7 minutes in a boiling bath of the following composition:

Sodium carbonate	2.0 ounces
Sodium hydroxide	2.0 ounces
Wetting agent	0.5 ounce
Sodium metasilicate	3.0 ounces
Laundry soap	0.5 ounce
Distilled water	1.0 gallon

After rinsing in cold tap water, the sheets were immersed for 2 to 4 minutes at room temperature in a pickling solution of the following composition:

<u>Parts by volume</u>	
Concentrated sulphuric acid	10
Concentrated nitric acid	10
Distilled water	80

The steel sheets were rinsed in tap water and then immersed for approximately 1 minute at room temperature in a "bright" acid bath of the composition:

<u>Parts by volume</u>	
Concentrated hydrochloric acid	60
30 percent hydrogen peroxide	2
Distilled water	38

Afterwards, the sheets were rinsed in running tap water, immersed in hot water, dipped in acetone, and air dried.

The aluminum sheets were degreased in a sodium metasilicate solution and etched in sodium dichromate-sulphuric acid in the same manner as described for Gluing Process 2.

Gluing Process 4.—One by 2-inch pieces of metal were drilled and deburred as described under Process 1. The steel pieces were degreased and etched as in Gluing Process 1. The aluminum was degreased as in Gluing Process 2.

Gluing Process 5.—The drilling and deburring of metal pieces was done as described under Gluing Process 1. The steel was degreased and etched as in Gluing Process 1. The aluminum pieces were cleaned as in Gluing Process 2.

Gluing Process 6.—The metal test pieces were prepared as in Gluing Process 3.

Preparation of Plywood and Veneer

Gluing Processes 1, 2, 3, 4, and 5.—Selected aircraft-grade 1/16-inch yellow birch veneer was bonded with phenol-resin film glue into three-ply, 3/16-inch plywood. The plywood panels were conditioned for at least 1 week at 80° F. and 30 percent relative humidity, then cut into pieces 3 by 8 inches in size, with the grain direction of the face plies parallel to the shorter dimension of the piece. The portion of plywood to which the metal was to be bonded was lightly sanded with No. 00 garnet sandpaper.

Gluing Process 6.—In this process, 1/28-inch sliced walnut veneer was used as a shim between the metal and plywood. The walnut veneer was conditioned to equilibrium at 30 percent relative humidity and 80° F., then cut into 1/2-inch strips about 9 inches long, with the grain direction in the shorter direction of the ply.

Assembly and Gluing

The glues were used as far as possible in accordance with the manufacturer's directions.

Gluing Process 1; Glue A.—The glue was thinned to brushing consistency with an equal volume of ethyl acetate. The glue was spread with a brush to both the metal and the plywood in the area of the lap. The first coat was allowed to air-dry at least 1 hour, then a second coat was applied. After the second coat, an open assembly period of 2 to 48 hours was allowed. Groups of 12 specimens were prepared by assembling two panels of six specimens each in a jig, as shown in figure 3. This assembly was set on the

platens of an electric hot press and heated without pressure for 15 minutes at 325° F., after which a pressure of 300 pounds per square inch was applied and the heating continued for an additional 15 minutes. The assembly was removed from the press while hot, but a short cooling period was allowed before the two panels were removed from the jig (fig. 4).

Gluing Process 2; Glues B and G.—The 8- by 8-inch metal pieces were masked with tape (fig. 5) so as to leave exposed slightly more than 1/2 inch of lap-joint area at the end of the 1- by 2-inch pieces into which they were subsequently cut.

Glue B was thinned to a thin spraying consistency with approximately two parts of a special solvent to one of glue. The amount of thinner was varied somewhat, according to the viscosity of different lots of glue. Four coats were applied by spraying to the unmasked areas of each piece, with about one-half hour allowed for air drying between coats. A spray pressure of about 45 pounds per square inch was used, the gun was held 8 to 10 inches from the panel, and the nozzle adjusted to give a fan-shaped, atomized spray.

After the fourth coat was applied, the metal pieces were exposed to room conditions overnight, then baked for 20 to 45 minutes in an electric oven at 310° to 325° F.² The cured film was about 0.002 inch thick and greenish-brown in color. It was lightly sanded with No. 1/2 emery cloth.

The 8- by 8-inch squares were next cut into 1- by 2-inch pieces, which were attached to the birch plywood with tape so that the primed surface protruded as shown at the left in figure 6. Glue G was then brush spread to both the cured adhesive primer and a piece of birch plywood in the area of the lap (fig. 6). After an open assembly period of 2 minutes, the metal and plywood were laid together and placed in a book press (fig. 7) between thin yellow-poplar veneer, sheets of rubber, and heavy birch plywood cauls. After the period of 10 to 15 minutes that was required to arrange six layers of 18 specimens each in the press, pressure of 100 to 150 pounds per square inch was applied. The pressure was maintained overnight (approximately 18 hours) at room temperature of 80° to 90° F. The assembly was taken from the press, tapes removed, separated into 18 individual panels, and each panel sawn into six specimens.

Gluing Process 3; Glue C.—One volume of the glue was thinned to spraying consistency with 0.8 volume of a special solvent. Eight-inch squares were employed as in Gluing Process 2. The adjustment of the spray gun was the same as used in spraying Glue B, but the air pressure was reduced to about 10 pounds per square inch. Six double passes of the spray gun were made to apply enough glue to the metal and plywood to result in a dry film thickness of approximately 0.002 inch. A flash-off period of about 10 minutes was allowed after each double pass of the spray. The final

²The manufacturer's recommendation was 15 minutes at 300° F. but under these conditions the glue film did not adhere properly to the metal, and longer baking at high temperature was found to give better adhesion.

coating was allowed to air dry overnight, then baked in an oven at 180° F. for 45 minutes. As in Process 2, the 8-inch squares were cut into the 1- by 2-inch metal pieces. The metal and plywood were assembled together in the pressing jig (fig. 3), and the assembly was cured for 20 minutes at 325° F. at a pressure of 300 pounds per square inch.

Gluing Process 4; Glues D and E.—The lap area of the 1- by 2-inch metal pieces was sprayed with Glue D at 40 pounds of air pressure, 10 double passes being made with the spray gun to build up a dry film thickness of about 0.003 inch. An air-drying period of 24 hours was then allowed for evaporation of solvent from the adhesive.

Two coats of glue E were applied by brush to the plywood, allowing 10 minutes for the first coat and 20 minutes for the second coat to air dry. The metal pieces were then assembled to the plywood, and the assembly was cured for 30 minutes at 325° F. and 100 pounds per square inch pressure.

Gluing Process 5; Glue F.—Two coats of liquid glue F were brushed on the lap area of the 1- by 2-inch metal pieces, allowing approximately 30 minutes between coats. Immediately after the second coat, the metal pieces were dipped into a mound of the powdered component of glue F so that a uniform layer of powder adhered to the liquid resin on the surface of the metal. Following this step, an open assembly period of 1 to 24 hours was allowed, then the 12 metal pieces and two plywood pieces were assembled in the jig (fig. 3) and placed in an electric hot press. The assembly was cured at 320° F. for 15 minutes at a pressure of 150 pounds per square inch and taken from the press without cooling. The panels were removed from the jig (fig. 4) after a short cooling period.

Gluing Process 6; Glues C and G.—The 8-inch metal squares were masked (fig. 5), coated, and cut into small pieces, as described under Gluing Process 2. Glue C was thinned, sprayed, and precured on the metal and the walnut shims, by the same method as used in Process 3. The small metal pieces and walnut shims, 1/2-inch wide, were assembled on a caul of yellow-poplar veneer so that the adhesive coatings on the metal and shims were in contact (fig. 8). The entire assembly was pressed in an electric hot press for 25 minutes at 325° to 330° F. at 175 pounds per square inch. After gluing the metal pieces to the walnut shims, the surface of the walnut was lightly sanded to remove any contamination. Glue G was then applied to the walnut shim and birch plywood, which were glued together by the procedure used in bonding the metal to the plywood for Process 2 (figs. 6 and 7).

It was evident during the preparation of the specimens with the walnut shims that some shims were unaccountably weak. All the shim specimens, therefore, were pretested with 500 pounds tension load, and those that failed were replaced to complete the sets.

Number of Panels and Specimens

For each glue and metal, 160 panels of 6 specimens in each were prepared, except for Process 4, glues D & E, for which only 34 panels were prepared with each metal. In all, a total of 11,928 specimens were prepared.

Painting the Specimens

The panels of each set were randomly distributed into two groups, one to be painted, the other to be left unpainted. To the specimens requiring painting were applied one brush coat of zinc chromate primer conforming to Federal Specification AN-TT-P-565, thinned with three parts of thinner to four parts of the primer, and two brush coats of aluminized glycerol phthalate spar varnish conforming to Federal Specification AN-TT-A-461. The paint was applied to the metal only and, if any paint overlapped on to the wood, the paint film was cut precisely to the glue joints with a knife.

Cutting the Specimens

After painting and numbering of the specimens, the plywood portion of the panel was cut to specimens of the desired dimensions (fig. 1).

Distribution of Test Specimens

The painted and unpainted specimens for each gluing process were sorted into 11 lots of 40 specimens each to be subjected to 11 exposure conditions. Distribution was such that only one specimen from each pair of panels (12 specimens) made in the same pressing operation would be included in each exposure condition. Each lot of 40 specimens was divided into 8 groups of 5 specimens for testing after certain exposure intervals, only one or two specimens from each pair of panels being tested at any test period.

Specimens glued by process 4 were included in only four exposure conditions, and therefore the distribution varied slightly, but the general distribution method was the same as for the other glues.

Exposure Conditions

All specimens were first conditioned for at least 1 week at 80° F. and 30 percent relative humidity. For each gluing process and combination of metal and wood used, 55 specimens were tested dry as controls without exposure. These control specimens were selected about equally from both the painted and unpainted specimens reserved for the first test. The other half of these reserved specimens (55) along with the extra specimens resulting from the distribution method were mounted on a board and exposed continuously to the weather.

The remaining groups of specimens prepared by the different gluing processes (excepting Process 4) were exposed to the following exposure conditions:

1. Continuous exposure to air of 80° F. and 30 percent relative humidity.
2. Continuous soaking in tap water at room temperature.
3. Continuous exposure to air of 80° F. and 97 percent relative humidity.
4. Alternate exposure for 2 weeks at 80° F. and 97 percent relative humidity, and 2 weeks at 80° F. and 30 percent relative humidity.
5. Continuous exposure to air at 158° F. and 20 percent relative humidity. The specimens were tested after conditioning 1 week at 80° F. and 30 percent relative humidity.
6. Alternate exposure for 1 day at 158° F., 20 percent relative humidity, and 1 day at -67° F. in a cabinet cooled with solid carbon dioxide. The specimens were tested after conditioning 1 week at 80° F. and 30 percent relative humidity.
7. Continuous soaking at exterior temperature in 100-octane gasoline.
8. Continuous soaking at exterior temperature in 73-octane gasoline.
9. Continuous soaking at exterior temperature in ethylene glycol.
10. Continuous soaking at exterior temperature in isopropyl alcohol de-icer fluid.
11. Continuous soaking at exterior temperature in aircraft lubricating oil.

In addition to the control and exterior exposure tests, specimens prepared by Gluing Process 4 were exposed to conditions 1, 2, 3, and 4.

It was planned to remove for testing five specimens of each kind from exposure conditions 1, 3, 4, 5, and 6 after 4, 8, 16, 24, 32, 52, and 104 weeks; from conditions 7, 8, 9, 10, and 11 after 2, 4, 6, 8, 12, 24, and 52 weeks; and from condition 2 after 3, 4, 6, 7, 8, 16, and 24 weeks. Specimens exposed to exterior conditions are to be removed after 12, 24, 52, and 104 weeks.

Testing

All specimens were tested by applying a tension force to the specimen in a standard plywood testing machine at a rate of 600 to 800 pounds per minute.

Results

The average shear-strength values and estimated percentages of wood and glue failure obtained on the unexposed control specimens and on the specimens exposed up to 52 weeks are given in tables 2 through 13. The area of failure was distinguished as to location (a) in the wood, (b) in the primary glue, (c) in the interface between the glue and metal, or (d) in the secondary glue in those processes in which a secondary glue was employed.

There was some difference in the level of the joint strengths shown by the control specimens for the several processes. Gluing Processes 1, 3, and 4 gave the highest average values (936 to 1,000 pounds per one-half square inch), processes 2 and 5 the next (716 to 855 pounds per one-half square inch), and process 6 the least (544 to 652 pounds per one-half square inch). There seemed to be no consistent superiority in strength of the specimens made with one metal over those made with the other metal.

Throughout this study there was little evidence that paint coatings applied to the metal portion of the specimen importantly improved the durability of the joint. In some instances, the effect of the exposure was delayed a few weeks, but even a short delay was not always evident. In analyzing the test data, the results on painted and unpainted specimens were usually so nearly indistinguishable that they were considered together.

Continuous exposure to 80° F. and 30 percent relative humidity (table 2).---Of the specimens glued by Processes 1, 2, and 5, there were no significant changes in joint quality during a year of storage at 80° F. and 30 percent relative humidity. The same was true for the aluminum specimens glued by Process 3, but with the steel specimens made by this process there was a drop in joint strength and wood failure even under these very mild conditions. Of the specimens glued by Process 4, there was a definite indication of decreasing joint quality during the year for both steel and aluminum specimens. The specimens glued by Process 6 showed a slight falling trend in joint quality, but it is not definite enough to be conclusive.

Continuous soaking in water (table 3).---The aluminum specimens glued by Process 1 averaged only 59 to 65 percent of the strength of the controls when soaked 3 weeks in water, but there was only a little further loss in strength after soaking for 24 weeks. There was appreciably more failure of the glue to the aluminum in the wet specimens than in the dry controls. The steel specimens glued by Process 1 averaged only 47 to 52 percent of their dry strength when soaked 3 weeks, but there was little change thereafter up to 24 weeks in water.

The aluminum specimens glued by Process 2 averaged 60 to 72 percent of their dry strength when soaked 3 weeks, but there was no apparent further change. There was considerably more failure of the glue at the interface with the aluminum in the wet specimens than in the dry. The steel specimens averaged only 30 to 47 percent of their dry strength after 3 weeks of soaking, but there was little change thereafter. Considerably more failure occurred at the steel interface in the wet specimens than in the dry.

The aluminum specimens glued by Process 3 had 56 to 66 percent of their dry strength when soaked 3 weeks, but no consistent change in the joints was apparent until between 16 and 24 weeks of soaking, when the joint strength dropped sharply to about one-third the dry strength value; considerable increase in the percentage of failure took place at the aluminum interface. The steel specimens glued by Process 3 had only 23 to 31 percent of their dry strengths after soaking 3 weeks and failed almost completely in the bond to the steel, but there was little apparent change thereafter up to 24 weeks.

The aluminum specimens glued by Process 4 had 57 to 63 percent of their dry strength when soaked 3 weeks and there was a considerable increase in the portion of the failure that occurred at the aluminum interface, but little change occurred between 3 and 24 weeks. The steel specimens lost almost all their strength in 3 weeks of soaking and failed entirely in adhesion of the glue to the steel.

The aluminum specimens glued by Process 5 had 78 to 85 percent of their dry strength and showed somewhat greater failure in adhesion to the aluminum after soaking 3 weeks in water, but little change thereafter up to 24 weeks. The steel specimens had only 30 to 40 percent of their dry strength after 3 weeks in water, and failed almost completely in adhesion to the steel.

The aluminum specimens glued by Process 6 had 46-69 percent of their dry strength when soaked 3 weeks in water, and there was appreciably more failure in adhesion of the glue to the metal in the wet specimens than in the dry, but there was little further change between 3 and 24 weeks in water. The steel specimens retained only 10 to 22 percent of their dry strength after 3 weeks in water and failed completely in adhesion to the steel.

Continuous exposure to 97 percent relative humidity (table 4).--The aluminum specimens glued by Process 1 fell to about 65 percent of their dry strength on becoming moist in the air of high relative humidity, but showed only slow or no decline thereafter for several months. Between 32 and 52 weeks, joint strength dropped sharply because of deterioration of the wood, as evidenced by high wood failure. The steel specimens showed similar behavior with less evidence of deterioration of the wood at 52 weeks.

Both aluminum and steel specimens glued by Process 2 lost strength on becoming moist in high relative humidity, but lost little strength thereafter until the wood began to fail.

Both aluminum and steel specimens glued by Process 3 showed progressive loss in shear strength which was undoubtedly influenced, particularly in the latter part of the year, by deterioration of the wood.

The aluminum specimens glued by Process 4 lost strength when they took up moisture in the air of high relative humidity, but showed little change thereafter up to 52 weeks. The steel specimens showed, in general, a progressive loss in strength with time of exposure and increase in the amount of adhesion failure of the glue to the steel.

With both aluminum and steel specimens glued by Process 5, there was relatively little change in joint strength in this exposure, although there was a general increase in adhesion failure to the steel.

Both the aluminum and steel specimens glued by Process 6 lost strength when they took up moisture at the high relative humidity, but showed little change thereafter except for the changes that were probably due to deterioration of the wood. The failure in adhesion was high for the steel specimens after they had been exposed to the high humidity for a few weeks.

Alternate exposure to 97 and 30 percent relative humidity (table 5).--
The aluminum and steel specimens glued by Processes 1 and 2 showed little change during the year of exposure to this cycle.

The aluminum specimens glued by Process 3 showed little change in this exposure over 1 year; the steel specimens showed a moderate decrease in strength of about 22 percent and a gradual increase in failure between the glue and the steel.

The aluminum specimens glued by Process 4 showed a moderate to considerable decrease in the strength of the specimens without a significant change in the nature of the failure. The steel specimens showed a considerable drop in strength, with increase in failure between glue and steel.

The aluminum and steel specimens glued by Process 5 showed no very great change under these cyclic conditions during the year of exposure. The aluminum specimens glued by Process 6 showed little change in 1 year in this cycle. The steel specimens dropped in strength and increased in adhesion failure to the steel.

Continuous exposure to 158° F. and 20 percent relative humidity (table 6).--In this exposure, the wood appeared to be reduced in strength by the high temperature, and the percentage of wood failure, therefore, increased except in those cases where the glues were affected by the exposure.

The aluminum specimens glued by Process 1 showed a moderate drop in strength with an increase in percentage of wood failure. The steel specimens showed little or no significant drop in strength but a slight to moderate increase in failure between glue and steel.

Both the aluminum and the steel specimens glued by Process 2 showed a considerable drop in strength and increase in the percentage of wood failure, but not an increase in the adhesion failure to the metal.

The aluminum specimens glued by Process 3 showed a considerable drop in joint strength and an appreciable increase in adhesion failure in the year at this exposure. The steel specimens, both painted and unpainted, rusted badly and lost practically all their strength in 1 year, failing at the interface between glue and steel.

In the aluminum specimens glued by Process 5, there was a slight drop in strength at the end of the year and an increase in wood failure, but no apparent change in the glue. With the steel specimens, there was a slight increase in the amount of failure in adhesion to the metal, but otherwise little change.

For the aluminum specimens glued by Process 6, there was a large drop in strength and an increase in the failure that occurred in the primary glue (Glue C) and at the interface between Glue C and the metal. The steel specimens rusted badly and failed completely at the metal interface after a year's time, with practically no strength left.

Alternate exposure to 158° F. and -67° F. (table 7).—The specimens exposed to this alternately hot and cold cycle behaved in general like the specimens subjected continuously to the hot, humid exposure, but with less change.

Continuous soaking in 100-octane gasoline (table 8).—Both aluminum and steel specimens glued by Process 1 showed some increase in joint strength during immersion for 2 to 6 weeks, then a sharp drop. At the end of the year, the specimens failed almost entirely in the glue.

Other than a slight increase in tendency to fail in adhesion to the metal, there was practically no change in the specimens glued by Process 2 that were soaked in this high-octane gasoline.

Both aluminum and steel specimens glued by Process 3 were affected by the gasoline, so that there was a large drop in joint strength and wood failure. After a few weeks, the specimens were failing largely in the glue. At the end of the year, the steel specimens failed to a considerable extent in the interface at the steel.

Very little change was caused by the gasoline in the specimens glued by Process 5.

The specimens glued by Process 6 showed a slight drop in 2 to 4 weeks in the gasoline, with an increase in the failure of the primary glue, but little change thereafter.

Continuous soaking in 73-octane gasoline (table 9).—Gasoline of 73-octane rating had less effect on the specimens glued by Process 1 than the 100-octane gasoline. Both aluminum and steel specimens showed some increase in the percentage of failure that occurred in the glue after soaking 1 year. The gasoline treatment produced an increase in shear strength for 24 weeks, after which there was a sharp decline.

The specimens glued by Process 2 showed little or no significant change during the year's immersion in gasoline.

For the specimens glued by Process 3 there was a considerable drop in joint strength in 52 weeks, and increased glue failure.

The specimens glued by Process 5 showed little or no significant change during the year's immersion in gasoline.

The specimens glued by Process 6 lost moderately in joint strength by soaking in gasoline for a year. The gasoline increased the failure within the primary glue (Glue C). Toward the end of the year, much of the failure in the steel specimens was at the interface between the glue and the steel.

Continuous soaking in ethylene glycol (table 10).--The specimens glued by Process 1 showed a moderate falling off in joint strength and a slight increase in the tendency to fail in the glue upon soaking 1 year in glycol.

The specimens glued by Process 2 also showed some falling off in joint strength but no significant change in the nature of the failure.

The specimens glued by Process 3 showed a considerable decrease in joint strength upon soaking 1 year in glycol but no very significant change in the nature of the failure.

The effect of the glycol on the specimens glued by Process 5 appeared to be small and perhaps without significance.

The changes in the aluminum specimens glued by Process 6 appeared to be small and without significance. The steel specimens, however, showed a slight decrease in strength but a considerable increase in the amount of adhesion failure.

Continuous soaking in isopropyl alcohol (table 11).--Glue A was softened by the isopropyl alcohol and the specimens bonded by Process 1 failed at low strengths almost entirely in the glue after 6 to 8 weeks of soaking.

Isopropyl alcohol apparently had no effect on Glues B and G, as there was no significant change in the specimens glued by Process 2.

Glue C may be slightly affected by isopropyl alcohol, for the specimens glued by Process 3 showed in general some decrease in strength towards the end of the year and an appreciable increase in glue failure.

There was apparently no effect by the isopropyl alcohol on the specimens glued with Glue E by Process 5.

The data on specimens glued by Process 6 also indicate slight effect by the alcohol on Glue C. There was a decrease in the amount of failure that occurred in the wood with the soaked specimens, and an appreciable increase in adhesion failure in the steel specimens at the end of the year of immersion.

Continuous soaking in aircraft lubricating oil (table 12).---From the results on the specimens glued by Process 1, the lubricating oil may have a slight effect on Glue A, but it was not revealed until the tests were made at the 52-week period and not consistently at that time.

There was no apparent effect of the lubricating oil on the glues of Process 2.

The results on specimens glued by Process 3 indicate that there may be a slow effect of the oil on Glue C, but the effect in a year of immersion was slight.

The results on specimens glued by Process 5 indicate that there may be a slow effect of the oil on Glue F, for some of the tests made at the end of the year showed an appreciable drop in shear strength and an increase in adhesion failure.

The results on specimens glued by Process 6 again indicate some slow effect of the oil on Glue C, but it was not revealed until tests were made at 52 weeks and not consistently at that time.

Continuous exposure to weather (table 13).---The unpainted aluminum specimens glued by Process 1 showed a moderate drop in strength and a considerable increase in adhesion failure during the year outdoors. The painted aluminum specimen and the steel specimen, painted or unpainted, showed little change that was significant.

The aluminum specimens glued by Process 2 showed little change during the year but the steel specimens showed an appreciable drop in strength and increase in adhesion failure.

The specimens glued by Processes 3 and 4 showed some drop in joint strength during the year's exposure without a consistent change in the nature of the failure.

The specimens glued by Processes 5 and 6 showed no significant changes during the year's exposure outdoors.

Table 1.--Designation of gluing processes and glues

Gluing process	Adhesive designa-	Type of adhesive	Manner of use
1	A	:Modified thermoplastic :resin	:Direct bonding
2	B	:Thermoplastic resin :modified with thermo- :setting resin and :pigment	:As metal primer
	G	:Room-temperature-setting: :resorcinol resin	:As secondary glue
3	C	:Thermosetting resin and :synthetic rubber	:Direct bonding
4	D	:Thermosetting mixture :of synthetic rubber and :plastics	:Direct bonding
	E	:Low-pressure thermo- :plastic resin	:Used in combination :with adhesive D
5	F	:Two components of :thermosetting resin :solution and thermo- :plastic powder	:Direct bonding
6	C	:Thermosetting resin and :synthetic rubber	:Direct bonding to :shim
	G	:Room-temperature-setting: :resorcinol resin	:As secondary glue :to shim

Table 2.—Average results of shear tests on glued wood-to-metal joints exposed continuously to 90° W. and 90 percent relative humidity

Gluing process	Exposure period	Aluminum to birch plywood										Steel to birch plywood									
		Unpainted					Painted					Unpainted					Painted				
		Average shear strength	Average thickness of glue	Average thickness of metal	Average thickness of glue	Average thickness of metal	Average shear strength	Average thickness of glue	Average thickness of metal	Average thickness of glue	Average shear strength	Average shear strength	Average shear strength	Average thickness of glue	Average thickness of metal	Average thickness of glue	Average shear strength	Average thickness of glue	Average thickness of metal	Average thickness of glue	Average shear strength
Specs		lb. per sq. in.	in.	in.	in.	in.	lb. per sq. in.	in.	in.	in.	lb. per sq. in.	lb. per sq. in.	lb. per sq. in.	in.	in.	in.	lb. per sq. in.	lb. per sq. in.	in.	in.	lb. per sq. in.
1	0 control	980	12	0	0	0	93	7	0	0	971	971	971	7	0	0	971	971	7	0	971
	4	1014	12	0	0	0	97	7	0	0	1022	1022	1022	7	0	0	1022	1022	7	0	1022
	16	1077	12	0	0	0	96	7	0	0	1088	1088	1088	7	0	0	1088	1088	7	0	1088
	24	1143	12	0	0	0	96	7	0	0	1155	1155	1155	7	0	0	1155	1155	7	0	1155
	32	1023	12	0	0	0	99	7	0	0	1035	1035	1035	7	0	0	1035	1035	7	0	1035
	104	958	12	0	0	0	99	7	0	0	970	970	970	7	0	0	970	970	7	0	970
2	0 control	716	12	0	0	0	52	7	0	0	727	727	727	7	0	0	727	727	7	0	727
	4	723	12	0	0	0	52	7	0	0	730	730	730	7	0	0	730	730	7	0	730
	16	679	12	0	0	0	54	7	0	0	688	688	688	7	0	0	688	688	7	0	688
	24	693	12	0	0	0	54	7	0	0	700	700	700	7	0	0	700	700	7	0	700
	32	697	12	0	0	0	54	7	0	0	700	700	700	7	0	0	700	700	7	0	700
	104	646	12	0	0	0	57	7	0	0	666	666	666	7	0	0	666	666	7	0	666
3	0 control	945	12	0	0	0	53	7	0	0	945	945	945	7	0	0	945	945	7	0	945
	4	904	12	0	0	0	54	7	0	0	904	904	904	7	0	0	904	904	7	0	904
	16	931	12	0	0	0	54	7	0	0	931	931	931	7	0	0	931	931	7	0	931
	24	881	12	0	0	0	54	7	0	0	881	881	881	7	0	0	881	881	7	0	881
	32	874	12	0	0	0	54	7	0	0	874	874	874	7	0	0	874	874	7	0	874
	104	906	12	0	0	0	51	7	0	0	906	906	906	7	0	0	906	906	7	0	906
4	0 control	998	12	0	0	0	53	7	0	0	998	998	998	7	0	0	998	998	7	0	998
	4	981	12	0	0	0	53	7	0	0	981	981	981	7	0	0	981	981	7	0	981
	16	948	12	0	0	0	53	7	0	0	948	948	948	7	0	0	948	948	7	0	948
	24	903	12	0	0	0	53	7	0	0	903	903	903	7	0	0	903	903	7	0	903
	32	912	12	0	0	0	53	7	0	0	912	912	912	7	0	0	912	912	7	0	912
	104	721	12	0	0	0	51	7	0	0	721	721	721	7	0	0	721	721	7	0	721
5	0 control	723	12	0	0	0	88	7	0	0	723	723	723	7	0	0	723	723	7	0	723
	4	783	12	0	0	0	88	7	0	0	783	783	783	7	0	0	783	783	7	0	783
	16	816	12	0	0	0	88	7	0	0	816	816	816	7	0	0	816	816	7	0	816
	24	742	12	0	0	0	88	7	0	0	742	742	742	7	0	0	742	742	7	0	742
	32	709	12	0	0	0	88	7	0	0	709	709	709	7	0	0	709	709	7	0	709
	104	735	12	0	0	0	88	7	0	0	735	735	735	7	0	0	735	735	7	0	735
6	0 control	994	12	0	0	0	67	7	0	0	994	994	994	7	0	0	994	994	7	0	994
	4	954	12	0	0	0	67	7	0	0	954	954	954	7	0	0	954	954	7	0	954
	16	964	12	0	0	0	67	7	0	0	964	964	964	7	0	0	964	964	7	0	964
	24	973	12	0	0	0	67	7	0	0	973	973	973	7	0	0	973	973	7	0	973
	32	974	12	0	0	0	67	7	0	0	974	974	974	7	0	0	974	974	7	0	974
	104	464	12	0	0	0	50	7	0	0	464	464	464	7	0	0	464	464	7	0	464

Averages are for 55 control specimens and 5 exposed specimens. Metal bonded directly to wood with primary glue. Birch and walnut failures combined.

Table 3.—Average results of shear tests on glued wood-to-metal joints soaked continuously in water at room temperature and tested wet

Gluing process	Exposure period	Alced to birch plywood										Steel to steel plywood									
		Unpainted					Painted					Unpainted					Painted				
		Average shear strength	Average wood failure	Average metal failure	Average secondary glue failure	Average strength	Average shear strength	Average wood failure	Average metal failure	Average secondary glue failure	Average strength	Average shear strength	Average wood failure	Average metal failure	Average secondary glue failure	Average strength	Average shear strength	Average wood failure	Average metal failure	Average secondary glue failure	Average strength
Weeks	1/2 sq. in.	lb. per sq. in.	Percent	Percent	Percent	Percent	Percent	Percent	Percent	Percent	Percent	Percent	Percent	Percent	Percent	Percent	Percent	Percent	Percent	Percent	
0 control	580	578	88	12	0	2	12	0	0	960	971	93	7	0	0	971	93	7	0	0	971
1	601	601	92	8	12	2	12	12	12	631	631	93	34	0	66	475	45	34	0	475	
2	601	601	92	8	12	2	12	12	12	601	601	93	34	0	48	496	51	1	0	496	
3	601	601	92	8	12	2	12	12	12	601	601	93	34	0	48	496	51	1	0	496	
4	601	601	92	8	12	2	12	12	12	601	601	93	34	0	48	496	51	1	0	496	
5	601	601	92	8	12	2	12	12	12	601	601	93	34	0	48	496	51	1	0	496	
6	601	601	92	8	12	2	12	12	12	601	601	93	34	0	48	496	51	1	0	496	
7	601	601	92	8	12	2	12	12	12	601	601	93	34	0	48	496	51	1	0	496	
8	601	601	92	8	12	2	12	12	12	601	601	93	34	0	48	496	51	1	0	496	
9	601	601	92	8	12	2	12	12	12	601	601	93	34	0	48	496	51	1	0	496	
10	601	601	92	8	12	2	12	12	12	601	601	93	34	0	48	496	51	1	0	496	
11	601	601	92	8	12	2	12	12	12	601	601	93	34	0	48	496	51	1	0	496	
12	601	601	92	8	12	2	12	12	12	601	601	93	34	0	48	496	51	1	0	496	
13	601	601	92	8	12	2	12	12	12	601	601	93	34	0	48	496	51	1	0	496	
14	601	601	92	8	12	2	12	12	12	601	601	93	34	0	48	496	51	1	0	496	
15	601	601	92	8	12	2	12	12	12	601	601	93	34	0	48	496	51	1	0	496	
16	601	601	92	8	12	2	12	12	12	601	601	93	34	0	48	496	51	1	0	496	
17	601	601	92	8	12	2	12	12	12	601	601	93	34	0	48	496	51	1	0	496	
18	601	601	92	8	12	2	12	12	12	601	601	93	34	0	48	496	51	1	0	496	
19	601	601	92	8	12	2	12	12	12	601	601	93	34	0	48	496	51	1	0	496	
20	601	601	92	8	12	2	12	12	12	601	601	93	34	0	48	496	51	1	0	496	
21	601	601	92	8	12	2	12	12	12	601	601	93	34	0	48	496	51	1	0	496	
22	601	601	92	8	12	2	12	12	12	601	601	93	34	0	48	496	51	1	0	496	
23	601	601	92	8	12	2	12	12	12	601	601	93	34	0	48	496	51	1	0	496	
24	601	601	92	8	12	2	12	12	12	601	601	93	34	0	48	496	51	1	0	496	
25	601	601	92	8	12	2	12	12	12	601	601	93	34	0	48	496	51	1	0	496	
26	601	601	92	8	12	2	12	12	12	601	601	93	34	0	48	496	51	1	0	496	
27	601	601	92	8	12	2	12	12	12	601	601	93	34	0	48	496	51	1	0	496	
28	601	601	92	8	12	2	12	12	12	601	601	93	34	0	48	496	51	1	0	496	
29	601	601	92	8	12	2	12	12	12	601	601	93	34	0	48	496	51	1	0	496	
30	601	601	92	8	12	2	12	12	12	601	601	93	34	0	48	496	51	1	0	496	
31	601	601	92	8	12	2	12	12	12	601	601	93	34	0	48	496	51	1	0	496	
32	601	601	92	8	12	2	12	12	12	601	601	93	34	0	48	496	51	1	0	496	
33	601	601	92	8	12	2	12	12	12	601	601	93	34	0	48	496	51	1	0	496	
34	601	601	92	8	12	2	12	12	12	601	601	93	34	0	48	496	51	1	0	496	
35	601	601	92	8	12	2	12	12	12	601	601	93	34	0	48	496	51	1	0	496	
36	601	601	92	8	12	2	12	12	12	601	601	93	34	0	48	496	51	1	0	496	
37	601	601	92	8	12	2	12	12	12	601	601	93	34	0	48	496	51	1	0	496	
38	601	601	92	8	12	2	12	12	12	601	601	93	34	0	48	496	51	1	0	496	
39	601	601	92	8	12	2	12	12	12	601	601	93	34	0	48	496	51	1	0	496	
40	601	601	92	8	12	2	12	12	12	601	601	93	34	0	48	496	51	1	0	496	
41	601	601	92	8	12	2	12	12	12	601	601	93	34	0	48	496	51	1	0	496	
42	601	601	92	8	12	2	12	12	12	601	601	93	34	0	48	496	51	1	0	496	
43	601	601	92	8	12	2	12	12	12	601	601	93	34	0	48	496	51	1	0	496	
44	601	601	92	8	12	2	12	12	12	601	601	93	34	0	48	496	51	1	0	496	
45	601	601	92	8	12	2	12	12	12	601	601	93	34	0	48	496	51	1	0	496	
46	601	601	92	8	12	2	12	12	12	601	601	93	34	0	48	496	51	1	0	496	
47	601	601	92	8	12	2	12	12	12	601	601	93	34	0	48	496	51	1	0	496	
48	601	601	92	8	12	2	12	12	12	601	601	93	34	0	48	496	51	1	0	496	
49	601	601	92	8	12	2	12	12	12	601	601	93	34	0	48	496	51	1	0	496	
50	601	601	92	8	12	2	12	12	12	601	601	93	34	0	48	496	51	1	0	496	
51	601	601	92	8	12	2	12	12	12	601	601	93	34	0	48	496	51	1	0	496	
52	601	601	92	8	12	2	12	12	12	601	601	93	34	0	48	496	51	1	0	496	
53	601	601	92	8	12	2	12	12	12	601	601	93	34	0	48	496	51	1	0	496	
54	601	601	92	8	12	2	12	12	12	601	601	93	34	0	48	496	51	1	0	496	
55	601	601	92	8	12	2	12	12	12	601	601	93	34	0	48	496	51	1	0	496	
56	601	601	92	8	12	2	12	12	12	601	601	93	34	0	48	496	51	1	0	496	
57	601	601	92	8	12	2	12	12	12	601	601	93	34	0	48	496	51	1	0	496	
58	601	601	92	8	12	2	12	12	12	601	601	93	34	0	48	496	51	1	0	496	
59	601	601	92	8	12	2	12	12	12	601	601	93	34	0	48	496	51	1	0	496	
60	601	601	92	8	12	2	12	12	12	601	601	93	34	0	48	496	51	1	0	496	
61	601	601	92	8	12	2	12	12	12	601	601	93	34	0	48	496	51	1	0	496	
62	601	601	92	8	12	2	12	12	12	601	601	93	34	0	48	496	51	1	0	496	
63	601	601	92	8	12	2	12	12	12	601	601	93	34	0	48	496	51	1	0	496	
64	601	601	92	8	12	2	12	12	12	601	601	93	34	0	48	496	51	1	0	496	
65	601	601	92	8	12	2	12	12	12	601	601	93	34	0	48	496	51	1	0	496	
66	601	601	92	8	12	2	12	12	12	601	601	93	34	0	48	496	51	1	0	496	
67	601	601	92	8	12	2	12	12	12	601	601	93	34	0	48	496	51	1	0	496	
68	601	601	92	8	12	2	12	12	12	601	601	93	34	0	48	496	51	1	0	496	
69	601	601	92	8	12	2	12	12	12	601	601	93	34	0	48	496	51	1	0	496	
70	601	601	92	8	12	2	12	12	12	601	601	93	34	0	48	496	51	1	0	496	
71	601	601	92	8	12	2	12	12	12	601	601	93	34	0	48	496	51	1	0	496	
72	601	601	92	8	12	2	12	12	12	601	601	93	34	0	48	496	51	1	0	496	
73	601	601	92	8	12	2	12	12	12	601	601	93	34	0	48	496	51	1	0	496	
74	601	601	92	8	12	2	12	12	12	601	601	93	34	0	48	496	51	1	0	496	
75	601	601	92	8	12	2	12	12	12	601	601	93	34	0	48	496	51	1	0	496	
76	601	601	92	8	12	2	12	12	12	601	601	93	34	0	48	496	51	1	0	496	
77	601	601	92	8	12	2	12	12	12	601	601										

Averages are for 55 control specimens and 5 exposed specimens.
Metal bonded directly to wood with primary glue.
Birch and walnut failures combined.

Table 4. Average results of shear tests on glued wood-to-metal joints exposed continuously to 80% R. and 97 percent relative humidity

Gluing process	Exposure period	Aluminum to Birch plywood										Steel to Birch plywood													
		Unpainted					Painted					Unpainted					Painted								
		Average shear strength	Average wood failure	Average glue failure	Average metal failure	Average secondary failure	Average shear strength	Average wood failure	Average glue failure	Average metal failure	Average secondary failure	Average shear strength	Average wood failure	Average glue failure	Average metal failure	Average secondary failure	Average shear strength	Average wood failure	Average glue failure	Average metal failure	Average secondary failure				
1	0 control	980	88	12	0	2	980	88	12	0	2	971	93	0	2	971	93	0	2	971	93	0	2		
	4	653	67	0	14	—	903	86	0	14	—	688	68	0	—	688	68	0	—	688	68	0	—		
	8	692	53	0	31	—	713	95	0	31	—	694	61	0	—	694	61	0	—	694	61	0	—		
	16	641	27	0	5	—	498	95	0	5	—	834	32	0	—	834	32	0	—	834	32	0	—		
	24	651	60	0	25	—	540	65	0	25	—	486	32	0	—	486	32	0	—	486	32	0	—		
	32	676	60	0	25	—	540	65	0	25	—	487	32	0	—	487	32	0	—	487	32	0	—		
	52	85	100	0	0	—	59	100	0	0	—	487	32	0	—	487	32	0	—	487	32	0	—		
	104																								
	0 control	716	52	0	12	36	716	52	0	12	36	855	58	0	38	855	58	0	38	855	58	0	38		
	4	581	47	0	45	36	531	46	0	42	33	640	45	0	33	640	45	0	33	640	45	0	33		
2	0 control	945	23	47	0	2	945	23	47	0	2	936	34	56	2	936	34	56	2	936	34	56	2		
	4	814	62	36	0	—	802	45	25	0	—	814	62	36	0	—	814	62	36	0	—	814	62	36	0
	8	708	48	92	0	—	673	39	61	0	—	708	48	92	0	—	708	48	92	0	—	708	48	92	0
	16	703	25	34	9	—	681	34	46	0	—	703	25	34	9	—	703	25	34	9	—	703	25	34	9
	24	965	44	36	0	—	700	52	48	0	—	965	44	36	0	—	965	44	36	0	—	965	44	36	0
	32	532	42	36	0	—	681	34	46	0	—	532	42	36	0	—	532	42	36	0	—	532	42	36	0
	52	536	42	36	0	—	681	34	46	0	—	536	42	36	0	—	536	42	36	0	—	536	42	36	0
	104																								
	0 control	928	30	36	14	2	928	30	36	14	2	1000	50	26	2	1000	50	26	2	1000	50	26	2		
	4	777	47	18	35	—	719	43	16	14	—	777	47	18	35	—	777	47	18	35	—	777	47	18	35
3	0 control	723	88	12	0	2	723	88	12	0	2	719	93	0	2	719	93	0	2	719	93	0	2		
	4	684	88	0	12	—	682	86	0	12	—	684	88	0	—	684	88	0	—	684	88	0	—		
	8	690	78	0	12	—	683	86	0	12	—	690	78	0	—	690	78	0	—	690	78	0	—		
	16	716	50	0	25	—	683	86	0	25	—	716	50	0	—	716	50	0	—	716	50	0	—		
	24	770	83	3	14	—	724	91	5	14	—	770	83	3	—	770	83	3	—	770	83	3	—		
	32	770	83	3	14	—	724	91	5	14	—	770	83	3	—	770	83	3	—	770	83	3	—		
	52	619	64	0	16	—	537	76	0	24	—	619	64	0	—	619	64	0	—	619	64	0	—		
	104																								
	0 control	928	30	36	14	2	928	30	36	14	2	1000	50	26	2	1000	50	26	2	1000	50	26	2		
	4	777	47	18	35	—	719	43	16	14	—	777	47	18	35	—	777	47	18	35	—	777	47	18	35
4	0 control	723	88	12	0	2	723	88	12	0	2	719	93	0	2	719	93	0	2	719	93	0	2		
	4	684	88	0	12	—	682	86	0	12	—	684	88	0	—	684	88	0	—	684	88	0	—		
	8	690	78	0	12	—	683	86	0	12	—	690	78	0	—	690	78	0	—	690	78	0	—		
	16	716	50	0	25	—	683	86	0	25	—	716	50	0	—	716	50	0	—	716	50	0	—		
	24	770	83	3	14	—	724	91	5	14	—	770	83	3	—	770	83	3	—	770	83	3	—		
	32	770	83	3	14	—	724	91	5	14	—	770	83	3	—	770	83	3	—	770	83	3	—		
	52	619	64	0	16	—	537	76	0	24	—	619	64	0	—	619	64	0	—	619	64	0	—		
	104																								
	0 control	928	30	36	14	2	928	30	36	14	2	1000	50	26	2	1000	50	26	2	1000	50	26	2		
	4	777	47	18	35	—	719	43	16	14	—	777	47	18	35	—	777	47	18	35	—	777	47	18	35
5	0 control	723	88	12	0	2	723	88	12	0	2	719	93	0	2	719	93	0	2	719	93	0	2		
	4	684	88	0	12	—	682	86	0	12	—	684	88	0	—	684	88	0	—	684	88	0	—		
	8	690	78	0	12	—	683	86	0	12	—	690	78	0	—	690	78	0	—	690	78	0	—		
	16	716	50	0	25	—	683	86	0	25	—	716	50	0	—	716	50	0	—	716	50	0	—		
	24	770	83	3	14	—	724	91	5	14	—	770	83	3	—	770	83	3	—	770	83	3	—		
	32	770	83	3	14	—	724	91	5	14	—	770	83	3	—	770	83	3	—	770	83	3	—		
	52	619	64	0	16	—	537	76	0	24	—	619	64	0	—	619	64	0	—	619	64	0	—		
	104																								
	0 control	928	30	36	14	2	928	30	36	14	2	1000	50	26	2	1000	50	26	2	1000	50	26	2		
	4	777	47	18	35	—	719	43	16	14	—	777	47	18	35	—	777	47	18	35	—	777	47	18	35
6	0 control	928	30	36	14	2	928	30	36	14	2	1000	50	26	2	1000	50	26	2	1000	50	26	2		
	4	777	47	18	35	—	719	43	16	14	—	777	47	18	35	—	777	47	18	35	—	777	47	18	35
	8	661	27	24	24	—	709	43	22	24	—	661	27	24	24	—	661	27	24	24	—	661	27	24	24
	16	804	24	24	24	—	652	41	18	41	—	804	24	24	24	—	804	24	24	24	—	804	24	24	24
	24	681	24	16	34	—	590	29	20	45	—	681	24	16	34	—	681	24	16	34	—	681	24	16	34
	32	696	24	16	34	—	590	29	20	45	—	696	24	16	34	—	696	24	16	34	—	696	24	16	34
	52	696	24	16	34	—	615	29	20	45	—	696	24	16	34	—	696	24	16	34	—	696	24	16	34
	104																								
	0 control	928	30	36	14	2	928	30	36	14	2	1000	50	26	2	1000	50	26	2	1000	50	26	2		
	4	777	47	18	35	—	719	43	16	14	—	777	47	18	35	—	777	47	18	35	—	777	47	18	35

1. All surfaces are for 20 control specimens and 5 exposed specimens.

Metal bonded directly to wood with primary glue.

3 Birch and walnut failures combined.

Table 5.—Average results of shear tests on glued wood-to-metal joints exposed alternately to 97 and 10 percent relative humidity at 80° F.

Gluing process	Exposure period	Aluminum to Birch plywood										Steel to Birch plywood													
		Unpainted					Painted					Unpainted					Painted								
		Average shear strength	Average adhesive failure	Average glue failure	Average metal failure	Average secondary glue failure	Average wood failure	Average glue failure	Average metal failure	Average secondary glue failure	Average shear strength	Average adhesive failure	Average glue failure	Average metal failure	Average secondary glue failure	Average wood failure	Average glue failure	Average metal failure	Average secondary glue failure	Average shear strength	Average adhesive failure	Average glue failure	Average metal failure	Average secondary glue failure	
lb. per sq. in.	Percent	Percent	Percent	Percent	Percent	Percent	Percent	Percent	Percent	lb. per sq. in.	Percent	Percent	Percent	Percent	Percent	Percent	Percent	Percent	lb. per sq. in.	Percent	Percent	Percent	Percent	Percent	
1	0 control	980	88	12	0	0	0	0	0	0	971	2	0	0	0	0	0	0	0	972	2	0	0	0	0
	4	896	93	0	7	0	12	0	17	0	794	0	2	0	0	0	0	0	0	895	0	2	0	0	0
	8	1048	86	2	12	0	0	0	0	0	1051	0	2	0	0	0	0	0	0	1051	0	2	0	0	0
	16	980	100	0	0	0	0	0	0	0	1071	0	0	0	0	0	0	0	0	1071	0	0	0	0	0
	24	1120	70	6	24	0	6	24	0	0	1071	0	6	0	0	0	0	0	0	1071	0	6	0	0	0
2	0 control	928	96	4	0	0	0	0	0	0	1000	0	0	0	0	0	0	0	0	1011	0	0	0	0	0
	4	716	52	0	12	0	0	12	0	0	855	36	0	41	0	0	0	0	855	36	0	41	0	0	
	8	681	51	0	39	0	0	0	33	0	855	29	0	14	0	0	0	0	855	29	0	14	0	0	
	16	874	72	0	13	0	0	0	0	0	855	16	0	11	0	0	0	0	855	16	0	11	0	0	
	24	760	78	0	9	0	0	0	0	0	855	13	0	35	0	0	0	0	855	13	0	35	0	0	
3	0 control	712	43	0	18	0	0	0	31	0	682	26	0	37	0	0	0	0	674	30	0	45	0	0	
	4	636	34	0	53	0	0	0	28	0	682	26	0	40	0	0	0	0	674	30	0	45	0	0	
	8	712	53	0	0	0	0	0	0	0	682	26	0	40	0	0	0	0	674	30	0	45	0	0	
	16	712	53	0	0	0	0	0	0	0	682	26	0	40	0	0	0	0	674	30	0	45	0	0	
	24	712	53	0	0	0	0	0	0	0	682	26	0	40	0	0	0	0	674	30	0	45	0	0	
4	0 control	987	83	17	0	0	0	0	0	0	936	2	0	0	0	0	0	0	936	2	0	0	0	0	
	4	1096	73	0	0	0	0	0	0	936	2	0	0	0	0	0	0	0	936	2	0	0	0	0	
	8	987	73	0	0	0	0	0	0	936	2	0	0	0	0	0	0	0	936	2	0	0	0	0	
	16	987	73	0	0	0	0	0	0	936	2	0	0	0	0	0	0	0	936	2	0	0	0	0	
	24	1001	74	0	0	0	0	0	0	936	2	0	0	0	0	0	0	0	936	2	0	0	0	0	
5	0 control	723	88	12	0	0	0	0	0	0	779	2	0	0	0	0	0	0	779	2	0	0	0	0	
	4	816	100	0	0	0	0	0	0	816	0	0	0	0	0	0	0	0	816	0	0	0	0	0	
	8	828	94	6	0	0	0	0	0	816	0	0	0	0	0	0	0	0	816	0	0	0	0	0	
	16	828	94	6	0	0	0	0	0	816	0	0	0	0	0	0	0	0	816	0	0	0	0	0	
	24	830	74	9	17	0	0	0	0	816	0	0	0	0	0	0	0	0	816	0	0	0	0	0	
6	0 control	954	83	2	0	0	0	0	0	0	692	31	0	19	0	0	0	0	692	31	0	19	0	0	
	4	534	70	0	0	0	0	0	0	534	31	0	19	0	0	0	0	0	534	31	0	19	0	0	
	8	567	78	0	0	0	0	0	0	534	31	0	19	0	0	0	0	0	534	31	0	19	0	0	
	16	560	78	0	0	0	0	0	0	534	31	0	19	0	0	0	0	0	534	31	0	19	0	0	
	24	608	56	0	0	0	0	0	0	534	31	0	19	0	0	0	0	0	534	31	0	19	0	0	

Averages are for 35 control specimens and 5 exposed specimens.
Metal bonded directly to wood with primary glue.
Birch and walnut failures combined.

Table 6—Average tensile of shear tests on glued wood-to-metal joints exposed continuously to high F- and 20 percent relative humidity

Gluing process	Exposure period	Aluminum to birch plywood										Steel to birch plywood													
		Unpainted					Painted					Unpainted					Painted								
		Average shear strength	Average wood failure	Average glue failure	Average metal failure	Average secondary glue failure	Average shear strength	Average wood failure	Average glue failure	Average metal failure	Average secondary glue failure	Average shear strength	Average wood failure	Average glue failure	Average metal failure	Average secondary glue failure	Average shear strength	Average wood failure	Average glue failure	Average metal failure	Average secondary glue failure				
lb. per 1/2 sq. in.	Percent	Percent	Percent	Percent	lb. per 1/2 sq. in.	Percent	Percent	Percent	Percent	lb. per 1/2 sq. in.	Percent	Percent	Percent	Percent	lb. per 1/2 sq. in.	Percent	Percent	Percent	Percent	lb. per 1/2 sq. in.	Percent	Percent	Percent	Percent	
1	0 control	980	88	12	0	0	960	86	12	0	971	971	2	0	0	971	971	2	0	0	971	971	2	0	0
	4	940	84	16	0	0	937	92	8	0	1015	1015	0	0	0	965	965	0	0	0	965	965	0	0	0
	8	971	94	3	0	0	921	81	5	14	994	994	0	0	0	971	971	0	0	0	971	971	0	0	0
	16	910	89	3	0	0	836	83	0	12	1041	1041	0	0	0	971	971	0	0	0	971	971	0	0	0
	24	925	80	0	20	0	1051	94	6	0	860	860	0	0	0	971	971	0	0	0	971	971	0	0	0
	32	1056	88	12	0	0	765	84	10	0	1042	1042	0	0	0	971	971	0	0	0	971	971	0	0	0
	52	754	100	0	0	0	705	99	1	0	942	942	0	0	0	971	971	0	0	0	971	971	0	0	0
	104																								
	0 control	716	52	0	12	0	716	52	0	12	895	895	36	0	0	895	895	36	0	0	895	895	36	0	0
	4	709	54	0	0	0	709	54	0	0	782	782	18	0	0	935	935	18	0	0	935	935	18	0	0
2	8	719	77	0	15	0	719	77	0	15	751	751	9	0	5	825	825	9	0	5	825	825	9	0	5
	16	708	73	0	20	0	708	73	0	20	699	699	12	0	12	734	734	12	0	12	734	734	12	0	12
	24	624	73	0	6	1	624	73	0	6	669	669	27	0	6	771	771	27	0	6	771	771	27	0	6
	32	624	62	0	0	1	502	72	0	0	661	661	28	0	0	524	524	28	0	0	524	524	28	0	0
	52	494	59	0	0	0	494	59	0	0	502	502	23	0	0	524	524	23	0	0	524	524	23	0	0
	104																								
	0 control	945	83	17	0	0	945	83	17	0	945	945	34	0	0	945	945	34	0	0	945	945	34	0	0
	4	977	87	14	0	0	1024	87	14	0	990	990	36	0	0	955	955	36	0	0	955	955	36	0	0
	8	927	82	14	0	0	927	82	14	0	976	976	35	0	0	828	828	35	0	0	828	828	35	0	0
	16	751	81	15	0	0	751	81	15	0	710	710	33	0	0	766	766	33	0	0	766	766	33	0	0
3	24	620	73	14	0	0	620	73	14	0	523	523	23	0	0	527	527	23	0	0	527	527	23	0	0
	32	523	64	9	0	0	523	64	9	0	497	497	25	0	0	427	427	25	0	0	427	427	25	0	0
	52	494	59	0	0	0	494	59	0	0	497	497	25	0	0	427	427	25	0	0	427	427	25	0	0
	104																								
	0 control	723	88	12	0	0	723	88	12	0	779	779	2	0	0	779	779	2	0	0	779	779	2	0	0
	4	795	88	12	0	0	795	88	12	0	831	831	0	0	0	742	742	0	0	0	742	742	0	0	0
	8	834	95	15	0	0	822	93	5	0	760	760	0	0	0	856	856	0	0	0	856	856	0	0	0
	16	760	90	10	0	0	753	90	10	0	774	774	0	0	0	753	753	0	0	0	753	753	0	0	0
	24	736	89	11	0	0	736	89	11	0	774	774	0	0	0	753	753	0	0	0	753	753	0	0	0
	32	672	83	11	0	0	672	83	11	0	774	774	0	0	0	753	753	0	0	0	753	753	0	0	0
6	0 control	554	67	2	0	0	554	67	2	0	554	554	31	0	0	652	652	31	0	0	652	652	31	0	0
	4	513	63	0	0	0	513	63	0	0	492	492	10	0	0	524	524	10	0	0	524	524	10	0	0
	8	518	57	0	0	0	518	57	0	0	492	492	10	0	0	524	524	10	0	0	524	524	10	0	0
	16	463	40	36	0	0	463	40	36	0	492	492	10	0	0	524	524	10	0	0	524	524	10	0	0
	24	441	34	47	0	0	441	34	47	0	492	492	10	0	0	524	524	10	0	0	524	524	10	0	0
	32	441	34	47	0	0	441	34	47	0	492	492	10	0	0	524	524	10	0	0	524	524	10	0	0
	52	382	31	61	0	0	382	31	61	0	492	492	10	0	0	524	524	10	0	0	524	524	10	0	0
	104																								
	0 control	554	67	2	0	0	554	67	2	0	554	554	31	0	0	652	652	31	0	0	652	652	31	0	0
	4	513	63	0	0	0	513	63	0	0	492	492	10	0	0	524	524	10	0	0	524	524	10	0	0

Averages are for 35 control specimens and 5 exposed specimens.
Metal bonded directly to wood with primary glue.
Birch and walnut failures combined.

Table 1.—Average results of shear tests on glued wood-to-metal joints exposed alternately to 15% P. and 50% P.

Gluing process	Exposure period	Aluminum to birch plywood										Steel to birch plywood														
		Unpainted					Painted					Unpainted					Painted									
		Average shear strength	Average glue strength	Average metal failure	Average glue failure	Average secondary glue failure	Average wood failure	Average metal failure	Average glue failure	Average secondary glue failure	Average shear strength	Average glue strength	Average metal failure	Average glue failure	Average secondary glue failure	Average wood failure	Average metal failure	Average glue failure	Average secondary glue failure	Average shear strength	Average glue strength	Average metal failure	Average glue failure	Average secondary glue failure		
1	0 control	4	8	16	24	32	52	104	lb. per sq. in.	Percent	Percent	Percent	Percent	Percent	Percent	Percent	Percent	Percent	Percent	lb. per sq. in.	Percent	Percent	Percent	Percent	Percent	
		960	990	920	947	1001	916	647		2	0	12	88	96	93	97	77	98	99	91	971	93	7	0	0	2
		980	990	920	947	1001	916	647		2	0	12	88	96	93	97	77	98	99	91	971	93	7	0	0	2
		980	990	920	947	1001	916	647		2	0	12	88	96	93	97	77	98	99	91	971	93	7	0	0	2
		980	990	920	947	1001	916	647		2	0	12	88	96	93	97	77	98	99	91	971	93	7	0	0	2
		980	990	920	947	1001	916	647		2	0	12	88	96	93	97	77	98	99	91	971	93	7	0	0	2
		980	990	920	947	1001	916	647		2	0	12	88	96	93	97	77	98	99	91	971	93	7	0	0	2
		980	990	920	947	1001	916	647		2	0	12	88	96	93	97	77	98	99	91	971	93	7	0	0	2
		980	990	920	947	1001	916	647		2	0	12	88	96	93	97	77	98	99	91	971	93	7	0	0	2
		980	990	920	947	1001	916	647		2	0	12	88	96	93	97	77	98	99	91	971	93	7	0	0	2
		980	990	920	947	1001	916	647		2	0	12	88	96	93	97	77	98	99	91	971	93	7	0	0	2
		980	990	920	947	1001	916	647		2	0	12	88	96	93	97	77	98	99	91	971	93	7	0	0	2
		980	990	920	947	1001	916	647		2	0	12	88	96	93	97	77	98	99	91	971	93	7	0	0	2
		980	990	920	947	1001	916	647		2	0	12	88	96	93	97	77	98	99	91	971	93	7	0	0	2
		980	990	920	947	1001	916	647		2	0	12	88	96	93	97	77	98	99	91	971	93	7	0	0	2
		980	990	920	947	1001	916	647		2	0	12	88	96	93	97	77	98	99	91	971	93	7	0	0	2
		980	990	920	947	1001	916	647		2	0	12	88	96	93	97	77	98	99	91	971	93	7	0	0	2
		980	990	920	947	1001	916	647		2	0	12	88	96	93	97	77	98	99	91	971	93	7	0	0	2
		980	990	920	947	1001	916	647		2	0	12	88	96	93	97	77	98	99	91	971	93	7	0	0	2
		980	990	920	947	1001	916	647		2	0	12	88	96	93	97	77	98	99	91	971	93	7	0	0	2
		980	990	920	947	1001	916	647		2	0	12	88	96	93	97	77	98	99	91	971	93	7	0	0	2
		980	990	920	947	1001	916	647		2	0	12	88	96	93	97	77	98	99	91	971	93	7	0	0	2
		980	990	920	947	1001	916	647		2	0	12	88	96	93	97	77	98	99	91	971	93	7	0	0	2
		980	990	920	947	1001	916	647		2	0	12	88	96	93	97	77	98	99	91	971	93	7	0	0	2
		980	990	920	947	1001	916	647		2	0	12	88	96	93	97	77	98	99	91	971	93	7	0	0	2
		980	990	920	947	1001	916	647		2	0	12	88	96	93	97	77	98	99	91	971	93	7	0	0	2
		980	990	920	947	1001	916	647		2	0	12	88	96	93	97	77	98	99	91	971	93	7	0	0	2
		980	990	920	947	1001	916	647		2	0	12	88	96	93	97	77	98	99	91	971	93	7	0	0	2
		980	990	920	947	1001	916	647		2	0	12	88	96	93	97	77	98	99	91	971	93	7	0	0	2
		980	990	920	947	1001	916	647		2	0	12	88	96	93	97	77	98	99	91	971	93	7	0	0	2
		980	990	920	947	1001	916	647		2	0	12	88	96	93	97	77	98	99	91	971	93	7	0	0	2
		980	990	920	947	1001	916	647		2	0	12	88	96	93	97	77	98	99	91	971	93	7	0	0	2
		980	990	920	947	1001	916	647		2	0	12	88	96	93	97	77	98	99	91	971	93	7	0	0	2
		980	990	920	947	1001	916	647		2	0	12	88	96	93	97	77	98	99	91	971	93	7	0	0	2
		980	990	920	947	1001	916	647		2	0	12	88	96	93	97	77	98	99	91	971	93	7	0	0	2
		980	990	920	947	1001	916	647		2	0	12	88	96	93	97	77	98	99	91	971	93	7	0	0	2
		980	990	920	947	1001	916	647		2	0	12	88	96	93	97	77	98	99	91	971	93	7	0	0	2
		980	990	920	947	1001	916	647		2	0	12	88	96	93	97	77	98	99	91	971	93	7	0	0	2
		980	990	920	947	1001	916	647		2	0	12	88	96	93	97	77	98	99	91	971	93	7	0	0	2
		980	990	920	947	1001	916	647		2	0	12	88	96	93	97	77	98	99	91	971	93	7	0	0	2
		980	990	920	947	1001	916	647		2	0	12	88	96	93	97	77	98	99	91	971	93	7	0	0	2
		980	990	920	947	1001	916	647		2	0	12	88	96	93	97	77	98	99	91	971	93	7	0	0	2
		980	990	920	947	1001	916	647		2	0	12	88	96	93	97	77	98	99	91	971	93	7	0	0	2
		980	990	920	947	1001	916	647		2	0	12	88	96	93	97	77	98	99	91	971	93	7	0	0	2
		980	990	920	947	1001	916	647		2	0	12	88	96	93	97	77	98	99	91	971	93	7	0	0	2
		980	990	920	947	1001	916	647		2	0	12	88	96	93	97	77	98	99	91	971	93	7	0	0	2
		980	990	920	947	1001	916	647		2	0	12	88	96	93	97	77	98	99	91	971	93	7	0	0	2
		980	990	920	947	1001	916	647		2	0	12	88	96	93	97	77	98	99	91	971	93	7	0	0	2
		980	990	920	947	1001	916	647		2	0	12	88	96	93	97	77	98	99	91	971	93	7	0	0	2
		980	990	920	947	1001	916	647		2	0	12	88	96	93	97	77	98	99	91	971	93	7	0	0	2
		980	990	920	947	1001	916	647		2	0	12	88	96	93	97	77	98	99	91	971	93	7	0	0	2
		980	990	920	947	1001	916	647		2	0	12	88	96	93	97	77	98	99	91	971	93	7	0	0	2
		980	990	920	947	1001	916	647		2	0	12	88	96	93	97	77	98	99	91	971	93	7	0	0	2
		980	990	920	947	1001	916	647		2	0	12	88	96	93	97	77	98	99	91	971	93	7	0	0	2
		980	990	920	947	1001	916	647		2	0	12	88	96	93	97	77	98	99	91	971	93	7	0	0	2
		980	990	920	947	1001	916	647		2	0	12	88	96	93	97	77	98	99	91	971	93	7	0	0	2
		980	990	920	947	1001	916	647		2	0	12	88	96	93	97	77	98	99	91	971	93	7	0	0	2
		980	990	920	947	1001	916	647		2	0	12	88	96	93	97	77	98	99	91	971	93	7	0	0	2
		980	990	920	947	1001	916	647		2	0	12	88	96	93	97	77	98	99	91	971	93	7	0	0	2
		980	990	920	947	1001	916	647		2	0	12	88	96	93	97	77	98	99	91	971	93	7	0	0	2
		980	990	920	947	1001	916	647		2	0	12	88	96	93	97	77	98	99	91	971	93	7	0	0	2
		980	990	920	947	1001	916	647		2	0	12	88	96	93	97	77	98	99	91	971	93	7	0	0	2
		980	990	920	947	1001	916	647		2	0	12	88	96	93	97	77	98	99	91	971	93	7	0	0	2
		980	990	920	947	1001	916	647		2	0	12	88	96	93	97	77	98	99	91	971	93	7	0	0	2
		980	990	920	947	1001	916	647		2	0	12	88	96	93	97	77	98</								

Averages are for 55 control specimens and 5 exposed specimens.

Metal bonded directly to wood with primary glue.

Birch and walnut failures combined.

Z M 72964 P

Table 8. Average results of shear tests on glued wood-to-metal joints coated continuously in 100-percent epoxy.

Gluing process	Exposure period	Aluminum to birch plywood										Steel to birch plywood									
		Uncoated					Painted					Uncoated					Painted				
		Average shear strength	Average wood failure	Average glue failure	Average metal failure	Average secondary glue failure	Average wood failure	Average glue failure	Average metal failure	Average secondary glue failure	Average shear strength	Average wood failure	Average glue failure	Average metal failure	Average secondary glue failure	Average shear strength	Average wood failure	Average glue failure	Average metal failure	Average secondary glue failure	Average shear strength
		lb. per sq. in.	Percent	Percent	Percent	Percent	lb. per sq. in.	Percent	Percent	Percent	lb. per sq. in.	Percent	Percent	Percent	Percent	lb. per sq. in.	Percent	Percent	Percent	Percent	lb. per sq. in.
1	0 control	960	88	12	0	0	960	86	12	0	971	91	6	7	0	971	91	9	0	0	971
	2	1225	97	13	0	0	1225	97	10	0	1103	94	6	4	0	1103	94	9	0	0	1103
	4	1254	95	13	0	0	1254	95	10	0	1311	96	12	4	0	1311	96	15	0	0	1311
	6	1105	85	15	0	0	1086	78	22	0	1086	85	12	4	0	1086	85	15	0	0	1086
	8	806	67	33	0	0	678	33	67	0	717	46	54	0	0	684	28	72	0	0	684
	12	710	51	49	0	0	668	32	68	0	687	29	71	0	0	627	18	82	0	0	627
	24	510	31	69	0	0	373	4	96	0	393	18	82	0	0	387	2	98	0	0	387
	52	497	0	100	0	0	305	0	100	0	366	6	94	0	0	357	6	94	0	0	357
	0 control	716	52	48	0	12	716	52	48	0	855	58	0	0	18	855	58	0	4	38	855
	2	644	42	58	0	22	644	42	58	0	744	39	0	0	16	744	39	0	13	25	744
2	0 control	742	62	38	0	14	695	29	71	0	833	76	0	0	10	833	76	0	13	19	833
	2	697	60	40	0	14	661	50	50	0	767	58	0	0	16	767	58	0	13	19	767
	4	701	72	28	0	3	701	72	28	0	741	72	0	0	2	741	72	0	3	12	741
	6	789	56	44	0	24	746	71	29	0	860	58	0	0	16	860	58	0	13	16	860
	12	750	60	40	0	21	798	82	18	0	850	73	0	0	24	850	73	0	13	16	850
	24	683	67	33	0	25	717	58	42	0	830	71	0	0	13	830	71	0	13	22	830
	52	645	53	47	0	25	645	53	47	0	716	54	0	0	10	716	54	0	10	22	716
	0 control	775	77	23	0	0	775	77	23	0	764	74	0	0	10	764	74	0	10	10	764
	2	796	80	20	0	0	777	77	23	0	696	64	0	0	10	696	64	0	10	10	696
	4	724	74	26	0	0	717	74	26	0	717	74	0	0	10	717	74	0	10	10	717
3	0 control	769	74	26	0	0	769	74	26	0	777	74	0	0	10	777	74	0	10	10	777
	2	769	74	26	0	0	769	74	26	0	777	74	0	0	10	777	74	0	10	10	777
	4	665	61	39	0	0	665	61	39	0	621	57	1	0	3	621	57	1	0	3	621
	6	615	53	47	0	0	549	54	46	0	701	70	0	0	10	701	70	0	10	10	701
	12	723	72	28	0	0	723	72	28	0	779	77	0	0	10	779	77	0	10	10	779
	24	719	71	29	0	0	686	68	32	0	779	77	0	0	10	779	77	0	10	10	779
	52	615	53	47	0	0	549	54	46	0	429	42	0	0	10	429	42	0	10	10	429
	0 control	723	72	28	0	0	723	72	28	0	779	77	0	0	10	779	77	0	10	10	779
	2	719	71	29	0	0	686	68	32	0	779	77	0	0	10	779	77	0	10	10	779
	4	753	75	25	0	0	669	66	34	0	812	81	0	0	10	812	81	0	10	10	812
5	0 control	670	60	40	0	18	670	60	40	0	857	85	0	0	0	857	85	0	0	0	857
	2	787	78	22	0	0	753	75	25	0	867	86	0	0	0	867	86	0	0	0	867
	4	787	78	22	0	0	753	75	25	0	867	86	0	0	0	867	86	0	0	0	867
	6	718	71	29	0	0	684	68	32	0	803	80	0	0	0	803	80	0	0	0	803
	12	718	71	29	0	0	684	68	32	0	803	80	0	0	0	803	80	0	0	0	803
	24	735	73	27	0	0	719	71	29	0	769	76	0	0	0	769	76	0	0	0	769
	52	719	71	29	0	0	638	63	37	0	867	86	0	0	0	867	86	0	0	0	867
	0 control	723	72	28	0	0	723	72	28	0	779	77	0	0	10	779	77	0	10	10	779
	2	719	71	29	0	0	686	68	32	0	779	77	0	0	10	779	77	0	10	10	779
	4	753	75	25	0	0	669	66	34	0	812	81	0	0	10	812	81	0	10	10	812
6	0 control	558	55	45	0	0	558	55	45	0	672	67	0	0	0	672	67	0	0	0	672
	2	475	47	53	0	0	475	47	53	0	52	52	0	0	0	52	52	0	0	0	52
	4	447	44	56	0	0	447	44	56	0	48	48	0	0	0	48	48	0	0	0	48
	6	439	43	57	0	0	439	43	57	0	49	49	0	0	0	49	49	0	0	0	49
	8	446	44	56	0	0	446	44	56	0	49	49	0	0	0	49	49	0	0	0	49
	12	446	44	56	0	0	446	44	56	0	49	49	0	0	0	49	49	0	0	0	49
	24	539	53	47	0	0	539	53	47	0	42	42	0	0	0	42	42	0	0	0	42
	52	434	43	57	0	0	434	43	57	0	17	17	0	0	0	17	17	0	0	0	17
	0 control	558	55	45	0	0	558	55	45	0	672	67	0	0	0	672	67	0	0	0	672
	2	475	47	53	0	0	475	47	53	0	52	52	0	0	0	52	52	0	0	0	52

Averages are for 55 control specimens and 5 exposed specimens.

Metal bonded directly to wood with primary glue.

Birch and walnut failures combined.

2 A 42935 F

Table 3.—Average results of shear tests on glued wood-to-metal joints soaked continuously in 75 octane gasoline

Gluing process	Exposure period	Aluminum to birch plywood										Steel to birch plywood									
		Unpainted					Painted					Unpainted					Painted				
		Average shear strength	Average secondary glue failure	Average metal failure	Average wood failure	Average adhesive failure	Average shear strength	Average secondary glue failure	Average metal failure	Average wood failure	Average adhesive failure	Average shear strength	Average secondary glue failure	Average metal failure	Average wood failure	Average adhesive failure	Average shear strength	Average secondary glue failure	Average metal failure	Average wood failure	Average adhesive failure
lb. per sq. in.	Percent	Percent	Percent	Percent	lb. per sq. in.	Percent	Percent	Percent	Percent	lb. per sq. in.	Percent	Percent	Percent	Percent	lb. per sq. in.	Percent	Percent	Percent	Percent		
1	0 control	980	1175	88	12	0	0	0	0	0	971	2	0	0	0	0	971	2	0	0	0
	2	1175	1290	97	3	0	0	0	0	0	1117	—	0	0	0	0	1117	—	0	0	0
	4	1305	1117	98	2	0	0	0	0	0	1288	—	0	0	0	0	1288	—	0	0	0
	6	1290	1094	95	4	0	0	0	0	0	901	—	0	0	0	0	901	—	0	0	0
	8	1360	1158	93	7	0	0	0	0	0	1070	—	0	0	0	0	1070	—	0	0	0
	12	1369	1177	82	12	0	0	0	0	0	1189	—	0	0	0	0	1189	—	0	0	0
2	0 control	716	725	52	0	12	0	0	0	0	665	36	0	0	0	0	655	38	0	0	0
	2	725	762	66	0	0	0	0	0	0	797	31	0	0	0	0	763	32	0	0	0
	4	762	786	68	0	0	0	0	0	0	692	15	0	0	0	0	698	16	0	0	0
	6	786	786	73	0	0	0	0	0	0	719	27	0	0	0	0	747	28	0	0	0
	8	786	786	67	0	0	0	0	0	0	775	25	0	0	0	0	877	26	0	0	0
	12	753	780	54	0	19	0	0	0	0	93	17	0	0	0	0	785	18	0	0	0
3	0 control	945	945	53	47	0	0	0	0	0	936	2	0	0	0	0	936	2	0	0	0
	2	893	762	44	4	0	0	0	0	0	753	17	0	0	0	0	768	17	0	0	0
	4	874	823	18	81	0	0	0	0	0	716	0	0	0	0	0	801	0	0	0	0
	6	861	842	13	87	0	0	0	0	0	664	0	0	0	0	0	682	0	0	0	0
	8	865	897	9	91	0	0	0	0	0	685	0	0	0	0	0	691	0	0	0	0
	12	824	801	2	98	0	0	0	0	0	804	0	0	0	0	0	829	0	0	0	0
5	0 control	723	723	88	12	0	0	0	0	0	719	2	0	0	0	0	779	2	0	0	0
	2	723	723	88	12	0	0	0	0	0	705	0	0	0	0	0	725	0	0	0	0
	4	723	723	88	12	0	0	0	0	0	715	0	0	0	0	0	725	0	0	0	0
	6	723	723	88	12	0	0	0	0	0	725	0	0	0	0	0	725	0	0	0	0
	8	723	723	88	12	0	0	0	0	0	725	0	0	0	0	0	725	0	0	0	0
	12	723	723	88	12	0	0	0	0	0	725	0	0	0	0	0	725	0	0	0	0
6	0 control	554	554	61	2	0	0	0	0	0	542	11	0	0	0	0	542	11	0	0	0
	2	554	554	61	2	0	0	0	0	0	542	11	0	0	0	0	542	11	0	0	0
	4	554	554	61	2	0	0	0	0	0	542	11	0	0	0	0	542	11	0	0	0
	6	554	554	61	2	0	0	0	0	0	542	11	0	0	0	0	542	11	0	0	0
	8	554	554	61	2	0	0	0	0	0	542	11	0	0	0	0	542	11	0	0	0
	12	554	554	61	2	0	0	0	0	0	542	11	0	0	0	0	542	11	0	0	0

Averages are for 55 control specimens and 5 exposed specimens.
 Metal bonded directly to wood with primary glue.
 Birch and walnut failures combined.

Table 10.—Average results of shear tests on glued wood-to-metal joints soaked continuously in ethylene alcohol anti-freeze fluid

Gluing process	Exposure period	Aluminum to Birch plywood										Painted										Unpainted										Steel to Walnut Shm to Birch									
		Unpainted					Painted					Unpainted					Painted					Unpainted					Painted					Unpainted					Painted				
		Average shear strength	Average glue failure	Average metal adhesion	Average secondary glue failure	Average percent failure	Average shear strength	Average glue failure	Average metal adhesion	Average secondary glue failure	Average percent failure	Average shear strength	Average glue failure	Average metal adhesion	Average secondary glue failure	Average percent failure	Average shear strength	Average glue failure	Average metal adhesion	Average secondary glue failure	Average percent failure	Average shear strength	Average glue failure	Average metal adhesion	Average secondary glue failure	Average percent failure	Average shear strength	Average glue failure	Average metal adhesion	Average secondary glue failure	Average percent failure	Average shear strength	Average glue failure	Average metal adhesion	Average secondary glue failure	Average percent failure					
Weeks	lb. per sq. in.	Percent	Percent	Percent	Percent	lb. per sq. in.	Percent	Percent	Percent	Percent	lb. per sq. in.	Percent	Percent	Percent	Percent	lb. per sq. in.	Percent	Percent	Percent	Percent	lb. per sq. in.	Percent	Percent	Percent	Percent	lb. per sq. in.	Percent	Percent	Percent	Percent	lb. per sq. in.	Percent	Percent	Percent	Percent						
1	0 control	900	88	12	0	0	88	12	0	0	0	88	12	0	0	0	88	12	0	0	0	88	12	0	0	0	88	12	0	0	0	88	12	0	0	0					
	2	904	95	12	0	0	95	12	0	0	0	95	12	0	0	0	95	12	0	0	0	95	12	0	0	0	95	12	0	0	0	95	12	0	0	0					
	4	924	92	12	0	0	92	12	0	0	0	92	12	0	0	0	92	12	0	0	0	92	12	0	0	0	92	12	0	0	0	92	12	0	0	0					
	6	866	91	14	0	0	91	14	0	0	0	91	14	0	0	0	91	14	0	0	0	91	14	0	0	0	91	14	0	0	0	91	14	0	0	0					
	8	802	86	14	0	0	86	14	0	0	0	86	14	0	0	0	86	14	0	0	0	86	14	0	0	0	86	14	0	0	0	86	14	0	0	0					
2	0 control	716	52	25	0	0	52	25	0	0	0	52	25	0	0	0	52	25	0	0	0	52	25	0	0	0	52	25	0	0	0	52	25	0	0	0					
	2	732	76	0	0	0	76	0	0	0	0	76	0	0	0	0	76	0	0	0	0	76	0	0	0	0	76	0	0	0	76	0	0	0	76	0	0				
	4	651	74	0	0	0	74	0	0	0	0	74	0	0	0	0	74	0	0	0	0	74	0	0	0	0	74	0	0	0	74	0	0	0	74	0	0				
	6	564	67	0	0	0	67	0	0	0	0	67	0	0	0	0	67	0	0	0	0	67	0	0	0	0	67	0	0	0	67	0	0	0	67	0	0				
	8	679	74	0	0	0	74	0	0	0	0	74	0	0	0	0	74	0	0	0	0	74	0	0	0	0	74	0	0	0	74	0	0	0	74	0	0				
3	0 control	945	53	47	0	0	53	47	0	0	0	53	47	0	0	0	53	47	0	0	0	53	47	0	0	0	53	47	0	0	0	53	47	0	0	53	47	0	0		
	2	911	74	46	0	0	74	46	0	0	0	74	46	0	0	0	74	46	0	0	0	74	46	0	0	0	74	46	0	0	0	74	46	0	0	74	46	0	0		
	4	844	74	46	0	0	74	46	0	0	0	74	46	0	0	0	74	46	0	0	0	74	46	0	0	0	74	46	0	0	0	74	46	0	0	74	46	0	0		
	6	790	50	46	0	0	50	46	0	0	0	50	46	0	0	0	50	46	0	0	0	50	46	0	0	0	50	46	0	0	0	50	46	0	0	50	46	0	0		
	8	653	78	22	0	0	78	22	0	0	0	78	22	0	0	0	78	22	0	0	0	78	22	0	0	0	78	22	0	0	0	78	22	0	0	78	22	0	0		
4	0 control	617	54	37	0	0	54	37	0	0	0	54	37	0	0	0	54	37	0	0	0	54	37	0	0	0	54	37	0	0	0	54	37	0	0	54	37	0	0		
	2	617	54	37	0	0	54	37	0	0	0	54	37	0	0	0	54	37	0	0	0	54	37	0	0	0	54	37	0	0	0	54	37	0	0	54	37	0	0		
	4	617	54	37	0	0	54	37	0	0	0	54	37	0	0	0	54	37	0	0	0	54	37	0	0	0	54	37	0	0	0	54	37	0	0	54	37	0	0		
	6	617	54	37	0	0	54	37	0	0	0	54	37	0	0	0	54	37	0	0	0	54	37	0	0	0	54	37	0	0	0	54	37	0	0	54	37	0	0		
	8	617	54	37	0	0	54	37	0	0	0	54	37	0	0	0	54	37	0	0	0	54	37	0	0	0	54	37	0	0	0	54	37	0	0	54	37	0	0		
5	0 control	723	88	12	0	0	88	12	0	0	0	88	12	0	0	0	88	12	0	0	0	88	12	0	0	0	88	12	0	0	0	88	12	0	0	88	12	0	0		
	2	757	89	11	0	0	89	11	0	0	0	89	11	0	0	0	89	11	0	0	0	89	11	0	0	0	89	11	0	0	0	89	11	0	0	89	11	0	0		
	4	714	96	8	0	0	96	8	0	0	0	96	8	0	0	0	96	8	0	0	0	96	8	0	0	0	96	8	0	0	0	96	8	0	0	96	8	0	0		
	6	612	61	20	0	0	61	20	0	0	0	61	20	0	0	0	61	20	0	0	0	61	20	0	0	0	61	20	0	0	0	61	20	0	0	61	20	0	0		
	8	605	95	9	0	0	95	9	0	0	0	95	9	0	0	0	95	9	0	0	0	95	9	0	0	0	95	9	0	0	0	95	9	0	0	95	9	0	0		
6	0 control	554	67	11	0	0	67	11	0	0	0	67	11	0	0	0	67	11	0	0	0	67	11	0	0	0	67	11	0	0	0	67	11	0	0	67	11	0	0		
	2	550	62	19	0	0	62	19	0	0	0	62	19	0	0	0	62	19	0	0	0	62	19	0	0	0	62	19	0	0	0	62	19	0	0	62	19	0	0		
	4	556	60	18	0	0	60	18	0	0	0	60	18	0	0	0	60	18	0	0	0	60	18	0	0	0	60	18	0	0	0	60	18	0	0	60	18	0	0		
	6	518	60	19	0	0	60	19	0	0	0	60	19	0	0	0	60	19	0	0	0	60	19	0	0	0	60	19	0	0	0	60	19	0	0	60	19	0	0		
	8	523	44	19	0	0	44	19	0	0	0	44	19	0	0	0	44	19	0	0	0	44	19	0	0	0	44	19	0	0	0	44	19	0	0	44	19	0	0		

Averages are for 55 control specimens and 5 exposed specimens.

1. Metal bonded directly to wood with primary glue.

2. Birch and walnut failures combined.

Table 11.—Average results of shear tests on glued wood-to-metal joints soaked continuously in isopropyl alcohol de-icer fluids.

Gluing process	Exposure period	Aluminum to birch plywood										Steel to birch plywood										Painted													
		Unsoaked					Painted					Unsoaked					Painted					Unsoaked					Painted								
		Average shear strength	Average wood failure	Average glue failure	Average metal failure	Average secondary glue failure	Average shear strength	Average wood failure	Average glue failure	Average metal failure	Average secondary glue failure	Average shear strength	Average wood failure	Average glue failure	Average metal failure	Average secondary glue failure	Average shear strength	Average wood failure	Average glue failure	Average metal failure	Average secondary glue failure	Average shear strength	Average wood failure	Average glue failure	Average metal failure	Average secondary glue failure	Average shear strength	Average wood failure	Average glue failure	Average metal failure	Average secondary glue failure				
lb. per sq. in.	Percent	Percent	Percent	Percent	lb. per sq. in.	Percent	Percent	Percent	Percent	lb. per sq. in.	Percent	Percent	Percent	Percent	lb. per sq. in.	Percent	Percent	Percent	Percent	lb. per sq. in.	Percent	Percent	Percent	Percent	lb. per sq. in.	Percent	Percent	Percent	Percent	lb. per sq. in.	Percent	Percent	Percent	Percent	
1	0 control	980	88	12	0	0	980	88	12	0	971	93	7	0	0	971	93	7	0	0	971	93	7	0	0	971	93	7	0	0	971	93	7	0	0
	2	893	86	12	0	0	893	86	12	0	875	85	12	0	0	875	85	12	0	0	875	85	12	0	0	875	85	12	0	0	875	85	12	0	0
	4	516	39	61	0	0	516	36	64	0	507	31	49	0	0	507	31	49	0	0	507	31	49	0	0	507	31	49	0	0	507	31	49	0	0
	8	391	32	68	0	0	391	0	100	0	391	32	68	0	0	391	32	68	0	0	391	32	68	0	0	391	32	68	0	0	391	32	68	0	0
	12	67	0	100	0	0	67	0	100	0	67	0	100	0	0	67	0	100	0	0	67	0	100	0	0	67	0	100	0	0	67	0	100	0	0
2	0 control	716	52	48	0	0	716	52	48	0	716	52	48	0	0	716	52	48	0	0	716	52	48	0	0	716	52	48	0	0	716	52	48	0	0
	2	770	63	37	0	0	770	63	37	0	770	63	37	0	0	770	63	37	0	0	770	63	37	0	0	770	63	37	0	0	770	63	37	0	0
	4	683	57	43	0	0	683	57	43	0	683	57	43	0	0	683	57	43	0	0	683	57	43	0	0	683	57	43	0	0	683	57	43	0	0
	8	721	60	40	0	0	721	60	40	0	721	60	40	0	0	721	60	40	0	0	721	60	40	0	0	721	60	40	0	0	721	60	40	0	0
	12	642	55	45	0	0	642	55	45	0	642	55	45	0	0	642	55	45	0	0	642	55	45	0	0	642	55	45	0	0	642	55	45	0	0
3	0 control	985	93	7	0	0	985	93	7	0	985	93	7	0	0	985	93	7	0	0	985	93	7	0	0	985	93	7	0	0	985	93	7	0	0
	2	896	86	14	0	0	896	86	14	0	896	86	14	0	0	896	86	14	0	0	896	86	14	0	0	896	86	14	0	0	896	86	14	0	0
	4	560	44	56	0	0	560	44	56	0	560	44	56	0	0	560	44	56	0	0	560	44	56	0	0	560	44	56	0	0	560	44	56	0	0
	8	869	36	64	0	0	869	36	64	0	869	36	64	0	0	869	36	64	0	0	869	36	64	0	0	869	36	64	0	0	869	36	64	0	0
	12	727	31	69	0	0	727	31	69	0	727	31	69	0	0	727	31	69	0	0	727	31	69	0	0	727	31	69	0	0	727	31	69	0	0
5	0 control	723	88	12	0	0	723	88	12	0	723	88	12	0	0	723	88	12	0	0	723	88	12	0	0	723	88	12	0	0	723	88	12	0	0
	2	877	94	6	0	0	877	94	6	0	877	94	6	0	0	877	94	6	0	0	877	94	6	0	0	877	94	6	0	0	877	94	6	0	0
	4	809	71	29	0	0	809	71	29	0	809	71	29	0	0	809	71	29	0	0	809	71	29	0	0	809	71	29	0	0	809	71	29	0	0
	8	792	100	0	0	0	792	100	0	0	792	100	0	0	0	792	100	0	0	0	792	100	0	0	0	792	100	0	0	0	792	100	0	0	0
	12	817	96	4	0	0	817	96	4	0	817	96	4	0	0	817	96	4	0	0	817	96	4	0	0	817	96	4	0	0	817	96	4	0	0
6	0 control	794	88	12	0	0	794	88	12	0	794	88	12	0	0	794	88	12	0	0	794	88	12	0	0	794	88	12	0	0	794	88	12	0	0
	2	877	94	6	0	0	877	94	6	0	877	94	6	0	0	877	94	6	0	0	877	94	6	0	0	877	94	6	0	0	877	94	6	0	0
	4	809	71	29	0	0	809	71	29	0	809	71	29	0	0	809	71	29	0	0	809	71	29	0	0	809	71	29	0	0	809	71	29	0	0
	8	792	100	0	0	0	792	100	0	0	792	100	0	0	0	792	100	0	0	0	792	100	0	0	0	792	100	0	0	0	792	100	0	0	0
	12	817	96	4	0	0	817	96	4	0	817	96	4	0	0	817	96	4	0	0	817	96	4	0	0	817	96	4	0	0	817	96	4	0	0

Averages are for 55 control specimens and 5 exposed specimens.

Steel bonded directly to wood with primary glue.

Birch and walnut failures combined.

Table 12 - Average results of shear tests on glued wood-to-metal joints - coated continuously in alternate lubrication oil

Sliding process	Exposure period	Aluminum Birch plywood										Steel to Birch plywood									
		Unpainted					Painted					Unpainted					Painted				
		Average	Average	Average	Average	Average	Average	Average	Average	Average	Average	Average	Average	Average	Average	Average	Average	Average	Average	Average	Average
		shear	shear	shear	shear	shear	shear	shear	shear	shear	shear	shear	shear	shear	shear	shear	shear	shear	shear	shear	shear
		strength	strength	strength	strength	strength	strength	strength	strength	strength	strength	strength	strength	strength	strength	strength	strength	strength	strength	strength	strength
		lb. per sq. in.	lb. per sq. in.	lb. per sq. in.	lb. per sq. in.	lb. per sq. in.	lb. per sq. in.	lb. per sq. in.	lb. per sq. in.	lb. per sq. in.	lb. per sq. in.	lb. per sq. in.	lb. per sq. in.	lb. per sq. in.	lb. per sq. in.	lb. per sq. in.	lb. per sq. in.	lb. per sq. in.	lb. per sq. in.	lb. per sq. in.	lb. per sq. in.
	Weeks	Percent failure	Percent failure	Percent failure	Percent failure	Percent failure	Percent failure	Percent failure	Percent failure	Percent failure	Percent failure	Percent failure	Percent failure	Percent failure	Percent failure	Percent failure	Percent failure	Percent failure	Percent failure	Percent failure	Percent failure
1	0 control	890	880	12	0	0	88	980	880	12	0	0	93	971	971	0	93	971	971	0	2
	2	1054	94	3	0	0	86	864	86	14	0	0	98	915	1066	0	92	1066	92	0	2
	4	995	94	3	0	0	86	898	86	14	0	0	98	915	1066	0	92	1066	92	0	2
	6	904	86	13	0	0	86	902	86	13	0	0	98	915	1066	0	92	1066	92	0	2
	8	914	90	10	0	0	86	902	86	13	0	0	98	915	1066	0	92	1066	92	0	2
2	0 control	829	81	11	0	0	80	1057	80	20	0	0	92	1099	1095	0	83	1095	83	0	2
	2	1056	81	11	0	0	80	1057	80	20	0	0	92	1099	1095	0	83	1095	83	0	2
	4	912	58	24	18	0	76	1092	76	24	0	0	74	1067	914	0	72	914	72	0	2
	6	716	52	0	12	0	52	716	52	0	12	0	58	855	855	0	56	855	56	0	2
	8	708	51	0	8	0	48	711	48	0	16	0	87	843	693	0	43	693	43	0	2
3	0 control	708	51	0	8	0	48	711	48	0	16	0	87	843	693	0	43	693	43	0	2
	2	674	56	0	0	0	56	674	56	0	0	0	35	756	756	0	23	756	23	0	2
	4	674	56	0	0	0	56	674	56	0	0	0	35	756	756	0	23	756	23	0	2
	6	720	78	0	0	0	78	720	78	0	0	0	52	806	806	0	43	806	43	0	2
	8	759	75	0	0	0	75	759	75	0	0	0	59	875	875	0	43	875	43	0	2
4	0 control	674	56	0	0	0	56	674	56	0	0	0	35	756	756	0	23	756	23	0	2
	2	945	53	47	0	0	47	945	53	47	0	0	34	936	936	0	10	936	10	0	2
	4	953	49	31	0	0	31	953	49	31	0	0	35	1036	1036	0	12	1036	12	0	2
	6	1091	49	21	0	0	21	1091	49	21	0	0	35	1036	1036	0	12	1036	12	0	2
	8	1024	58	52	0	0	52	1024	58	52	0	0	35	1036	1036	0	12	1036	12	0	2
5	0 control	997	31	69	0	0	69	997	31	69	0	0	24	931	931	0	23	931	23	0	2
	2	1037	57	43	0	0	43	1037	57	43	0	0	29	990	990	0	20	990	20	0	2
	4	951	47	53	0	0	53	951	47	53	0	0	29	990	990	0	20	990	20	0	2
	6	841	41	59	0	0	59	841	41	59	0	0	30	880	880	0	15	880	15	0	2
	8	723	68	12	0	0	12	723	68	12	0	0	97	779	779	0	0	779	0	0	2
6	0 control	762	91	9	0	0	9	762	91	9	0	0	84	800	800	0	0	800	0	0	2
	2	705	95	6	0	0	6	705	95	6	0	0	100	897	897	0	0	897	0	0	2
	4	726	92	4	0	0	4	726	92	4	0	0	95	916	916	0	0	916	0	0	2
	6	844	96	4	0	0	4	844	96	4	0	0	96	916	916	0	0	916	0	0	2
	8	756	82	18	0	0	18	756	82	18	0	0	95	916	916	0	0	916	0	0	2
7	0 control	796	93	7	0	0	7	796	93	7	0	0	95	916	916	0	0	916	0	0	2
	2	796	93	7	0	0	7	796	93	7	0	0	95	916	916	0	0	916	0	0	2
	4	608	66	0	34	0	34	608	66	0	34	0	22	493	493	0	82	493	82	0	2
	6	608	66	0	34	0	34	608	66	0	34	0	22	493	493	0	82	493	82	0	2
	8	608	66	0	34	0	34	608	66	0	34	0	22	493	493	0	82	493	82	0	2
8	0 control	554	63	2	0	0	2	554	63	2	0	0	60	552	552	0	0	552	0	0	2
	2	513	72	3	0	0	3	513	72	3	0	0	47	560	560	0	0	560	0	0	2
	4	530	70	0	0	0	0	530	70	0	0	0	47	560	560	0	0	560	0	0	2
	6	418	64	0	0	0	0	418	64	0	0	0	45	560	560	0	0	560	0	0	2
	8	418	64	0	0	0	0	418	64	0	0	0	45	560	560	0	0	560	0	0	2
9	0 control	554	63	2	0	0	2	554	63	2	0	0	60	552	552	0	0	552	0	0	2
	2	513	72	3	0	0	3	513	72	3	0	0	47	560	560	0	0	560	0	0	2
	4	530	70	0	0	0	0	530	70	0	0	0	45	560	560	0	0	560	0	0	2
	6	418	64	0	0	0	0	418	64	0	0	0	45	560	560	0	0	560	0	0	2
	8	418	64	0	0	0	0	418	64	0	0	0	45	560	560	0	0	560	0	0	2

Averages are for 55 control specimens and 5 exposed specimens.
 Metal bonded directly to wood with primary glue.
 Birch and walnut failures combined.

Table 13. Average results at shear tests on glued wood-to-metal joints exposed to weather mlt-of-dura

Gluing process	Exposure period	Aluminum to birch plywood										Steel to birch plywood									
		Unpainted					Painted					Unpainted					Painted				
		Average shear strength	Average wood failure	Average metal adhesion	Average glue failure	Average secondary glue failure	Average strength	Average wood failure	Average metal adhesion	Average glue failure	Average secondary glue failure	Average strength	Average wood failure	Average metal adhesion	Average glue failure	Average secondary glue failure	Average strength	Average wood failure	Average metal adhesion	Average glue failure	Average secondary glue failure
Weeks	lb. per sq. in.	Percent	Percent	Percent	Percent	Percent	lb. per sq. in.	Percent	Percent	Percent	Percent	lb. per sq. in.	Percent	Percent	Percent	Percent	lb. per sq. in.	Percent	Percent	Percent	Percent
0 control	960	88	12	0	0	2	971	88	12	0	0	971	88	12	0	0	971	88	12	0	0
12	1064	95	5	0	0	2	1064	95	5	0	0	1064	95	5	0	0	1064	95	5	0	0
24	731	57	8	35	0	2	801	57	8	35	0	801	57	8	35	0	801	57	8	35	0
52	684	65	2	33	0	2	684	65	2	33	0	684	65	2	33	0	684	65	2	33	0
104																					
0 control	716	52	0	12	0	36	716	52	0	12	0	716	52	0	12	0	716	52	0	12	0
12	613	37	0	53	0	10	613	37	0	53	0	613	37	0	53	0	613	37	0	53	0
24	732	58	0	24	0	18	732	58	0	24	0	732	58	0	24	0	732	58	0	24	0
52	596	53	0	31	0	18	596	53	0	31	0	596	53	0	31	0	596	53	0	31	0
104																					
0 control	945	53	47	0	0	2	945	53	47	0	0	945	53	47	0	0	945	53	47	0	0
12	873	45	54	1	0	2	873	45	54	1	0	873	45	54	1	0	873	45	54	1	0
24	850	45	56	1	0	2	850	45	56	1	0	850	45	56	1	0	850	45	56	1	0
52																					
104																					
0 control	928	50	36	14	0	2	928	50	36	14	0	928	50	36	14	0	928	50	36	14	0
12	824	61	20	19	0	2	824	61	20	19	0	824	61	20	19	0	824	61	20	19	0
24																					
52																					
104																					
0 control	723	22	12	0	0	2	723	22	12	0	0	723	22	12	0	0	723	22	12	0	0
12	933	98	1	2	0	2	933	98	1	2	0	933	98	1	2	0	933	98	1	2	0
24	757	86	0	14	0	2	757	86	0	14	0	757	86	0	14	0	757	86	0	14	0
52	774	95	0	5	0	2	774	95	0	5	0	774	95	0	5	0	774	95	0	5	0
104																					
0 control	524	63	2	0	0	21	524	63	2	0	0	524	63	2	0	0	524	63	2	0	0
12	531	91	3	1	0	21	531	91	3	1	0	531	91	3	1	0	531	91	3	1	0
24	575	60	0	0	0	21	575	60	0	0	0	575	60	0	0	0	575	60	0	0	0
52																					
104																					

Averages are for 55 control specimens and 5 exposed specimens.
Metal bonded directly to wood with primary glue.
Birch and walnut failures combined.

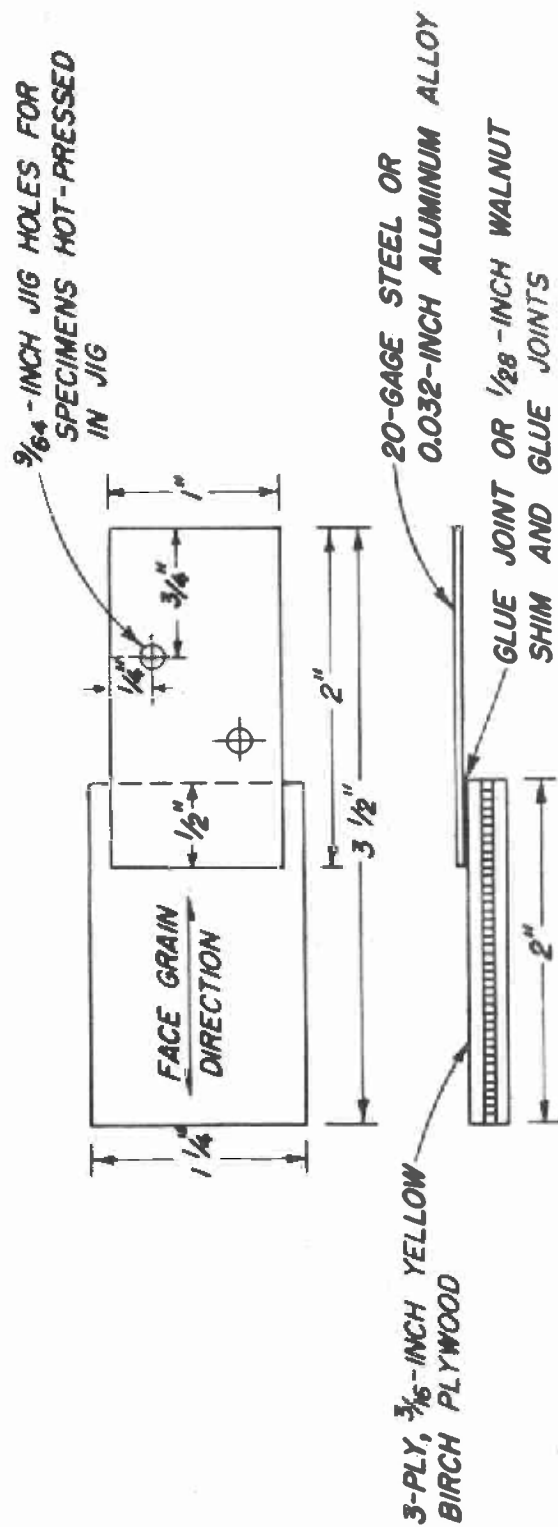


Figure 1.--Plywood-to-metal glue-joint test specimen with and without walnut shim.

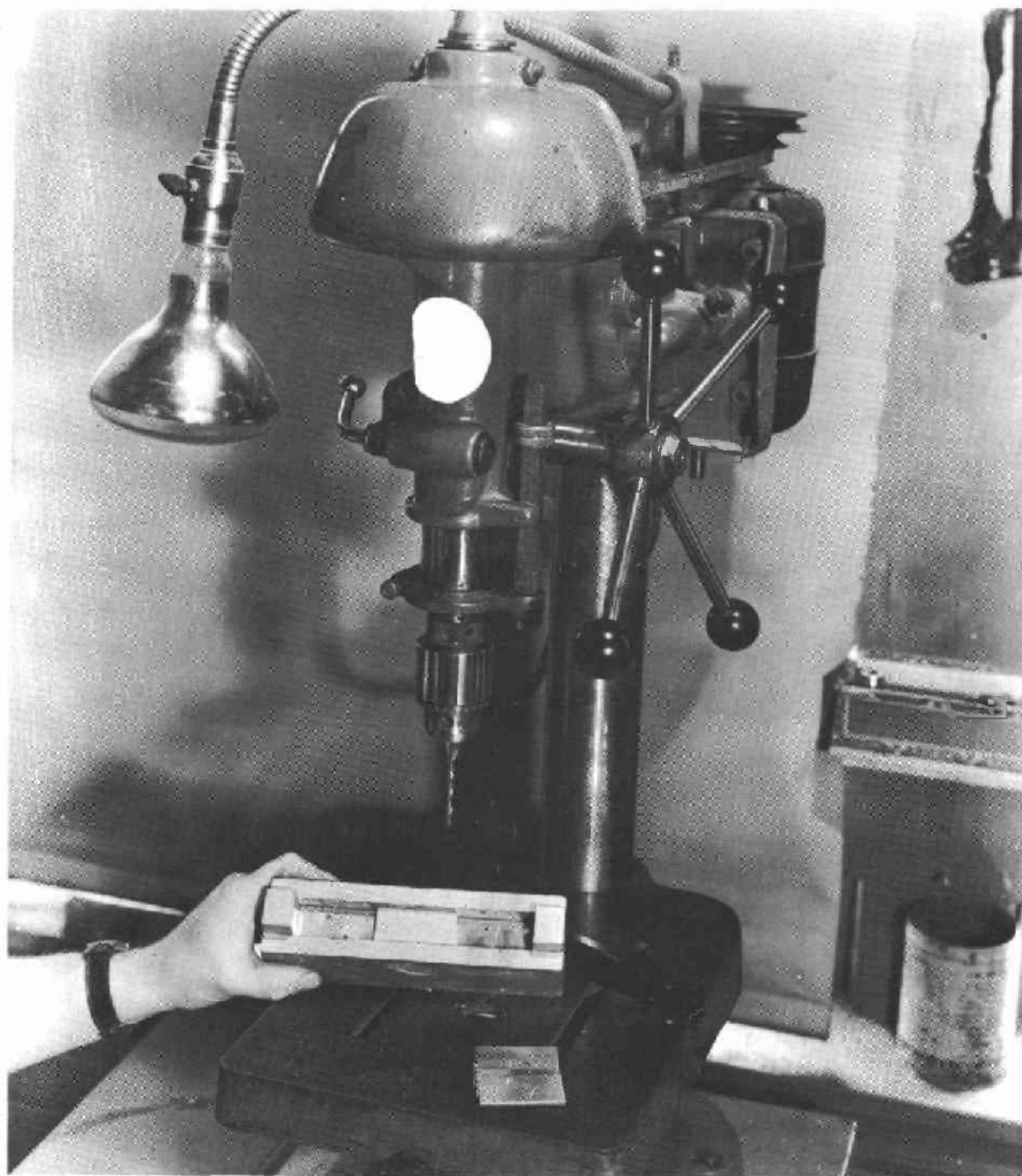


Figure 2.--Jig for locating alinement holes in metal pieces.

Z M 73507 F



Figure 3.--Hot-press gluing of wood-to-metal joint specimens showing electric hot press, pressing jig, and specimens.

Z M 73508 F

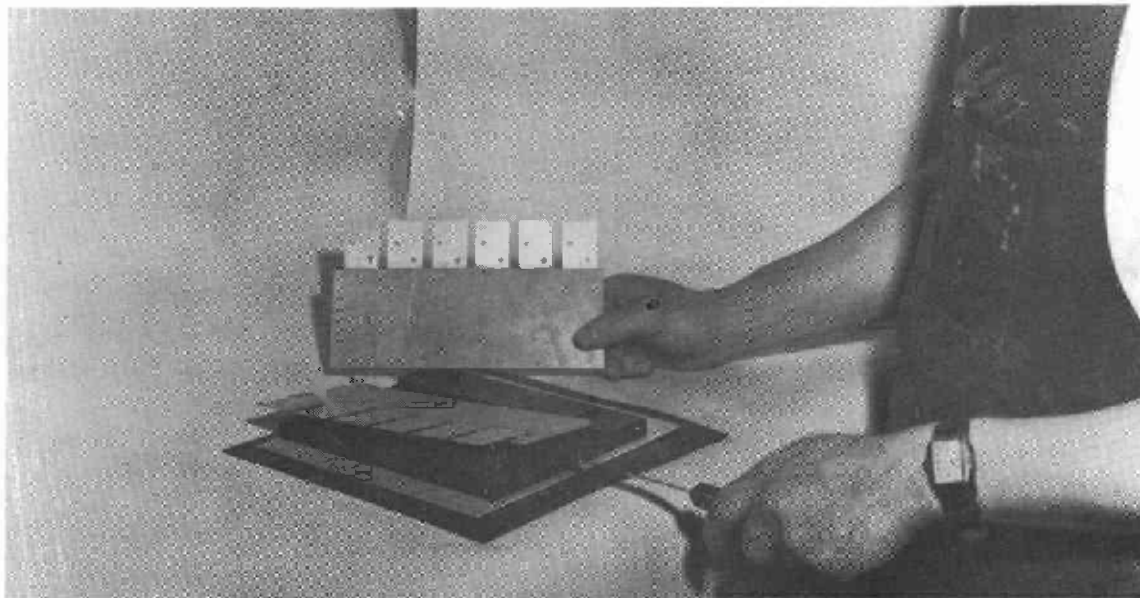


Figure 4.--Removing two panels of wood-to-metal joints from jig after gluing in a hot press.

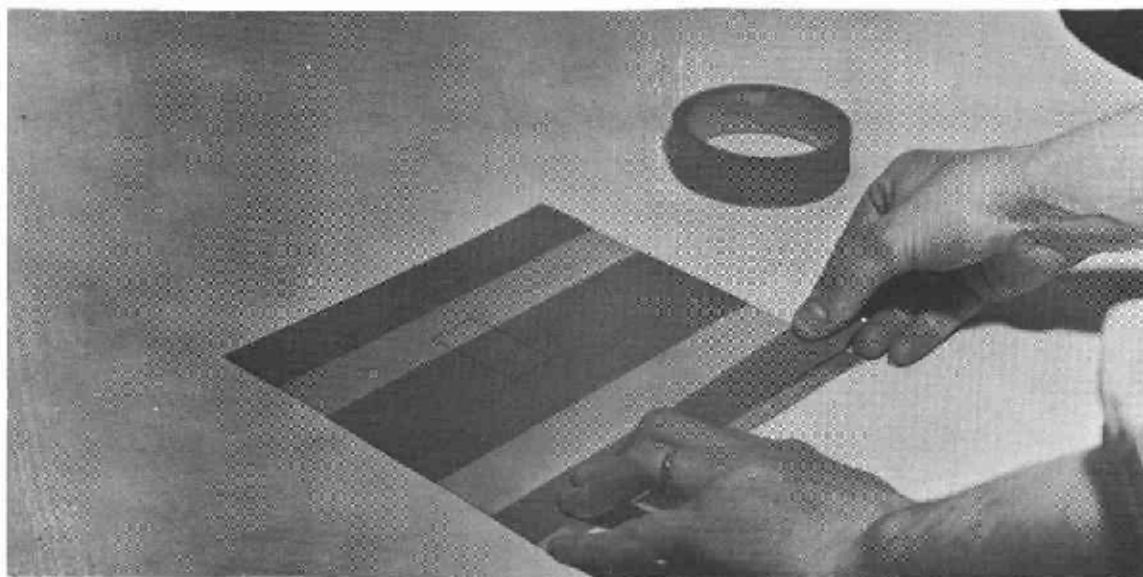


Figure 5.--Masking of the 8- by 8-inch metal sheets before applying the glue. (Outlined area marks the position of the metal portion of one specimen).

Z M 73509 F

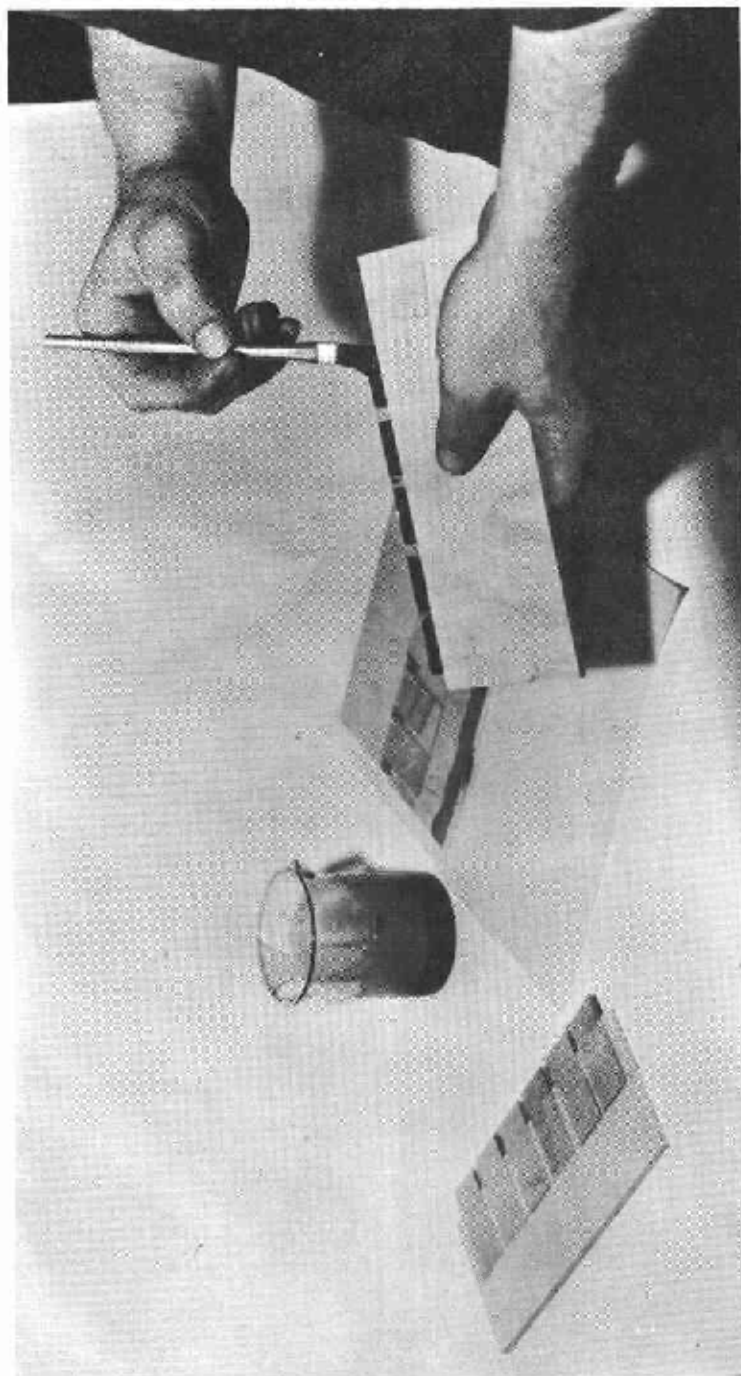


Figure 6.--Applying the secondary glue to the primed metal surface in the preparation of the wood-to-metal glued joint specimens.

Z M 73510 F

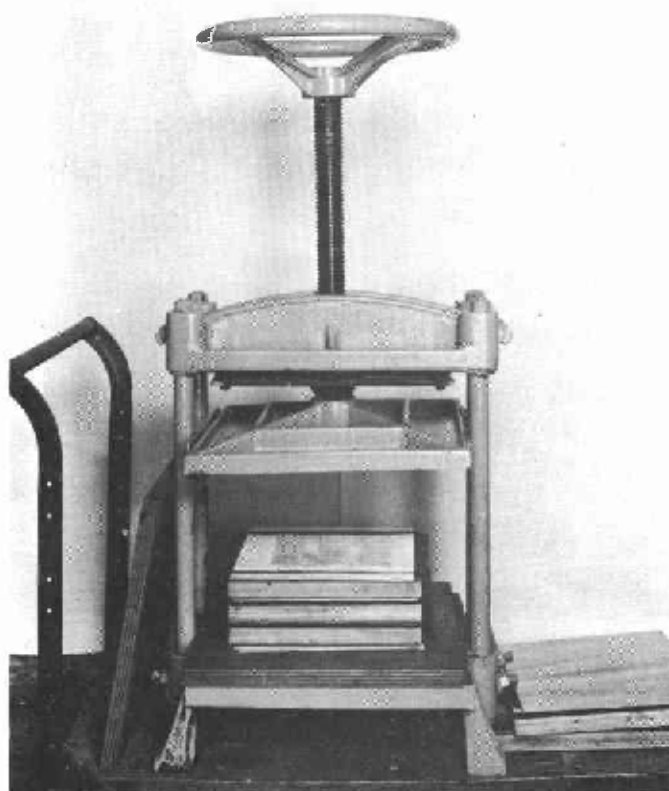


Figure 7.--Press used for the secondary gluing of the wood-to-metal joint specimens.

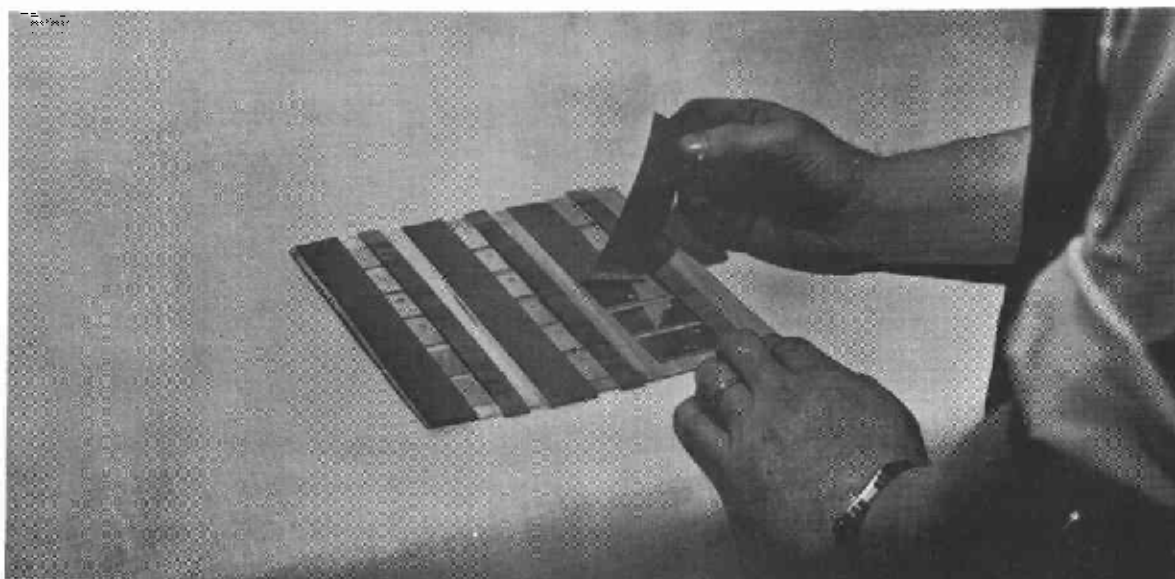


Figure 8.--Taping walnut shims and metal pieces to yellow-poplar cauls.